

**Davidon Homes (Park Ridge Subdivision #8846)
Second Addendum to the
Project Level EIR for FUA #2 Specific Plan
City of Antioch, Contra Costa County, California**

Prepared for:

City of Antioch

Community Development Department

200 'H' Street

Antioch, CA 94509

925.779.7035

Contact: Alexis Morris, Senior Planner

Prepared by:

FirstCarbon Solutions

1350 Treat Boulevard, Suite 380

Walnut Creek, CA 94597

925.357.2562

Contact: Mary Bean, Project Director

Elizabeth Johnson, Project Manager

Report Date: July 8, 2016

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Table of Contents

| | |
|---|-----------|
| Section 1: Introduction | 1 |
| 1.1 - Initial Study/Environmental Checklist | 1 |
| 1.2 - Environmental Analysis and Conclusions | 1 |
| 1.3 - Determination | 3 |
| 1.4 - Mitigation Monitoring and Reporting Program..... | 4 |
| Section 2: Project Description | 5 |
| 2.1 - Location and Setting | 5 |
| 2.2 - Project Background | 5 |
| 2.3 - Project Characteristics..... | 6 |
| 2.4 - Discretionary Approvals | 6 |
| Section 3: CEQA checklist | 13 |
| 3.1 - Explanation of Checklist Evaluation Categories..... | 13 |
| 3.2 - Discussion and Mitigation Sections..... | 14 |
| XVI. Transportation | 15 |
| Section 4: References | 23 |
| Section 5: List of Preparers..... | 25 |
| 5.1 - Lead Consultant..... | 25 |
| 5.2 - Technical Subconsultant | 25 |
| Appendix A: Traffic Impact Analyses | |
| A.1 - 2016 Traffic Impact Analysis prepared by W-Trans for the Laurel Ranch Subdivision Addendum | |
| A.2 - Traffic Technical Memorandum prepared by Fehr & Peers for 2009 Park Ridge Addendum | |

List of Tables

| | |
|---|----|
| Table 1: Trip Generation Summary | 17 |
| Table 2: Existing and Existing Plus Project Intersection Operations | 18 |
| Table 3: Cumulative and Cumulative Plus Project Intersection Operation..... | 18 |
| Table 4: Queuing Summary | 20 |

List of Exhibits

| | |
|--|----|
| Exhibit 1: Regional Location Map | 7 |
| Exhibit 2: Local Vicinity Map, Aerial Base | 9 |
| Exhibit 3: Laurel Road Reconfiguration | 11 |

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SECTION 1: INTRODUCTION

This Addendum, checklist, and attached supporting documents have been prepared to determine whether and to what extent the Final Environmental Impact Report (1996 Final EIR) for the East Lone Tree Specific Plan (officially known as the Future Urbanization Area 2 East Lone Tree Specific Plan Area Project-Level EIR) remains sufficient to address the potential impacts of the proposed changes to the Park Ridge Subdivision Project (proposed project):

- Reconfiguration of the proposed Laurel Road/Treeline Way/"D" Lane intersection, and
- Removal of condition of approval #91 requiring construction of a signalized intersection at the above intersection, or
- Whether additional documentation is required under the California Environmental Quality Act (CEQA) (Pub. Resources Code, Section 21000, et seq.).

1.1 - Initial Study/Environmental Checklist

Pursuant to Public Resources Code Section 21166, and CEQA Guidelines Sections 15162 and 15164, subd. (a), the attached initial study/checklist has been prepared to evaluate the proposed project. The attached initial study/checklist uses the standard environmental checklist categories provided in Appendix G of the CEQA Guidelines, but provides answer columns for evaluation consistent with the considerations listed under CEQA Guidelines Section 15162, subd. (a).

1.2 - Environmental Analysis and Conclusions

CEQA Guidelines Section 15164, subd. (a) provides that the lead agency or a responsible agency shall prepare an addendum to a previously certified EIR or Negative Declaration (ND) if some changes or additions are necessary but none of the conditions described in CEQA Guidelines Section 15162 calling for preparation of a subsequent EIR or ND have occurred (CEQA Guidelines, Section 15164, subd. (a)).

An addendum need not be circulated for public review but can be included in or attached to the Final EIR or ND (CEQA Guidelines Section 15164, subd. (c)). The decision-making body shall consider the addendum with the Final EIR prior to making a decision on the project (CEQA Guidelines Section 15164, subd. (d)). An agency must also include a brief explanation of the decision not to prepare a subsequent EIR or ND pursuant to Section 15162 (CEQA Guidelines Section 15164, subd. (e)).

Consequently, once an EIR or ND has been certified for a project, no subsequent EIR or ND is required under CEQA unless, based on substantial evidence:

1. Substantial changes are proposed in the project which will require major revisions of the previous EIR [or ND] . . . due to the involvement of new significant environmental effects or a substantial increase in the severity of previously identified significant effects;¹
2. Substantial changes occur with respect to the circumstances under which the project is undertaken which will require major revisions of the previous EIR [or ND] . . . due to the involvement of new significant environmental effects or a substantial increase in the severity of previously identified significant effects; or
3. New information of substantial importance, which was not known and could not have been known with the exercise of reasonable diligence at the time the previous EIR was certified as complete or the ND was adopted . . . shows any of the following:
 - a) The project will have one or more significant effects not discussed in the previous EIR [or ND] or negative declaration;
 - b) Significant effects previously examined will be substantially more severe than shown in the previous EIR [or ND];
 - c) Mitigation measures or alternatives previously found not to be feasible would in fact be feasible, and would substantially reduce one or more significant effects of the project, but the project proponents decline to adopt the mitigation measure or alternative; or
 - d) Mitigation measures or alternatives which are considerably different from those analyzed in the previous EIR [or ND] would substantially reduce one or more significant effects on the environment, but the project proponents decline to adopt the mitigation measure or alternative (CEQA Guidelines, Section 15162, subd. (a); see also Pub. Resources Code, Section 21166).

This addendum, checklist, and attached documents constitute substantial evidence supporting the conclusion that preparation of a supplemental or subsequent EIR or ND is not required prior to approval of the proposed project by the City of Antioch, and provides the required documentation under CEQA.

1.2.1 - Findings

As illustrated herein, the project is consistent with the 1996 Final EIR, and would involve only minor changes. There are no substantial changes proposed in the project or in the circumstances in which the project will be undertaken that require major revisions of the 1996 Final EIR, or preparation of a new subsequent or supplemental EIR or ND, due to the involvement of new significant environmental effects or a substantial increase in the severity of previously identified significant effects.

1.2.2 - Conclusions

Based on the analysis contained in this Addendum, the Antioch Planning Commission or Antioch City Council may approve the Laurel Road/Treeline Way/"D" Lane intersection reconfiguration and

¹ CEQA Guidelines Section 15382 defines "significant effect on the environment" as ". . . a substantial, or potentially substantial adverse change in any of the physical conditions within the area affected by the project, including land, air, water, minerals, flora, fauna, ambient noise, and objects of historic or aesthetic significance . . ." (see also Public Resources Code, Section 21068).

approve the removal of condition of approval #91 as part of the Park Ridge Subdivision Project. The impacts of the proposed project remain within the impacts previously analyzed in the 1996 Final EIR (CEQA Guidelines Section 15164).

The proposed project does not require any major revisions to the 1996 Final EIR. No new significant information or changes in circumstances surrounding the project have occurred since the certification of the EIR. The reconfiguration of the intersection would not result in new impacts that were not previously disclosed; and as evaluated in this addendum, the construction of a stop-controlled intersection rather than a signalized intersection would not result in new transportation impacts that were not previously disclosed. Therefore, the previous CEQA analysis completed for the Park Ridge Subdivision Project, which includes the proposed Laurel Road/Treeline Way/"D" Lane intersection, remains adequate. The applicable mitigation measures from the 1996 Final EIR will be imposed on the proposed project as described herein.

1.3 - Determination

CEQA allows the preparation of an addendum to a previously certified EIR if some changes or additions are made to the previous EIR and no conditions are present that would require the preparation of a subsequent EIR (PRC Section 21166, CEQA Guidelines Sections 15162, 15164). As explained throughout this Addendum and summarized below, no such conditions are present.

1.3.1 - Statement of Findings

1. Substantial changes are not proposed to the project that would require major revisions to the 1996 Final EIR, due to the involvement of new significant environmental effects or a substantial increase in the severity of a previously identified effect.
2. Substantial changes have not occurred with respect to the circumstances under which the project is undertaken requiring major revisions to the 1996 Final EIR, due to the involvement of new significant environmental effects or a substantial increase in the severity of a previously identified effect.
3. There is no new information of substantial importance which was not known and could not have been known at the time the 1996 Final EIR was certified showing any of the following:
 - A. The project will have a new significant effect not previously discussed in the 1996 Final EIR.
 - B. The project will not cause any significant effect examined in the 1996 Final EIR to be substantially more severe.
 - C. The mitigation measures in the 1996 Final EIR and adopted in the CEQA Findings for the Project remain feasible. All mitigation measures identified in this Addendum and required for the proposed project as identified in the 1996 Final EIR that are necessary to reduce the potentially significant impacts to a level of insignificance will be made a requirement of the project and are acceptable by the project proponent.

1.3.2 - Evidence Supporting Findings

An updated Traffic Analysis was prepared as part of this Addendum to evaluate the changes in the traffic conditions in the vicinity of the project area since 1996. As explained in Section XVI Transportation, the proposed project will not cause any new significant traffic impacts or increase the severity of the traffic impacts already evaluated in the 1996 Final EIR and the subsequent 2009 Addendum. The reconfiguration of the Laurel Road/Treeline Road/"D" Lane intersection was evaluated in the 2016 Addendum to the 1996 Final EIR for the Laurel Ranch Subdivision, and those findings are presented in this Addendum. The analysis demonstrates that this intersection would operate satisfactorily as a non-signalized, stop-controlled intersection, and does not meet the warrant for signalization.

Additional analysis is also presented in Section XVI, Transportation, to describe the potential effects of the reconfiguration of the intersection of "Lane D" and Laurel Road on the proposed crossing of the Delta De Anza Trail at Laurel Road. No new impacts were identified related to the operation of the trail at this location.

All potential impacts that were known or could have been known were adequately analyzed in the 1996 Final EIR (aesthetics, light, and glare; air quality; biological resources; cultural resources; geology and soils; greenhouse gases; hazards and hazardous materials; hydrology and water quality; land use; mineral resources; noise; population and housing; public services; recreation; transportation; and utility systems).

As summarized above and explained throughout this Addendum, this Addendum is appropriate for the proposed project since (1) substantial changes are not proposed in the project which will require major revisions to the 1996 Final EIR, (2) there are no substantial changes with respect to the circumstances under which the project is being undertaken that would require major revisions to the 1996 Final EIR, and (3) there is no new information which was not known or could not have been known at the time the 1996 Final EIR was certified.

1.4 - Mitigation Monitoring and Reporting Program

As required by Public Resources Code Section 21081.6, subd. (a)(1), a mitigation monitoring and reporting program (MMRP) has been prepared for the project in order to monitor the implementation of the mitigation measures that have been adopted for the project. Any long-term monitoring of mitigation measures imposed on the overall development will be implemented through the MMRP.

SECTION 2: PROJECT DESCRIPTION

2.1 - Location and Setting

2.1.1 - Location

The project site is located in the City of Antioch, Contra Costa County, California (Exhibit 1). The project site is bounded by single-family residential uses (west and south), open space and an Oakley Water District elevated tank site and open space (north), and State Route 4 (SR-4) (east) (Exhibit 2). The project site is located on the Antioch, California 7.5-minute United States Geological Survey topographical quadrangle, Township 2 North, Range 2 East, Section 6 (Latitude 37° 58'48" North; Longitude 121° 44'24" West).

2.2 - Project Background

2.2.1 - East Lone Tree Specific Plan

In 1988, the Antioch City Council adopted a General Plan Update that designated a 785-acre area- which included the project site-as “Future Urban Area 2.” The General Plan Update envisioned various urban uses in this area including business park, office, and light industrial; however, it did not set forth any development targets.

In 1992, the Infrastructure Plan Environmental Impact Report (EIR) identified a range of development potential for “Future Urban Area 2” that consisted of 227 to 313 acres of commercial and employment land uses, and 1,300 to more than 2,600 dwelling units. Future Urban Area 2 was annexed into the City of Antioch in two phases, one in 1993, and one in 1995.

In 1996, the City of Antioch adopted the East Lone Tree Specific Plan and certified the associated Final EIR (1996 Final EIR), officially known as “Future Urbanization Area 2 East Lone Tree Specific Plan Area Project-Level EIR.” The Specific Plan contemplated the development of 1,322 dwelling units, regional retail uses, a school, and parks.

2.2.2 - Park Ridge Subdivision

The Park Ridge Subdivision #8846 consists of the subdivision and development of 169.7 acres within the Future Urbanization Area (FUA) #2 Specific Plan area, located between the State Route 4 Bypass and Canada Valley Road, south of Laurel Road. The project sponsor, Davidon Homes, proposes to develop a total of 525 single-family residential homes, and related public facilities. The project site adjoins existing or approved development to the west and south, and adjoins the State Route 4 Bypass to the east.

Development of the project, as proposed, includes a neighborhood park facility (8.22 acres), a major public open space preserve (25.5 acres) and the extension of Country Hills Drive along the east boundary of the site adjoining the State Route 4 Bypass, as called for in the Specific Plan.

An Addendum to the 1996 Final EIR was prepared and adopted for the Park Ridge Subdivision in 2009 (2009 Addendum) to address refinements to the land plan. The 2009 Addendum transportation analysis evaluated the need for a signalized intersection at the intersection of Laurel Road/Treeline Way/"D" Lane and found that the level of service and delay did not meet the warrant for signalization. However the City Council, in approving the project, included a condition of approval (#91) requiring the construction of a fully signalized intersection. The Park Ridge project, and related roadway improvements have not yet been constructed.

2.3 - Project Characteristics

2.3.1 - Project Summary

Stop-controlled intersection

The proposed intersection of Laurel Road/Treeline Way/"D" Lane would be located along the future extension of Laurel Road west of State Route 4, and would serve both Laurel Ranch Subdivision to the north, and Park Ridge Subdivision to the south as shown in Exhibit 3.

Exhibit 3 illustrates the proposed revised intersection configuration and traffic movements:

- From Treeline Way, the intersection would include right-in, right-out, and a left-in access from a left hand median turn pocket on Laurel Road.
- From "D" Lane, access would consist of right-in and right out only.

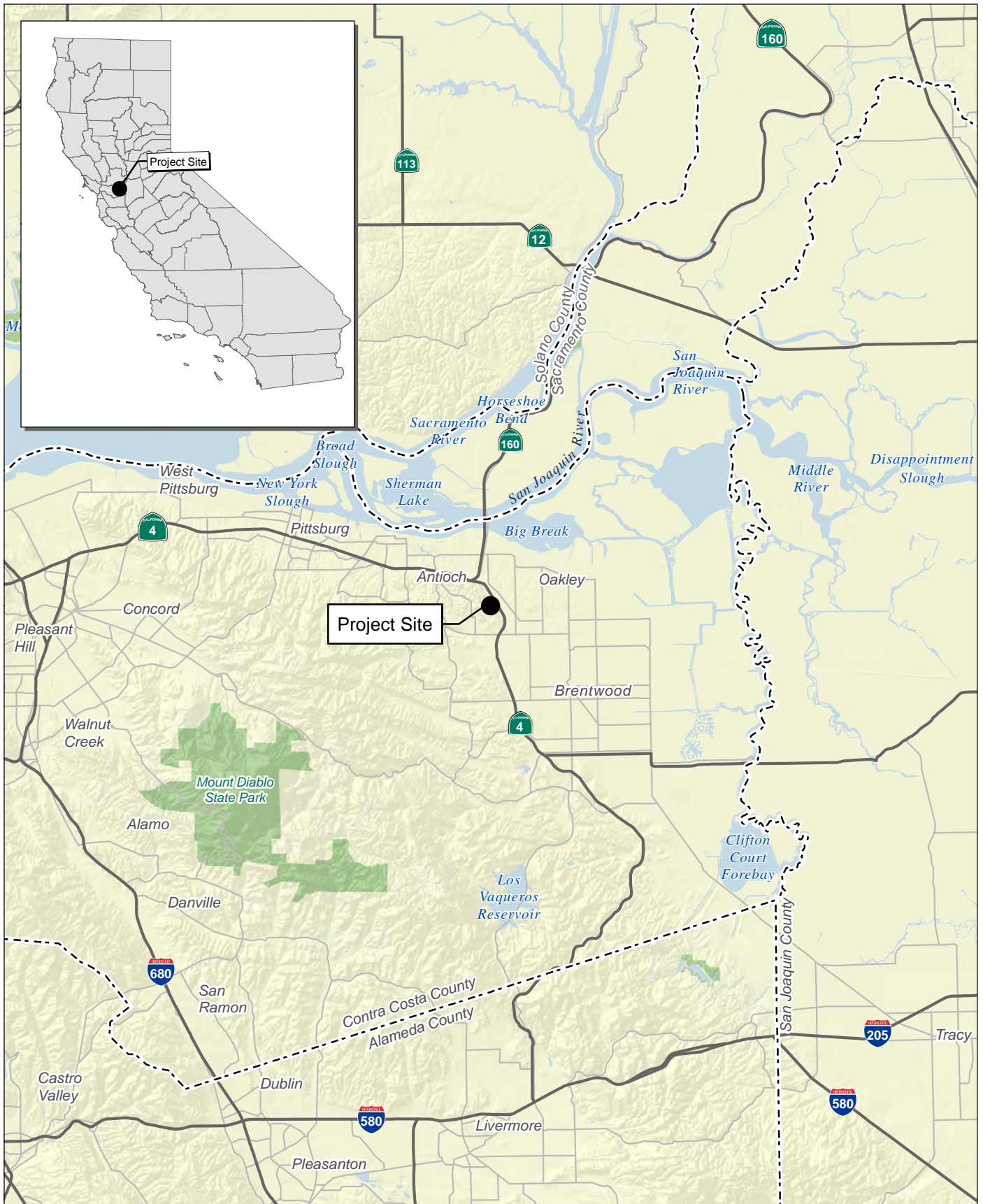
Recreational Trail Facilities

Both the Park Ridge and Laurel Ranch Subdivisions include construction of a connecting trail to the Delta De Anza Regional trail along their western boundaries. The trail would cross Laurel Road as shown in Exhibit 3. To ensure that pedestrians using the Delta De Anza Trail can cross Laurel Road safely, a pedestrian crossing will be installed just to the west of Treeline Way and "D" Lane, in general alignment with the proposed regional trail.

2.4 - Discretionary Approvals

The proposed project would require the following discretionary approval:

- Removal of the signalized intersection as a condition of approval for the Park Ridge Vesting Tentative Subdivision Map



Source: Census 2000 Data, The CaSIL, FCS GIS 2013.

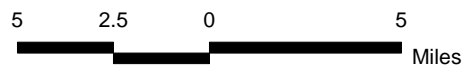
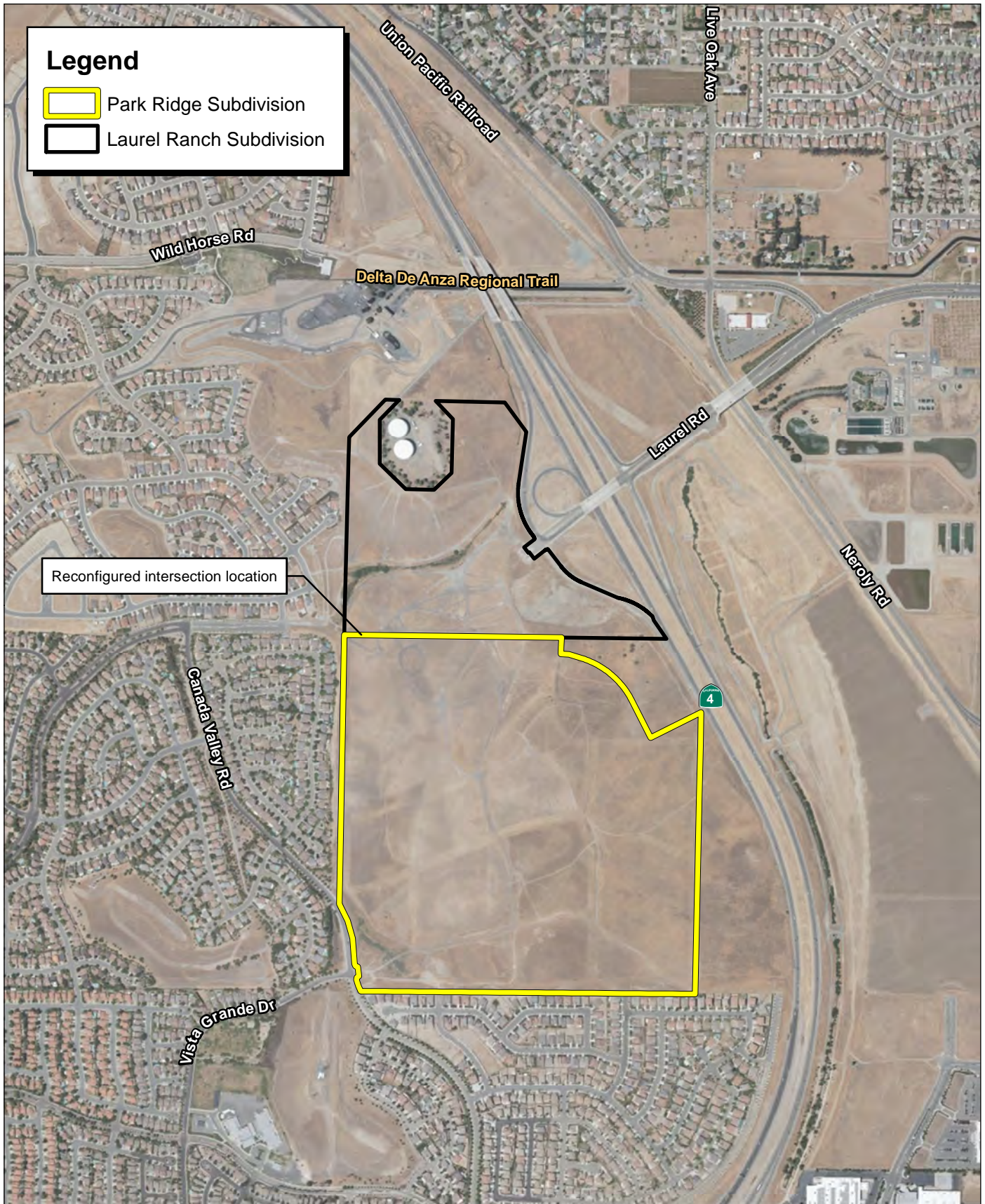


Exhibit 1 Regional Location Map

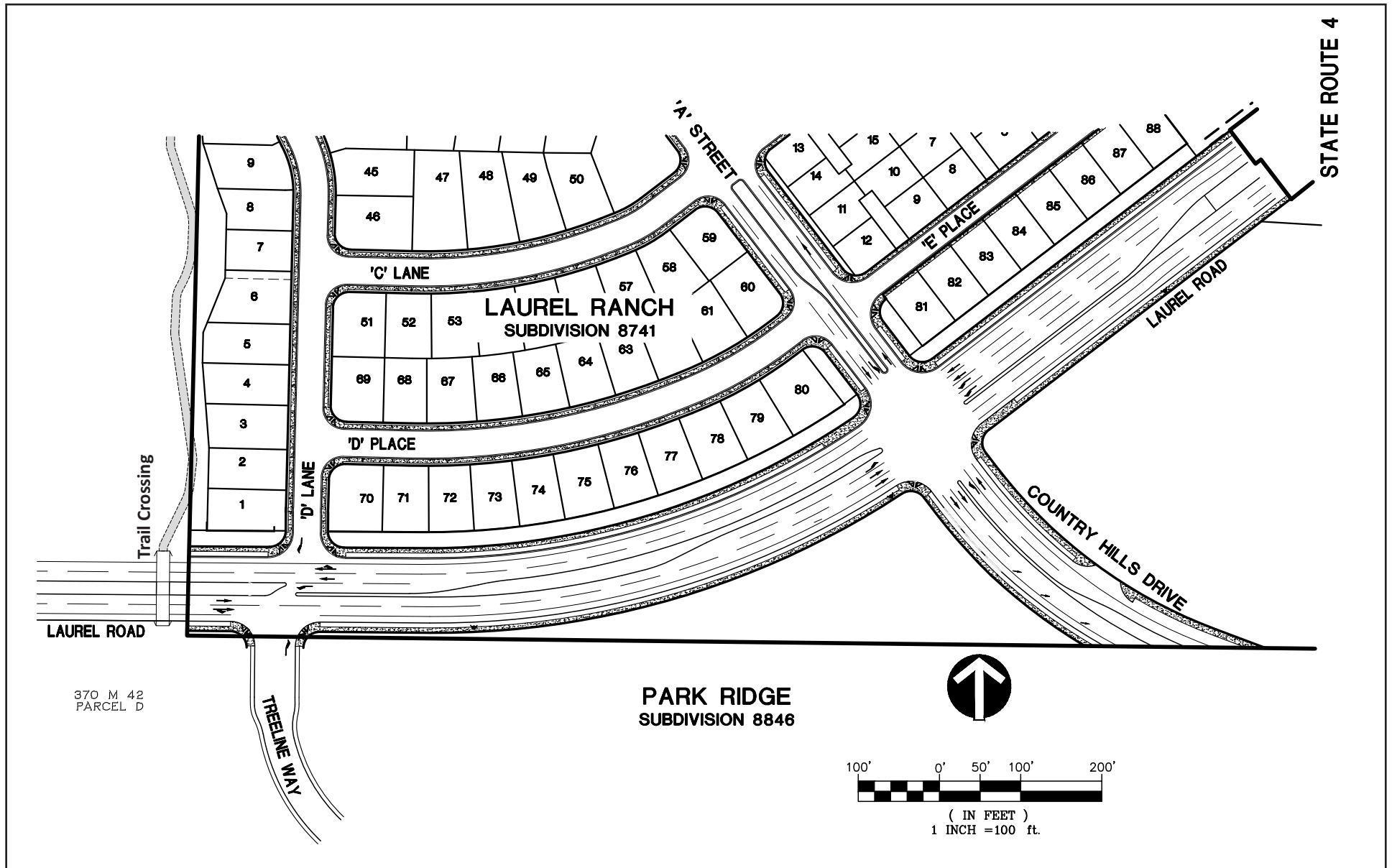
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Source: ESRI Imagery, 2014



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Source: DK Consulting, 2016



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Exhibit 3 Laurel Road Reconfiguration

CITY OF ANTIOCH • DAVIDON HOMES (PARK RIDGE SUBDIVISION #8846)
2ND ADDENDUM TO PROJECT LEVEL EIR FOR FUTURE URBANIZATION AREA #2 SPECIFIC PLAN

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SECTION 3: CEQA CHECKLIST

The purpose of the checklist is to evaluate the categories in terms of any changed condition (e.g., changed circumstances, project changes, or new information of substantial importance) that may result in a changed environmental result (e.g., a new significant impact or substantial increase in the severity of a previously identified significant effect) (CEQA Guidelines Section 15162).

The questions posed in the checklist come from Appendix G of the CEQA Guidelines. A “no” answer does not necessarily mean that there are no potential impacts relative to the environmental category, but that there is no change in the condition or status of the impact since it was analyzed and addressed with mitigation measures in the 1996 Final EIR prepared for the project. These environmental categories might be answered with a “no” in the checklist, since the proposed project does not introduce changes that would result in a modification to the conclusion of the certified EIR.

3.1 - Explanation of Checklist Evaluation Categories

(1) Conclusion in Prior EIR and Related Documents

This column summarizes the conclusion of the EIR relative to the environmental issue listed under each topic.

(2) Do the Proposed Changes Involve New Impacts?

Pursuant to CEQA Guidelines Section 15162, subd. (a)(1), this column indicates whether the changes represented by the revised Project will result in new significant environmental impacts not previously identified or mitigated by the EIR, or whether the changes will result in a substantial increase in the severity of a previously identified significant impact.

(3) New Circumstances Involving New Impacts?

Pursuant to CEQA Guidelines Section 15162, subd. (a)(2), this column indicates whether there have been substantial changes with respect to the circumstances under which the Project is undertaken that will require major revisions to the EIR, due to the involvement of new significant environmental effects or a substantial increase in the severity of previously identified significant effects.

(4) New Information Requiring New Analysis or Verification?

Pursuant to CEQA Guidelines Section 15162, subd. (a)(3)(A-D), this column indicates whether new information of substantial importance, which was not known and could not have been known with the exercise of reasonable diligence at the time the EIR was certified as complete, shows any of the following:

- (A) The Project will have one or more significant effects not discussed in the previous EIR [or ND];

- (B) Significant effects previously examined will be substantially more severe than shown in the previous EIR [or ND];
- (C) Mitigation measures or alternatives previously found not to be feasible would in fact be feasible, and would substantially reduce one or more significant effects of the Project, but the project proponents decline to adopt the mitigation measure or alternative; or
- (D) Mitigation measures or alternatives which are considerable different from those analyzed in the previous EIR [or ND] would substantially reduce one or more significant effect of the environment, but the project proponents decline to adopt the mitigation measure or alternative.

If the additional analysis completed as part of this environmental review were to find that the conclusions of the EIR remain the same and no new significant impacts are identified, or identified impacts are not found to be substantially more severe, or additional mitigation is not necessary, then the question would be answered “no” and no additional environmental document would be required.

(5) Mitigation Measures Implemented or Address Impacts

Pursuant to CEQA Guidelines Section 15162, subd. (a)(3), this column indicates whether the EIR provided mitigation measures to address effects in the related impact category. These mitigation measures will be implemented with the construction of the project, as applicable. If “NA” is indicated, both the 1996 Final EIR and this Initial Study/Addendum have concluded that the impact either would not occur with this project or would not be significant, and, therefore, no additional mitigation measures are needed.

3.2 - Discussion and Mitigation Sections

(1) Discussion

A discussion of the elements of the checklist is provided under each environmental category in order to clarify the answers. The discussion provides information about the particular environmental issue, how the project relates to the issue, and the status of any mitigation that may be required or that has already been implemented.

(2) Relevant Mitigation Measures

Applicable mitigation measures from the EIR that apply to the project are listed under each environmental category.

(3) Conclusions

A discussion of the conclusion relating to the analysis is contained in each section.

| Environmental Issue Area | Conclusion in 1996 EIR | Do the Proposed Changes Involve New Impacts? | New Circumstances Involving New Impacts? | New Information Requiring New Analysis or Verification? | 1996 EIR Mitigation Measures |
|---|---|---|---|--|------------------------------|
| XVI. Transportation | | | | | |
| <i>Would the project:</i> | | | | | |
| a) Conflict with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the circulation system, taking into account all modes of transportation including mass transit and non-motorized travel and relevant components of the circulation system, including but not limited to intersections, streets, highways and freeways, pedestrian and bicycle paths, and mass transit? | Less than significant after mitigation. | No. The proposed project does not involve changes that would result in new impacts on measures of effectiveness of transportation. | No. There are no new circumstances that would result in new or more severe impacts on measures of effectiveness of transportation. | No. No new information has been disclosed pertaining to the proposed project that would require additional analysis of measures of effectiveness of transportation. | B11, 12, 13 |
| f) Conflict with adopted policies, plans, or programs regarding public transit, bicycle, or pedestrian facilities, or otherwise decrease the performance or safety of such facilities. | Less than significant after mitigation. | No. The proposed project does not involve changes that would result in new impacts on public transit, bicycle, or pedestrian facilities. | No. There are no new circumstances that would result in new or more severe impacts on public transit, bicycle, or pedestrian facilities. | No. No new information has been disclosed pertaining to the proposed project that would require additional analysis of public transit, bicycle, or pedestrian facilities. | B11, 12, 13 |

Discussion and Mitigation

The intersection of Treeline Way and Laurel Road was evaluated by Fehr & Peers Transportation Consultants as part of the 2009 Addendum prepared for the Park Ridge Project.

W-Trans, a traffic engineering and transportation planning consultant, evaluated the reconfiguration of the intersection of “D” Lane and Laurel Road as part of an addendum prepared for the Laurel Ranch Project in 2016. Both of these analyses are summarized here to document the effect of the proposed reconfiguration of the intersection. The complete W-Trans Traffic Impact Analysis and Fehr & Peers Technical Memorandum are attached in Appendix A.

Would the project:

- a) **Conflict with an applicable plan, ordinance or policy establishing measures of effectiveness for the performance of the circulation system, taking into account all modes of transportation including mass transit and non-motorized travel and relevant components of the circulation system, including but not limited to intersections, streets, highways and freeways, pedestrian and bicycle paths, and mass transit?**

The 1996 Final EIR did not include specific analysis of the Laurel Road/Treeline Way intersection. As part of the 2009 Addendum for the Park Ridge Project, Fehr & Peers Transportation Consultants evaluated the operation of the side-street stop-controlled Laurel Road/Treeline Way intersection under Cumulative Plus Project conditions. The analysis concluded that the intersection would operate at level of service (LOS) F during the AM and PM peak hours, based on the HCM methodology. However, because the intersection serves low traffic volumes it would not meet the CA MUTCD peak-hour volume signal warrant. Thus, the proposed project would not cause an impact at this intersection because the significance criterion for unsignalized intersections requires the intersection to operate at an unacceptable LOS **and** satisfy the CA MUTCD peak-hour signal warrant. Based on this conclusion, the 2009 Addendum did not recommend any mitigation or signalization at this intersection. The City Council, in approving the Project, imposed a condition of approval (#91) requiring a signal at this location although it is not required based on the established CEQA significance criteria.

In 2016, the land owners for the Laurel Ranch Project, submitted a revised Final Tentative Map which moves the location of “D” Lane to the east, offsetting it from Treeline Way, and making a signalized intersection infeasible. The Laurel Ranch Project proposes right in/right out access at “D” Lane.

It is now proposed that site access from Treeline Way would consist of a right-in, right-out, and a left-in from a left hand median turn pocket. Exhibit 3 illustrates the revised Laurel Road configuration and proposed traffic movements. As a result, condition of approval #91 is proposed to be revised as follows:

A median on Laurel Road at Treeline Way shall be designed and constructed to allow for left turn ingress into the project and right turn only egress onto Laurel Road. A pedestrian crossing on Laurel Road, west of Treeline Way, and in general alignment with the proposed regional trail system, shall be constructed.

As part of the Laurel Ranch Addendum, W-Trans collected new traffic counts in September 2015 and evaluated project impacts based on the current unit counts for both the Laurel Ranch and Park Ridge Projects in the near term and cumulative scenarios. As discussed below, the project intersections

would continue to operate acceptably. The intersection of Laurel Road/Treeline Way, as noted previously, would not meet the warrant for signalization, based on the low traffic volumes on Treeline Way.

Table 1 summarizes the trip generation associated with the Laurel Ranch Subdivision project. As shown in the table, the proposed project would generate 1,780 daily trips, 140 AM peak-hour trips, and 187 PM peak-hour trips. (Note: the traffic analysis was conducted using an earlier figure of 187 units so presents a more conservative analysis.)

Table 1: Trip Generation Summary

| Land Use | Units | Daily | | AM Peak Hour | | | | PM Peak Hour | | | |
|--------------------------------|--------|-------|-------|--------------|-------|----|-----|--------------|-------|-----|-----|
| | | Rate | Trips | Rate | Trips | In | Out | Rate | Trips | In | Out |
| Proposed | | | | | | | | | | | |
| Single Family Detached Housing | 187 du | 9.52 | 1,780 | 0.75 | 140 | 35 | 105 | 1.00 | 187 | 118 | 69 |
| Note: du = dwelling unit | | | | | | | | | | | |

Intersection Operations

Intersection operations were evaluated based on the significance threshold established by the jurisdiction in which they are located or the agency that maintains them. The study area is located in the City of Antioch in Contra Costa County. The East County Regional Transportation Planning Committee, under the Contra Costa Transportation Planning Authority and in conjunction with local agencies, developed the Draft East County Action Plan for Routes of Regional Significance, which establishes objectives for arterial routes. Local agencies, such as the City of Antioch, have adopted the plan and resulting objectives.

In the study area, if one or more legs of the study intersection are ramps for SR-4, the intersection is maintained by Caltrans; otherwise, the intersection falls under the jurisdiction of the City of Antioch. For the intersection of Lone Tree Way/Empire Avenue, the jurisdiction is both the City of Antioch and the City of Brentwood. The Caltrans recommended target LOS is the transition from LOS C to D. The cities of Antioch and Brentwood have the recommended objective target of LOS D.

W-Trans evaluated the proposed project's impacts on intersection operations. Table 2 summarizes Existing (without project) Conditions and Existing Plus Project intersection operations. Note that the Existing Plus Project scenario accounts for the planned extension of Laurel Road from the SR-4 interchange to its current terminus west of the project site, while the Existing Conditions scenario does not. As shown in the table, all intersections would operate at acceptable LOS. Therefore, impacts would be less than significant, and would remain the same or less than those identified in the 1996 Final EIR.

Table 2: Existing and Existing Plus Project Intersection Operations

| Study Intersection Approach | Existing Conditions | | | | Existing plus Project | | | |
|--|---------------------|-----|---------|-----|-----------------------|-----|---------|-----|
| | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. SR-4 WB Ramps/Hillcrest Ave | 7.7 | A | 8.0 | B | 7.7 | A | 8.0 | B |
| 2. SR-4 EB Ramps/Hillcrest Ave | 26.5 | C | 25.5 | C | 26.6 | C | 25.5 | C |
| 3. Hillcrest Rd/Laurel Rd | 10.4 | B | 8.5 | A | 13.7 | B | 12.9 | A |
| 4. Laurel Rd/Canada Valley Rd | — | — | — | — | 9.1 | A | 8.0 | A |
| 5. SR-4 EB Ramps/Laurel Rd | 1.4 | A | 1.0 | A | 7.8 | A | 14.4 | B |
| 6. SR-4 WB Ramps/Laurel Rd | 9.5 | A | 15.4 | B | 21.0 | C | 30.9 | C |
| 7. SR-4 EB Ramps/Lone Tree Way | 14.7 | B | 16.3 | B | 14.7 | B | 16.3 | B |
| 8. SR-4 WB Ramps/Lone Tree Way | 8.2 | A | 10.8 | B | 8.3 | A | 10.9 | B |
| 9. Lone Tree Way/Empire Ave | 15.2 | B | 18.8 | B | 15.3 | B | 18.9 | B |
| 10. Laurel Rd/Country Hills Dr | — | — | — | — | 4.5 | A | 4.7 | A |
| Notes: Delay is measured in average seconds per vehicle LOS = Level of Service | | | | | | | | |

Table 3 summarizes Cumulative (without project) Conditions and Cumulative Plus Project intersection operations. The Cumulative Conditions represent the projected traffic conditions in the year 2040. This includes the completion of all seven phases of the Park Ridge project as well as the completion of any proposed roadway infrastructure improvements in the study area. Note that both scenarios account for the planned extension of Laurel Road from the SR-4 interchange to its current terminus west of the project site. While the intersections of SR-4 Eastbound Ramps/Hillcrest Avenue and SR-4 Eastbound Ramps/Lone Tree Way would still operate below the desired Caltrans threshold, the intersections would continue to operate acceptably, based on the East County Action Plan. Therefore, impacts would be less than significant, and would remain the same or less than those identified in the 1996 Final EIR.

Table 3: Cumulative and Cumulative Plus Project Intersection Operation

| Study Intersection Approach | Cumulative Conditions | | | | Cumulative plus Project | | | |
|--------------------------------|-----------------------|-----|---------|-----|-------------------------|-----|---------|-----|
| | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. SR-4 WB Ramps/Hillcrest Ave | — | — | — | — | — | — | — | — |
| 2. SR-4 EB Ramps/Hillcrest Ave | 13.9 | B | 51.0 | D | 13.9 | B | 51.0 | D |
| 3. Hillcrest Rd/Laurel Rd | 68.8 | E | 107.3 | F | 71.6 | E | 108.9 | F |

Table 3 (cont.): Cumulative and Cumulative Plus Project Intersection Operation

| Study Intersection Approach | Cumulative Conditions | | | | Cumulative plus Project | | | |
|--|-----------------------|-----|-------------|----------|-------------------------|-----|-------------|----------|
| | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 4. Laurel Rd/Canada Valley Rd | 19.6 | B | 43.7 | D | 19.9 | B | 45.4 | D |
| 5. SR-4 EB Ramps/Laurel Rd | 17.4 | B | 25.4 | C | 18.8 | B | 30.3 | C |
| 6. SR-4 WB Ramps/Laurel Rd | 15.8 | B | 21.4 | C | 17.3 | B | 23.0 | C |
| 7. SR-4 EB Ramps/Lone Tree Way | 30.2 | C | 49.7 | D | 30.3 | C | 49.7 | D |
| 8. SR-4 WB Ramps/Lone Tree Way | 13.4 | B | 21.2 | C | 13.4 | B | 21.3 | C |
| 9. Lone Tree Way/Empire Ave | 18.6 | B | 27.4 | C | 18.6 | B | 27.5 | C |
| 10. Laurel Rd/Country Hills Dr | 20.3 | C | 13.9 | B | 37.6 | D | 23.2 | C |
| 11. Laurel Rd/Slatten Ranch Rd | 30.6 | C | 55.9 | E | 30.9 | C | 57.0 | E |
| Notes: Delay is measured in average seconds per vehicle LOS = Level of Service; Bold text = deficient operation | | | | | | | | |

Reconfiguration of Laurel Road/Treeline Way (Proposed Project)

As part of the Davidon Homes (Park Ridge Subdivision) Addendum to the Project Level EIR, the intersection of D Lane-Treeline Way/Laurel Road had no turning movement restrictions and was analyzed with stop-controlled side streets. Based on the significance criterion for unsignalized intersections, it did not meet this signal warrant and as such would not result in a significant impact.

It was determined that if the intersection were to be signalized, it would operate at an acceptable LOS. This traffic analysis and the following queueing analysis demonstrate that there would be no additional traffic impacts from the proposed design of this intersection with no signalization.

The project was analyzed as depicted in Exhibit 3, in which the Laurel Road median would be designed to allow westbound left turns into the Park Ridge project directly to the south of D Lane. The queueing analysis, shown in Table 4 for the proposed left-turn pocket indicated that there would be sufficient length to accommodate the projected queues from the Park Ridge Project.

Table 4: Queuing Summary

| Intersection Approach | Estimated Available Storage | 95 th Percent Queues | | | |
|---|--------------------------------|---------------------------------|-----|--------------|-----|
| | | AM Peak Hour | | PM Peak Hour | |
| | | C | C+P | C | C+P |
| Laurel Rd/D Lane | | | | | |
| WB Left-Turn | 200* | 36 | 52 | 75 | 68 |
| Notes: 95 th Percent Queue based on the calculated potential from five averaged SIMTRAFFIC runs * = Estimates of storage length based on potential space according to site plan, measured in feet C = Cumulative Conditions; C+P = Future plus Project Conditions | | | | | |

According to the queuing calculations, there would be adequate space in the proposed Laurel Road median to incorporate a left-turn pocket at the intersection of Laurel Road and D Lane (Treeline Way). (While the median can accommodate a storage length of approximately 200 feet, the queuing calculations indicate that the storage length could be shorter, if desired). Impacts would be less than significant from queuing at the study intersection, including the new design of the intersection of Laurel Road and D Lane (Treeline Way) allowing westbound left turns from Laurel Road into Treeline Way, and impacts would remain the same or less than those identified in the 1996 Final EIR.

f) Conflict with adopted policies, plans, or programs regarding public transit, bicycle, or pedestrian facilities, or otherwise decrease the performance or safety of such facilities?

For the 1996 Final EIR, pedestrian or bicycle paths had not yet been specified for the project, but incorporation of the Mitigation B11, 12, and 13 has resulted in adequate bike and pedestrian connections.

Sidewalks would be installed along Laurel Road and along the internal streets as shown in Exhibit 3.

To improve connectivity with the other nearby trail networks, particularly the Delta De Anza trail located just north of the Laurel Ranch project, the internal trail from the Park Ridge Subdivision would cross Laurel Road west of the Treeline Way intersection (Exhibit 3). The crossing would include striping on the pavement to identify the crossing for motorists and a pedestrian crossing signal light.

There would be no impacts beyond those identified in the 1996 Final EIR.

Relevant Mitigation Measures

The following mitigation measures from the 1996 Final EIR are implemented by the proposed project.

MM B11, B12, B13 Intersections, roadways, sidewalks and bike lanes will be designed in subsequent plans to meet City standards.

Conclusion

The conclusions from the 1996 Final EIR remain unchanged when considering the proposed revisions to condition of approval #91 and the development of the proposed project.

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SECTION 4: REFERENCES

- City of Antioch. 2009. Davidon Homes (Park Ridge Subdivision #8846) Addendum to Project Level EIR for FUA#2 Specific Plan. Website: <http://www.ci.antioch.ca.us/CityGov/CommDev/PlanningDivision/docs/Park-Ridge-Development/EIR-Addendum-Final.pdf>.
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SECTION 5: LIST OF PREPARERS

5.1 - Lead Consultant

FirstCarbon Solutions
1350 Treat Boulevard, Suite 380
Walnut Creek, CA 94597
Phone: 925.357.2562
Fax: 925.357.2572

Project Director Mary Bean
Project Manager Elizabeth Johnson
Editor Ed Livingston
GIS/Graphics John De Martino
Word Processor Ericka Rodriguez
Reprographics Octavio Perez

5.2 - Technical Subconsultant

W-Trans
475 14th Street, Suite 290
Oakland, CA 94612

Principal Mark Spencer

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Appendix A: **Traffic Impact Analyses**

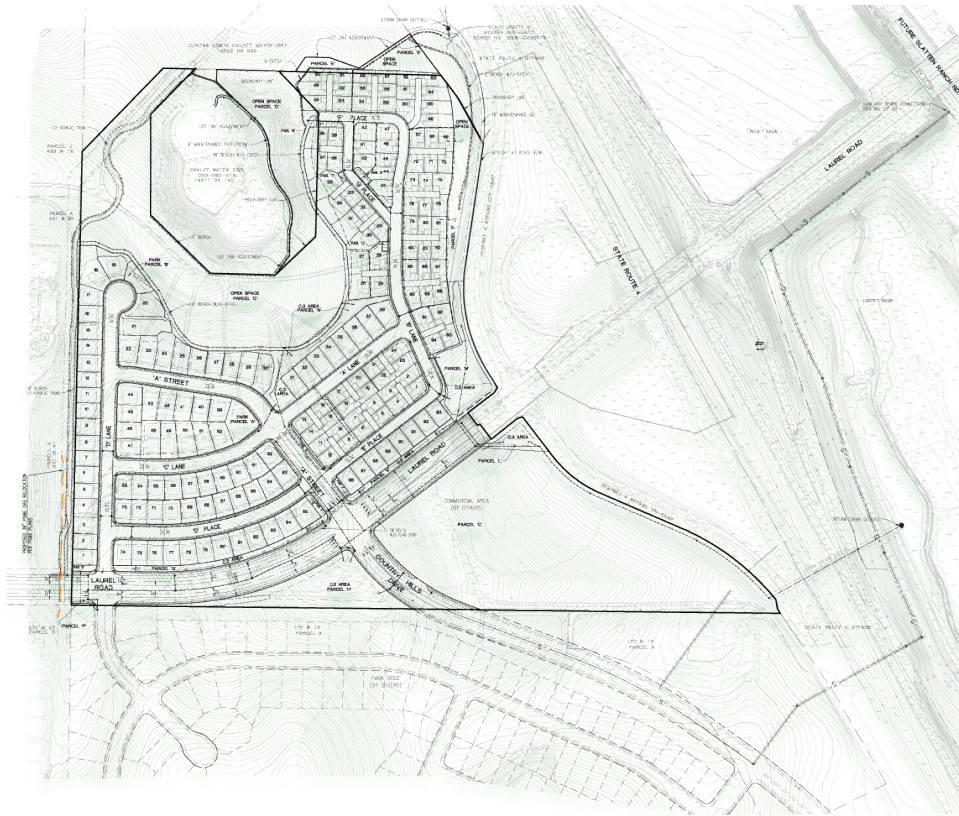
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A.1 - 2016 Traffic Impact Analysis prepared by W-Trans for the Laurel Ranch Subdivision Addendum

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Transportation Impact Analysis for Laurel Ranch



Prepared for the City of Antioch

Submitted by
W-Trans

December 15, 2015



**TRAFFIC ENGINEERING
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Table of Contents

| | |
|--|----|
| Executive Summary | 1 |
| Introduction..... | 2 |
| Transportation Setting..... | 4 |
| Capacity Analysis | 9 |
| Alternative Modes | 27 |
| Access and Circulation..... | 28 |
| Conclusions and Recommendations..... | 29 |
| Study Participants and References..... | 30 |

Figures

| | |
|--|----|
| 1. Study Area and Lane Configurations..... | 3 |
| 2. Existing Traffic Volumes..... | 10 |
| 3. Existing plus Nearby Future Project Traffic Volumes | 11 |
| 4. Future Lane Configurations..... | 14 |
| 5. Future Traffic Volumes | 15 |
| 6. Site Plan | 17 |
| 7. Trip Distribution..... | 18 |
| 8. Existing Project Traffic Volumes | 20 |
| 9. Future Project Traffic Volumes..... | 23 |

Tables

| | |
|---|----|
| 1. Signalized Intersection Level of Service Criteria | 6 |
| 2. Level of Service Standards | 7 |
| 3. Existing Peak Hour Intersection Levels of Service | 9 |
| 4. Existing plus Nearby Future Project Peak Hour Intersection Levels of Service | 12 |
| 5. Cumulative Conditions Peak Hour Intersection Levels of Service | 13 |
| 6. Trip Generation Summary | 16 |
| 7. Trip Distribution Assumptions..... | 19 |
| 8. Existing and Existing plus Project Peak Hour Intersection Levels of Service | 21 |
| 9. Existing plus Nearby Project and Existing plus Nearby Project plus Project Peak Hour Intersection Levels of Service..... | 22 |
| 10. Cumulative and Cumulative plus Project Peak Hour Levels of Service..... | 24 |
| 11. 95 th Percentile Project Driveway Queues Exceeding Available Storage..... | 25 |
| 12. 95 th Percentile Left-Turn Queues Exceeding Available Storage for Alternative Access 2..... | 26 |

Appendices

- A. CCTA 2010 HCM Methodology
- B. Intersection Level of Service Calculations
- C. Project Driveway Queuing Calculations
- D. Alternative Access Calculations
- E. Sight Distance

Executive Summary

The proposed Laurel Ranch subdivision would result in the construction of 187 single family dwellings. The anticipated trip generation averages 1,780 trips per day, including 140 a.m. peak hour trips and 187 trips during the p.m. peak hour.

All analysis was conducted in accordance with the guidelines set forth by Caltrans, the Contra Cost Transit Authority (CCTA), the East County Action Plan, and the General Plans for the Cities of Antioch and Brentwood. The study area includes eleven intersections. All the study intersections are located along routes of regional significance, or "suburban arterial routes" according to the East County Action Plan. As such the corresponding Multimodal Transportation Service Objectives (MTSOs) for the intersections were evaluated.

The project site would be located west of State Route (SR) 4 and north of the future Laurel Road extension, from which access would be taken, on an undeveloped site. Extension of Laurel Road and associated nearby improvements were assumed to be completed in conjunction with the project.

Analysis of the currently existing study intersections indicate they are operating acceptably under Existing conditions. With the addition of project-generated Laurel Ranch subdivision trips, including the planned roadway modifications, all study intersections analyzed would be expected to operate acceptably.

Under the Existing plus Nearby Future Projects scenario, project trips from Phase 1 of the nearby Park Ridge Subdivision were added. With the addition of the Laurel Ranch project trips and associated roadway improvements, the study intersections analyzed would be expected to continue operating acceptably according to the standards set forth by the regulating agencies.

Under the Cumulative No Project scenario, including several roadway improvements, several study intersections are expected to operate deficiently based on the projected growth from the area. For the intersections projected to be operating deficiently in the future, the delay added from the addition of the project trips would be minimal and within the threshold set forth by the City; no significant cumulative impacts are therefore anticipated.

Vehicles would access the project via the signalized Laurel Road/Country Hills Drive intersection and the stop-controlled access road at D Lane. Only right turns in and out of the driveway would be allowed at D Lane as there is a median restricting left turns. A queuing analysis for the two project driveways, with lengths as shown in the site plan, indicated that sufficient storage space is available for the projected queues.

As part of the *Davidon Homes (Park Ridge Subdivision) Addendum to the Project Level EIR*, the intersection of D Lane-Treeline Way/Laurel Road had no turning movement restrictions and was analyzed with stop-controlled side streets. Based on the significance criterion for unsignalized intersections, it did not meet this signal warrant and as such would not result in a significant impact. It was determined that if the intersection were to be signalized it, it would operate at an acceptable level of service.

An alternative access was analyzed in which the Laurel Road median would be modified to allow westbound left turns into the Park Ridge project directly to the south of D Lane. The queuing analysis for the proposed left-turn pocket indicated that there would be sufficient length to accommodate the projected queues from the Park Ridge Project.

Pedestrian, bicycle, and transit facilities would be provided along the project frontage. These include sidewalks, bike lanes, and eastbound and westbound Tri Delta Transit bus stops. With the completion of the project and the extension of Laurel Road, it is recommended that the sidewalks be constructed to connect with the existing network. Also, landscaping maintenance would be required at D Lane to maintain a clear line of site for motorists existing D Lane onto Laurel Road.

Introduction

This report presents an analysis of the potential transportation impacts that would be associated with occupation of the proposed Laurel Ranch Housing Development, consisting of 187 single family homes, to be located in the currently unoccupied area north of the future Laurel Road connection in the City of Antioch. The transportation impact study was completed in accordance with the criteria established by the California Department of Transportation (Caltrans), the Contra Costa Transit Authority (CCTA), and the City of Antioch, as found in the East County Action Plan, and it is consistent with standard traffic engineering techniques.

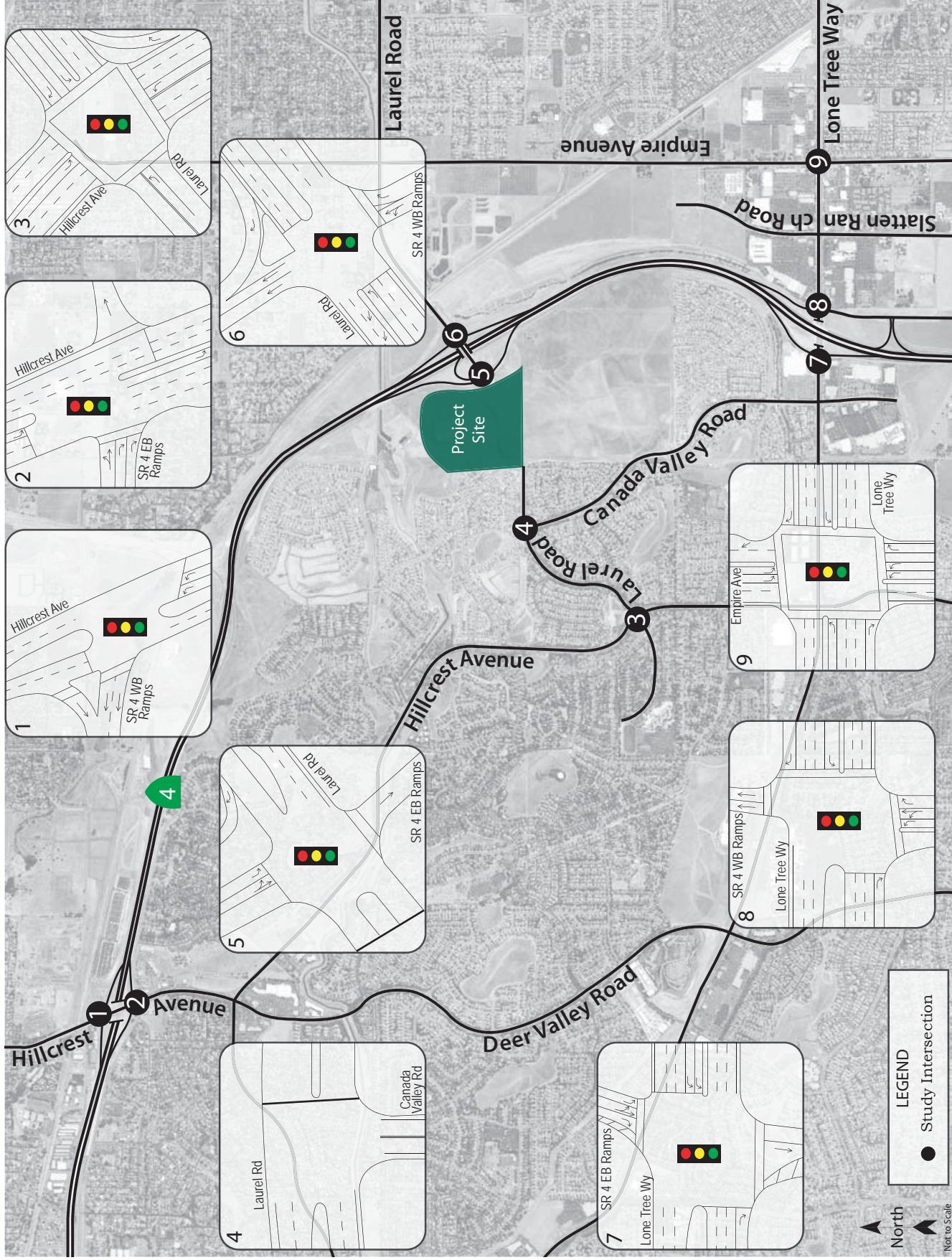
Prelude

The purpose of a transportation impact study is to provide City of Antioch staff and policy makers with data that they can use to make an informed decision regarding the potential impacts of the Laurel Ranch project, and any associated improvements that would be required in order to mitigate these impacts to a level of insignificance as defined by the City of Antioch's General Plan, CCTA guidelines, or other policies. Vehicular traffic impacts are typically evaluated by determining the number of new trips that the proposed use would be expected to generate, distributing these trips to the surrounding street system based on existing travel patterns or anticipated travel patterns specific to the proposed project, then analyzing the impact the new traffic would be expected to have on critical intersections or roadway segments. Impacts relative to access for pedestrians, bicyclists, and to transit are also addressed.

Project Profile

The proposed Laurel Ranch Subdivision has been through several iterations. The City has been planning to convert the former agricultural land into residential uses for several decades. Following the most recent addendum to the Laurel Ranch Subdivision, the project as proposed has a reduced unit count.

The project site as proposed would allow for the development of 187 single family homes on the undeveloped agricultural land. The site is located west of the newly constructed SR 4 Bypass and north of the future Laurel extension and north of the future Laurel Road/Country Hills Drive intersection, as shown in Figure 1.



Transportation Setting

Operational Analysis

Study Area and Periods

The study area consists of the following intersections:

1. State Route (SR) 4 Westbound Ramps/Hillcrest Avenue
2. SR 4 Eastbound Ramps/Hillcrest Avenue
3. Hillcrest Road/Laurel Road
4. Laurel Road/Canada Valley Road
5. SR 4 Eastbound Ramps/Laurel Road
6. SR 4 Westbound Ramps/Laurel Road
7. SR 4 Eastbound Ramps/Lone Tree Way
8. SR 4 Westbound Ramps/Lone Tree Way
9. Lone Tree Way/Empire Avenue
10. Laurel Road/County Hills Drive¹
11. Laurel Road/Slatten Ranch Road

Operating conditions during the a.m. and p.m. peak periods were evaluated to capture the highest potential impacts for the proposed project as well as the highest volumes on the local transportation network. The morning peak hour occurs between 7:00 and 9:00 a.m. and reflects conditions during the home to work or school commute, while the p.m. peak hour occurs between 4:00 and 6:00 p.m. and typically reflects the highest level of congestion during the homeward bound commute.

Study Intersections

SR 4 Westbound Ramps/Hillcrest Avenue, as of the time of this study, is a signalized tee-intersection with protected left-turn phasing for the eastbound direction. The west leg is the on-ramp for westbound SR 4 and the location of the only crosswalk.

SR 4 Eastbound Ramps/Hillcrest Avenue is a four-legged intersection with protected left-turn phasing. The west and east legs are the off- and on-ramps, respectively, for eastbound SR 4 and the location of the only crosswalks at the intersection.

Hillcrest Road/Laurel Road is a four-legged intersection with protected left-turn phasing on Hillcrest Avenue and permitted left-turn phasing on Laurel Road. The northbound right turn is channelized and yield-controlled.

Laurel Road/Canada Valley Road, as of the time of the study, is a tee-intersection only open to vehicular traffic on the west leg of Laurel Road and the south leg of Canada Valley Road. As such, the intersection is unsignalized with no conflicting movements.

SR 4 Eastbound Ramps/Laurel Road, at the time of the study, is a tee-intersection. In the area, SR 4 is directionally more north-south than east-west. The west leg of Laurel Road has yet to be completed. The north and south leg

¹ Future Intersections

of the intersection are the off- and on-ramps, respectively, for eastbound SR 4. The westbound right-turn lane leads to a cloverleaf on-ramp onto SR 4 East about 400 feet east of the intersection.

SR 4 Westbound Ramps/Laurel Road is a four-legged intersection with the north and south legs as the on- and off-ramps, respectively, for westbound SR 4. All left turns have protected left-turn phases.

SR 4 Eastbound Ramps/Lone Tree Way is a four-legged intersection with protected left-turn phasing on all inbound approaches. The north leg is the off-ramp for eastbound SR 4 and the south leg is the on-ramp. There are pedestrian crossings provided on the north and south leg.

SR 4 Westbound On-Ramps-Jeffery Way/Lone Tree Way is a four-legged intersection with protected left-turn phasing on inbound approaches. The north leg is the SR 4 on-ramp.

Lone Tree Way/Empire Avenue is a four-legged intersection with protected left-turn phasing all around. U-Turns are allowed at every approach. There are crosswalks on every approach.

The locations of the study intersections and the existing lane configurations and controls are shown in Figure 1.

Analysis Methodology

Intersection Level of Service Methodologies

In accordance with the Contra Costa Transportation Authority's (CCTA) *Technical Procedures*, 2013, the study intersections were analyzed using methodologies published in the *Highway Capacity Manual* (HCM), Transportation Research Board, 2010. This source contains methodologies for various types of intersection control, all of which are related to a measurement of delay in average number of seconds per vehicle. In addition, the intersections in the study area were evaluated following the CCTA "Guidelines for Use of the 2010 Highway Capacity Manual Operational Method Methodology."

The Levels of Service for intersections controlled by a traffic signal were evaluated using the signalized methodology from the HCM. This methodology is based on factors including traffic volumes, green time for each movement, phasing, whether or not the signals are coordinated, truck traffic, and pedestrian activity. Average stopped delay per vehicle in seconds is used as the basis for evaluation in this LOS methodology. Detailed methodology assumptions applied to the operational analysis are provided Appendix A.

The LOS for the intersections with side street stop controls were analyzed using the "Two-Way Stop-Controlled" intersection capacity method from the *Highway Capacity Manual* (HCM), Transportation Research Board, 2010. This methodology determines a level of service for each minor turning movement by estimating the level of average delay in seconds per vehicle. Results are presented for individual movements together with the weighted overall average delay for the intersection. The ranges of delay associated with the various stop-controlled levels of service are indicated in Table 1.

Table 1 – Signalized Intersection Level of Service Criteria

| | |
|-------|---|
| LOS A | Delay of 0 to 10 seconds. Most vehicles arrive during the green phase, so do not stop at all. |
| LOS B | Delay of 10 to 20 seconds. More vehicles stop than with LOS A, but many drivers still do not have to stop. |
| LOS C | Delay of 20 to 35 seconds. The number of vehicles stopping is significant, although many still pass through without stopping. |
| LOS D | Delay of 35 to 55 seconds. The influence of congestion is noticeable, and most vehicles have to stop. |
| LOS E | Delay of 55 to 80 seconds. Most, if not all, vehicles must stop and drivers consider the delay excessive. |
| LOS F | Delay of more than 80 seconds. Vehicles may wait through more than one cycle to clear the intersection. |

Reference: *Highway Capacity Manual*, Transportation Research Board, 2010

Regulatory Setting

Caltrans

Caltrans has set forth guidelines for traffic operations based on measures of effectiveness (MOEs) for varying State Highway facilities. In general, Caltrans recommends a target LOS at the transition between LOS C and LOS D. If the existing location operates worse than the target LOS, then the existing LOS should be maintained.

Contra Costa Transportation Authority

The CCTA has established Multimodal Transportation Service Objectives (MTSO) to maintain county-wide connectivity. Under CCTA, the East County Regional Transportation Planning Committee (RTPC) worked closely with local jurisdictions to develop the *Draft East County Action Plan for Routes of Regional Significance* (TRANSPLAN, 2014) in which the committee selects the MTSOs to be applied to the planning area. For this study, each of the intersections are located along suburban arterial routes, or Routes of Regional Significance. In the proposed project study area, these routes are Hillcrest Avenue, Laurel Road, and Lone Tree Way. The corresponding MTSO used in accordance with the planning area is "Signalized Intersection LOS."

City of Antioch

The City of Antioch, in General Plan Growth Management Policy 3.4.1.1, has adopted the routes of regional significance standards set forth for by the East County Action Plan. This threshold is detailed below:

- Maintain an LOS D or better at all signalized intersection.
- Within Priority Development Areas, any physical improvement identified as a result of applying the above standard shall be evaluated for its effects on all intersection users, including pedestrians, cyclists, and transit users.

In addition, the following standard was used in the nearby project, *Davidon Homes (Park Ridge Subdivision #8846) Addendum to the Project Level EIR for FUA #2 Specific Plan (2009)*:

- A significant impact occurs if the average delay at an intersection operating at an unacceptable level (LOS E or F) increases by more than 5 seconds (2003 General Plan EIR).

City of Brentwood

The City of Brentwood, located south of Antioch, has jurisdiction over the study intersections on Lone Tree Way. In General Plan Circulation Policy 2.1-4, the City of Brentwood has also adopted the routes of regional significance standards set forth in the Action Plan.

- Maintain an LOS D or better at all signalized intersection.

Summary of Applicable Standards

The traffic operations analysis included 11 key study intersections. Table 2 provides a summary of each study intersection, its control type, and the respective applicable standard.

Table 2 – Level of Service Standards

| Intersection | Control Type | Jurisdiction | LOS Standard |
|--------------------------------|-----------------------|---------------------------------|--------------|
| 1. SR 4 WB Ramps/Hillcrest Ave | Signal | Caltrans | C/D* |
| 2. SR 4 EB Ramps/Hillcrest Ave | Signal | Caltrans | C/D* |
| 3. Hillcrest Rd/Laurel Rd | Signal | City of Antioch | LOS D |
| 4. Laurel Rd/Canada Valley Rd | Uncontrolled/Signal** | City of Antioch | LOS D |
| 5. SR 4 EB Ramps/Laurel Rd | Signal | Caltrans | C/D* |
| 6. SR 4 WB Ramps/Laurel Rd | Signal | Caltrans | C/D* |
| 7. SR 4 EB Ramps/Lone Tree Way | Signal | Caltrans | C/D* |
| 8. SR 4 WB Ramps/Lone Tree Way | Signal | Caltrans | C/D* |
| 9. Lone Tree Way/Empire Ave | Signal | Cities of Antioch and Brentwood | LOS D |
| 10. Laurel Rd/Country Hills Dr | Signal | City of Antioch | LOS D |
| 11. Laurel Rd/Slatten Ranch Rd | Signal | City of Antioch | LOS D |

Notes LOS= Level of Service; * = Caltrans target LOS is the transition between LOS C and D; ** = depending on the scenario analyzed and whether the Laurel Road Connection is completed, the intersection is either uncontrolled, and not analyzed, or signalized

Alternative Modes

Pedestrian Facilities

Pedestrian facilities include trails/paths, sidewalks, crosswalks, pedestrian signal phases, curb ramps, curb extensions, and various streetscape amenities such as lighting, benches, etc. In general, a network of sidewalks, crosswalks, pedestrian signals, and curb ramps provide access for pedestrians in the vicinity of the proposed project site where development exists; however, where there is no development, like the connection of Laurel Road, there are sidewalk gaps, obstacles, and barriers can be found adjacent to the project site. Between the location of the proposed project site and the adjacent development to the west there exists a public trail that provides connectivity with the Delta De Anza Regional Trail which provides access between the Cities of Pittsburg/Bay Point and the City of Oakley.

At the future adjacent intersection of SR 4 Eastbound Ramps/Laurel Road, there are currently no sidewalks provided on the north side of Laurel Road from the existing westerly terminus to just east of the westbound channelized right-turn.

Bicycle Facilities

The *Highway Design Manual*, Caltrans, 2012, classifies bikeways into three categories:

- **Class I Multi-Use Path** – a completely separated right-of-way for the exclusive use of bicycles and pedestrians with cross flows of motorized traffic minimized.

- **Class II Bike Lane** – a striped and signed lane for one-way bike travel on a street or highway.
- **Class III Bike Route** – signing only for shared use with motor vehicles within the same travel lane on a street or highway.

In the project area, there are Class II bike lanes on the existing portions of Laurel Road and on Hillcrest Avenue between the Davison Drive-Deer Valley Road/Hillcrest Avenue intersection and the existing southern terminus. As mentioned previously, just north of the project site is the multi-use Delta de Anza Regional Trail.

Transit Facilities

Tri Delta Transit

Tri Delta Transit (TDT) provides fixed route bus service in the Cities of Antioch, Brentwood, Oakley, Bay Point, Pittsburg, Discovery Bay, and Concord. Route 380, which is the closest to the project site, has its nearest stop approximately 0.5 miles from the proposed project. TDT Route 380 provides weekday service to destinations from the Pittsburg/Bay Point Bart Station to the Tri Delta Transit Center in the City of Oakley. Headways range from 30 minutes to an hour depending on the time of day. The Eastbound Route operates from 4:00 a.m. to 11:30 p.m. and the Westbound Route operates from 3:00 a.m. to 11:00 p.m.

Within a mile of the proposed project site, at the intersection of Hillcrest Avenue and Laurel Road, there are stops for Routes 385 and 392. Route 385 is weekday route providing service between the Antioch Park and Ride, Heritage High School, John Muir Medical Center, and the Brentwood Park-and-Ride. Route 392 is a weekend service that provides service to The Pittsburg Bay Point Station and other park-and-rides.

Two bicycles can be carried on most TDT buses. Bike rack space is on a first come, first served basis. Additional bicycles are allowed on the buses at the discretion of the driver.

Dial-a-ride, also known as paratransit, or door-to-door service, is available for those who are unable to independently use the transit system due to a physical or mental disability. Tri Delta Paratransit is designed to serve the needs of individuals with disabilities within the Eastern Contra Costa County.

County Connections

County Connection Transit provides one regional route to the Hillcrest Park-and-Ride lot, which is the Route 93X identified as the Kirker Pass Express route. The route operates during commute hours with headways ranging from 30 to 60 minutes and provides access to the Walnut Creek Bart Station.

Bart Extension/Bay Area Rapid Transit

Bart Extension (eBART) is a park-and-ride service located on the future site of the Antioch BART Station. eBART is located north of SR 4 and East of Hillcrest Avenue. Tri Delta Transit provides direct routes from the park-and-ride to the nearest BART station, Pittsburg/Bay Point. In addition, the Antioch park-and-ride lot has a dozen other routes that use the facilities.

The Bay Area Rapid Transit District (BART) provides heavy-rail rapid transit service within Alameda, Contra Costa, San Francisco and San Mateo Counties. The future Hillcrest Antioch Station, located in the median of SR 4, will be approximately three miles from the proposed project site. One BART line would provide service from the existing Pittsburg/Bay Point station to the proposed terminating Antioch Station to the north. Connecting services will terminate in Richmond, Dublin-Pleasanton, Fremont, and Millbrae-San Francisco International Airport.

Capacity Analysis

Existing Conditions

The Existing Conditions scenario provides an evaluation of current operation based on existing traffic volumes during the a.m. and p.m. peak periods. Turning movement counts were collected at the study intersections on September 22, 2015 when nearby schools were in session.

The roadway geometries can be seen in Figure 1. This condition does not include project-generated traffic volumes.

Intersection Levels of Service

Under existing conditions, all intersections operate within an acceptable level of service. While the two-legged intersection of Laurel Road/Canada Valley Road has vehicles using it, there are no conflicting movements, so the intersection operates freely with no delay. As an uncontrolled intersection, it was therefore not analyzed. The existing traffic volumes are shown in Figure 2. A summary of the intersection level of service calculations is contained in Table 3, and copies of the Level of Service calculations are provided in Appendix B.

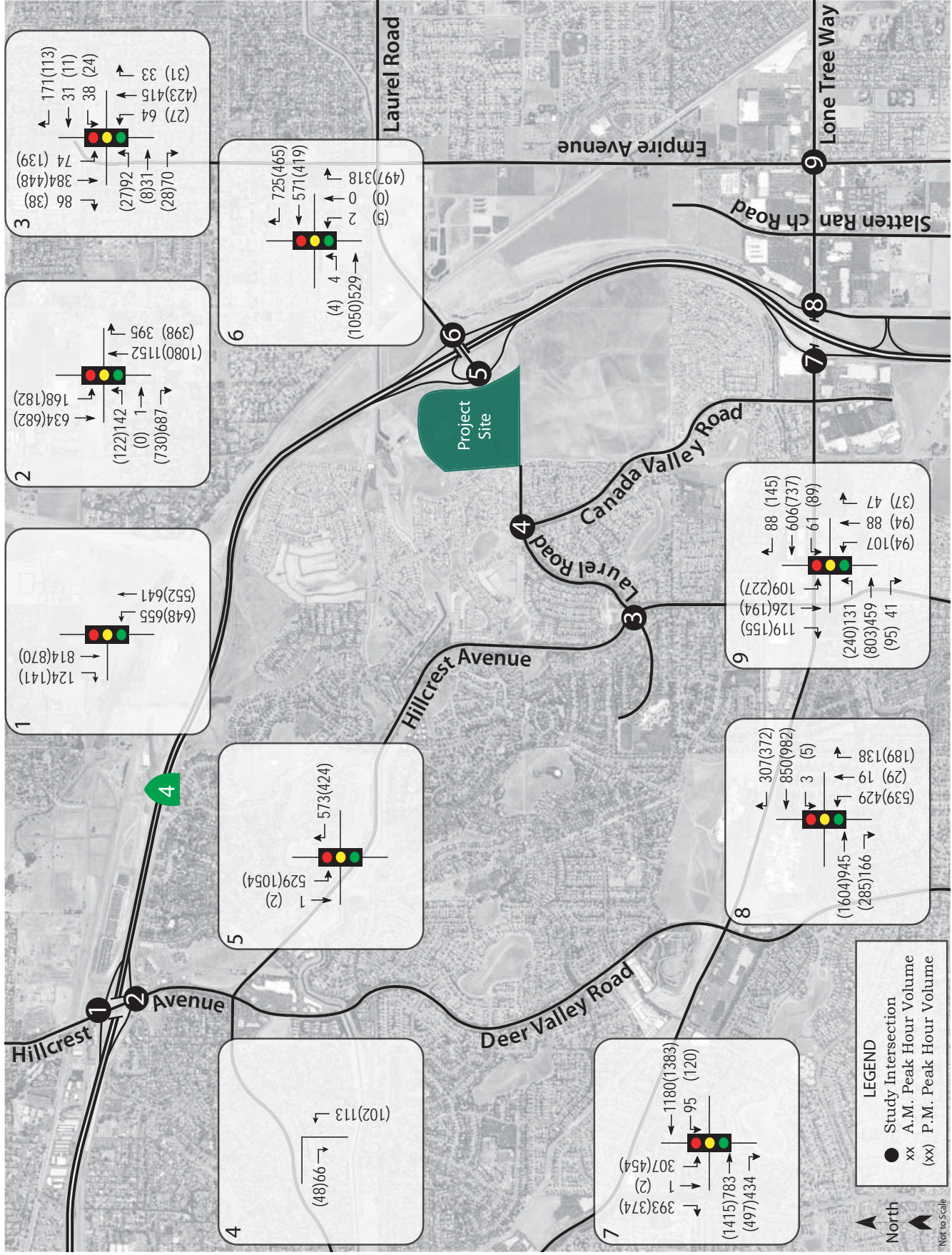
Table 3 – Existing Peak Hour Intersection Levels of Service

| Study Intersection Approach | AM Peak | | PM Peak | |
|--------------------------------|---------|-----|---------|-----|
| | Delay | LOS | Delay | LOS |
| 1. SR 4 WB Ramps/Hillcrest Ave | 7.7 | A | 8.0 | B |
| 2. SR 4 EB Ramps/Hillcrest Ave | 26.5 | C | 25.5 | C |
| 3. Hillcrest Rd/Laurel Rd | 10.4 | B | 8.5 | A |
| 4. Laurel Rd/Canada Valley Rd* | - | - | - | - |
| 5. SR 4 EB Ramps/Laurel Rd | 1.4 | A | 1.0 | A |
| 6. SR 4 WB Ramps/Laurel Rd | 9.5 | A | 15.4 | B |
| 7. SR 4 EB Ramps/Lone Tree Way | 14.7 | B | 16.3 | B |
| 8. SR 4 WB Ramps/Lone Tree Way | 8.2 | A | 10.8 | B |
| 9. Lone Tree Way/Empire Ave | 15.2 | B | 18.8 | B |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; * = uncontrolled intersection under construction

Existing Plus Nearby Future Projects

Short-term operating conditions were determined with traffic from phase one of the *Davidon Homes (Park Ridge Subdivision #8846) Addendum to the Project Level EIR for FUA #2 Specific Plan (2009)* added to the existing volumes. The project as planned would be completed in seven phases and include 525 homes. Only Phase One of the project was used for the near-term analysis and includes 123 single family dwellings to be built on the southern portion of the project site, connecting to several existing roads, including Canada Valley Drive. Under this condition, the assumptions for road geometries and distributions from the Park Ridge study were used; the extension of Laurel Road was assumed to be unconstructed. These results are summarized in Table 4, and Short-Term volumes are shown in Figure 3.



Transportation Impact Analysis for Laurel Ranch
Figure 2 – Existing Traffic Volumes

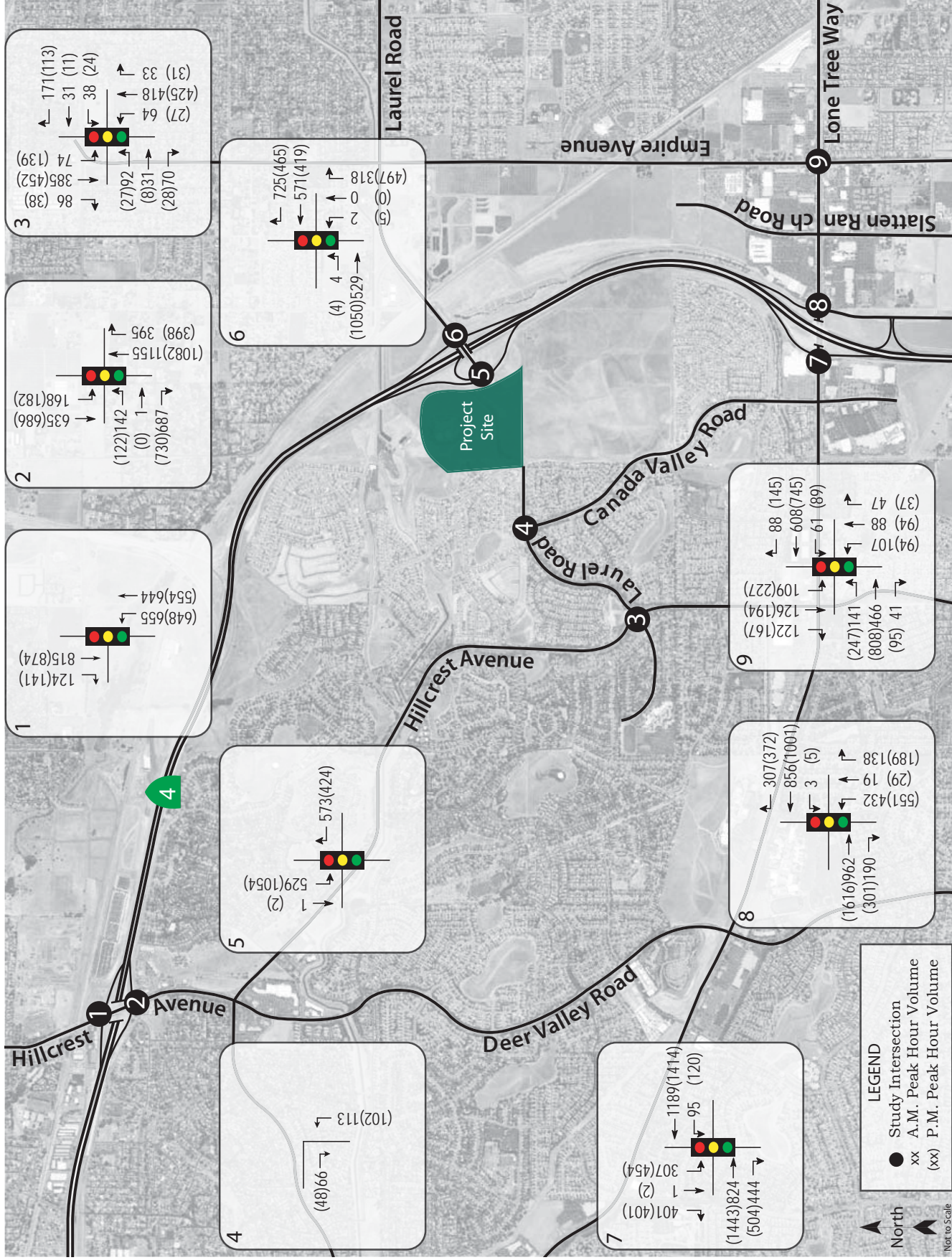


Table 4 – Existing plus Nearby Future Project Peak Hour Intersection Levels of Service

| Study Intersection Approach | AM Peak | | PM Peak | |
|--------------------------------|---------|-----|---------|-----|
| | Delay | LOS | Delay | LOS |
| 1. SR 4 WB Ramps/Hillcrest Ave | 7.7 | A | 8.0 | B |
| 2. SR 4 EB Ramps/Hillcrest Ave | 26.6 | C | 25.5 | C |
| 3. Hillcrest Rd/Laurel Rd | 10.4 | B | 8.5 | A |
| 4. Laurel Rd/Canada Valley Rd* | - | - | - | - |
| 5. SR 4 EB Ramps/Laurel Rd | 1.4 | A | 1.0 | A |
| 6. SR 4 WB Ramps/Laurel Rd | 9.5 | A | 15.4 | B |
| 7. SR 4 EB Ramps/Lone Tree Way | 15.1 | B | 22.6 | B |
| 8. SR 4 WB Ramps/Lone Tree Way | 8.3 | A | 11.1 | B |
| 9. Lone Tree Way/Empire Ave | 16.0 | B | 19.6 | B |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; * = uncontrolled intersection under construction

Cumulative No Project Conditions

Several approaches were used in determining the cumulative base volumes for the year 2040. For the Cumulative Conditions, no development is assumed on the project parcel.

Where possible, previously projected future volumes were taken from studies for other nearby development and incrementally increased based on the growth assumptions used and projected growth from the CCTA model for the year 2040.

For the intersections located on Laurel Road, future volumes were projected from the Park Ridge study's 2025 Cumulative plus Project scenario. For the intersection of Hillcrest Avenue/Laurel Road, the growth per year was determined from the study's existing counts and future projections. This growth per year (growth factor) was then applied to the Laurel Ranch existing counts to project the year 2040 volumes. Where existing counts from the Park Ridge project were unavailable, the projected growth was determined using the CCTA model volumes.

For the intersection of Hillcrest Avenue/SR 4 EB Ramps, 2035 volumes from the *Hillcrest Station Area Specific Plan* (2008), were projected based on the Plan's growth per year determined from the existing and future traffic volumes. This growth per year was then applied to the Laurel Ranch project's existing counts to achieve the year 2040 volumes. Under the Cumulative Scenario, study intersection 1, Hillcrest Avenue/WB SR 4 Ramps, was not analyzed. According to the 4eastcounty.org website, the ramps are to be relocated to Slatten Ranch Road, just west of the future Hillcrest Avenue BART station. Because few project and nearby future project trips were predicted to use the intersection, further analysis of the relocated interchange was not conducted.

Future 2040 peak hour volume projections for the intersections on Lone Tree Way are directly from the Brentwood General Plan Update (2014); this scenario represents Cumulative 2040 traffic conditions that would be expected upon Brentwood's build out to City limits as identified in their Updated General Plan.

Under the Cumulative Conditions, the following roadway modification projects were assumed:

- The connection of Laurel Road from the existing terminus east at Canada Valley Road to the SR 4 eastbound ramps would be completed. The extension would include the following elements:
 - A southbound right-turn pocket would be added to the SR 4 Eastbound Ramps at Laurel Road.

- The intersection at Country Hills Drive/Laurel Road would be completed. The intersection geometry used was from the site plan and protected left-turn phasing was assumed.
- The intersection of Canada Valley Drive/Laurel Road would be signalized. The intersection geometry from the Park Ridge study was used and protected left-turn phasing was assumed.
- Country Hills Drive would be extended north to Laurel Road.
- The Hillcrest Avenue overpass would be widened. The project would add a second eastbound left-turn lane on the off-ramp and widen to the neck. In addition, a second southbound left-turn lane would be constructed.
- Hillcrest Avenue/SR 4 Westbound Ramps would be relocated to Slatten Ranch Road.
- The eastbound lanes of Lone Tree Way/SR 4 Eastbound Ramps would be modified to provide two through lanes and two right-turn lanes.
- Slatten Ranch Road would be constructed. From the north, it would connect to Sunset Drive/Hillcrest Avenue and intersect Laurel Road, and to the south, it would connect to an existing portion already built that is north of Lone Tree Way. The intersection geometry was the same used in the Park Ridge study analysis.

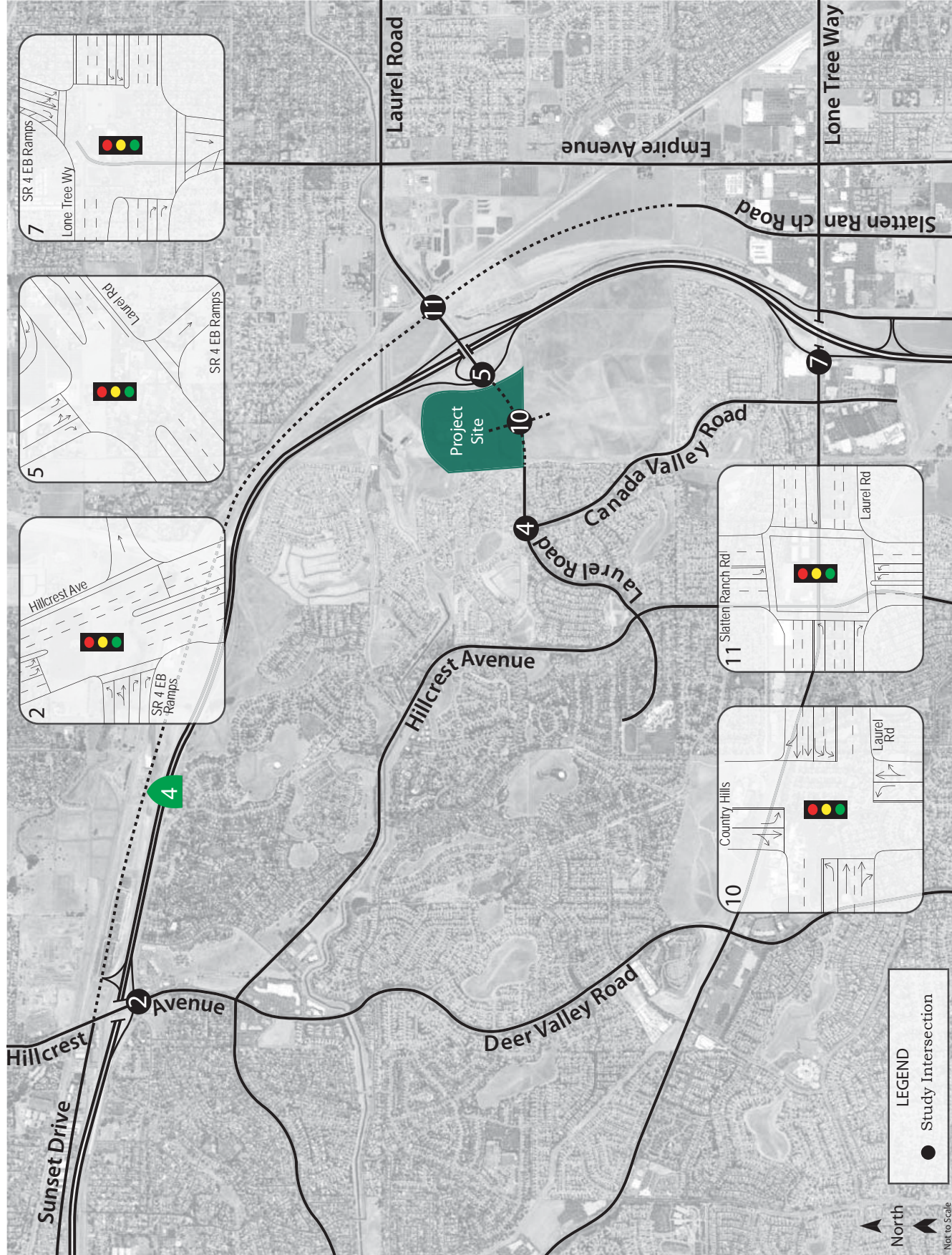
In addition, all seven phases of the Park Ridge project, for a total of 525 single family homes, were assumed completed as well as the Antioch BART Station.

Under the anticipated Future volumes, assuming completion of the improvements noted above and with the addition of the above projects, the study intersections are expected to operate acceptably with the exception of Hillcrest Road/Laurel Road in the a.m. and p.m. peak hours and Laurel Road/Slatten Ranch Road in the p.m. peak hour. While the intersections of SR 4 Eastbound Ramps/Hillcrest Avenue and SR 4 Eastbound Ramps/Lone Tree Way are expected to operate above the desired Caltrans threshold, operation would be acceptable based on the East County Action Plan. Future geometries and volumes are shown in Figures 4 and 5, respectively, and operating conditions are summarized in Table 5.

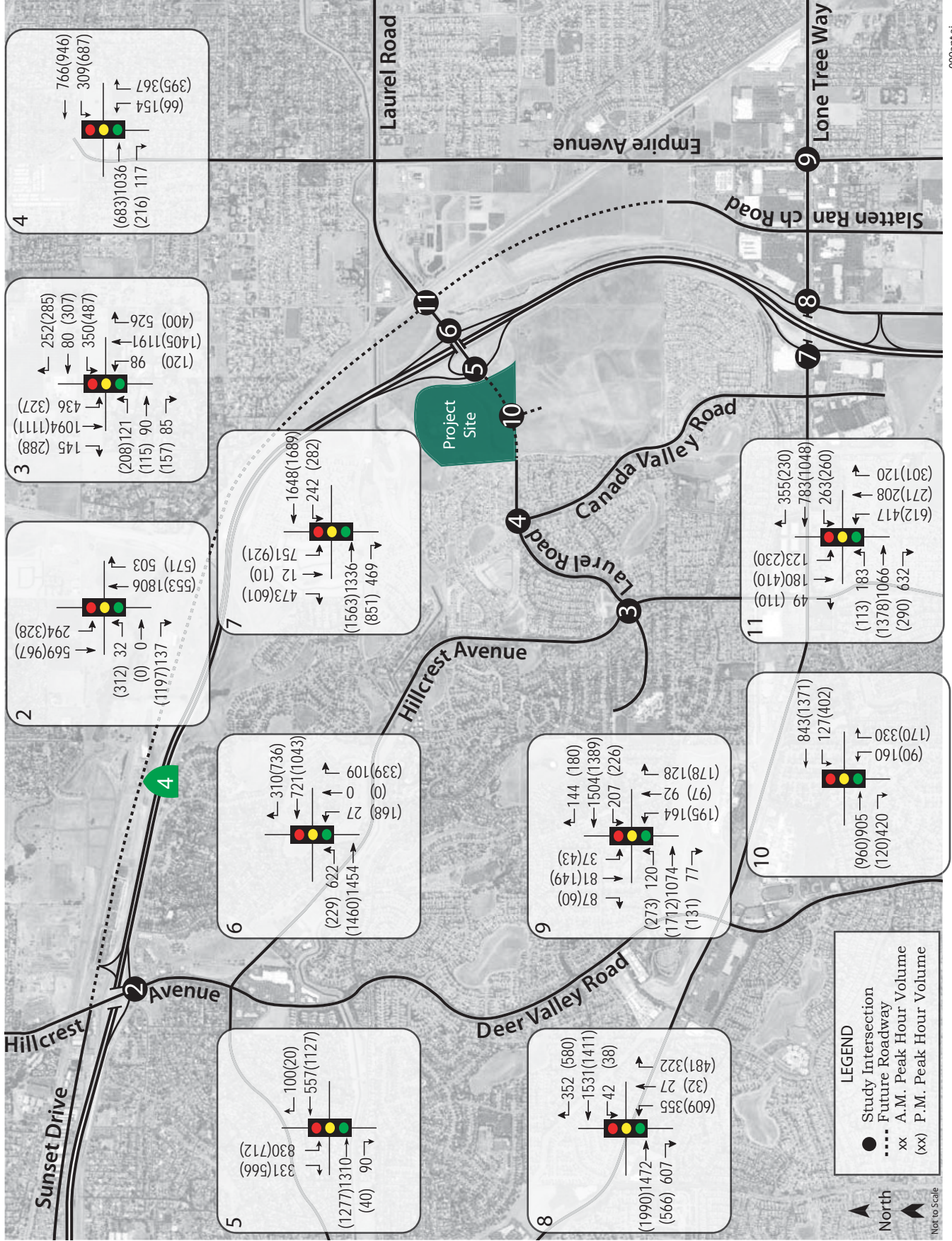
Table 5 – Cumulative No Project Conditions Peak Hour Intersection Levels of Service

| Study Intersection <i>Approach</i> | AM Peak | | PM Peak | |
|---------------------------------------|-------------|----------|--------------|----------|
| | Delay | LOS | Delay | LOS |
| 1. SR 4 WB Ramps/Hillcrest Ave | - | - | - | - |
| 2. SR 4 EB Ramps/Hillcrest Ave | 13.9 | B | 51.0 | D |
| 3. Hillcrest Rd/Laurel Rd | 68.8 | E | 107.3 | F |
| 4. Laurel Rd/Canada Valley Rd | 19.6 | B | 43.7 | D |
| 5. SR 4 EB Ramps/Laurel Rd | 17.4 | B | 25.4 | C |
| 6. SR 4 WB Ramps/Laurel Rd | 15.8 | B | 21.4 | C |
| 7. SR 4 EB Ramps/Lone Tree Way | 30.2 | C | 49.7 | D |
| 8. SR 4 WB Ramps/Lone Tree Way | 13.4 | B | 21.2 | C |
| 9. Lone Tree Way/Empire Ave | 18.6 | B | 27.4 | C |
| 10. Laurel Rd/Country Hills Dr | 20.3 | C | 13.9 | B |
| 11. Laurel Rd/Slatten Ranch Rd | 30.6 | C | 55.9 | E |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service
Bold text = deficient operation



Transportation Impact Analysis for Laurel Ranch
Figure 4 – Future Lane Configurations



Transportation Impact Analysis for Laurel Ranch
Figure 5 – Future Traffic Volumes

Project Description

The project consists of 187 single family homes on 54 acres, located north of the future Laurel Road connection and west of the SR 4 Eastbound Ramps. The site would be accessed by a signalized intersection at Laurel Road/Country Hills Drive and a stop-controlled driveway west of the intersection with right-in and right-out access only. Currently the site is unused. The proposed project site plan is shown in Figure 6.

Trip Generation

The anticipated trip generation for the proposed project was estimated using standard rates published by the Institute of Transportation Engineers (ITE) in *Trip Generation Manual*, 9th Edition, 2012 for “Single Family Detached Housing” (ITE LU 210). Because the site is currently unoccupied, there are no existing trips being generated by the site.

Total Project Trip Generation

The expected trip generation potential for the proposed project is indicated in Table 6. The proposed project is expected to generate an average of 1,780 trips per day, including 140 trips during the a.m. peak hour and 187 during the p.m. peak hour. These new trips represent the increase in traffic associated with the project compared to existing volumes.

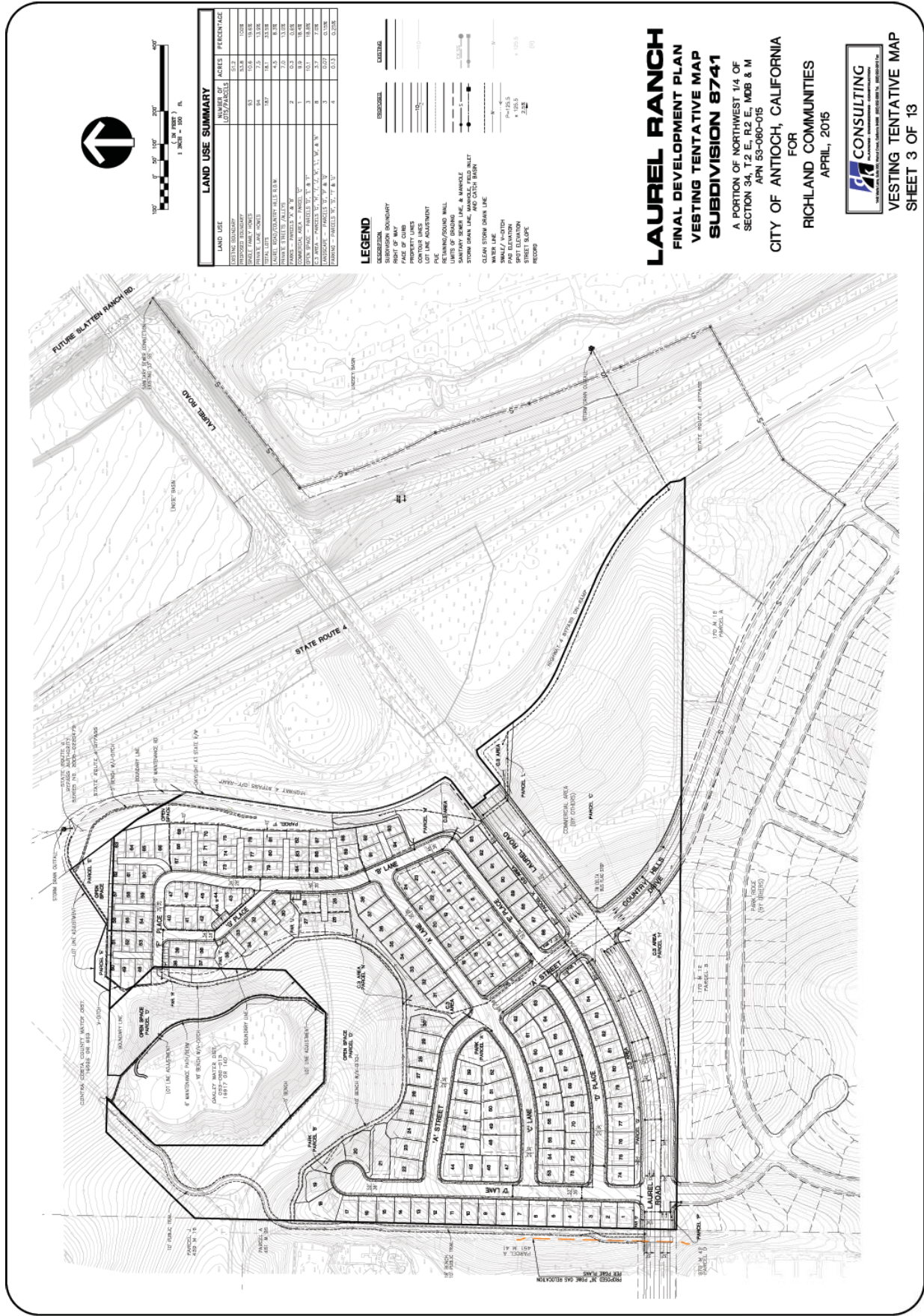
Table 6 – Trip Generation Summary

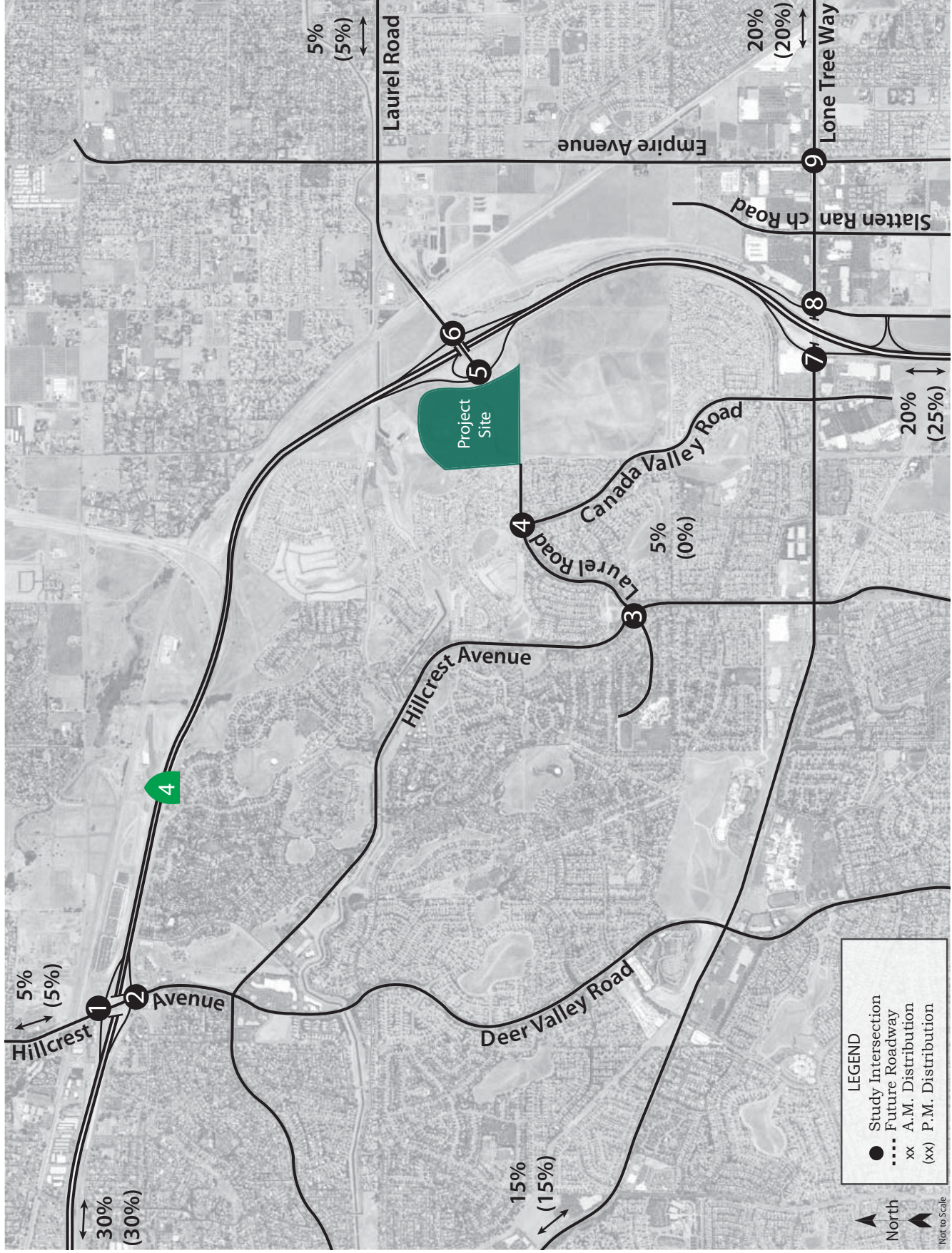
| Land Use | Units | Daily | | AM Peak Hour | | | | PM Peak Hour | | | |
|--------------------------------|--------|-------|-------|--------------|-------|----|-----|--------------|-------|-----|-----|
| | | Rate | Trips | Rate | Trips | In | Out | Rate | Trips | In | Out |
| Single Family Detached Housing | 187 du | 9.52 | 1,780 | 0.75 | 140 | 35 | 105 | 1.00 | 187 | 118 | 69 |

Note: du = dwelling unit

Trip Distribution

The pattern used to allocate new project trips to the street network was based on existing traffic patterns as identified by the City as well as recent transportation studies completed for other projects in the study area. These applied distribution assumptions and resulting trips are shown in Figure 7 and detailed in Table 7.





Transportation Impact Analysis for Laurel Ranch
Figure 7 – Trip Distribution

Table 7 – Trip Distribution Assumptions

| Route | AM Percent | PM Percent | AM Trips | PM Trips |
|------------------------------------|-----------------------|-----------------------|---------------------|---------------------|
| To/From the North (West) via SR 4 | 30% | 30% | 42 | 56 |
| To/From the South (East) via SR 4 | 20% | 25% | 28 | 47 |
| To/From the East via Lone Tree Way | 20% | 20% | 28 | 38 |
| To/From the West via Lone Tree Way | 15% | 15% | 21 | 28 |
| To/From the East via Laurel Rd | 5% | 5% | 7 | 9 |
| To/From eBART via Hillcrest Ave* | 5% | 5% | 7 | 9 |
| To/From Carmen Dragon School | 5% | 0% | 7 | 0 |
| TOTAL | 100% | 100% | 140 | 187 |

Note: * The route will be via Slatten Ranch Rd under the Cumulative Scenario

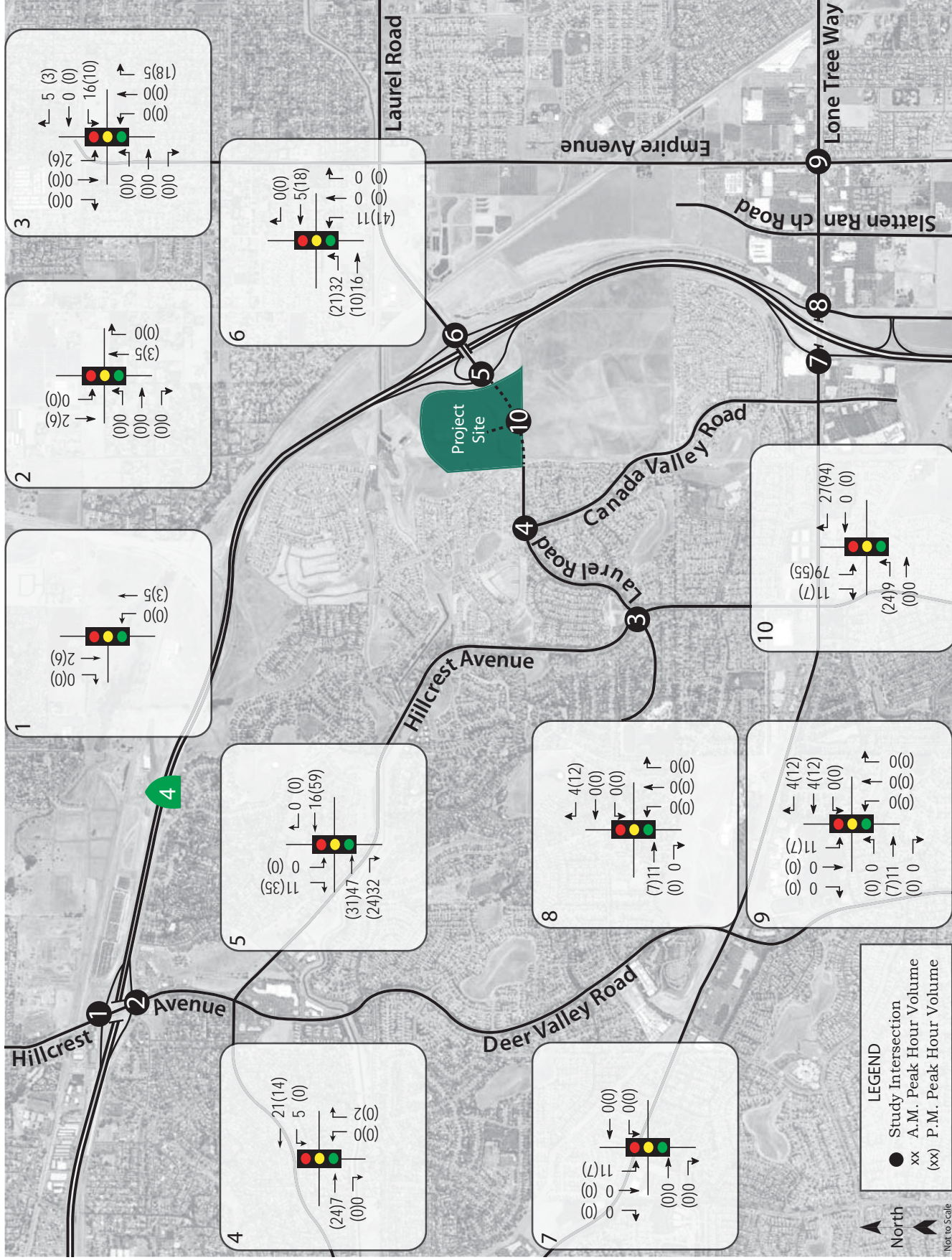
Intersection Operation

Existing plus Project Conditions

Because the proposed Laurel Ranch Project would be accessed exclusively through Laurel Road the improvements assumed under the Cumulative Condition would instead be first implemented with the project completion. The roadway modifications include all the improvements associated with the Laurel Road extension described in the Cumulative scenario. Based on the site plan, it was assumed that the signalized project intersection at Country Hills Drive/Laurel Road would have all four legs constructed; however, since no development was assumed to have occurred directly south, no vehicle trips would be on that leg and the intersection was analyzed as a tee-intersection.

In addition, the Laurel Road connection would provide improved access to SR 4 for the residential communities to the west, while also providing more direct access to and from the City of Oakley and the surrounding area. With the Laurel Road connection, existing traffic patterns would shift. New base volumes along Laurel Road were estimated using the existing counts and the projected growth trends from the CCTA model.

Upon the addition of project-related traffic to the Existing volumes, and with the shifts in traffic anticipated due to the extension of Laurel road, the study intersections are expected to operate at LOS C or better. These results are summarized in Table 8. Added project traffic volumes are shown in Figure 8.



Transportation Impact Analysis for Laurel Ranch
Figure 8 – Existing Project Traffic Volumes

Table 8 – Existing and Existing plus Project Peak Hour Intersection Levels of Service

| Study Intersection Approach | Existing Conditions | | | | Existing plus Project | | | |
|--------------------------------|---------------------|-----|---------|-----|-----------------------|-----|---------|-----|
| | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. SR 4 WB Ramps/Hillcrest Ave | 7.7 | A | 8.0 | B | 7.7 | A | 8.0 | B |
| 2. SR 4 EB Ramps/Hillcrest Ave | 26.5 | C | 25.5 | C | 26.6 | C | 25.5 | C |
| 3. Hillcrest Rd/Laurel Rd | 10.4 | B | 8.5 | A | 13.7 | B | 12.9 | A |
| 4. Laurel Rd/Canada Valley Rd | - | - | - | - | 9.1 | A | 8.0 | A |
| 5. SR 4 EB Ramps/Laurel Rd | 1.4 | A | 1.0 | A | 7.8 | A | 14.4 | B |
| 6. SR 4 WB Ramps/Laurel Rd | 9.5 | A | 15.4 | B | 21.0 | C | 30.9 | C |
| 7. SR 4 EB Ramps/Lone Tree Way | 14.7 | B | 16.3 | B | 14.7 | B | 16.3 | B |
| 8. SR 4 WB Ramps/Lone Tree Way | 8.2 | A | 10.8 | B | 8.3 | A | 10.9 | B |
| 9. Lone Tree Way/Empire Ave | 15.2 | B | 18.8 | B | 15.3 | B | 18.9 | B |
| 10. Laurel Rd/Country Hills Dr | - | - | - | - | 4.5 | A | 4.7 | A |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service

Finding – The study intersections are expected to continue operating acceptably with the shift in traffic volumes due to the Laurel Road connection and upon the addition of project-generated traffic, and the project would result in less-than-significant intersection impacts.

Existing plus Nearby Project plus Project Conditions

Similarly to the Existing plus Project conditions, the completion of the Laurel Ranch project would include the roadway improvements along Laurel Road assumed in the Cumulative Scenario. With this connection, the trips generated from the nearby project, Park Ridge, would use the SR 4 ramps on Laurel Road instead of the ramps on Lone Tree Way. This assumption matches the route assignments used in the Park Ridge study with Laurel Road connection completed. The same new base volumes from the Existing plus Project scenario were used in the analysis, then the Park Ridge trips were added in addition to the project traffic.

Upon the addition of project-related traffic to the Existing plus Nearby Project condition volumes and assumed geometric changes with new base volumes, the study intersections are expected to operate acceptably at LOS C or better. These results are summarized in Table 9.

Table 9 – Existing plus Nearby Project and Existing plus Nearby Project plus Project Peak Hour Intersection Levels of Service

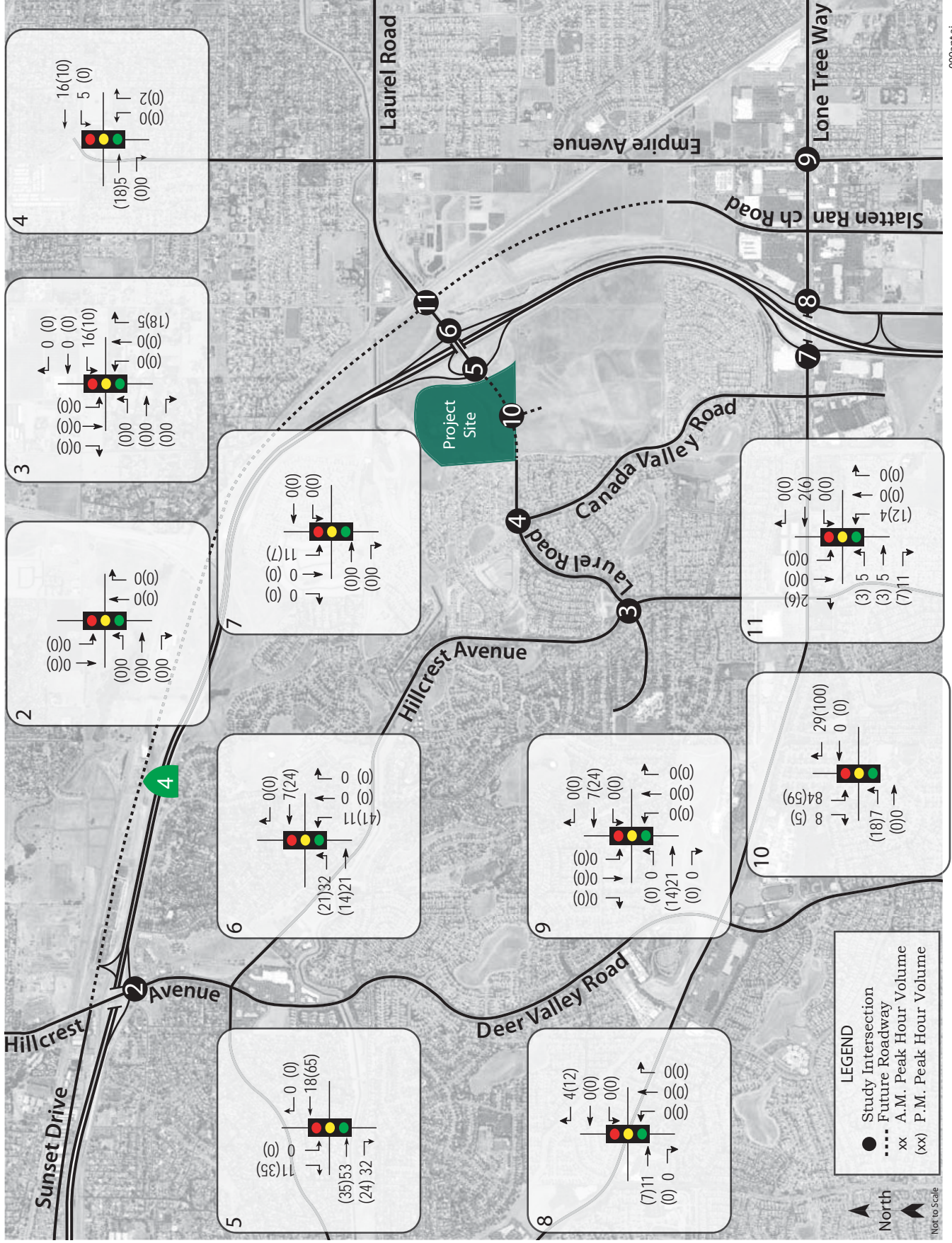
| Study Intersection <i>Approach</i> | Existing plus Nearby Project | | | | Existing plus Nearby Project plus Project | | | |
|---------------------------------------|------------------------------|-----|---------|-----|---|-----|---------|-----|
| | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. SR 4 WB Ramps/Hillcrest Ave | 7.7 | A | 8.0 | B | 7.7 | A | 8.0 | B |
| 2. SR 4 EB Ramps/Hillcrest Ave | 26.6 | C | 25.5 | C | 26.6 | C | 25.9 | C |
| 3. Hillcrest Rd/Laurel Rd | 10.4 | B | 8.5 | A | 13.8 | B | 12.9 | B |
| 4. Laurel Rd/Canada Valley Rd | - | - | - | - | 9.6 | A | 9.0 | A |
| 5. SR 4 EB Ramps/Laurel Rd | 1.4 | A | 1.0 | A | 8.0 | A | 15.3 | B |
| 6. SR 4 WB Ramps/Laurel Rd | 9.5 | A | 15.4 | B | 22.3 | A | 32.7 | C |
| 7. SR 4 EB Ramps/Lone Tree Way | 15.1 | B | 22.6 | B | 14.7 | B | 16.3 | B |
| 8. SR 4 WB Ramps/Lone Tree Way | 8.3 | A | 11.1 | B | 8.3 | A | 10.9 | B |
| 9. Lone Tree Way/Empire Ave | 16.0 | B | 19.6 | B | 15.7 | B | 19.0 | B |
| 10. Laurel Rd/Country Hills Dr | - | - | - | - | 4.5 | A | 4.7 | A |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service

Finding – The study intersections are expected to continue operating acceptably upon the addition of project-generated traffic and completion of the Laurel Road connection project.

Cumulative plus Project Conditions

Upon the addition of project-generated traffic to the anticipated Future volumes, as seen in Figure 9, and with the planned improvements, the study intersections are expected to operate acceptably, with the exception of the same four intersections and peak periods that would operate at a deficient level under the Cumulative No Project Scenario. While the intersections of SR 4 Eastbound Ramps/Hillcrest Avenue and SR 4 Eastbound Ramps/Lone Tree Way would still operate below the desired Caltrans threshold, the intersections would continue to operate acceptably based on the East County Action Plan. The Cumulative plus Project operating conditions are summarized in Table 10.



Transportation Impact Analysis for Laurel Ranch
 Figure 9 – Future Project Traffic Volumes



Table 10 – Cumulative and Cumulative plus Project Peak Hour Levels of Service

| Study Intersection Approach | Cumulative Conditions | | | | Cumulative plus Project | | | |
|--------------------------------|-----------------------|----------|--------------|----------|-------------------------|----------|--------------|----------|
| | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. SR 4 WB Ramps/Hillcrest Ave | - | - | - | - | - | - | - | - |
| 2. SR 4 EB Ramps/Hillcrest Ave | 13.9 | B | 51.0 | D | 13.9 | B | 51.0 | D |
| 3. Hillcrest Rd/Laurel Rd | 68.8 | E | 107.3 | F | 71.6 | E | 108.9 | F |
| 4. Laurel Rd/Canada Valley Rd | 19.6 | B | 43.7 | D | 19.9 | B | 45.4 | D |
| 5. SR 4 EB Ramps/Laurel Rd | 17.4 | B | 25.4 | C | 18.8 | B | 30.3 | C |
| 6. SR 4 WB Ramps/Laurel Rd | 15.8 | B | 21.4 | C | 17.3 | B | 23.0 | C |
| 7. SR 4 EB Ramps/Lone Tree Way | 30.2 | C | 49.7 | D | 30.3 | C | 49.7 | D |
| 8. SR 4 WB Ramps/Lone Tree Way | 13.4 | B | 21.2 | C | 13.4 | B | 21.3 | C |
| 9. Lone Tree Way/Empire Ave | 18.6 | B | 27.4 | C | 18.6 | B | 27.5 | C |
| 10. Laurel Rd/Country Hills Dr | 20.3 | C | 13.9 | B | 37.6 | D | 23.2 | C |
| 11. Laurel Rd/Slatten Ranch Rd | 30.6 | C | 55.9 | E | 30.9 | C | 57.0 | E |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; **Bold** text = deficient operation

Finding – The study intersections previously operating acceptably would continue to do so with project traffic added. Where operation is LOS D or worse, the increase in delay due to the project is less than five seconds and therefore within the acceptable threshold as set forth by the regulating agencies, and the project would not result in any significant cumulative intersection impacts.

CCTA Regional Roadway Analysis

According to the East County Action Plan, one of the MTSOs for all freeway segments in East County is a delay index. However, following the CCTA Final Technical Procedures (2013), the threshold for analysis of freeway MTSOs would not be satisfied. As stated, “when the proposed project adds more than 50 net new peak hour vehicle trips to a freeway ramp, then the impact of the project on freeway MTSOs should be evaluated.” Therefore, because the proposed project would not add more than 50 net new peak hour trips to any one of the ten freeway ramps from the five study intersections under the Cumulative scenario, the freeway MTSOs were not required to be analyzed.

Queuing

Project Access Roadways

Queuing analysis was performed for the project driveways in order to determine adequacy of turn pocket lengths in reference to projected queue lengths. Analysis for the project driveways was performed under volumes for the Cumulative and Cumulative plus Project scenarios. As noted in the site plan, there are two roads that access Laurel Road; one is the signalized study intersection of Country Hills Drive/Laurel Road and the second is Laurel Road/“Lane D”, a side street stop-controlled intersection with only right-in and right-out access due to the median on Laurel Road.

Under the Cumulative Scenarios, the projected 95th percentile queues in left-turn pockets at the study intersection and the queue at the unsignalized intersection of Laurel Road/D Lane were determined using the SIMTRAFFIC

application of Synchro, and averaging the projected 95th percentile queue for each of five runs. The 95th percentile queue represents the peak of the peak, or queues that only have a five percent chance of being exceeded. The estimated available storage lengths for the intersections are all approximations based on the site plan for the project. Summarized in Table 11 are the predicted queue lengths for approaches to intersections. Copies of the SIMTRAFFIC projections are contained in Appendix C.

Table 11 – 95th Percentile Project Driveway Queues

| Intersection Approach | Estimated Available Storage* | 95 th Percent Queues | | | |
|----------------------------|------------------------------|---------------------------------|-----|--------------|-----|
| | | AM Peak Hour | | PM Peak Hour | |
| | | C | C+P | C | C+P |
| Laurel Rd/Country Hills Dr | | | | | |
| SB Left-Turn | 100 | - | 76 | - | 64 |
| NB Left-Turn | 250 | 147 | 154 | 81 | 96 |
| WB Left-Turn #1 | 200 | 61 | 61 | 116 | 106 |
| WB Left-Turn #2 | 200 | 94 | 82 | 127 | 165 |
| EB Left-Turn | 215 | - | 25 | - | 28 |
| Laurel Road/Lane D | | | | | |
| SB Right-Turn | 100 | - | 42 | - | 20 |

Notes: 95th Percent Queue based on the calculated potential from five averaged SIMTRAFFIC runs

* = Storage length estimated based on site plan, measured in feet

C = cumulative conditions; C+P = future plus project conditions;

The results of the 95th percentile queuing analysis indicate that the estimated available storage lengths, as proposed, would be adequate to accommodate future volumes in addition to proposed Laurel Ranch and Park Ridge project traffic volumes.

Finding – The project would not result in queues exceeding the estimated available storage.

Alternative Access Queuing Analysis

In addition, a proposed second access alternative for the side-street stop-controlled intersection Laurel Road/ D Lane-Treeline Way (Park Ridge project access road) was analyzed for potential vehicle queue lengths.

As part of the *Davidon Homes (Park Ridge Subdivision) Addendum to the Project Level EIR*, the intersection of D Lane-Treeline Way/Laurel Road had no turning movement restrictions and was analyzed with stop-controlled side streets. Under the cumulative scenario with the completion of both the Laurel Ranch Project and the Park Ridge Project, the intersection as a whole was expected to operate at LOS A but the southbound side street, specifically the left-turn from D Lane, was projected to operate deficiently at LOS F with 67 seconds of delay in the a.m. peak hour and 68 seconds during the p.m. peak hour. Based on the significance criterion for unsignalized intersections, the project would only cause a significant impact if the intersection operated at an unacceptable LOS overall and satisfied the CA MUTCD peak hour signal warrant. As documented in the Park Ridge EIR report, it was determined that the intersection did not meet this signal warrant and as such would not result in a significant impact. If the intersection were to be signalized, it would operate at an acceptable level.

In the Park Ridge project analysis, this intersection was assumed with no median or turning movement restrictions. However, the geometry assumed for Laurel Ranch's access Alternative 2 would allow westbound left turns from Laurel Road into the Park Ridge project in addition to the right turns in, but restrict egress to right turns out. The

access to the Laurel Ranch project would continue to be right-in and right-out only. The traffic volumes accessing Treeline Way were the same assumed in the Park Ridge study.

Under the Cumulative scenarios, the projected 95th percent queues in westbound left-turn pocket on Laurel Road to Treeline Way were also determined using the SIMTRAFFIC application of Synchro. Summarized in Table 12 are the predicted queue lengths for access Alternative 2 for the Park Ridge project. Copies of the SIMTRAFFIC projections are contained in Appendix D.

Table 12 – 95th Percentile Left-Turn Queues on Westbound Laurel Rd at D Lane, Alternative Access 2

| Intersection Approach | Estimated Available Storage | 95th Percent Queues | | | |
|---|--|---------------------------------------|------------|---------------------|------------|
| | | AM Peak Hour | | PM Peak Hour | |
| | | C | C+P | C | C+P |
| Laurel Rd/Lane D-Treeline Way WB Left-Turn | 200* | 36 | 52 | 75 | 68 |

Notes: 95th Percent Queue based on the calculated potential from five averaged SIMTRAFFIC runs; * = Storage length estimated based on potential space according to site plan, measured in feet; C = Cumulative Conditions; C+P = Future plus Project Conditions

According to the queuing calculations, there would be adequate space in the proposed Laurel Road median to incorporate a left-turn pocket. While the median can accommodate a storage length of approximately 200 feet, based on the queuing calculations, the storage length can be shorter if desired.

Finding – Projected queue lengths from Alternative 2 can be accommodated in the available length of the Laurel Road median.

Alternative Modes

Pedestrian Facilities

Given the proximity of other residential neighborhoods, schools, open space, and commercial areas near the site, it is reasonable to assume that some Laurel Ranch residents would want to walk, bicycle, and/or use transit to reach what the surrounding area has to offer.

Project Site – Based on the site plan, sidewalks are planned along both sides of Laurel Road fronting the project site. However, the site plan shows a connection with the existing sidewalk network only on the south side of Laurel Road near the SR 4 Eastbound on-ramps; the north side of Laurel Road does not have existing facilities west of the channelized westbound right-turn. The proposed sidewalks to the south and west of the Country Hills Drive/Laurel Road intersection do not indicate a connection with proposed nearby facilities.

In addition, there is no indication of pedestrian crossings at the signalized study intersection.

As part of the Park Ridge subdivision, much of the internal land would remain as open space and include pedestrian trails. To improve connectivity with the other nearby trail networks, particularly the Delta De Anza trail located just north of the Laurel Ranch project, the internal trails from the Park Ridge Subdivision would cross Laurel Road in the vicinity of the Laurel Ranch Project. This would require some manner of pedestrian facilities, such as a pedestrian signal or rectangular rapid flashing beacons (RRFB) which are described in more detail in the Park Ridge EIR.

Starting from the open space trailhead on the Park Ridge subdivision street of Treeline Court, the trail would continue through the court and Treeline Way to meet at the intersection of Laurel Road/Treeline Way. Just to the west of this intersection, on the north side of Laurel Road, is the existing trail that connects to Delta De Anza Trail. The improvements to Laurel Road would connect the north and south side pedestrian facilities in the vicinity of this area.

Finding – There would be a gap in pedestrian facilities serving the project site if no sidewalk connections to the existing facilities are provided.

Recommendation – The proposed pedestrian facilities should connect either with the existing or proposed sidewalk facilities on the north and south side Laurel Road to the east and west of the project site. In addition to pedestrian curb ramps at the intersection, crosswalks with pedestrian phase should be included in the project.

Bicycle Facilities

Proposed bicycle facilities include bike lanes on Laurel Road fronting the site and connecting to existing facilities to the west. Together with shared use of minor streets, adequate access for bicyclists would be provided.

Finding – Bicycle facilities proposed for the project site are expected to be adequate.

Recommendation – Bike lanes should be provided on Laurel Road as indicated on preliminary site plans.

Transit

According to the site plan, there would be proposed Tri Delta Bus stop locations on the northwest and southeast corners of the Laurel Road/Country Hills Drive intersection. Given these additional stops and the existing stops located west of Canada Valley Road, transit routes are expected to be adequate to accommodate project-generated transit trips.

Finding – Proposed and existing transit facilities serving the project site are expected to be adequate.

Access and Circulation

Site Access

As mentioned in the queuing analysis section, there would be two project access points: the signalized study intersection of Country Hills Drive/Laurel Road and the side-street stop-controlled intersection of Laurel Road/D Lane, which would be limited to right-turn in and out only. Access through the signalized study intersection was assumed to have protected left-turn phasing. Access through the unsignalized intersection would remain right-in and right-out for both access alternatives proposed at the intersection. Further details of the alternative access can be found in the Queuing section.

On-site circulation was reviewed based on the design as presented in the preliminary plans under the assumption that the design of the subdivision adhered to the proper ordinances and regulations set forth by the regulatory agencies. Review of the site plan indicated no circulation issues.

Sight Distance

At unsignalized intersections a substantially clear line of sight should be maintained between the driver of a vehicle waiting at the crossroad and the driver of an approaching vehicle. Adequate time must be provided for the waiting vehicle to turn right, without requiring the through traffic to radically alter their speed. Sight distance should be measured from a 3.5-foot height at the location of the driver on the minor road to a 4.25-foot object height in the center of the approaching lane of the major road. Set-back for the driver on the crossroad shall be a minimum of 15 feet, measured from the edge of the traveled way.

Sight distance along Laurel Road at D Lane was evaluated based on sight distance criteria contained in the *Highway Design Manual* published by Caltrans. The recommended sight distance at intersections of public streets is based on corner sight distances, which uses the approach travel speeds as the basis for determining the recommended sight distance.

Sight distance at the intersection was measured using the site plan. Based on the posted speed limit on Laurel Road between Hillcrest Avenue and Canada Valley Drive of 45 mph, the minimum corner sight distance needed is 495 feet. Because the intersection would be restricted to right-turn only movements, only sight distance to the east was reviewed. Based on the site plan, the lines of sight would be adequate. A graphic of the sight distance is provided in Appendix E.

However, in order to maintain these sight lines for vehicles leaving the site, it is recommended that landscaping be trimmed such that tree canopies are at least seven feet above the ground; other landscaping within the sight lines should be limited to low-lying vegetation no greater than three feet in height. In addition, signs and monuments planned along the project's frontage should be placed in a manner that does not obstruct sight distance at the project intersections.

Finding – Sight distance lines at the unsignalized intersection of Laurel Road/D Lane would require landscaping maintenance.

Recommendation – In order to maintain adequate sight lines for vehicles leaving the site it is recommended that landscaping be trimmed such that tree canopies are at least seven feet above the ground; other landscaping within the sight lines should be limited to low-lying vegetation no greater than three feet in height.

Conclusions and Recommendations

Conclusions

- The project is expected to generate an average of 1,780 trips per day, including 140 a.m. peak hour trips and 187 trips during the p.m. peak hour.
- Study intersections analyzed under existing conditions operate acceptably and are expected to continue to do so in the near-term as well as for the cumulative scenarios with the addition of the project traffic and the associated roadway improvements.
- Under the projected future volumes, the study intersections are expected to operate acceptably with the exception of Hillcrest Road/Laurel Road in the a.m. and p.m. peak hours and Laurel Road/Slatten Ranch Road during the p.m. peak hour. The intersections of SR 4 Eastbound Ramps/Hillcrest Avenue and SR 4 Eastbound Ramps/Lone Tree Way are projected to operate below the desired Caltrans threshold, but acceptably based on the East County Action Plan.
- Queuing analysis for the proposed project driveway indicates the projected queue lengths would not exceed the estimated available storage.
- Under access Alternative 2, which would allow westbound left turns into the Park Ridge project, there would be sufficient storage space to accommodate the projected queue lengths.
- Proposed pedestrian facilities as shown on the site plan include sidewalks but do not include a connection to existing facilities. The site plan does not indicate if the signalized intersection would include pedestrian crossings.
- Bicycle and transit facilities, including the addition of bike lanes on Laurel Road based on the site plan, were determined to be adequate for the project.
- No circulation issues were identified on-site.
- Maintaining adequate sight distance at the unsignalized intersection of Laurel Road/D Lane would require landscaping maintenance.

Recommendations

- The sidewalks fronting the project site should connect to existing facilities.
- Pedestrian crosswalks, with a pedestrian phase, should be included in the design of the traffic signal at the Country Hills Drive/Laurel Road intersection.
- In order to maintain adequate sight lines for vehicles leaving the site on D Lane, it is recommended that landscaping be trimmed such that tree canopies are at least seven feet above the ground; other landscaping within the sight lines should be limited to low-lying vegetation no greater than three feet in height.
- Bike lanes should be provided on Laurel Road as indicated on preliminary site plans.

Study Participants and References

Study Participants

| | |
|---------------------|------------------------------|
| Principal in Charge | Mark E. Spencer, PE |
| Assistant Engineer | Briana Byrne, EIT |
| Technician/Graphics | Deborah J. Mizell |
| Editing/Formatting | Angela McCoy |
| Report Review | Dalene J. Whitlock, PE, PTOE |

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ANT009



Appendix A

Intersection LOS Methodology Clarifications and Modifications to CCTA Guidelines

Intersection LOS Methodology Clarifications and Modifications to CCTA Guidelines

The study intersections were analyzed using the Synchro analysis software, employing methodologies published in the *Highway Capacity Manual* (HCM), Transportation Research Board, 2010 and in accordance with *Technical Procedures* established by the Contra Costa Transportation Authority (CCTA), January 16, 2013. During the course of preparing the analysis, it was necessary to make assumptions and modifications when applying these methodologies. This document summarizes these assumptions.

HCM 2010 Methodology Limitation

The HCM 2010 methodology currently has limitations in determining LOS for certain shared lane configurations, including approaches with through-left lanes that are opposed by more than one through lane. The developers of Synchro, the software used for this analysis, have developed methodologies to approximate the LOS for intersections that have been affected by this limitation. This approximation was applied to the each of study intersections.

Right turn on Red

HCM 2010 methodologies require the number of vehicles observed to complete a right-turn on red movement (RTOR); however, such data was not available for the study intersections. Therefore, the RTOR volumes were estimated using the following method. This method is consistent with recommended methodologies presented in the HCM 2010 when field collected data is not available.

- RTOR volumes were entered only if the right turn movement is served by an exclusive lane and there is a complementary left-turn phase on the cross street
- RTOR may not exceed the number of shadowed left turners on a per lane basis
- RTOR may not exceed 50% of the total right turn volume
- RTOR volumes were not entered channelized yield-controlled right turns, as HCM 2010 methodologies address these movements separately
- RTOR volumes were only entered if there are projected to be 10 or more such movements during a peak hour

Lane Utilization Factor

Lane utilization factors calculated by Synchro were used for the analysis.

Traffic Signal Timing

Traffic signal timing was optimized using Synchro. The following assumptions were applied to the signal timing optimization:

- Assume a minimum 100 second cycle length for all actuated signals
- Green times were allocated by Synchro

Peak Hour Factor

Per CCTA guidance, the peak hour factor (PHF) for intersections is to be 0.92 at intersections with a peak hour entering volume of 1,000 vehicles or more. For intersections with less than 1,000 vehicles entering per peak hour, the PHF is to be 0.90. Under each scenario, every intersection has at least 1,000 vehicles entering so a base PHF of 0.92 was used. However, from the counts conducted at each study intersection, some intersections experience peak hour factors approaching 0.95 to 1.00. For the purposes of this

analysis, the PHF for those intersections was capped at 0.95. Unless otherwise stated in the below table, the PHF used for the analysis was 0.92.

Peak Hour Factor Adjustments

| Intersections | AM Peak | PM Peak |
|---|---------|---------|
| State Route 4 Westbound Ramps/ Hillcrest Avenue | -- | -- |
| State Route 4 Eastbound Ramps/ Hillcrest Avenue | -- | 0.95 |
| Hillcrest Road/ Laurel Road | -- | 0.95 |
| Laurel Road/ Canada Valley Road | -- | -- |
| State Route 4 Eastbound Ramps/ Laurel Road | -- | -- |
| State Route 4 Westbound Ramps/ Laurel Road | -- | -- |
| State Route 4 Eastbound Ramps/ Lone Tree Way | -- | 0.95 |
| State Route 4 Westbound Ramps/ Lone Tree Way | -- | 0.95 |
| Lone Tree Way/ Empire Avenue | -- | 0.95 |
| Laurel Road / County Hills Drive | -- | -- |
| Laurel Road / Slatten Ranch Road | -- | -- |

Note: Unless stated otherwise in the table, a PHF of 0.92 was used for all intersections

Appendix B

Intersection Level of Service Calculations

HCM 2010 Signalized Intersection Summary

1: Hillcrest Ave & SR4 WB Ramps

10/24/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------------|-----|------|------|------|------|------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 655 | 641 | 814 | 124 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/in | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 712 | 697 | 885 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 989 | 1686 | 1884 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 712 | 697 | 885 | 0 |
| Grip Sat Flow(s),veh/h/in | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.7 | 2.4 | 7.3 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.7 | 2.4 | 7.3 | 0.0 |
| Prop In Lane | | | 1.00 | | | |
| Lane Grp Cap(c), veh/h | | | 989 | 1686 | 1884 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.41 | 0.47 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2862 | 3813 | 4000 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 14.8 | 0.3 | 6.6 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.2 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/in | | | 4.2 | 1.0 | 3.5 | 0.0 |
| LnGrp Delay(d),s/veh | | | 15.8 | 0.4 | 6.8 | 0.0 |
| LnGrp LOS | | | B | A | A | |
| Approach Vol, veh/h | | | | 1409 | 885 | |
| Approach Delay, s/veh | | | | 8.2 | 6.8 | |
| Approach LOS | | | | A | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.4 | | | 17.5 | 29.0 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 39.0 | 53.0 |
| Max Q Clear Time (g, c+H1), s | | 4.4 | | | 10.7 | 9.3 |
| Green Ext Time (p, c), s | | 17.7 | | | 2.8 | 15.7 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 7.7 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

2: Hillcrest Ave & SR 4 EB Ramps

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 142 | 1 | 687 | 0 | 0 | 0 | 0 | 1152 | 395 | 168 | 634 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/in | 1900 | 1845 | 1845 | | | | 0 | 1845 | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 154 | 1 | 747 | | | | 0 | 1252 | 429 | 183 | 689 | 0 |
| Adj No. of Lanes | 0 | 1 | 2 | | | | 0 | 3 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | | | | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | 511 | 3 | 808 | | | | 0 | 1660 | 568 | 221 | 2166 | 0 |
| Arrive On Green | 0.29 | 0.29 | 0.29 | | | | 0.00 | 0.45 | 0.45 | 0.13 | 0.82 | 0.00 |
| Sat Flow, veh/h | 1746 | 11 | 2760 | | | | 0 | 3876 | 1268 | 1757 | 3597 | 0 |
| Grip Volume(v), veh/h | 155 | 0 | 747 | | | | 0 | 1133 | 548 | 183 | 689 | 0 |
| Grip Sat Flow(s),veh/h/in | 1757 | 0 | 1380 | | | | 0 | 1679 | 1621 | 1757 | 1752 | 0 |
| Q Serve(g, s), s | 6.1 | 0.0 | 23.5 | | | | 0.0 | 25.2 | 25.3 | 9.1 | 8.4 | 0.0 |
| Cycle Q Clear(g, c), s | 6.1 | 0.0 | 23.5 | | | | 0.0 | 25.2 | 25.3 | 9.1 | 8.4 | 0.0 |
| Prop In Lane | 0.99 | | 1.00 | | | | 0.00 | | 0.78 | 1.00 | 0.00 | |
| Lane Grp Cap(c), veh/h | 514 | 0 | 808 | | | | 0 | 1503 | 725 | 221 | 2166 | 0 |
| V/C Ratio(X) | 0.30 | 0.00 | 0.92 | | | | 0.00 | 0.75 | 0.76 | 0.83 | 0.32 | 0.00 |
| Avail Cap(c,a), veh/h | 531 | 0 | 833 | | | | 0 | 1614 | 779 | 354 | 2547 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | | | | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 24.5 | 0.0 | 30.7 | | | | 0.0 | 20.6 | 20.6 | 38.2 | 8.1 | 0.0 |
| Incr Delay (d2), s/veh | 0.3 | 0.0 | 15.7 | | | | 0.0 | 1.9 | 4.0 | 8.7 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/in | 3.0 | 0.0 | 10.7 | | | | 0.0 | 12.0 | 12.1 | 5.0 | 4.0 | 0.0 |
| LnGrp Delay(d),s/veh | 24.9 | 0.0 | 46.4 | | | | 0.0 | 22.5 | 24.6 | 46.8 | 8.2 | 0.0 |
| LnGrp LOS | C | | D | | | | C | C | D | D | A | |
| Approach Vol, veh/h | | | 902 | | | | | 1881 | | | 872 | |
| Approach Delay, s/veh | | | 42.7 | | | | | 23.2 | | | 16.3 | |
| Approach LOS | | | D | | | | | C | | | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | | 6 | | | | | |
| Phs Duration (G+Y+Rc), s | 15.2 | 44.0 | | 30.2 | | | 59.3 | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | | | |
| Max Green Setting (Gmax), s | 18.0 | 43.0 | | 27.0 | | | 65.0 | | | | | |
| Max Q Clear Time (g, c+H1), s | 11.1 | 27.3 | | 25.5 | | | 10.4 | | | | | |
| Green Ext Time (p, c), s | 0.3 | 12.8 | | 0.7 | | | 30.9 | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 26.5 | | | | | | | | | |
| HCM 2010 LOS | | | C | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 92 | 31 | 70 | 38 | 31 | 171 | 64 | 415 | 33 | 74 | 384 | 86 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Sat Flow, veh/h/ln | 100 | 34 | 76 | 41 | 34 | 106 | 70 | 451 | 0 | 80 | 417 | 93 |
| Adj Flow Rate, veh/h | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Adj No. of Lanes | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Peak Hour Factor | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Percent Heavy Veh. % | 437 | 99 | 220 | 389 | 358 | 304 | 101 | 1336 | 0 | 111 | 1104 | 244 |
| Cap. veh/h | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.06 | 0.38 | 0.00 | 0.06 | 0.39 | 0.39 |
| Arrive On Green | 1232 | 508 | 1136 | 1266 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 2854 | 631 |
| Sat Flow, veh/h | 100 | 0 | 110 | 41 | 34 | 106 | 70 | 451 | 0 | 80 | 255 | 255 |
| Grip Volume(v), veh/h | 1232 | 0 | 1644 | 1266 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1733 |
| Grip Sat Flow(s),veh/h/ln | 2.4 | 0.0 | 1.9 | 1.0 | 0.5 | 1.9 | 1.3 | 3.0 | 0.0 | 1.5 | 3.5 | 3.5 |
| Q Serve(g, s) | 2.9 | 0.0 | 1.9 | 2.9 | 0.5 | 1.9 | 1.3 | 3.0 | 0.0 | 1.5 | 3.5 | 3.5 |
| Cycle Q Clear(g, c), s | 1.00 | 0.89 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.36 |
| Prop In Lane | 437 | 0 | 319 | 389 | 358 | 304 | 101 | 1336 | 0 | 111 | 678 | 670 |
| Lane Grp Cap(c), veh/h | 0.23 | 0.00 | 0.35 | 0.11 | 0.10 | 0.35 | 0.69 | 0.34 | 0.00 | 0.72 | 0.38 | 0.38 |
| V/C Ratio(X) | 1350 | 0 | 1538 | 1328 | 1725 | 1466 | 901 | 4124 | 0 | 954 | 2115 | 2092 |
| Avail Cap(c,a), veh/h | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| HCM Platoon Ratio | 12.2 | 0.0 | 11.5 | 12.8 | 11.0 | 11.6 | 15.3 | 7.3 | 0.0 | 15.2 | 7.3 | 7.3 |
| Uniform Delay (d), s/veh | 0.3 | 0.0 | 0.6 | 0.1 | 0.1 | 0.7 | 8.3 | 0.1 | 0.0 | 8.6 | 0.3 | 0.4 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.8 | 0.0 | 0.9 | 0.3 | 0.3 | 0.9 | 0.9 | 1.5 | 0.0 | 1.0 | 1.7 | 1.7 |
| %ile BackOfQ(50%), veh/ln | 12.4 | 0.0 | 12.2 | 12.9 | 11.1 | 12.2 | 23.6 | 7.4 | 0.0 | 23.9 | 7.6 | 7.7 |
| LnGrp Delay(d),s/veh | B | B | B | B | B | B | C | A | C | C | A | A |
| LnGrp LOS | B | B | B | B | B | B | C | A | C | C | A | A |
| Approach Vol, veh/h | 210 | | | 181 | | | 521 | | | | 590 | |
| Approach Delay, s/veh | 12.3 | | | 12.2 | | | 9.6 | | | | 9.9 | |
| Approach LOS | B | | | B | | | A | | | | A | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|------|------|------|------|---|---|
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 | | |
| Phs Duration (G+Y+Rc), s | 6.1 | 16.6 | 10.4 | 5.9 | 16.8 | 10.4 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 18.0 | 39.0 | 31.0 | 17.0 | 40.0 | 31.0 | | |
| Max Q Clear Time (g_c+H1), s | 3.5 | 5.0 | 4.9 | 3.3 | 5.5 | 4.9 | | |
| Green Ext Time (p_c), s | 0.1 | 7.3 | 1.7 | 0.1 | 7.3 | 1.7 | | |

| | |
|----------------------|------|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 10.4 |
| HCM 2010 LOS | B |

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|--------|------|------|--------|------|------|------|------|-------|-------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 0 | 0 | 0 | 0 | 0 | 573 | 0 | 0 | 0 | 529 | 1 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1900 | 1845 | 1845 | 1900 | 1900 |
| Adj Sat Flow, veh/h/ln | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 576 | 0 | 0 |
| Adj Flow Rate, veh/h | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 |
| Adj No. of Lanes | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Peak Hour Factor | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Percent Heavy Veh. % | 0 | 47 | 0 | 0 | 47 | 0 | 0 | 0 | 0 | 1649 | 866 | 0 |
| Cap. veh/h | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.47 | 0.00 | 0.00 |
| Arrive On Green | 0 | -71942 | 0 | 0 | -71942 | 0 | 0 | 0 | 0 | 3514 | 1845 | 0 |
| Sat Flow, veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 576 | 0 | 0 |
| Grip Volume(v), veh/h | 0 | 1752 | 0 | 0 | 1752 | 0 | 0 | 0 | 0 | 1757 | 1845 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Q Serve(g, s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Prop In Lane | 0 | 47 | 0 | 0 | 47 | 0 | 0 | 0 | 0 | 1649 | 866 | 0 |
| Lane Grp Cap(c), veh/h | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 | 0.00 | 0.00 |
| V/C Ratio(X) | 0 | 16741 | 0 | 0 | 16741 | 0 | 0 | 0 | 0 | 26107 | 13706 | 0 |
| Avail Cap(c,a), veh/h | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| HCM Platoon Ratio | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.4 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.4 | 0.0 | 0.0 |
| LnGrp LOS | | | | | | | | | | A | | |
| Approach Vol, veh/h | 0 | | | 0 | | | 0 | | | 576 | | |
| Approach Delay, s/veh | 0.0 | | | 0.0 | | | 0.0 | | | 1.4 | | |
| Approach LOS | | | | A | | | A | | | A | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|---|------|---|---|------|---|------|
| Assigned Phs | | | 4 | | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | 0.0 | | | 7.5 | | 0.0 |
| Change Period (Y+Rc), s | | | 4.0 | | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | 36.0 | | | 56.0 | | 36.0 |
| Max Q Clear Time (g_c+H1), s | | | 0.0 | | | 2.8 | | 0.0 |
| Green Ext Time (p_c), s | | | 0.0 | | | 2.3 | | 0.0 |

| | |
|----------------------|-----|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 1.4 |
| HCM 2010 LOS | A |


















Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/24/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  | | | | | |  |  | | |
| Volume (veh/h) | 4 | 529 | 0 | 0 | 571 | 725 | 2 | 0 | 318 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Ob), veh | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Ped-Bike Adj(A, pbt) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Adj Sat Flow, veh/h | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | | | |
| Adj Flow Rate, veh/h | 4 | 575 | 0 | 0 | 621 | 0 | 2 | 0 | 346 | | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | |
| Percent Heavy Veh, % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | | | |
| Cap. veh/h | 8 | 1855 | 0 | 0 | 1502 | 672 | 488 | 0 | 435 | | | |
| Arrive On Green | 0.00 | 0.53 | 0.00 | 0.00 | 0.43 | 0.00 | 0.28 | 0.00 | 0.28 | | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | | |
| Grp Volume(v), veh/h | 4 | 575 | 0 | 0 | 621 | 0 | 2 | 0 | 346 | | | |
| Grp Sat Flow(s), veh/h | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | | |
| Q Serve(g, s) | 0.1 | 3.8 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 0.0 | 8.5 | | | |
| Cycle Q Clear(g, c), s | 0.1 | 3.8 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 0.0 | 8.5 | | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 8 | 1855 | 0 | 0 | 1502 | 672 | 488 | 0 | 435 | | | |
| V/C Ratio(X) | 0.52 | 0.31 | 0.00 | 0.00 | 0.41 | 0.00 | 0.00 | 0.00 | 0.80 | | | |
| Avail Cap(c, a), veh/h | 170 | 4652 | 0 | 0 | 3976 | 1779 | 1569 | 0 | 1400 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 20.6 | 5.5 | 0.00 | 0.00 | 8.2 | 0.00 | 10.8 | 0.00 | 13.9 | | | |
| Incr Delay (d2), s/veh | 46.2 | 0.1 | 0.00 | 0.00 | 0.2 | 0.00 | 0.00 | 0.00 | 3.3 | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.0 | | | |
| %ile BackOfQ(50%), veh/h | 0.1 | 1.9 | 0.00 | 0.00 | 2.5 | 0.00 | 0.00 | 0.00 | 4.1 | | | |
| LnGrp Delay(d), s/veh | 66.8 | 5.6 | 0.00 | 0.00 | 8.4 | 0.00 | 10.8 | 0.00 | 17.2 | | | |
| LnGrp LOS | E | A | | | A | | B | | B | | | |
| Approach Vol, veh/h | 579 | | | 621 | | | 348 | | | | | |
| Approach Delay, s/veh | 6.0 | | | 8.4 | | | 17.2 | | | | | |
| Approach LOS | A | | | A | | | B | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |













Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume (veh/h) | 0 | 783 | 434 | 95 | 1180 | 0 | 0 | 0 | 0 | 307 | 1 | 393 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbt}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 0 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 851 | 472 | 103 | 1283 | 0 | | | | 335 | 0 | 427 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2277 | 709 | 174 | 2825 | 0 | | | | 1138 | 0 | 508 |
| Arrive On Green | 0.00 | 0.45 | 0.45 | 0.05 | 0.56 | 0.00 | | | | 0.32 | 0.00 | 0.32 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 851 | 472 | 103 | 1283 | 0 | | | | 335 | 0 | 427 |
| Grip Sat Flow(s)/veh/h | 0 | 1679 | 1568 | 1704 | 1679 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 7.7 | 16.4 | 2.1 | 10.4 | 0.0 | | | | 4.9 | 0.0 | 17.6 |
| Cycle Q Clear(g, c), s | 0.0 | 7.7 | 16.4 | 2.1 | 10.4 | 0.0 | | | | 4.9 | 0.0 | 17.6 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2277 | 709 | 174 | 2825 | 0 | | | | 1138 | 0 | 508 |
| V/C Ratio(X) | 0.00 | 0.37 | 0.67 | 0.59 | 0.45 | 0.00 | | | | 0.29 | 0.00 | 0.84 |
| Avail Cap(c,a), veh/h | 0 | 2466 | 768 | 344 | 3263 | 0 | | | | 2378 | 0 | 1061 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 12.5 | 14.9 | 32.2 | 9.0 | 0.0 | | | | 17.6 | 0.0 | 21.8 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 2.0 | 3.2 | 0.1 | 0.0 | | | | 0.1 | 0.0 | 3.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/h | 0.0 | 3.6 | 7.5 | 1.0 | 4.8 | 0.0 | | | | 2.4 | 0.0 | 8.1 |
| LnGrp Delay(d),s/veh | 0.0 | 12.6 | 16.9 | 35.4 | 9.1 | 0.0 | | | | 17.7 | 0.0 | 25.7 |
| LnGrp LOS | | B | B | D | A | | | | | B | | C |
| Approach Vol, veh/h | 1323 | | | 1386 | | | | | | 762 | | |
| Approach Delay, s/veh | 14.2 | | | 11.0 | | | B | | | 22.2 | | |
| Approach LOS | B | | | | | | C | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 945 | 166 | 8 | 3 | 850 | 307 | 429 | 19 | 138 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1027 | 90 | 3 | 924 | 334 | 481 | 0 | 147 | 0 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2718 | 846 | 6 | 3145 | 979 | 746 | 0 | 333 | 0 | 0 |
| Arrive On Green | 0.00 | 0.54 | 0.54 | 0.00 | 0.62 | 0.62 | 0.21 | 0.00 | 0.21 | 0.00 | 0.21 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1027 | 90 | 3 | 924 | 334 | 481 | 0 | 147 | 0 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 5.8 | 1.4 | 0.1 | 4.1 | 5.0 | 6.1 | 0.0 | 4.0 | 0.0 | 4.0 |
| Cycle Q Clear(g, c), s | 0.0 | 5.8 | 1.4 | 0.1 | 4.1 | 5.0 | 6.1 | 0.0 | 4.0 | 0.0 | 4.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2718 | 846 | 6 | 3145 | 979 | 746 | 0 | 333 | 0 | 333 |
| V/C Ratio(X) | 0.00 | 0.38 | 0.11 | 0.52 | 0.29 | 0.34 | 0.64 | 0.00 | 0.44 | 0.00 | 0.44 |
| Avail Cap(c,a), veh/h | 0 | 3799 | 1183 | 501 | 5647 | 1758 | 2851 | 0 | 1183 | 0 | 1183 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 6.5 | 5.5 | 24.4 | 4.2 | 4.4 | 17.6 | 0.0 | 16.8 | 0.0 | 16.8 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 0.1 | 58.4 | 0.1 | 0.2 | 0.9 | 0.0 | 0.9 | 0.0 | 0.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 2.7 | 0.6 | 0.1 | 1.9 | 2.2 | 3.0 | 0.0 | 1.8 | 0.0 | 1.8 |
| LnGrp Delay(d),s/veh | 0.0 | 6.6 | 5.6 | 82.8 | 4.3 | 4.6 | 18.6 | 0.0 | 17.7 | 0.0 | 17.7 |
| LnGrp LOS | A | A | A | F | A | A | B | B | B | B | B |
| Approach Vol, veh/h | 1117 | | | 1261 | | | 628 | | | | |
| Approach Delay, s/veh | 6.5 | | | 4.6 | | | 18.4 | | | | |
| Approach LOS | A | | | A | | | B | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|---|---|---|---|------|
| Assigned Phs | 2 | 3 | 4 | | | | | 8 |
| Phs Duration (G+Y+Rc), s | 14.4 | 4.2 | 30.5 | | | | | 34.6 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | | 4.0 |
| Max Green Setting (Gmax), s | 37.0 | 14.0 | 37.0 | | | | | 55.0 |
| Max Q Clear Time (g, c+H1), s | 8.1 | 2.1 | 7.8 | | | | | 7.0 |
| Green Ext Time (p, c), s | 2.3 | 0.0 | 18.1 | | | | | 23.6 |

| Intersection Summary | |
|----------------------|-----|
| HCM 2010 Ctrl Delay | 8.2 |
| HCM 2010 LOS | A |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | SBR |
|---------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s),veh/h/ln | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c,a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(l) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |

| Timer | |
|--|--|
| User approved ignoring U-Turning movement. | |

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/24/2015

| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU |
|--|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | 43 | 131 | 459 | 41 | 61 | 606 | 88 | 15 | 107 | 88 | 47 |
| Volume (veh/h) | 7 | 4 | 0 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 25 |
| Number | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Initial Q (Qb), veh | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Sat Flow, veh/h/ln | 142 | 499 | 23 | 66 | 659 | 48 | 116 | 96 | 26 | 1 | 1 |
| Adj Flow Rate, veh/h | 1 | 3 | 1 | 1 | 3 | 1 | 2 | 1 | 1 | 1 | 1 |
| Adj No. of Lanes | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Peak Hour Factor | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Percent Heavy Veh. % | 0.11 | 0.34 | 0.34 | 0.05 | 0.29 | 0.29 | 0.07 | 0.16 | 0.16 | 0.16 | 0.16 |
| Arrive On Green | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | 3408 | 1845 | 1568 | 1568 | 1568 |
| Sat Flow, veh/h | 142 | 499 | 23 | 66 | 659 | 48 | 116 | 96 | 26 | 1 | 1 |
| Grip Volume(v), veh/h | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | 1704 | 1845 | 1568 | 1568 | 1568 |
| Grip Sat Flow(s),veh/h/ln | 3.3 | 3.1 | 0.4 | 1.6 | 4.6 | 1.0 | 1.4 | 2.0 | 0.6 | 0.6 | 0.6 |
| Q Serve(g, s), s | 3.3 | 3.1 | 0.4 | 1.6 | 4.6 | 1.0 | 1.4 | 2.0 | 0.6 | 0.6 | 0.6 |
| Cycle Q Clear(g, c), s | 192 | 1731 | 539 | 89 | 1437 | 448 | 239 | 294 | 250 | 250 | 250 |
| Prop In Lane | 0.74 | 0.29 | 0.04 | 0.74 | 0.46 | 0.11 | 0.49 | 0.33 | 0.10 | 0.10 | 0.10 |
| Lane Grp Cap(c), veh/h | 1979 | 6501 | 2024 | 371 | 1891 | 589 | 320 | 693 | 589 | 589 | 589 |
| V/C Ratio(X) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Avail Cap(c,a), veh/h | 18.4 | 10.2 | 9.3 | 19.9 | 12.5 | 11.2 | 19.1 | 15.9 | 15.3 | 15.3 | 15.3 |
| Upstream Filter(l) | 5.5 | 0.1 | 0.0 | 11.2 | 0.2 | 0.1 | 1.5 | 0.6 | 0.2 | 0.2 | 0.2 |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 1.9 | 1.4 | 0.2 | 1.0 | 2.1 | 0.4 | 0.7 | 1.0 | 0.3 | 0.3 | 0.3 |
| Initial Q Delay(d3),s/veh | 23.9 | 10.3 | 9.3 | 31.1 | 12.7 | 11.3 | 20.6 | 16.5 | 15.5 | 15.5 | 15.5 |
| %ile BackOfQ(50%), veh/ln | C | B | A | C | B | B | C | B | B | B | B |
| LnGrp Delay(d),s/veh | 664 | 132 | B | 773 | 14.2 | B | 238 | 18.4 | B | B | B |
| LnGrp LOS | C | B | A | C | B | B | C | B | B | B | B |
| Approach Vol, veh/h | 132 | B | 773 | 14.2 | B | 238 | 18.4 | B | B | B | B |
| Approach Delay, s/veh | 13.2 | B | 14.2 | B | 14.2 | B | 18.4 | B | B | B | B |
| Approach LOS | B | B | B | B | B | B | B | B | B | B | B |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Phs Duration (G+Y+Rc), s | 7.0 | 10.8 | 6.2 | 18.6 | 7.0 | 10.8 | 8.7 | 16.2 | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Max Green Setting (Gmax), s | 4.0 | 16.0 | 9.0 | 55.0 | 4.0 | 16.0 | 48.0 | 16.0 | | | |
| Max Q Clear Time (g, c+H1), s | 3.4 | 4.0 | 3.6 | 5.1 | 3.4 | 5.3 | 5.3 | 6.6 | | | |
| Green Ext Time (p, c), s | 0.0 | 1.7 | 0.0 | 9.6 | 0.0 | 1.6 | 0.4 | 4.9 | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | | | | | | | |
| HCM 2010 LOS | | | | | | | | | | | |
| Notes | | | | | | | | | | | |
| User approved ignoring U-Turning movement. | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/24/2015

| Movement | SBL | SBT | SBR |
|---------------------------|------|------|------|
| Lane Configurations | 55 | 11 | 11 |
| Volume (veh/h) | 109 | 126 | 119 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1845 | 1845 | 1900 |
| Adj Sat Flow, veh/h/ln | 118 | 137 | 129 |
| Adj Flow Rate, veh/h | 2 | 2 | 0 |
| Adj No. of Lanes | 0.92 | 0.92 | 0.92 |
| Peak Hour Factor | 3 | 3 | 3 |
| Percent Heavy Veh. % | 0.07 | 0.16 | 0.16 |
| Arrive On Green | 3408 | 1778 | 1546 |
| Sat Flow, veh/h | 118 | 135 | 131 |
| Grip Volume(v), veh/h | 1704 | 1752 | 1572 |
| Grip Sat Flow(s),veh/h/ln | 1.4 | 3.0 | 3.3 |
| Q Serve(g, s), s | 1.4 | 3.0 | 3.3 |
| Cycle Q Clear(g, c), s | 1.4 | 3.0 | 3.3 |
| Prop In Lane | 1.00 | 0.98 | 0.98 |
| Lane Grp Cap(c), veh/h | 241 | 280 | 251 |
| V/C Ratio(X) | 0.49 | 0.48 | 0.52 |
| Avail Cap(c,a), veh/h | 320 | 658 | 590 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.1 | 16.3 | 16.4 |
| Incr Delay (d2), s/veh | 1.5 | 1.3 | 1.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.7 | 1.5 | 1.5 |
| LnGrp Delay(d),s/veh | 20.6 | 17.6 | 18.1 |
| LnGrp LOS | C | B | B |
| Approach Vol, veh/h | 384 | 18.7 | B |
| Approach Delay, s/veh | 18.7 | B | B |
| Approach LOS | B | B | B |
| Timer | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
1: Hillcrest Ave & SR4 WB Ramps

10/24/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
|-------------------------------|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | |
| Volume (veh/h) | 0 | 0 | 648 | 552 | 870 | 141 | |
| Number | | | 5 | 2 | 6 | 16 | |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | | |
| Ped-Bike Adj(A_pbT) | | | 1.00 | | | 1.00 | |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 | |
| Adj Flow Rate, veh/h | | | 704 | 600 | 946 | 0 | |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 | |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 | |
| Cap. veh/h | | | 979 | 1685 | 1893 | 0 | |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 | |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 | |
| Grip Volume(v), veh/h | | | 704 | 600 | 946 | 0 | |
| Grip Sat Flow(s),veh/h/ln | | | 1704 | 1845 | 1752 | 0 | |
| Q Serve(g, s), s | | | 8.6 | 1.9 | 7.9 | 0.0 | |
| Cycle Q Clear(g, c), s | | | 8.6 | 1.9 | 7.9 | 0.0 | |
| Prop In Lane | | | 1.00 | | | 0.00 | |
| Lane Grp Cap(c), veh/h | | | 979 | 1685 | 1893 | 0 | |
| V/C Ratio(X) | | | 0.72 | 0.36 | 0.50 | 0.00 | |
| Avail Cap(c,a), veh/h | | | 2722 | 3822 | 4161 | 0 | |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(l) | | | 1.00 | 1.00 | 1.00 | 0.00 | |
| Uniform Delay (d), s/veh | | | 14.8 | 0.3 | 6.7 | 0.0 | |
| Incr Delay (d2), s/veh | | | 1.0 | 0.1 | 0.2 | 0.0 | |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | | | 4.1 | 0.9 | 3.7 | 0.0 | |
| LnGrp Delay(d),s/veh | | | 15.8 | 0.4 | 6.9 | 0.0 | |
| LnGrp LOS | | | B | A | A | A | |
| Approach Vol, veh/h | | | 1304 | | | | 946 |
| Approach Delay, s/veh | | | 8.7 | | | | 6.9 |
| Approach LOS | | | A | | | | A |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 8 |
| Assigned Phs | | 2 | | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.3 | | | | 17.3 | 29.0 |
| Change Period (Y+Rc), s | | 4.0 | | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | | 37.0 | 55.0 |
| Max Q Clear Time (g, c+H1), s | | 3.9 | | | | 10.6 | 9.9 |
| Green Ext Time (p, c), s | | 16.8 | | | | 2.7 | 15.1 |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | | | 8.0 | | | | A |
| HCM 2010 LOS | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|-----|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 122 | 0 | 730 | 0 | 0 | 0 | 0 | 1080 | 398 | 182 | 682 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | 1.00 | | | | 1.00 | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1900 | 1845 | 1845 | | 0 | 1845 | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | | | 128 | 0 | 768 | | 0 | 1137 | 419 | 192 | 718 | 0 |
| Adj No. of Lanes | | | 0 | 1 | 2 | | 0 | 3 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.95 | 0.95 | 0.95 | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | | | 540 | 0 | 848 | | 0 | 1537 | 566 | 231 | 2106 | 0 |
| Arrive On Green | | | 0.31 | 0.00 | 0.31 | | 0.00 | 0.42 | 0.42 | 0.13 | 0.60 | 0.00 |
| Sat Flow, veh/h | | | 1757 | 0 | 2760 | | 0 | 3795 | 1337 | 1757 | 3597 | 0 |
| Grip Volume(v), veh/h | | | 128 | 0 | 768 | | 0 | 1052 | 504 | 192 | 718 | 0 |
| Grip Sat Flow(s),veh/h/ln | | | 1757 | 0 | 1380 | | 0 | 1679 | 1609 | 1757 | 1752 | 0 |
| Q Serve(g, s), s | | | 4.7 | 0.0 | 23.3 | | 0.0 | 22.9 | 22.9 | 9.3 | 9.0 | 0.0 |
| Cycle Q Clear(g, c), s | | | 4.7 | 0.0 | 23.3 | | 0.0 | 22.9 | 22.9 | 9.3 | 9.0 | 0.0 |
| Prop In Lane | | | 1.00 | | 1.00 | | 0.00 | | 0.83 | 1.00 | 0.00 | 0.00 |
| Lane Grp Cap(c), veh/h | | | 540 | 0 | 848 | | 0 | 1422 | 681 | 231 | 2106 | 0 |
| V/C Ratio(X) | | | 0.24 | 0.00 | 0.91 | | 0.00 | 0.74 | 0.74 | 0.83 | 0.34 | 0.00 |
| Avail Cap(c,a), veh/h | | | 584 | 0 | 918 | | 0 | 1541 | 738 | 383 | 2533 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | 0.00 | 1.00 | | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 22.6 | 0.0 | 29.0 | | 0.0 | 21.1 | 21.1 | 36.9 | 8.7 | 0.0 |
| Incr Delay (d2), s/veh | | | 0.2 | 0.0 | 11.9 | | 0.0 | 1.8 | 3.7 | 7.6 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 2.3 | 0.0 | 10.3 | | 0.0 | 10.9 | 10.8 | 5.0 | 4.3 | 0.0 |
| LnGrp Delay(d),s/veh | | | 22.8 | 0.0 | 40.8 | | 0.0 | 22.9 | 24.8 | 44.4 | 8.8 | 0.0 |
| LnGrp LOS | | | C | | D | | | C | C | D | A | |
| Approach Vol, veh/h | | | 896 | | | | 1556 | | | | 910 | |
| Approach Delay, s/veh | | | 38.3 | | | | 23.5 | | | | 16.3 | |
| Approach LOS | | | D | | | | C | | | | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | 1 | 2 | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | | 15.5 | 40.9 | | | | | | | | | |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | | | | | | | | | |
| Max Green Setting (Gmax), s | | 19.0 | 40.0 | | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | | 11.3 | 24.9 | | | | | | | | | |
| Green Ext Time (p, c), s | | 0.3 | 12.0 | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 25.5 | | | | C | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 27 | 8 | 28 | 24 | 11 | 113 | 27 | 423 | 31 | 139 | 448 | 38 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Sat Flow, veh/h/ln | 28 | 8 | 29 | 25 | 12 | 60 | 28 | 445 | 0 | 146 | 472 | 40 |
| Adj Flow Rate, veh/h | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Adj No. of Lanes | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Peak Hour Factor | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Percent Heavy Veh. % | 360 | 34 | 125 | 343 | 182 | 154 | 49 | 1374 | 0 | 197 | 1559 | 132 |
| Cap. veh/h | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.03 | 0.39 | 0.00 | 0.11 | 0.48 | 0.48 |
| Arrive On Green | 1310 | 350 | 1270 | 1352 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 3272 | 276 |
| Sat Flow, veh/h | 28 | 0 | 37 | 25 | 12 | 60 | 28 | 445 | 0 | 146 | 252 | 260 |
| Grip Volume(v), veh/h | 1310 | 0 | 1621 | 1352 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1796 |
| Grip Sat Flow(s),veh/h/ln | 0.6 | 0.0 | 0.6 | 0.5 | 0.2 | 1.1 | 0.5 | 2.7 | 0.0 | 2.4 | 2.7 | 2.7 |
| Q Serve(g, s) | 0.8 | 0.0 | 0.6 | 1.2 | 0.2 | 1.1 | 0.5 | 2.7 | 0.0 | 2.4 | 2.7 | 2.7 |
| Cycle Q Clear(g, c), s | 1.00 | 0.78 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.15 |
| Prop In Lane | 360 | 0 | 160 | 343 | 182 | 154 | 49 | 1374 | 0 | 197 | 835 | 855 |
| Lane Grp Cap(c), veh/h | 0.08 | 0.00 | 0.23 | 0.07 | 0.07 | 0.39 | 0.57 | 0.32 | 0.00 | 0.74 | 0.30 | 0.30 |
| V/C Ratio(X) | 1272 | 0 | 1288 | 1285 | 1486 | 1246 | 582 | 4411 | 0 | 1513 | 3134 | 3212 |
| Avail Cap(c,a), veh/h | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| HCM Platoon Ratio | 12.7 | 0.0 | 12.6 | 13.1 | 12.4 | 12.8 | 14.5 | 6.4 | 0.0 | 13.0 | 4.8 | 4.8 |
| Upstream Filter(l) | 0.1 | 0.0 | 0.7 | 0.1 | 0.2 | 1.6 | 10.2 | 0.1 | 0.0 | 5.4 | 0.2 | 0.2 |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 0.3 | 0.2 | 0.1 | 0.5 | 0.4 | 1.3 | 0.0 | 1.5 | 1.3 | 1.3 |
| Initial Q Delay(d3),s/veh | 12.8 | 0.0 | 13.3 | 13.2 | 12.5 | 14.4 | 24.7 | 6.5 | 0.0 | 18.4 | 5.0 | 5.0 |
| %ile BackOfQ(50%), veh/ln | B | B | B | B | B | B | C | A | A | B | A | A |
| LnGrp Delay(d),s/veh | 65 | 13.1 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | 7.6 | 8.0 | 8.0 | 8.0 |
| LnGrp LOS | B | B | B | B | B | B | C | A | A | B | A | A |
| Approach Vol, veh/h | 65 | 13.1 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 | 7.6 | 8.0 | 8.0 | 8.0 |
| Approach Delay, s/veh | B | B | B | B | B | B | C | A | A | B | A | A |
| Approach LOS | B | B | B | B | B | B | C | A | A | B | A | A |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|---|---|
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 | | |
| Phs Duration (G+Y+Rc), s | 7.4 | 15.8 | 7.0 | 4.8 | 18.4 | 7.0 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 26.0 | 38.0 | 24.0 | 10.0 | 54.0 | 24.0 | | |
| Max Q Clear Time (g, c+H1), s | 4.4 | 4.7 | 2.8 | 2.5 | 4.7 | 3.2 | | |
| Green Ext Time (p, c), s | 0.4 | 7.2 | 0.6 | 0.0 | 7.5 | 0.5 | | |

| | |
|----------------------|-----|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 8.5 |
| HCM 2010 LOS | A |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|--------|------|------|--------|------|------|------|------|-------|------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 0 | 0 | 0 | 0 | 0 | 0 | 424 | 0 | 0 | 1054 | 2 | 2 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1845 | 1900 | 1845 | 1900 | 1845 | 1900 | 1845 | 1900 | 1845 | 1845 | 1845 | 1900 |
| Adj Sat Flow, veh/h/ln | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1149 | 0 | 0 |
| Adj Flow Rate, veh/h | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 |
| Adj No. of Lanes | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Peak Hour Factor | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Percent Heavy Veh. % | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 2456 | 1289 | 0 |
| Cap. veh/h | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.70 | 0.00 | 0.00 |
| Arrive On Green | 0 | -71942 | 0 | 0 | -71942 | 0 | 0 | 0 | 0 | 3514 | 1845 | 0 |
| Sat Flow, veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1149 | 0 | 0 |
| Grip Volume(v), veh/h | 0 | 1752 | 0 | 0 | 1752 | 0 | 0 | 0 | 0 | 1757 | 1845 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 |
| Q Serve(g, s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Prop In Lane | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 2456 | 1289 | 0 |
| Lane Grp Cap(c), veh/h | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.47 | 0.00 | 0.00 |
| V/C Ratio(X) | 0 | 5905 | 0 | 0 | 5905 | 0 | 0 | 0 | 0 | 18516 | 9721 | 0 |
| Avail Cap(c,a), veh/h | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| HCM Platoon Ratio | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Upstream Filter(l) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 |
| LnGrp LOS | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | A | A | A |
| Approach Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1149 | 0 | 0 |
| Approach Delay, s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | 0 | 0 |
| Approach LOS | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | A | A | A |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|-----|-----|-----|-----|------|------|---|---|
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 | | |
| Phs Duration (G+Y+Rc), s | 0.0 | 0.0 | 0.0 | 0.0 | 13.3 | 0.0 | | |
| Change Period (Y+Rc), s | 0.0 | 0.0 | 0.0 | 0.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 0.0 | 0.0 | 0.0 | 0.0 | 70.0 | 22.0 | | |
| Max Q Clear Time (g, c+H1), s | 0.0 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | | |
| Green Ext Time (p, c), s | 0.0 | 0.0 | 0.0 | 0.0 | 5.5 | 0.0 | | |

| | |
|----------------------|-----|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 1.0 |
| HCM 2010 LOS | A |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|------------------------------|------|------|------|------|------|------|------|------|------|-----|-----|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 4 | 1050 | 0 | 0 | 419 | 465 | 5 | 0 | 497 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | | |
| Adj Flow Rate, veh/h | 4 | 1141 | 0 | 0 | 455 | 0 | 5 | 0 | 540 | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | | |
| Cap. veh/h | 8 | 1703 | 0 | 0 | 1466 | 656 | 681 | 0 | 608 | | |
| Arrive On Green | 0.00 | 0.49 | 0.00 | 0.00 | 0.42 | 0.00 | 0.39 | 0.00 | 0.39 | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | |
| Grip Volume(v), veh/h | 4 | 1141 | 0 | 0 | 455 | 0 | 5 | 0 | 540 | | |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | |
| Q Serve(g, s) | 0.1 | 15.7 | 0.0 | 0.0 | 5.5 | 0.0 | 0.1 | 0.0 | 20.3 | | |
| Cycle Q Clear(g, c), s | 0.1 | 15.7 | 0.0 | 0.0 | 5.5 | 0.0 | 0.1 | 0.0 | 20.3 | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | | |
| Lane Grp Cap(c), veh/h | 8 | 1703 | 0 | 0 | 1466 | 656 | 681 | 0 | 608 | | |
| V/C Ratio(X) | 0.53 | 0.67 | 0.00 | 0.00 | 0.31 | 0.00 | 0.01 | 0.00 | 0.89 | | |
| Avail Cap(c,a), veh/h | 111 | 2328 | 0 | 0 | 1885 | 843 | 1389 | 0 | 1240 | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | |
| Uniform Delay (d), s/veh | 31.4 | 12.4 | 0.0 | 0.0 | 12.3 | 0.0 | 11.9 | 0.0 | 18.1 | | |
| Incr Delay (d2), s/veh | 47.6 | 0.5 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 4.7 | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| %ile BackOfQ(50%), veh/ln | 0.2 | 7.6 | 0.0 | 0.0 | 2.7 | 0.0 | 0.1 | 0.0 | 9.5 | | |
| LnGrp Delay(d), s/veh | 79.0 | 12.8 | 0.0 | 0.0 | 12.4 | 0.0 | 11.9 | 0.0 | 22.8 | | |
| LnGrp LOS | E | B | | | B | | B | | C | | |
| Approach Vol, veh/h | 1145 | | | | | | | | | | |
| Approach Delay, s/veh | 13.1 | | | | | | | | | | |
| Approach LOS | B | | | | | | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 2 | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 28.5 | | | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | | | | | | | | | | |
| Max Green Setting (Gmax), s | 50.0 | | | | | | | | | | |
| Max Q Clear Time (g_c+H1), s | 22.3 | | | | | | | | | | |
| Green Ext Time (p_c), s | 2.2 | | | | | | | | | | |

| | | | | | | | | | | | |
|----------------------|------|--|--|--|--|--|--|--|--|--|--|
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 15.4 | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|----------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1415 | 497 | 120 | 1383 | 0 | 0 | 0 | 0 | 454 | 2 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 0 | | | | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1489 | 523 | 126 | 1456 | 0 | | | | 479 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | | | | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | | | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | | | | 3 | 3 |
| Cap. veh/h | 0 | 2468 | 768 | 200 | 3017 | 0 | | | | 1055 | 0 |
| Arrive On Green | 0.00 | 0.49 | 0.49 | 0.06 | 0.60 | 0.00 | | | | 0.30 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | | | | 3514 | 0 |
| Grip Volume(v), veh/h | 0 | 1489 | 523 | 126 | 1456 | 0 | | | | 479 | 0 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1679 | 1568 | 1704 | 1679 | 0 | | | | 1757 | 0 |
| Q Serve(g, s) | 0.0 | 17.0 | 20.3 | 2.9 | 13.0 | 0.0 | | | | 8.8 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 17.0 | 20.3 | 2.9 | 13.0 | 0.0 | | | | 8.8 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2468 | 768 | 200 | 3017 | 0 | | | | 1055 | 0 |
| V/C Ratio(X) | 0.00 | 0.60 | 0.68 | 0.63 | 0.48 | 0.00 | | | | 0.45 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 2535 | 789 | 343 | 3295 | 0 | | | | 1769 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 14.7 | 15.5 | 36.6 | 9.0 | 0.0 | | | | 22.5 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.4 | 2.3 | 3.3 | 0.1 | 0.0 | | | | 0.3 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 7.9 | 9.2 | 1.4 | 6.0 | 0.0 | | | | 4.3 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 15.1 | 17.8 | 39.8 | 9.1 | 0.0 | | | | 22.8 | 0.0 |
| LnGrp LOS | | B | B | D | A | | | | | C | C |
| Approach Vol, veh/h | 2012 | | | | | | | | | | |
| Approach Delay, s/veh | 15.8 | | | | | | | | | | |
| Approach LOS | B | | | | | | | | | | |

| | | | | | | | | | | | |
|------------------------------|-----|---|---|---|---|---|---|---|--|--|--|
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 3 | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 8.7 | | | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | | | | | | | | | | |
| Max Green Setting (Gmax), s | 8.0 | | | | | | | | | | |
| Max Q Clear Time (g_c+H1), s | 4.9 | | | | | | | | | | |
| Green Ext Time (p_c), s | 0.1 | | | | | | | | | | |

| | | | | | | | | | | | |
|----------------------|------|--|--|--|--|--|--|--|--|--|--|
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 16.3 | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1604 | 285 | 20 | 5 | 982 | 372 | 539 | 29 | 189 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1688 | 153 | 5 | 1034 | 392 | 589 | 0 | 197 | 0 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 3011 | 937 | 9 | 3328 | 1036 | 786 | 0 | 351 | 0 | 0 |
| Arrive On Green | 0.00 | 0.60 | 0.60 | 0.01 | 0.66 | 0.66 | 0.22 | 0.00 | 0.22 | 0.00 | 0.22 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1688 | 153 | 5 | 1034 | 392 | 589 | 0 | 197 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 14.1 | 3.0 | 0.2 | 6.1 | 7.8 | 10.8 | 0.0 | 7.7 | 0.0 | 7.7 |
| Cycle Q Clear(g, c), s | 0.0 | 14.1 | 3.0 | 0.2 | 6.1 | 7.8 | 10.8 | 0.0 | 7.7 | 0.0 | 7.7 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 3011 | 937 | 9 | 3328 | 1036 | 786 | 0 | 351 | 0 | 0 |
| V/C Ratio(X) | 0.00 | 0.56 | 0.16 | 0.54 | 0.31 | 0.38 | 0.75 | 0.00 | 0.56 | 0.00 | 0.56 |
| Avail Cap(c.a), veh/h | 0 | 3011 | 937 | 507 | 4578 | 1425 | 1470 | 1.00 | 656 | 0 | 656 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 8.4 | 6.2 | 34.4 | 5.0 | 5.3 | 25.1 | 0.0 | 23.9 | 0.0 | 23.9 |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.1 | 40.6 | 0.1 | 0.2 | 1.5 | 0.0 | 1.4 | 0.0 | 1.4 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 6.5 | 1.3 | 0.2 | 2.8 | 3.4 | 5.4 | 0.0 | 3.5 | 0.0 | 3.5 |
| LnGrp Delay(d), s/veh | 0.0 | 8.7 | 6.3 | 75.0 | 5.1 | 5.5 | 26.5 | 0.0 | 25.3 | 0.0 | 25.3 |
| LnGrp LOS | A | A | A | E | A | A | C | C | C | C | C |
| Approach Vol, veh/h | 1841 | | | 1431 | | | 786 | | | | |
| Approach Delay, s/veh | 8.5 | | | 5.4 | | | 26.2 | | | | |
| Approach LOS | A | | | A | | | C | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|------|---|---|---|---|------|
| Assigned Phs | 2 | 3 | 4 | | | | | 8 |
| Phs Duration (G+Y+Rc), s | 19.5 | 4.4 | 45.4 | | | | | 49.8 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | | 4.0 |
| Max Green Setting (Gmax), s | 29.0 | 20.0 | 39.0 | | | | | 63.0 |
| Max Q Clear Time (g_c+H1), s | 12.8 | 2.2 | 16.1 | | | | | 9.8 |
| Green Ext Time (p_c), s | 2.7 | 0.0 | 19.8 | | | | | 36.0 |

| | |
|----------------------|------|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 10.8 |
| HCM 2010 LOS | B |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way
















10/24/2015

| Movement | SBR |
|----------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s), veh/h/ln | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c.a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(I) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3), s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d), s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |

| Timer |
|--|
| User approved ignoring U-Turning movement. |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

| |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU | | | | |
| Lane Configurations | 5 | 5 | 4 | 4 | 4 | 4 | 4 | 5 | 4 | 4 | 4 | | | | |
| Volume (veh/h) | 101 | 240 | 803 | 95 | 90 | 737 | 145 | 16 | 94 | 94 | 37 | | | | |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 18 | 5 | 2 | 2 | 12 | | | | |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | | | | |
| Adj Flow Rate, veh/h | 253 | 845 | 58 | 95 | 776 | 100 | 100 | 99 | 99 | 22 | 22 | | | | |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 2 | 1 | 1 | 1 | | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | | | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | | | |
| Cap. veh/h | 320 | 2075 | 646 | 123 | 1509 | 470 | 191 | 239 | 203 | | | | | | |
| Arrive On Green | 0.18 | 0.41 | 0.41 | 0.07 | 0.30 | 0.30 | 0.06 | 0.13 | 0.13 | 0.13 | | | | | |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | 3408 | 1845 | 1568 | | | | | | |
| Grp Volume(v), veh/h | 253 | 845 | 58 | 95 | 776 | 100 | 99 | 99 | 22 | | | | | | |
| Grp Sat Flow(s),veh/h/ln | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | 1704 | 1845 | 1568 | | | | | | |
| Q Serve(g, s), s | 7.7 | 6.6 | 1.3 | 3.0 | 7.1 | 2.7 | 1.6 | 2.8 | 0.7 | | | | | | |
| Cycle Q Clear(g, c), s | 7.7 | 6.6 | 1.3 | 3.0 | 7.1 | 2.7 | 1.6 | 2.8 | 0.7 | | | | | | |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Lane Grp Cap(c), veh/h | 320 | 2075 | 646 | 123 | 1509 | 470 | 191 | 239 | 203 | | | | | | |
| V/C Ratio(X) | 0.79 | 0.41 | 0.09 | 0.77 | 0.51 | 0.21 | 0.52 | 0.41 | 0.11 | | | | | | |
| Avail Cap(c, a), veh/h | 1381 | 4318 | 1344 | 377 | 1509 | 470 | 365 | 560 | 476 | | | | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Uniform Delay (d), s/veh | 21.9 | 11.6 | 10.1 | 25.6 | 16.2 | 14.7 | 25.7 | 22.4 | 21.5 | | | | | | |
| Incr Delay (d2), s/veh | 4.4 | 0.1 | 0.1 | 9.8 | 0.3 | 0.2 | 2.2 | 1.1 | 0.2 | | | | | | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | | | |
| %ile BackOfQ(50%), veh/ln | 4.1 | 3.1 | 0.6 | 1.8 | 3.3 | 1.2 | 0.8 | 1.5 | 0.3 | | | | | | |
| LnGrp Delay(d),s/veh | 26.2 | 11.8 | 10.1 | 35.4 | 16.5 | 14.9 | 27.8 | 23.6 | 21.7 | | | | | | |
| LnGrp LOS | C | B | B | D | B | B | C | C | C | | | | | | |
| Approach Vol, veh/h | 1156 | | | 971 | | | 220 | | | | | | | | |
| Approach Delay, s/veh | 14.8 | | | 18.2 | | | 25.3 | | | | | | | | |
| Approach LOS | B | | | B | | | C | | | | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | | | | |
| Phs Duration (G+Y+Rc), s | 9.7 | 11.3 | 7.9 | 27.1 | 7.1 | 13.9 | 14.2 | 20.8 | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | | | | |
| Max Green Setting (Gmax), s | 7.0 | 17.0 | 12.0 | 48.0 | 6.0 | 18.0 | 44.0 | 16.0 | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 5.8 | 4.8 | 5.0 | 8.6 | 3.6 | 7.9 | 9.7 | 9.1 | | | | | | | |
| Green EXT Time (p, c), s | 0.1 | 2.2 | 0.1 | 14.4 | 0.1 | 2.0 | 0.7 | 5.0 | | | | | | | |
| Intersection Summary | | | | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 18.8 | | | | | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | | | | | |
| Notes | | | | | | | | | | | | | | | |

| Movement | SBL | SBT | SBR |
|---------------------------|------|------|------|
| Lane Configurations | 5 | 4 | 4 |
| Volume (veh/h) | 227 | 194 | 155 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 239 | 204 | 163 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 350 | 335 | 254 |
| Arrive On Green | 0.10 | 0.18 | 0.18 |
| Sat Flow, veh/h | 3408 | 1900 | 1443 |
| Grip Volume(v), veh/h | 239 | 187 | 180 |
| Grip Sat Flow(s),veh/h/ln | 1704 | 1752 | 1590 |
| Q Serve(g, s), s | 3.8 | 5.5 | 5.9 |
| Cycle Q Clear(g, c), s | 3.8 | 5.5 | 5.9 |
| Prop In Lane | 1.00 | 1.00 | 0.91 |
| Lane Grp Cap(c), veh/h | 350 | 309 | 280 |
| V/C Ratio(X) | 0.68 | 0.61 | 0.64 |
| Avail Cap(c,a), veh/h | 426 | 563 | 511 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 24.2 | 21.3 | 21.4 |
| Incr Delay (d2), s/veh | 3.4 | 1.9 | 2.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 2.0 | 2.8 | 2.7 |
| LnGrp Delay(d),s/veh | 27.6 | 23.2 | 23.9 |
| LnGrp LOS | C | C | C |
| Approach Vol, veh/h | 606 | | |
| Approach Delay, s/veh | 25.1 | | |
| Approach LOS | C | | |
| Timer | | | |

HCM 2010 Signalized Intersection Summary

1: Hillcrest Ave & SR4 WB Ramps

10/24/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------------|-----|------|------|------|------|-------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 655 | 644 | 815 | 124 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 712 | 700 | 886 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 988 | 1686 | 1886 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 712 | 700 | 886 | 0 |
| Grip Sat Flow(s), veh/h/ln | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.7 | 2.4 | 7.3 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.7 | 2.4 | 7.3 | 0.0 |
| Prop In Lane | | | 1.00 | | | |
| Lane Grp Cap(c), veh/h | | | 988 | 1686 | 1886 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.42 | 0.47 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2856 | 3805 | 3991 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 14.8 | 0.3 | 6.6 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.2 | 0.2 | 0.0 |
| Initial Q Delay(d3), s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 4.2 | 1.0 | 3.5 | 0.0 |
| LnGrp Delay(d), s/veh | | | 15.8 | 0.4 | 6.8 | 0.0 |
| LnGrp LOS | | | B | A | A | |
| Approach Vol, veh/h | | | | 1412 | 886 | |
| Approach Delay, s/veh | | | | 8.2 | 6.8 | |
| Approach LOS | | | | A | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 7 8 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.5 | | | 17.5 | 29.1 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 39.0 | 53.0 |
| Max Q Clear Time (g, c+H1), s | | 4.4 | | | 10.7 | 9.3 |
| Green Ext Time (p, c), s | | 17.8 | | | 2.8 | 15.8 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 7.7 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

2: Hillcrest Ave & SR 4 EB Ramps

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|-----|------|------|-----|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 142 | 1 | 687 | 0 | 0 | 0 | 0 | 1155 | 395 | 168 | 635 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1900 | | | | 1845 | | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | | | 154 | | | | 1747 | | 1255 | 429 | 183 | 690 |
| Adj No. of Lanes | | | 0 | | | | 1 | | 3 | 0 | 1 | 2 |
| Peak Hour Factor | | | 0.92 | | | | 0.92 | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | | | | 3 | | 3 | 3 | 3 | 0 |
| Cap. veh/h | | | 511 | | | | 808 | | 1662 | 567 | 221 | 2166 |
| Arrive On Green | | | 0.29 | | | | 0.29 | | 0.00 | 0.45 | 0.13 | 0.62 |
| Sat Flow, veh/h | | | 1746 | | | | 2760 | | 3879 | 1266 | 1757 | 3597 |
| Grip Volume(v), veh/h | | | 155 | | | | 0 | | 1135 | 549 | 183 | 690 |
| Grip Sat Flow(s), veh/h/ln | | | 1757 | | | | 0 | | 1679 | 1621 | 1757 | 1752 |
| Q Serve(g, s), s | | | 6.1 | | | | 0.0 | | 25.2 | 25.3 | 9.1 | 8.4 |
| Cycle Q Clear(g, c), s | | | 6.1 | | | | 0.0 | | 25.2 | 25.3 | 9.1 | 8.4 |
| Prop In Lane | | | 0.99 | | | | 1.00 | | 0.78 | 1.00 | 1.00 | 0.00 |
| Lane Grp Cap(c), veh/h | | | 514 | | | | 0 | | 1503 | 726 | 221 | 2166 |
| V/C Ratio(X) | | | 0.30 | | | | 0.93 | | 0.75 | 0.76 | 0.83 | 0.32 |
| Avail Cap(c,a), veh/h | | | 530 | | | | 0 | | 1613 | 779 | 353 | 2546 |
| HCM Platoon Ratio | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 24.6 | | | | 0.0 | | 20.6 | 20.6 | 38.2 | 8.1 |
| Incr Delay (d2), s/veh | | | 0.3 | | | | 0.0 | | 1.9 | 4.0 | 8.7 | 0.1 |
| Initial Q Delay(d3), s/veh | | | 0.0 | | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 3.0 | | | | 0.0 | | 12.1 | 12.1 | 5.0 | 4.1 |
| LnGrp Delay(d), s/veh | | | 24.9 | | | | 0.0 | | 22.6 | 24.7 | 46.9 | 8.2 |
| LnGrp LOS | | | C | | | | D | | C | C | D | A |
| Approach Vol, veh/h | | | | | | | 902 | | 1884 | | | 873 |
| Approach Delay, s/veh | | | | | | | 42.7 | | 23.2 | | | 16.3 |
| Approach LOS | | | | | | | D | | C | | | B |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | 1 | 2 | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | | 15.2 | 44.1 | | | | | | | | | |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | | | | | | | | | |
| Max Green Setting (Gmax), s | | 18.0 | 43.0 | | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | | 11.1 | 27.3 | | | | | | | | | |
| Green Ext Time (p, c), s | | 0.3 | 12.7 | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | | | 26.6 | | | | | |
| HCM 2010 LOS | | | | | | | C | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary 3: Hillcrest Ave & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 92 | 31 | 70 | 38 | 31 | 171 | 64 | 418 | 33 | 74 | 385 | 86 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT) | | | | | | | | | | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 100 | 34 | 76 | 41 | 34 | 106 | 70 | 454 | 0 | 80 | 418 | 93 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 437 | 98 | 220 | 389 | 357 | 304 | 101 | 1339 | 0 | 110 | 1107 | 244 |
| Arrive On Green | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.06 | 0.38 | 0.00 | 0.06 | 0.39 | 0.39 |
| Sat Flow, veh/h | 1232 | 508 | 1136 | 1266 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 2856 | 630 |
| Grip Volume(v), veh/h | 100 | 0 | 110 | 41 | 34 | 106 | 70 | 454 | 0 | 80 | 255 | 256 |
| Grip Sat Flow(s), veh/h/ln | 1232 | 0 | 1644 | 1266 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1733 |
| Q Serve(g, s) | 2.4 | 0.0 | 1.9 | 1.0 | 0.5 | 1.9 | 1.3 | 3.1 | 0.0 | 1.5 | 3.5 | 3.5 |
| Cycle Q Clear(g, c), s | 2.9 | 0.0 | 1.9 | 2.9 | 0.5 | 1.9 | 1.3 | 3.1 | 0.0 | 1.5 | 3.5 | 3.5 |
| Prop In Lane | 1.00 | 0.89 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.36 | 0.36 |
| Lane Grp Cap(c), veh/h | 437 | 0 | 318 | 389 | 357 | 304 | 101 | 1339 | 0 | 110 | 679 | 672 |
| V/C Ratio(X) | 0.23 | 0.00 | 0.35 | 0.11 | 0.10 | 0.35 | 0.70 | 0.34 | 0.00 | 0.72 | 0.38 | 0.38 |
| Avail Cap(c,a), veh/h | 1348 | 0 | 1535 | 1325 | 1722 | 1464 | 889 | 4117 | 0 | 952 | 2111 | 2088 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 12.2 | 0.0 | 11.6 | 12.8 | 11.0 | 11.6 | 15.4 | 7.3 | 0.0 | 15.3 | 7.3 | 7.3 |
| Incr Delay (d2), s/veh | 0.3 | 0.0 | 0.6 | 0.1 | 0.1 | 0.7 | 8.3 | 0.1 | 0.0 | 8.6 | 0.3 | 0.4 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.8 | 0.0 | 0.9 | 0.3 | 0.3 | 0.9 | 0.9 | 1.5 | 0.0 | 1.0 | 1.7 | 1.7 |
| LnGrp Delay(d), s/veh | 12.5 | 0.0 | 12.2 | 12.9 | 11.1 | 12.3 | 23.7 | 7.4 | 0.0 | 23.9 | 7.6 | 7.7 |
| LnGrp LOS | B | B | B | B | B | B | C | A | C | C | A | A |
| Approach Vol, veh/h | 210 | | | 181 | | | 524 | | | 591 | | |
| Approach Delay, s/veh | 12.3 | | | 12.2 | | | 9.6 | | | 9.8 | | |
| Approach LOS | B | | | B | | | A | | | A | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|------|------|------|------|---|---|
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 | | |
| Phs Duration (G+Y+Rc), s | 6.1 | 16.7 | 10.4 | 5.9 | 16.9 | 10.4 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 18.0 | 39.0 | 31.0 | 17.0 | 40.0 | 31.0 | | |
| Max Q Clear Time (g_c+H1), s | 3.5 | 5.1 | 4.9 | 3.3 | 5.5 | 4.9 | | |
| Green Ext Time (p_c), s | 0.1 | 7.3 | 1.7 | 0.1 | 7.3 | 1.7 | | |

| Intersection Summary | | | | | | | |
|----------------------|--|--|--|------|--|--|--|
| HCM 2010 Ctrl Delay | | | | 10.4 | | | |
| HCM 2010 LOS | | | | B | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary 5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|--------|------|------|--------|------|------|--------|------|-------|-------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 0 | 0 | 0 | 0 | 0 | 573 | 0 | 0 | 529 | 1 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 0 | 6 | 16 |
| Initial Q (Qb), veh | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped-Bike Adj(A_pbT) | | | | | | | | | | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 576 | 0 | 0 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 47 | 0 | 0 | 47 | 0 | 0 | 47 | 0 | 1649 | 866 | 0 |
| Arrive On Green | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.47 | 0.00 | 0.00 |
| Sat Flow, veh/h | 0 | -71942 | 0 | 0 | -71942 | 0 | 0 | -71942 | 0 | 3514 | 1845 | 0 |
| Grip Volume(v), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 576 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1752 | 0 | 0 | 1752 | 0 | 0 | 1752 | 0 | 1757 | 1845 | 0 |
| Q Serve(g, s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Prop In Lane | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Lane Grp Cap(c), veh/h | 0 | 47 | 0 | 0 | 47 | 0 | 0 | 47 | 0 | 1649 | 866 | 0 |
| V/C Ratio(X) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 | 0.00 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 16741 | 0 | 0 | 16741 | 0 | 0 | 16741 | 0 | 26107 | 13706 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.4 | 0.0 | 0.0 |
| LnGrp LOS | | | | | | | | | | A | | |
| Approach Vol, veh/h | 0 | | | 0 | | | 0 | | | 576 | | |
| Approach Delay, s/veh | 0.0 | | | 0.0 | | | 0.0 | | | 1.4 | | |
| Approach LOS | | | | A | | | | | | A | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|---|------|---|---|------|---|------|
| Assigned Phs | | | 4 | | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | 0.0 | | | 7.5 | | 0.0 |
| Change Period (Y+Rc), s | | | 4.0 | | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | 36.0 | | | 56.0 | | 36.0 |
| Max Q Clear Time (g_c+H1), s | | | 0.0 | | | 2.8 | | 0.0 |
| Green Ext Time (p_c), s | | | 0.0 | | | 2.3 | | 0.0 |

| Intersection Summary | | | | | | | |
|----------------------|--|--|--|-----|--|--|--|
| HCM 2010 Ctrl Delay | | | | 1.4 | | | |
| HCM 2010 LOS | | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions































Synchro 8 Report

User approved volume balancing among the lanes for turning movement.

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/24/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | | | |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume (veh/h) | 4 | 529 | 0 | 0 | 571 | 725 | 2 | 0 | 318 | 0 | 0 | 0 | | | |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | | | | |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| Ped-Bike Adj(A, pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Adj Sat Flow, veh/h | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | | | | | | |
| Adj Flow Rate, veh/h | 4 | 575 | 0 | 0 | 621 | 0 | 2 | 0 | 346 | | | | | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | | | |
| Percent Heavy Veh, % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | | | | | | |
| Cap. veh/h | 8 | 1855 | 0 | 0 | 1502 | 672 | 488 | 0 | 435 | | | | | | |
| Arrive On Green | 0.00 | 0.53 | 0.00 | 0.00 | 0.43 | 0.00 | 0.28 | 0.00 | 0.28 | | | | | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | | | | | |
| Grp Volume(v), veh/h | 4 | 575 | 0 | 0 | 621 | 0 | 2 | 0 | 346 | | | | | | |
| Grp Sat Flow(s), veh/h | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | | | | | |
| Q Serve(g, s) | 0.1 | 3.8 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 0.0 | 8.5 | | | | | | |
| Cycle Q Clear(g, c), s | 0.1 | 3.8 | 0.0 | 0.0 | 5.1 | 0.0 | 0.0 | 0.0 | 8.5 | | | | | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Lane Grp Cap(c), veh/h | 8 | 1855 | 0 | 0 | 1502 | 672 | 488 | 0 | 435 | | | | | | |
| V/C Ratio(X) | 0.52 | 0.31 | 0.00 | 0.00 | 0.41 | 0.00 | 0.00 | 0.00 | 0.80 | | | | | | |
| Avail Cap(c, a), veh/h | 170 | 4652 | 0 | 0 | 3976 | 1779 | 1569 | 0 | 1400 | | | | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | | | | | |
| Uniform Delay (d), s/veh | 20.6 | 5.5 | 0.0 | 0.0 | 8.2 | 0.0 | 10.8 | 0.0 | 13.9 | | | | | | |
| Incr Delay (d2), s/veh | 46.2 | 0.1 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.0 | 3.3 | | | | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | | | |
| %ile BackOfQ(50%), veh/h | 0.1 | 1.9 | 0.0 | 0.0 | 2.5 | 0.0 | 0.0 | 0.0 | 4.1 | | | | | | |
| LnGrp Delay(d), s/veh | 66.8 | 5.6 | 0.0 | 0.0 | 8.4 | 0.0 | 10.8 | 0.0 | 17.2 | | | | | | |
| LnGrp LOS | E | A | | | A | | B | | B | | | | | | |
| Approach Vol, veh/h | 579 | | | 621 | | | 348 | | | | | | | | |
| Approach Delay, s/veh | 6.0 | | | 8.4 | | | 17.2 | | | | | | | | |
| Approach LOS | A | | | A | | | B | | | | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|-----|-----|------|------|------|
| Lane Configurations | ↔↔↔ | ↔↔↔ | ↔↔↔ | ↔↔↔ | ↔↔↔ | ↔↔↔ | | | | ↔↔↔ | ↔↔↔ | ↔↔↔ |
| Volume (veh/h) | 0 | 824 | 444 | 95 | 1189 | 0 | 0 | 0 | 0 | 307 | 1 | 401 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/hIn | 0 | 1845 | 1845 | 1845 | 1845 | 0 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 896 | 483 | 103 | 1292 | 0 | | | | 335 | 0 | 436 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 0 | 3 | 3 | 3 | 3 | 0 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2268 | 706 | 174 | 2810 | 0 | | | | 1155 | 0 | 515 |
| Arrive On Green | 0.00 | 0.45 | 0.45 | 0.05 | 0.56 | 0.00 | | | | 0.33 | 0.00 | 0.33 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | | | | 3514 | 0 | 1568 |
| Grp Volume(v), veh/h | 0 | 896 | 483 | 103 | 1292 | 0 | | | | 335 | 0 | 436 |
| Grp Sat Flow(s)/veh/hIn | 0 | 1679 | 1568 | 1704 | 1679 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 8.4 | 17.3 | 2.1 | 10.8 | 0.0 | | | | 5.0 | 0.0 | 18.3 |
| Cycle Q Clear(g, c), s | 0.0 | 8.4 | 17.3 | 2.1 | 10.8 | 0.0 | | | | 5.0 | 0.0 | 18.3 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2268 | 706 | 174 | 2810 | 0 | | | | 1155 | 0 | 515 |
| V/C Ratio(X) | 0.00 | 0.40 | 0.68 | 0.59 | 0.46 | 0.00 | | | | 0.29 | 0.00 | 0.85 |
| Avail Cap(c,a), veh/h | 0 | 2424 | 755 | 338 | 3209 | 0 | | | | 2338 | 0 | 1043 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 13.0 | 15.4 | 32.8 | 9.3 | 0.0 | | | | 17.6 | 0.0 | 22.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 2.4 | 3.2 | 0.1 | 0.0 | | | | 0.1 | 0.0 | 3.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/hIn | 0.0 | 3.9 | 7.8 | 1.1 | 4.9 | 0.0 | | | | 2.4 | 0.0 | 8.4 |
| LnGrp Delay(d),s/veh | 0.0 | 13.1 | 17.8 | 36.0 | 9.4 | 0.0 | | | | 17.7 | 0.0 | 26.0 |
| LnGrp LOS | | B | B | D | A | | | | | B | | C |
| Approach Vol, veh/h | 1379 | | | 1395 | | | 771 | | | | | |
| Approach Delay, s/veh | 14.7 | | | 11.4 | | | 22.4 | | | | | |
| Approach LOS | B | | | B | | | C | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ←←← | ←←← | ←←← | ←←← | ←←← | ←←← | ←←← | ←←← | ←←← | ←←← | ←←← |
| Volume (veh/h) | 0 | 962 | 190 | 8 | 3 | 856 | 307 | 432 | 19 | 138 | 0 |
| Number | 7 | 4 | 14 | 3 | 3 | 8 | 18 | 5 | 2 | 12 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1046 | 104 | 3 | 930 | 334 | 485 | 0 | 145 | 0 | 145 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2777 | 865 | 6 | 3187 | 992 | 740 | 0 | 330 | 0 | 330 |
| Arrive On Green | 0.00 | 0.55 | 0.55 | 0.00 | 0.63 | 0.63 | 0.21 | 0.00 | 0.21 | 0.00 | 0.21 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1046 | 104 | 3 | 930 | 334 | 485 | 0 | 145 | 0 | 145 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 6.0 | 1.6 | 0.1 | 4.3 | 5.1 | 6.5 | 0.0 | 4.1 | 0.0 | 4.1 |
| Cycle Q Clear(g, c), s | 0.0 | 6.0 | 1.6 | 0.1 | 4.3 | 5.1 | 6.5 | 0.0 | 4.1 | 0.0 | 4.1 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2777 | 865 | 6 | 3187 | 992 | 740 | 0 | 330 | 0 | 330 |
| V/C Ratio(X) | 0.00 | 0.38 | 0.12 | 0.52 | 0.29 | 0.34 | 0.66 | 0.00 | 0.44 | 0.00 | 0.44 |
| Avail Cap(c.a), veh/h | 0 | 4136 | 1288 | 206 | 5120 | 1594 | 2748 | 0 | 1226 | 0 | 1226 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 6.5 | 5.5 | 25.4 | 4.2 | 4.4 | 18.5 | 0.0 | 17.6 | 0.0 | 17.6 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 0.1 | 58.5 | 0.1 | 0.2 | 1.0 | 0.0 | 0.9 | 0.0 | 0.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 2.7 | 0.7 | 0.1 | 1.9 | 2.2 | 3.2 | 0.0 | 1.9 | 0.0 | 1.9 |
| LnGrp Delay(d),s/veh | 0.0 | 6.6 | 5.6 | 84.0 | 4.3 | 4.6 | 19.5 | 0.0 | 18.5 | 0.0 | 18.5 |
| LnGrp LOS | A | A | A | F | A | A | B | B | B | B | B |
| Approach Vol, veh/h | 1150 | | | 1267 | | | 630 | | | | |
| Approach Delay, s/veh | 6.5 | | | 4.5 | | | 19.2 | | | | |
| Approach LOS | A | | | A | | | B | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|-----|------|---|---|---|---|------|
| Assigned Phs | 2 | 3 | 4 | | | | | 8 |
| Phs Duration (G+Y+Rc), s | 14.8 | 4.2 | 32.2 | | | | | 36.4 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | | 4.0 |
| Max Green Setting (Gmax), s | 40.0 | 6.0 | 42.0 | | | | | 52.0 |
| Max Q Clear Time (g, c+H1), s | 8.5 | 2.1 | 8.0 | | | | | 7.1 |
| Green Ext Time (p, c), s | 2.3 | 0.0 | 20.2 | | | | | 23.4 |

| Intersection Summary | | | | | | | | |
|----------------------|-----|--|--|--|--|--|--|--|
| HCM 2010 Ctrl Delay | 8.3 | | | | | | | |
| HCM 2010 LOS | A | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | SBR |
|----------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s), veh/h/ln | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c.a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(l) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |























| Timer |
|--|
| User approved ignoring U-Turning movement. |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/24/2015

| |  |  |  |  |  |  |  |  |  |  |  | |
|-------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
| Lane Configurations | |  |  |  |  |  |  |  |  |  |  |  |
| Volume (veh/h) | 43 | 141 | 466 | 41 | 61 | 608 | 88 | 15 | 107 | 88 | 47 | 25 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 18 | 5 | 2 | 2 | 12 | |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 153 | 507 | 23 | 66 | 661 | 48 | 116 | 96 | 26 | | | |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 2 | 1 | 1 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 204 | 1903 | 593 | 87 | 1568 | 488 | 227 | 299 | 254 | | | |
| Arrive On Green | 0.12 | 0.38 | 0.38 | 0.05 | 0.31 | 0.31 | 0.07 | 0.16 | 0.16 | | | |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | 3408 | 1845 | 1568 | | | |
| Grp Volume(v), veh/h | 153 | 507 | 23 | 66 | 661 | 48 | 116 | 96 | 26 | | | |
| Grp Sat Flow(s),veh/h/ln | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | 1704 | 1845 | 1568 | | | |
| Q Serve(g, s), s | 3.9 | 3.2 | 0.4 | 1.7 | 4.8 | 1.0 | 1.5 | 2.1 | 0.7 | | | |
| Cycle Q Clear(g, c), s | 3.9 | 3.2 | 0.4 | 1.7 | 4.8 | 1.0 | 1.5 | 2.1 | 0.7 | | | |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 204 | 1903 | 593 | 87 | 1568 | 488 | 227 | 299 | 254 | | | |
| V/C Ratio(X) | 0.75 | 0.27 | 0.04 | 0.76 | 0.42 | 0.10 | 0.51 | 0.32 | 0.10 | | | |
| Avail Cap(c, a), veh/h | 867 | 3999 | 1245 | 490 | 2918 | 909 | 805 | 910 | 774 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 20.0 | 10.0 | 9.2 | 21.9 | 12.7 | 11.4 | 21.0 | 17.3 | 16.6 | | | |
| Incr Delay (d2), s/veh | 5.5 | 0.1 | 0.0 | 12.8 | 0.2 | 0.1 | 1.8 | 0.6 | 0.2 | | | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%),veh/ln | 2.2 | 1.5 | 0.2 | 1.1 | 2.2 | 0.4 | 0.8 | 1.1 | 0.3 | | | |
| LnGrp Delay(d),s/veh | 25.5 | 10.1 | 9.2 | 34.7 | 12.9 | 11.5 | 22.8 | 17.9 | 16.8 | | | |
| LnGrp LOS | C | B | A | C | B | B | C | B | B | | | |
| Approach Vol, veh/h | 683 | | | 775 | | | 238 | | | | | |
| Approach Delay, s/veh | 13.5 | | | 14.7 | | | 20.1 | | | | | |
| Approach LOS | B | | | B | | | C | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 7.1 | 11.6 | 6.3 | 21.6 | 7.1 | 11.6 | 9.4 | 18.5 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 11.0 | 23.0 | 13.0 | 37.0 | 11.0 | 23.0 | 23.0 | 27.0 | | | | |
| Max Q Clear Time (g, c+H1), s | 3.6 | 4.1 | 3.7 | 5.2 | 3.5 | 5.6 | 5.9 | 6.8 | | | | |
| Green Ext Time (p, c), s | 0.2 | 2.0 | 0.1 | 9.0 | 0.2 | 2.0 | 0.3 | 7.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 16.0 | | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/24/2015

| Movement | SBL | SBT | SBR |
|---------------------------|------|------|------|
| Lane Configurations | 55 | 11 | 11 |
| Volume (veh/h) | 109 | 126 | 122 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 118 | 137 | 133 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 229 | 285 | 255 |
| Arrive On Green | 0.07 | 0.16 | 0.16 |
| Sat Flow, veh/h | 3408 | 1752 | 1568 |
| Grip Volume(v), veh/h | 118 | 137 | 133 |
| Grip Sat Flow(s),veh/h/ln | 1704 | 1752 | 1568 |
| Q Serve(g, s), s | 1.6 | 3.3 | 3.6 |
| Cycle Q Clear(g, c), s | 1.6 | 3.3 | 3.6 |
| Prop In Lane | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 229 | 285 | 255 |
| V/C Ratio(X) | 0.52 | 0.48 | 0.52 |
| Avail Cap(c,a), veh/h | 805 | 865 | 774 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 21.0 | 17.7 | 17.8 |
| Incr Delay (d2), s/veh | 1.8 | 1.3 | 1.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.8 | 1.7 | 1.7 |
| LnGrp Delay(d),s/veh | 22.8 | 19.0 | 19.5 |
| LnGrp LOS | C | B | B |
| Approach Vol, veh/h | 388 | | |
| Approach Delay, s/veh | 20.3 | | |
| Approach LOS | C | | |
| Timer | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
1: Hillcrest Ave & SR4 WB Ramps

10/24/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------------|-----|------|------|------|------|-------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 648 | 554 | 874 | 141 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 704 | 602 | 950 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 978 | 1686 | 1897 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 704 | 602 | 950 | 0 |
| Grip Sat Flow(s),veh/h/ln | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.6 | 1.9 | 7.9 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.6 | 1.9 | 7.9 | 0.0 |
| Prop In Lane | | | 1.00 | | | |
| Lane Grp Cap(c), veh/h | | | 978 | 1686 | 1897 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.36 | 0.50 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2711 | 3807 | 4144 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 14.9 | 0.3 | 6.7 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.1 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 4.1 | 0.9 | 3.7 | 0.0 |
| LnGrp Delay(d),s/veh | | | 15.9 | 0.4 | 6.9 | 0.0 |
| LnGrp LOS | | | B | A | A | |
| Approach Vol, veh/h | | | | 1306 | 950 | |
| Approach Delay, s/veh | | | | 8.8 | 6.9 | |
| Approach LOS | | | | A | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 7 8 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.5 | | | 17.3 | 29.2 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 37.0 | 55.0 |
| Max Q Clear Time (g, c+H1), s | | 3.9 | | | 10.6 | 9.9 |
| Green Ext Time (p, c), s | | 16.9 | | | 2.7 | 15.2 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 8.0 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 122 | 0 | 730 | 0 | 0 | 0 | 0 | 1082 | 398 | 182 | 688 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1900 | 1845 | 1845 | | | | 0 | 1845 | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 128 | 0 | 768 | | | | 0 | 1139 | 419 | 192 | 722 | 0 |
| Adj No. of Lanes | 0 | 1 | 2 | | | | 0 | 3 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | | | | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | 540 | 0 | 848 | | | | 0 | 1538 | 566 | 231 | 2107 | 0 |
| Arrive On Green | 0.31 | 0.00 | 0.31 | | | | 0.00 | 0.42 | 0.42 | 0.13 | 0.60 | 0.00 |
| Sat Flow, veh/h | 1757 | 0 | 2760 | | | | 0 | 3797 | 1335 | 1757 | 3597 | 0 |
| Grip Volume(v), veh/h | 128 | 0 | 768 | | | | 0 | 1053 | 505 | 192 | 722 | 0 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 0 | 1380 | | | | 0 | 1679 | 1609 | 1757 | 1752 | 0 |
| Q Serve(g, s), s | 4.7 | 0.0 | 23.3 | | | | 0.0 | 23.0 | 23.0 | 9.3 | 9.0 | 0.0 |
| Cycle Q Clear(g, c), s | 4.7 | 0.0 | 23.3 | | | | 0.0 | 23.0 | 23.0 | 9.3 | 9.0 | 0.0 |
| Prop In Lane | 1.00 | | 1.00 | | | | 0.00 | | 0.83 | 1.00 | 0.00 | |
| Lane Grp Cap(c), veh/h | 540 | 0 | 848 | | | | 0 | 1422 | 682 | 231 | 2107 | 0 |
| V/C Ratio(X) | 0.24 | 0.00 | 0.91 | | | | 0.00 | 0.74 | 0.74 | 0.83 | 0.34 | 0.00 |
| Avail Cap(c,a), veh/h | 584 | 0 | 918 | | | | 0 | 1540 | 738 | 383 | 2532 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | | | | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 22.6 | 0.0 | 29.0 | | | | 0.0 | 21.1 | 21.1 | 36.9 | 8.7 | 0.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 11.9 | | | | 0.0 | 1.8 | 3.7 | 7.6 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 2.3 | 0.0 | 10.3 | | | | 0.0 | 10.9 | 10.8 | 5.0 | 4.3 | 0.0 |
| LnGrp Delay(d),s/veh | 22.8 | 0.0 | 40.9 | | | | 0.0 | 22.9 | 24.8 | 44.5 | 8.8 | 0.0 |
| LnGrp LOS | C | | D | | | | C | C | C | D | A | |
| Approach Vol, veh/h | | | 896 | | | | | 1558 | | | 914 | |
| Approach Delay, s/veh | | | 38.3 | | | | | 23.5 | | | 16.3 | |
| Approach LOS | | | D | | | | | C | | | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | | 6 | | | | | |
| Phs Duration (G+Y+Rc), s | 15.5 | 40.9 | | 30.8 | | | 56.4 | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | | 4.0 | | | | | |
| Max Green Setting (Gmax), s | 19.0 | 40.0 | | 29.0 | | | 63.0 | | | | | |
| Max Q Clear Time (g, c+H1), s | 11.3 | 25.0 | | 25.3 | | | 11.0 | | | | | |
| Green Ext Time (p, c), s | 0.3 | 12.0 | | 1.5 | | | 28.3 | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 25.5 | | | | | | | | | |
| HCM 2010 LOS | | | C | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
| Volume (veh/h) | 27 | 8 | 28 | 24 | 11 | 113 | 27 | 425 | 31 | 139 | 452 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 28 | 8 | 29 | 25 | 12 | 60 | 28 | 447 | 0 | 146 | 476 |
| Adj No. of Lanes | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 359 | 34 | 125 | 342 | 181 | 154 | 49 | 1378 | 0 | 197 | 1564 |
| Arrive On Green | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.03 | 0.39 | 0.00 | 0.11 | 0.48 |
| Sat Flow, veh/h | 1310 | 350 | 1270 | 1352 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 3274 |
| Grip Volume(v), veh/h | 28 | 0 | 37 | 25 | 12 | 60 | 28 | 447 | 0 | 146 | 254 |
| Grip Sat Flow(s), veh/h/ln | 1310 | 0 | 1621 | 1352 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 |
| Q Serve(g, s) | 0.6 | 0.0 | 0.6 | 0.5 | 0.2 | 1.1 | 0.5 | 2.7 | 0.0 | 2.4 | 2.7 |
| Cycle Q Clear(g, c), s | 0.8 | 0.0 | 0.6 | 1.2 | 0.2 | 1.1 | 0.5 | 2.7 | 0.0 | 2.4 | 2.7 |
| Prop In Lane | 1.00 | 0.78 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.15 |
| Lane Grp Cap(c), veh/h | 359 | 0 | 159 | 342 | 181 | 154 | 49 | 1378 | 0 | 197 | 837 |
| V/C Ratio(X) | 0.08 | 0.00 | 0.23 | 0.07 | 0.07 | 0.39 | 0.57 | 0.32 | 0.00 | 0.74 | 0.30 |
| Avail Cap(c,a), veh/h | 1289 | 0 | 1285 | 1281 | 1482 | 1243 | 580 | 4399 | 0 | 1509 | 3126 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 12.7 | 0.0 | 12.6 | 13.1 | 12.4 | 12.8 | 14.5 | 6.4 | 0.0 | 13.0 | 4.8 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 0.7 | 0.1 | 0.2 | 1.6 | 10.3 | 0.1 | 0.0 | 5.4 | 0.2 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.2 | 0.0 | 0.3 | 0.2 | 0.1 | 0.5 | 0.4 | 1.3 | 0.0 | 1.5 | 1.3 |
| LnGrp Delay(d), s/veh | 12.8 | 0.0 | 13.3 | 13.2 | 12.5 | 14.4 | 24.8 | 6.5 | 0.0 | 18.4 | 5.0 |
| LnGrp LOS | B | B | B | B | B | C | C | A | A | B | A |
| Approach Vol, veh/h | 65 | | | | 97 | | | 475 | | | 662 |
| Approach Delay, s/veh | 13.1 | | | | 13.9 | | | 7.6 | | | 8.0 |
| Approach LOS | B | | | | B | | | A | | | A |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|---|------|------|------|---|------|
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | 7.4 | 15.9 | | 7.0 | 4.8 | 18.5 | | 7.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | 26.0 | 38.0 | | 24.0 | 10.0 | 54.0 | | 24.0 |
| Max Q Clear Time (g, c+H1), s | 4.4 | 4.7 | | 2.8 | 2.5 | 4.7 | | 3.2 |
| Green Ext Time (p, c), s | 0.4 | 7.2 | | 0.6 | 0.0 | 7.6 | | 0.5 |

Intersection Summary

| | |
|---------------------|-----|
| HCM 2010 Ctrl Delay | 8.5 |
| HCM 2010 LOS | A |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|----------------------------|------|--------|------|------|--------|------|------|-------|------|------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
| Volume (veh/h) | 0 | 0 | 0 | 0 | 0 | 0 | 424 | 0 | 0 | 1054 | 2 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 0 | 0 | 0 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1149 | 0 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 2456 | 1289 | 0 | 0 |
| Arrive On Green | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.70 | 0.00 | 0.00 | 0.00 |
| Sat Flow, veh/h | 0 | -71942 | 0 | 0 | -71942 | 0 | 0 | 3514 | 1845 | 0 | 0 |
| Grip Volume(v), veh/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1149 | 0 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1752 | 0 | 0 | 1752 | 0 | 0 | 1757 | 1845 | 0 | 0 |
| Q Serve(g, s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 | 0.0 |
| Prop In Lane | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 |
| Lane Grp Cap(c), veh/h | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 2456 | 1289 | 0 | 0 |
| V/C Ratio(X) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.47 | 0.00 | 0.00 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 5905 | 0 | 0 | 5905 | 0 | 0 | 18516 | 9721 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 | 0.0 |
| LnGrp LOS | | | | | | | | A | | | |
| Approach Vol, veh/h | 0 | | | | 0 | | | 1149 | | | |
| Approach Delay, s/veh | 0.0 | | | | 0.0 | | | 1.0 | | | |
| Approach LOS | | | | | A | | | A | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|---|---|---|------|---|------|---|------|
| Assigned Phs | | | | 4 | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 0.0 | | 13.3 | | 0.0 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 22.0 | | 70.0 | | 22.0 |
| Max Q Clear Time (g, c+H1), s | | | | 0.0 | | 3.9 | | 0.0 |
| Green Ext Time (p, c), s | | | | 0.0 | | 5.5 | | 0.0 |

Intersection Summary

| | |
|---------------------|-----|
| HCM 2010 Ctrl Delay | 1.0 |
| HCM 2010 LOS | A |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

User approved volume balancing among the lanes for turning movement.

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|-----|-----|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 4 | 1050 | 0 | 0 | 419 | 465 | 5 | 0 | 497 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | | |
| Adj Flow Rate, veh/h | 4 | 1141 | 0 | 0 | 455 | 0 | 5 | 0 | 540 | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | | |
| Cap. veh/h | 8 | 1703 | 0 | 0 | 1466 | 656 | 681 | 0 | 608 | | |
| Arrive On Green | 0.00 | 0.49 | 0.00 | 0.00 | 0.42 | 0.00 | 0.39 | 0.00 | 0.39 | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | |
| Grip Volume(v), veh/h | 4 | 1141 | 0 | 0 | 455 | 0 | 5 | 0 | 540 | | |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | |
| Q Serve(g, s) | 0.1 | 15.7 | 0.0 | 0.0 | 5.5 | 0.0 | 0.1 | 0.0 | 20.3 | | |
| Cycle Q Clear(g, c), s | 0.1 | 15.7 | 0.0 | 0.0 | 5.5 | 0.0 | 0.1 | 0.0 | 20.3 | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | | |
| Lane Grp Cap(c), veh/h | 8 | 1703 | 0 | 0 | 1466 | 656 | 681 | 0 | 608 | | |
| V/C Ratio(X) | 0.53 | 0.67 | 0.00 | 0.00 | 0.31 | 0.00 | 0.01 | 0.00 | 0.89 | | |
| Avail Cap(c,a), veh/h | 111 | 2328 | 0 | 0 | 1885 | 843 | 1389 | 0 | 1240 | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | |
| Uniform Delay (d), s/veh | 31.4 | 12.4 | 0.0 | 0.0 | 12.3 | 0.0 | 11.9 | 0.0 | 18.1 | | |
| Incr Delay (d2), s/veh | 47.6 | 0.5 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 | 4.7 | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| %ile BackOfQ(50%), veh/ln | 0.2 | 7.6 | 0.0 | 0.0 | 2.7 | 0.0 | 0.1 | 0.0 | 9.5 | | |
| LnGrp Delay(d), s/veh | 79.0 | 12.8 | 0.0 | 0.0 | 12.4 | 0.0 | 11.9 | 0.0 | 22.8 | | |
| LnGrp LOS | E | B | | | B | | B | | C | | |
| Approach Vol, veh/h | 1145 | | | | | | | | | | |
| Approach Delay, s/veh | 13.1 | | | | | | | | | | |
| Approach LOS | B | | | | | | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 2 | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 28.5 | | | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | | | | | | | | | | |
| Max Green Setting (Gmax), s | 50.0 | | | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 22.3 | | | | | | | | | | |
| Green Ext Time (p, c), s | 2.2 | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 15.4 | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1443 | 504 | 120 | 1414 | 0 | 0 | 0 | 0 | 454 | 2 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 0 | | | | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1519 | 531 | 126 | 2828 | 0 | | | | 479 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | | | | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.50 | 0.95 | | | | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | | | | 3 | 3 |
| Cap. veh/h | 0 | 2443 | 761 | 197 | 2973 | 0 | | | | 1106 | 0 |
| Arrive On Green | 0.00 | 0.49 | 0.49 | 0.06 | 0.59 | 0.00 | | | | 0.31 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | | | | 3514 | 0 |
| Grip Volume(v), veh/h | 0 | 1519 | 531 | 126 | 2828 | 0 | | | | 479 | 0 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1679 | 1568 | 1704 | 1679 | 0 | | | | 1757 | 0 |
| Q Serve(g, s) | 0.0 | 18.7 | 22.2 | 3.0 | 44.2 | 0.0 | | | | 9.1 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 18.7 | 22.2 | 3.0 | 44.2 | 0.0 | | | | 9.1 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2443 | 761 | 197 | 2973 | 0 | | | | 1106 | 0 |
| V/C Ratio(X) | 0.00 | 0.62 | 0.70 | 0.64 | 0.95 | 0.00 | | | | 0.43 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 2443 | 761 | 323 | 3047 | 0 | | | | 1709 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 16.0 | 16.9 | 38.9 | 16.1 | 0.0 | | | | 22.9 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.5 | 2.8 | 3.4 | 7.7 | 0.0 | | | | 0.3 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 8.7 | 10.2 | 1.5 | 22.3 | 0.0 | | | | 4.4 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 16.5 | 19.7 | 42.3 | 23.9 | 0.0 | | | | 23.2 | 0.0 |
| LnGrp LOS | | B | B | D | C | | | | | C | C |
| Approach Vol, veh/h | 2050 | | | | | | | | | | |
| Approach Delay, s/veh | 17.3 | | | | | | | | | | |
| Approach LOS | B | | | | | | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 3 | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 8.9 | | | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | | | | | | | | | | |
| Max Green Setting (Gmax), s | 8.0 | | | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 5.0 | | | | | | | | | | |
| Green Ext Time (p, c), s | 0.1 | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 22.6 | | | | | | | | | | |
| HCM 2010 LOS | C | | | | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1616 | 301 | 20 | 5 | 1001 | 372 | 551 | 29 | 189 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/in | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1701 | 1701 | 5 | 1054 | 392 | 602 | 0 | 197 | 0 | 197 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 3014 | 938 | 9 | 3322 | 1034 | 803 | 0 | 358 | 0 | 358 |
| Arrive On Green | 0.00 | 0.60 | 0.60 | 0.01 | 0.66 | 0.66 | 0.23 | 0.00 | 0.23 | 0.00 | 0.23 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1701 | 170 | 5 | 1054 | 392 | 602 | 0 | 197 | 0 | 197 |
| Grip Sat Flow(s),veh/h/in | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 14.6 | 3.5 | 0.2 | 6.4 | 8.1 | 11.4 | 0.0 | 7.9 | 0.0 | 7.9 |
| Cycle Q Clear(g, c), s | 0.0 | 14.6 | 3.5 | 0.2 | 6.4 | 8.1 | 11.4 | 0.0 | 7.9 | 0.0 | 7.9 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 3014 | 938 | 9 | 3322 | 1034 | 803 | 0 | 358 | 0 | 358 |
| V/C Ratio(X) | 0.00 | 0.56 | 0.18 | 0.54 | 0.32 | 0.38 | 0.75 | 0.00 | 0.55 | 0.00 | 0.55 |
| Avail Cap(c,a), veh/h | 0 | 3380 | 1053 | 98 | 3944 | 1228 | 1769 | 0 | 789 | 0 | 789 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 8.7 | 6.5 | 35.5 | 5.2 | 5.5 | 25.7 | 0.0 | 24.3 | 0.0 | 24.3 |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.1 | 40.8 | 0.1 | 0.2 | 1.4 | 0.0 | 1.3 | 0.0 | 1.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/in | 0.0 | 6.7 | 1.5 | 0.2 | 2.9 | 3.6 | 5.7 | 0.0 | 3.5 | 0.0 | 3.5 |
| LnGrp Delay(d),s/veh | 0.0 | 8.9 | 6.6 | 76.2 | 5.3 | 5.8 | 27.1 | 0.0 | 25.7 | 0.0 | 25.7 |
| LnGrp LOS | A | A | A | E | A | A | C | C | C | C | C |
| Approach Vol, veh/h | 1871 | | | | | | | | | | |
| Approach Delay, s/veh | 8.7 | | | | | | | | | | |
| Approach LOS | A | | | | | | | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|-----|------|------|------|------|------|------|
| Assigned Phs | 2 | 3 | 4 | 4 | 4 | 4 | 4 | 8 |
| Phs Duration (G+Y+Rc), s | 20.3 | 4.4 | 46.8 | 46.8 | 46.8 | 46.8 | 46.8 | 51.2 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 36.0 | 4.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 56.0 |
| Max Q Clear Time (g, c+H1), s | 13.4 | 2.2 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 | 10.1 |
| Green Ext Time (p, c), s | 2.9 | 0.0 | 26.1 | 26.1 | 26.1 | 26.1 | 26.1 | 35.6 |

| Intersection Summary | | | | | | | | |
|----------------------|------|--|--|--|--|--|--|--|
| HCM 2010 Ctrl Delay | 11.1 | | | | | | | |
| HCM 2010 LOS | B | | | | | | | |

| Notes |
|--|
| User approved volume balancing among the lanes for turning movement. |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/24/2015

| Movement | SBR |
|---------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/in | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s),veh/h/in | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c,a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(I) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/in | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |

| Timer |
|--|
| User approved ignoring U-Turning movement. |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/24/2015

| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU |
|-------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | 5 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| Volume (veh/h) | 101 | 247 | 808 | 95 | 89 | 745 | 145 | 16 | 94 | 94 | 37 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 12 | 59 |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 260 | 851 | 58 | 94 | 784 | 100 | 99 | 99 | 22 | 22 | 22 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 2 | 1 | 1 | 1 | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 322 | 2138 | 666 | 122 | 1563 | 487 | 184 | 248 | 211 | 211 | 211 |
| Arrive On Green | 0.18 | 0.42 | 0.42 | 0.07 | 0.31 | 0.31 | 0.05 | 0.13 | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | 3408 | 1845 | 1568 | 1568 | 1568 |
| Grp Volume(V), veh/h | 260 | 851 | 58 | 94 | 784 | 100 | 99 | 99 | 22 | 22 | 22 |
| Grp Sat Flow(s),veh/h/ln | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | 1704 | 1845 | 1568 | 1568 | 1568 |
| Q Serve(g, s), s | 8.5 | 7.0 | 1.3 | 3.2 | 7.6 | 2.8 | 1.7 | 2.9 | 0.7 | 0.7 | 0.7 |
| Cycle Q Clear(g, c), s | 8.5 | 7.0 | 1.3 | 3.2 | 7.6 | 2.8 | 1.7 | 2.9 | 0.7 | 0.7 | 0.7 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 322 | 2138 | 666 | 122 | 1563 | 487 | 184 | 248 | 211 | 211 | 211 |
| V/C Ratio(X) | 0.81 | 0.40 | 0.09 | 0.77 | 0.50 | 0.21 | 0.54 | 0.40 | 0.10 | 0.10 | 0.10 |
| Avail Cap(c, a), veh/h | 790 | 3273 | 1019 | 351 | 2014 | 627 | 398 | 646 | 549 | 549 | 549 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 23.5 | 12.0 | 10.3 | 27.5 | 16.9 | 15.2 | 27.7 | 23.8 | 22.8 | 22.8 | 22.8 |
| Incr Delay (d2), s/veh | 4.8 | 0.1 | 0.1 | 9.9 | 0.3 | 0.2 | 2.5 | 1.0 | 0.2 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%) veh/ln | 4.5 | 3.3 | 0.6 | 1.9 | 3.5 | 1.2 | 0.9 | 1.6 | 0.3 | 0.3 | 0.3 |
| LnGrp Delay(d),s/veh | 28.3 | 12.1 | 10.4 | 37.4 | 17.1 | 15.4 | 30.1 | 24.8 | 23.0 | 23.0 | 23.0 |
| LnGrp LOS | C | B | B | D | B | B | C | C | C | C | C |
| Approach Vol, veh/h | 1169 | | | 978 | | | 220 | | | | |
| Approach Delay, s/veh | 156 | | | 18.9 | | | 27.0 | | | | |
| Approach LOS | B | | | B | | | C | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Phs Duration (G+Y+Rc), s | 10.3 | 12.1 | 8.2 | 29.5 | 7.2 | 15.1 | 15.0 | 22.6 | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Max Green Setting (Gmax), s | 12.0 | 21.0 | 12.0 | 39.0 | 7.0 | 26.0 | 27.0 | 24.0 | | | |
| Max Q Clear Time (g, c+H1), s | 6.0 | 4.9 | 5.2 | 9.0 | 3.7 | 8.5 | 10.5 | 9.6 | | | |
| Green EXT Time (p, c), s | 0.4 | 2.6 | 0.1 | 13.8 | 0.1 | 2.7 | 0.6 | 9.0 | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 19.6 | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | |
| Notes | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/24/2015

| Movement | SBL | SBT | SBR |
|---------------------------|------|------|------|
| Lane Configurations | 5 | 4 | 4 |
| Volume (veh/h) | 227 | 194 | 167 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 239 | 204 | 176 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 359 | 340 | 279 |
| Arrive On Green | 0.11 | 0.19 | 0.19 |
| Sat Flow, veh/h | 3408 | 1832 | 1500 |
| Grip Volume(v), veh/h | 239 | 195 | 185 |
| Grip Sat Flow(s),veh/h/ln | 1704 | 1752 | 1580 |
| Q Serve(g, s), s | 4.0 | 6.1 | 6.5 |
| Cycle Q Clear(g, c), s | 4.0 | 6.1 | 6.5 |
| Prop In Lane | 1.00 | 1.00 | 0.95 |
| Lane Grp Cap(c), veh/h | 359 | 326 | 294 |
| V/C Ratio(X) | 0.67 | 0.60 | 0.63 |
| Avail Cap(c,a), veh/h | 682 | 759 | 685 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 25.8 | 22.4 | 22.5 |
| Incr Delay (d2), s/veh | 2.1 | 1.8 | 2.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%) veh/ln | 2.0 | 3.1 | 3.0 |
| LnGrp Delay(d),s/veh | 28.0 | 24.1 | 24.8 |
| LnGrp LOS | C | C | C |
| Approach Vol, veh/h | 619 | | |
| Approach Delay, s/veh | 25.8 | | |
| Approach LOS | C | | |
| Timer | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Nearby Future Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 32 | 0 | 137 | 0 | 0 | 0 | 0 | 1806 | 503 | 294 | 569 | 0 |
| Number | 7 | 4 | 14 | 0 | 0 | 0 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 35 | 0 | 149 | 0 | 0 | 0 | 1963 | 547 | 320 | 618 | 0 | 0 |
| Adj No. of Lanes | 2 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 2 | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 |
| Cap, veh/h | 259 | 0 | 231 | 0 | 0 | 0 | 2636 | 702 | 406 | 2915 | 0 | 0 |
| Arrive On Green | 0.07 | 0.00 | 0.07 | 0.00 | 0.00 | 0.00 | 0.67 | 0.67 | 0.12 | 0.83 | 0.00 | 0.00 |
| Sat Flow, veh/h | 3514 | 0 | 3136 | 0 | 0 | 0 | 4127 | 1055 | 3408 | 3597 | 0 | 0 |
| Grip Volume(v), veh/h | 35 | 0 | 149 | 0 | 0 | 0 | 1650 | 860 | 320 | 618 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 0 | 1568 | 0 | 0 | 0 | 1679 | 1659 | 1704 | 1752 | 0 | 0 |
| Q Serve(g, s) | 0.8 | 0.0 | 3.9 | 0.0 | 0.0 | 0.0 | 27.4 | 30.5 | 7.7 | 3.0 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.8 | 0.0 | 3.9 | 0.0 | 0.0 | 0.0 | 27.4 | 30.5 | 7.7 | 3.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.64 | 1.00 | 0.64 | 1.00 | 0.00 | 0.00 |
| Lane Grp Cap(c), veh/h | 259 | 0 | 231 | 0 | 0 | 0 | 2234 | 1104 | 406 | 2915 | 0 | 0 |
| V/C Ratio(X) | 0.14 | 0.00 | 0.64 | 0.00 | 0.00 | 0.00 | 0.74 | 0.78 | 0.79 | 0.21 | 0.00 | 0.00 |
| Avail Cap(c,a), veh/h | 664 | 0 | 593 | 0 | 0 | 0 | 2339 | 1156 | 523 | 3146 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 36.7 | 0.0 | 38.1 | 0.0 | 0.0 | 0.0 | 9.3 | 9.8 | 36.3 | 1.5 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 3.0 | 0.0 | 0.0 | 0.0 | 1.2 | 3.3 | 6.1 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.4 | 0.0 | 1.8 | 0.0 | 0.0 | 0.0 | 12.8 | 14.6 | 4.0 | 1.5 | 0.0 | 0.0 |
| LnGrp Delay(d), s/veh | 36.9 | 0.0 | 41.1 | 0.0 | 0.0 | 0.0 | 10.5 | 13.2 | 42.3 | 1.5 | 0.0 | 0.0 |
| LnGrp LOS | D | D | D | D | D | D | B | B | D | A | A | A |
| Approach Vol, veh/h | 184 | | | 2510 | | | 938 | | | | | |
| Approach Delay, s/veh | 40.3 | | | 11.4 | | | 15.4 | | | | | |
| Approach LOS | D | | | B | | | B | | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|---|------|---|------|---|---|
| Assigned Phs | 1 | 2 | | 4 | | 6 | | |
| Phs Duration (G+Y+Rc), s | 14.1 | 60.3 | | 10.2 | | 74.4 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | 4.0 | | |
| Max Green Setting (Gmax), s | 13.0 | 59.0 | | 16.0 | | 76.0 | | |
| Max Q Clear Time (g, c+1), s | 9.7 | 32.5 | | 5.9 | | 5.0 | | |
| Green Ext Time (p, c), s | 0.4 | 23.8 | | 0.4 | | 54.9 | | |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 13.9 | | | | | | | |
| HCM 2010 LOS | B | | | | | | | |
| Notes | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|-------|------|------|------|------|------|-------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 121 | 90 | 85 | 350 | 80 | 252 | 98 | 1191 | 526 | 436 | 1094 | 145 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 132 | 98 | 92 | 380 | 87 | 138 | 107 | 1295 | 0 | 474 | 1189 | 158 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 354 | 248 | 232 | 299 | 521 | 443 | 134 | 1419 | 0 | 337 | 1619 | 214 |
| Arrive On Green | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.08 | 0.40 | 0.00 | 0.19 | 0.52 | 0.52 |
| Sat Flow, veh/h | 1140 | 877 | 823 | 1177 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 3112 | 412 |
| Grip Volume(v), veh/h | 132 | 0 | 190 | 380 | 87 | 138 | 107 | 1295 | 0 | 474 | 688 | 679 |
| Grip Sat Flow(s), veh/h/ln | 1140 | 0 | 1699 | 1177 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1772 |
| Q Serve(g, s) | 9.8 | 0.0 | 9.0 | 19.0 | 3.5 | 6.9 | 5.9 | 34.6 | 0.0 | 19.0 | 29.3 | 29.6 |
| Cycle Q Clear(g, c), s | 13.3 | 0.0 | 9.0 | 28.0 | 3.5 | 6.9 | 5.9 | 34.6 | 0.0 | 19.0 | 29.3 | 29.6 |
| Prop In Lane | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.23 |
| Lane Grp Cap(c), veh/h | 354 | 0 | 480 | 299 | 521 | 443 | 134 | 1419 | 0 | 337 | 912 | 922 |
| V/C Ratio(X) | 0.37 | 0.00 | 0.40 | 1.27 | 0.17 | 0.31 | 0.80 | 0.91 | 0.00 | 1.41 | 0.73 | 0.74 |
| Avail Cap(c,a), veh/h | 354 | 0 | 480 | 299 | 521 | 443 | 160 | 1450 | 0 | 337 | 912 | 922 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 31.8 | 0.0 | 28.7 | 42.4 | 26.8 | 28.0 | 45.0 | 27.8 | 0.0 | 40.1 | 18.4 | 18.5 |
| Incr Delay (d2), s/veh | 0.7 | 0.0 | 0.5 | 145.9 | 0.1 | 0.4 | 21.1 | 9.0 | 0.0 | 200.3 | 3.1 | 3.1 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 3.1 | 0.0 | 4.3 | 20.2 | 1.8 | 3.0 | 3.7 | 18.3 | 0.0 | 27.9 | 14.9 | 15.1 |
| LnGrp Delay(d), s/veh | 32.4 | 0.0 | 29.3 | 188.3 | 26.9 | 28.4 | 66.2 | 36.9 | 0.0 | 240.3 | 21.5 | 21.6 |
| LnGrp LOS | C | C | C | F | C | C | E | D | F | C | C | C |
| Approach Vol, veh/h | 322 | | | 605 | | | 1402 | | | 1821 | | |
| Approach Delay, s/veh | 30.6 | | | 128.6 | | | 39.1 | | | 78.5 | | |
| Approach LOS | C | | | F | | | D | | | E | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|---|---|
| Assigned Phs | 1 | 2 | 4 | 4 | 5 | 6 | | |
| Phs Duration (G+Y+Rc), s | 23.0 | 44.1 | 32.0 | 11.5 | 55.6 | 32.0 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 19.0 | 41.0 | 28.0 | 9.0 | 51.0 | 28.0 | | |
| Max Q Clear Time (g, c+H1), s | 21.0 | 36.6 | 15.3 | 7.9 | 31.6 | 30.0 | | |
| Green Ext Time (p, c), s | 0.0 | 3.5 | 3.6 | 0.0 | 16.6 | 0.0 | | |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 68.8 | | | | | | | |
| HCM 2010 LOS | E | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/27/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
|-------------------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | |
| Volume (veh/h) | 1036 | 117 | 309 | 766 | 154 | 367 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 1126 | 127 | 336 | 833 | 167 | 200 | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 1491 | 168 | 385 | 2591 | 279 | 249 | |
| Arrive On Green | 0.47 | 0.47 | 0.22 | 0.74 | 0.16 | 0.16 | |
| Sat Flow, veh/h | 3269 | 358 | 1757 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 620 | 633 | 336 | 833 | 167 | 200 | |
| Grip Sat Flow(s), veh/h/ln | 1752 | 1782 | 1757 | 1752 | 1757 | 1568 | |
| Q Serve(g, s), s | 22.9 | 23.0 | 14.5 | 6.4 | 6.9 | 9.7 | |
| Cycle Q Clear(g, c), s | 22.9 | 23.0 | 14.5 | 6.4 | 6.9 | 9.7 | |
| Prop In Lane | 0.20 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 823 | 836 | 385 | 2591 | 279 | 249 | |
| V/C Ratio(X) | 0.75 | 0.76 | 0.87 | 0.32 | 0.60 | 0.80 | |
| Avail Cap(c.a), veh/h | 914 | 929 | 581 | 3165 | 489 | 419 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 17.1 | 17.2 | 29.6 | 3.5 | 30.7 | 31.9 | |
| Incr Delay (d2), s/veh | 3.2 | 3.2 | 9.4 | 0.1 | 2.1 | 5.9 | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | 11.8 | 12.0 | 8.0 | 3.0 | 3.5 | 4.6 | |
| LnGrp Delay(d), s/veh | 20.4 | 20.4 | 39.0 | 3.6 | 32.8 | 37.8 | |
| LnGrp LOS | C | C | D | A | C | D | |
| Approach Vol, veh/h | 1253 | | 1169 | 367 | | | |
| Approach Delay, s/veh | 20.4 | | 13.8 | 35.5 | | | |
| Approach LOS | C | | B | D | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| Assigned Phs | | 2 | 3 | 4 | | | 8 |
| Phs Duration (G+Y+Rc), s | | 16.5 | 21.2 | 40.9 | | | 62.1 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Max Green Setting (Gmax), s | | 21.0 | 26.0 | 41.0 | | | 71.0 |
| Max Q Clear Time (g, c+H1), s | | 11.7 | 16.5 | 25.0 | | | 8.4 |
| Green Ext Time (p, c), s | | 0.8 | 0.7 | 11.9 | | | 27.0 |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | | | 19.6 | | | | |
| HCM 2010 LOS | | | B | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1310 | 90 | 0 | 557 | 100 | 0 | 0 | 0 | 830 | 0 | 331 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1424 | 98 | 0 | 605 | 0 | 0 | 605 | 0 | 902 | 0 | 360 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1906 | 131 | 0 | 2007 | 0 | 0 | 1140 | 0 | 1140 | 0 | 509 |
| Arrive On Green | 0.00 | 0.57 | 0.00 | 0.57 | 0.00 | 0.57 | 0.00 | 0.32 | 0.00 | 0.32 | 0.00 | 0.32 |
| Sat Flow, veh/h | 0 | 3421 | 228 | 0 | 3689 | 0 | 0 | 3514 | 0 | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 747 | 775 | 0 | 605 | 0 | 0 | 902 | 0 | 902 | 0 | 360 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1752 | 1804 | 0 | 1752 | 0 | 0 | 1757 | 0 | 1757 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 24.7 | 25.0 | 0.0 | 6.9 | 0.0 | 0.0 | 18.1 | 0.0 | 18.1 | 0.0 | 15.6 |
| Cycle Q Clear(g, c), s | 0.0 | 24.7 | 25.0 | 0.0 | 6.9 | 0.0 | 0.0 | 18.1 | 0.0 | 18.1 | 0.0 | 15.6 |
| Prop In Lane | 0.00 | 0.13 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 1003 | 1033 | 0 | 2007 | 0 | 0 | 1140 | 0 | 1140 | 0 | 509 |
| V/C Ratio(X) | 0.00 | 0.74 | 0.75 | 0.00 | 0.30 | 0.00 | 0.00 | 0.79 | 0.00 | 0.79 | 0.00 | 0.71 |
| Avail Cap(c.a), veh/h | 0 | 1174 | 1209 | 0 | 2348 | 0 | 0 | 1811 | 0 | 1811 | 0 | 808 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 12.4 | 12.4 | 0.0 | 8.6 | 0.0 | 0.0 | 23.8 | 0.0 | 23.8 | 0.0 | 23.0 |
| Incr Delay (d2), s/veh | 0.0 | 2.2 | 2.2 | 0.0 | 0.1 | 0.0 | 0.0 | 1.3 | 0.0 | 1.3 | 0.0 | 1.8 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 12.4 | 12.9 | 0.0 | 3.3 | 0.0 | 0.0 | 9.0 | 0.0 | 9.0 | 0.0 | 7.0 |
| LnGrp Delay(d), s/veh | 0.0 | 14.6 | 14.7 | 0.0 | 8.7 | 0.0 | 0.0 | 25.1 | 0.0 | 25.1 | 0.0 | 24.8 |
| LnGrp LOS | | B | B | | A | | | C | | C | | C |
| Approach Vol, veh/h | | 1522 | | | 605 | | | 1262 | | 1262 | | |
| Approach Delay, s/veh | | 14.6 | | | 8.7 | | | 25.0 | | 25.0 | | |
| Approach LOS | | B | | | A | | | C | | C | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | | | 48.4 | | 29.2 | | 48.4 | | | | |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 | | | | |
| Max Green Setting (Gmax), s | | | | 52.0 | | 40.0 | | 52.0 | | | | |
| Max Q Clear Time (g, c+H1), s | | | | 27.0 | | 20.1 | | 27.0 | | | | |
| Green Ext Time (p, c), s | | | | 17.5 | | 5.1 | | 24.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 17.4 | | | | | | | | | |
| HCM 2010 LOS | | | B | | | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------|------|------|------|------|------|------|------|------|------|-----|-----|-----|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 622 | 1454 | 0 | 0 | 721 | 310 | 27 | 0 | 109 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Ped-Bike Adj(A _{pbt}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Adj Sat Flow, veh/h | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | | | |
| Adj Flow Rate, veh/h | 676 | 1580 | 0 | 0 | 784 | 0 | 29 | 0 | 118 | | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | | | |
| Cap. veh/h | 735 | 2793 | 0 | 0 | 1143 | 511 | 174 | 0 | 155 | | | |
| Arrive On Green | 0.42 | 0.80 | 0.00 | 0.00 | 0.33 | 0.00 | 0.10 | 0.00 | 0.10 | | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | | |
| Grip Volume(v), veh/h | 676 | 1580 | 0 | 0 | 784 | 0 | 29 | 0 | 118 | | | |
| Grip Sat Flow(s), veh/h | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | | |
| Q Serve(g, s) | 27.9 | 12.8 | 0.0 | 0.0 | 14.9 | 0.0 | 1.2 | 0.0 | 5.6 | | | |
| Cycle Q Clear(g, c), s | 27.9 | 12.8 | 0.0 | 0.0 | 14.9 | 0.0 | 1.2 | 0.0 | 5.6 | | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 735 | 2793 | 0 | 0 | 1143 | 511 | 174 | 0 | 155 | | | |
| V/C Ratio(X) | 0.92 | 0.57 | 0.00 | 0.00 | 0.69 | 0.00 | 0.17 | 0.00 | 0.76 | | | |
| Avail Cap(c.a), veh/h | 1031 | 3429 | 0 | 0 | 1189 | 532 | 390 | 0 | 348 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 21.1 | 2.9 | 0.0 | 0.0 | 22.4 | 0.0 | 31.6 | 0.0 | 33.7 | | | |
| Incr Delay (d2), s/veh | 10.0 | 0.2 | 0.0 | 0.0 | 1.6 | 0.0 | 0.4 | 0.0 | 7.5 | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%), veh/h | 15.4 | 6.0 | 0.0 | 0.0 | 7.4 | 0.0 | 0.6 | 0.0 | 2.7 | | | |
| LnGrp Delay(d), s/veh | 31.1 | 3.1 | 0.0 | 0.0 | 24.0 | 0.0 | 32.1 | 0.0 | 41.1 | | | |
| LnGrp LOS | C | A | | | C | | C | | D | | | |
| Approach Vol, veh/h | 2256 | | | 784 | | | 147 | | | | | |
| Approach Delay, s/veh | 11.5 | | | 24.0 | | | 39.4 | | | | | |
| Approach LOS | B | | | C | | | D | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 2 | | | 4 | | | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 11.6 | | | 65.1 | | | 36.1 | 29.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 17.0 | | | 75.0 | | | 45.0 | 26.0 | | | | |
| Max Q Clear Time (g, c+H1), s | 7.6 | | | 14.8 | | | 29.9 | 16.9 | | | | |
| Green Ext Time (p, c), s | 0.3 | | | 36.0 | | | 2.2 | 8.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 15.8 | | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions All Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------|------|------|------|------|------|------|------|------|-----|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1336 | 469 | 242 | 1648 | 0 | 0 | 0 | 0 | 751 | 12 | 473 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbt}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 0 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1452 | 510 | 263 | 1791 | 0 | | | | 825 | 0 | 514 |
| Adj No. of Lanes | 0 | 2 | 2 | 2 | 3 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1560 | 1229 | 276 | 2854 | 0 | | | | 1238 | 0 | 552 |
| Arrive On Green | 0.00 | 0.45 | 0.45 | 0.08 | 0.57 | 0.00 | | | | 0.35 | 0.00 | 0.35 |
| Sat Flow, veh/h | 0 | 3597 | 2760 | 3408 | 5202 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1452 | 510 | 263 | 1791 | 0 | | | | 825 | 0 | 514 |
| Grip Sat Flow(s), veh/h | 0 | 1752 | 1380 | 1704 | 1679 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 38.7 | 12.4 | 7.6 | 23.6 | 0.0 | | | | 19.6 | 0.0 | 31.2 |
| Cycle Q Clear(g, c), s | 0.0 | 38.7 | 12.4 | 7.6 | 23.6 | 0.0 | | | | 19.6 | 0.0 | 31.2 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 1560 | 1229 | 276 | 2854 | 0 | | | | 1238 | 0 | 552 |
| V/C Ratio(X) | 0.00 | 0.93 | 0.42 | 0.95 | 0.63 | 0.00 | | | | 0.67 | 0.00 | 0.93 |
| Avail Cap(c.a), veh/h | 0 | 1562 | 1230 | 276 | 2856 | 0 | | | | 1281 | 0 | 572 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 25.9 | 18.6 | 45.2 | 14.4 | 0.0 | | | | 27.1 | 0.0 | 30.8 |
| Incr Delay (d2), s/veh | 0.0 | 10.3 | 0.2 | 41.3 | 0.4 | 0.0 | | | | 1.3 | 0.0 | 21.7 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 20.8 | 4.7 | 5.1 | 10.9 | 0.0 | | | | 9.7 | 0.0 | 16.8 |
| LnGrp Delay(d), s/veh | 0.0 | 36.3 | 18.9 | 86.4 | 14.8 | 0.0 | | | | 28.3 | 0.0 | 52.5 |
| LnGrp LOS | D | D | B | F | B | C | | | | C | | D |
| Approach Vol, veh/h | 1962 | | | 2054 | | | 1339 | | | | | |
| Approach Delay, s/veh | 31.7 | | | 24.0 | | | 37.6 | | | | | |
| Approach LOS | C | | | C | | | D | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | | 3 | 4 | | | 6 | | | | | |
| Phs Duration (G+Y+Rc), s | | | 12.0 | 48.0 | | | 38.8 | 60.0 | | | | |
| Change Period (Y+Rc), s | | | 4.0 | 4.0 | | | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | | | 8.0 | 44.0 | | | 36.0 | 56.0 | | | | |
| Max Q Clear Time (g, c+H1), s | | | 9.6 | 40.7 | | | 33.2 | 25.6 | | | | |
| Green Ext Time (p, c), s | | | 0.0 | 3.2 | | | 1.6 | 28.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 30.2 | | | | | | | | | | | |
| HCM 2010 LOS | C | | | | | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions All Access 1

Synchro 8 Report

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ←←← | ←←← | ← | ←←← | ←←← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 0 | 1472 | 607 | 8 | 42 | 1531 | 352 | 355 | 27 | 322 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1600 | 443 | 46 | 1664 | 383 | 407 | 0 | 323 | 0 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2958 | 921 | 59 | 3382 | 1053 | 797 | 0 | 356 | 0 | 0 |
| Arrive On Green | 0.00 | 0.59 | 0.59 | 0.03 | 0.67 | 0.67 | 0.23 | 0.00 | 0.23 | 0.00 | 0.23 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1600 | 443 | 46 | 1664 | 383 | 407 | 0 | 323 | 0 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 15.1 | 12.8 | 2.0 | 12.8 | 8.4 | 8.0 | 0.0 | 15.8 | 0.0 | 15.8 |
| Cycle Q Clear(g, c), s | 0.0 | 15.1 | 12.8 | 2.0 | 12.8 | 8.4 | 8.0 | 0.0 | 15.8 | 0.0 | 15.8 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2958 | 921 | 59 | 3382 | 1053 | 797 | 0 | 356 | 0 | 356 |
| V/C Ratio(X) | 0.00 | 0.54 | 0.48 | 0.79 | 0.49 | 0.36 | 0.51 | 0.00 | 0.91 | 0.00 | 0.91 |
| Avail Cap(c,a), veh/h | 0 | 2958 | 921 | 825 | 4731 | 1473 | 803 | 0 | 358 | 0 | 358 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 9.8 | 9.3 | 37.8 | 6.3 | 5.6 | 26.6 | 0.0 | 29.6 | 0.0 | 29.6 |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.4 | 20.1 | 0.1 | 0.2 | 0.5 | 0.0 | 25.9 | 0.0 | 25.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 7.0 | 5.6 | 1.3 | 5.9 | 3.6 | 3.9 | 0.0 | 9.4 | 0.0 | 9.4 |
| LnGrp Delay(d),s/veh | 0.0 | 10.0 | 9.7 | 57.9 | 6.5 | 5.8 | 27.2 | 0.0 | 55.6 | 0.0 | 55.6 |
| LnGrp LOS | | B | A | E | A | A | C | | E | | E |
| Approach Vol, veh/h | 2043 | | | 2093 | | | 730 | | | | |
| Approach Delay, s/veh | 10.0 | | | 7.5 | | | 39.7 | | | | |
| Approach LOS | A | | | A | | | D | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|---|------|------|------|---|---|---|------|
| Assigned Phs | | 2 | 3 | 4 | | | | 8 |
| Phs Duration (G+Y+Rc), s | | 21.9 | 6.6 | 50.3 | | | | 56.9 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | | 4.0 |
| Max Green Setting (Gmax), s | | 18.0 | 37.0 | 33.0 | | | | 74.0 |
| Max Q Clear Time (g, c+H1), s | | 17.8 | 40.0 | 17.1 | | | | 14.8 |
| Green Ext Time (p, c), s | | 0.1 | 0.1 | 15.2 | | | | 38.1 |

| | |
|----------------------|------|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 13.4 |
| HCM 2010 LOS | B |



























Notes
 User approved volume balancing among the lanes for turning movement.

| Movement | SBR |
|---------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s),veh/h/ln | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c,a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(I) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |

| | |
|--|--|
| Timer | |
| User approved ignoring U-Turning movement. | |

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/27/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | |
|---------------------------|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|--|
| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU | | | | | | | | | | | |
| Lane Configurations | |  |  |  |  |  | | | | | | | | | | | | | | | | |
| Volume (veh/h) | 43 | 120 | 1074 | 77 | 207 | 1504 | 144 | 15 | 164 | 92 | 128 | | | | | | | | | | 25 | |
| Number | | 7 | 4 | 14 | 3 | 8 | 18 | | 5 | 2 | 12 | | | | | | | | | | | |
| Initial Q (Ob), veh | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | | | | | | | | | | 0 | |
| Ped-Bike Adj(A_pbT) | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | | | | | | | | | 1.00 | |
| Parking Bus, Adj | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | | | | | | | | | 1.00 | |
| Adj Sat Flow, veh/h/ln | | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | | 1845 | 1845 | 1845 | | | | | | | | | | 1845 | |
| Adj Flow Rate, veh/h | | 130 | 1167 | 48 | 225 | 1635 | 117 | | 178 | 100 | 114 | | | | | | | | | | 114 | |
| Adj No. of Lanes | | 1 | 3 | 1 | 1 | 3 | 1 | | 2 | 1 | 1 | | | | | | | | | | 1 | |
| Peak Hour Factor | | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | 0.92 | 0.92 | 0.92 | | | | | | | | | | 0.92 | |
| Percent Heavy Veh. % | | 3 | 3 | 3 | 3 | 3 | 3 | | 3 | 3 | 3 | | | | | | | | | | 3 | |
| Cap. veh/h | | 172 | 2006 | 625 | 279 | 2314 | 720 | | 288 | 293 | 249 | | | | | | | | | | 249 | |
| Arrive On Green | | 0.10 | 0.40 | 0.40 | 0.16 | 0.46 | 0.46 | | 0.08 | 0.16 | 0.16 | | | | | | | | | | 0.16 | |
| Sat Flow, veh/h | | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | | 3408 | 1845 | 1568 | | | | | | | | | | 1568 | |
| Grp Volume(v), veh/h | | 130 | 1167 | 48 | 225 | 1635 | 117 | | 178 | 100 | 114 | | | | | | | | | | 114 | |
| Grp Sat Flow(s),veh/h/ln | | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | | 1704 | 1845 | 1568 | | | | | | | | | | 1568 | |
| Q Serve(g, s) | | 4.6 | 11.5 | 1.2 | 7.8 | 16.5 | 2.8 | | 3.2 | 3.1 | 4.2 | | | | | | | | | | 4.2 | |
| Cycle Q Clear(g, c) | | 4.6 | 11.5 | 1.2 | 7.8 | 16.5 | 2.8 | | 3.2 | 3.1 | 4.2 | | | | | | | | | | 4.2 | |
| Prop In Lane | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | | | | | | | | | 1.00 | |
| Lane Grp Cap(c), veh/h | | 172 | 2006 | 625 | 279 | 2314 | 720 | | 288 | 293 | 249 | | | | | | | | | | 249 | |
| V/C Ratio(X) | | 0.76 | 0.58 | 0.08 | 0.81 | 0.71 | 0.16 | | 0.66 | 0.34 | 0.46 | | | | | | | | | | 0.46 | |
| Avail Cap(c, a), veh/h | | 1106 | 3251 | 1012 | 581 | 2314 | 720 | | 268 | 523 | 444 | | | | | | | | | | 444 | |
| HCM Platoon Ratio | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | | | | | | | | | 1.00 | |
| Upstream Filter(I) | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | | | | | | | | | | 1.00 | |
| Uniform Delay (d), s/veh | | 27.9 | 15.0 | 11.9 | 25.8 | 13.7 | 10.0 | | 28.4 | 23.8 | 24.2 | | | | | | | | | | 24.2 | |
| Incr Delay (d2), s/veh | | 6.6 | 0.3 | 0.1 | 5.4 | 1.0 | 0.1 | | 6.0 | 0.7 | 1.3 | | | | | | | | | | 1.3 | |
| Initial Q Delay(d3),s/veh | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | | | | | | | | | 0.0 | |
| %ile BackOfQ(50%),veh/ln | | 2.5 | 5.3 | 0.5 | 4.2 | 7.8 | 1.2 | | 1.7 | 1.6 | 1.9 | | | | | | | | | | 1.9 | |
| LnGrp Delay(d),s/veh | | 34.5 | 15.2 | 11.9 | 31.2 | 14.7 | 10.1 | | 34.5 | 24.4 | 25.5 | | | | | | | | | | 25.5 | |
| LnGrp LOS | | C | B | B | C | B | B | | C | C | C | | | | | | | | | | C | |
| Approach Vol, veh/h | 1345 | | | 1977 | | | 392 | | | | | | | | | | | | | | | |
| Approach Delay, s/veh | 17.0 | | | 16.3 | | | 29.3 | | | | | | | | | | | | | | | |
| Approach LOS | B | | | B | | | C | | | | | | | | | | | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/27/2015

| Movement | SBL | SBT | SBR |
|---------------------------|------|------|------|
| Lane Configurations | 37 | 81 | 87 |
| Volume (veh/h) | 1 | 6 | 16 |
| Number | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 40 | 88 | 95 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 109 | 196 | 176 |
| Arrive On Green | 0.03 | 0.11 | 0.11 |
| Sat Flow, veh/h | 3408 | 1752 | 1568 |
| Grip Volume(v), veh/h | 40 | 88 | 95 |
| Grip Sat Flow(s),veh/h/ln | 1704 | 1752 | 1568 |
| Q Serve(g, s), s | 0.7 | 3.0 | 3.6 |
| Cycle Q Clear(g, c), s | 0.7 | 3.0 | 3.6 |
| Prop In Lane | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 109 | 196 | 176 |
| V/C Ratio(X) | 0.37 | 0.45 | 0.54 |
| Avail Cap(c,a), veh/h | 215 | 469 | 420 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 30.1 | 26.4 | 26.7 |
| Incr Delay (d2), s/veh | 2.1 | 1.6 | 2.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.4 | 1.5 | 1.7 |
| LnGrp Delay(d),s/veh | 32.2 | 28.0 | 29.2 |
| LnGrp LOS | C | C | C |
| Approach Vol, veh/h | 223 | | |
| Approach Delay, s/veh | 29.3 | | |
| Approach LOS | C | | |
| Timer | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Country Hills Road & Laurel Road

10/27/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
|---------------------------------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | |
| Volume (veh/h) | 905 | 420 | 127 | 843 | 160 | 330 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A _{pbT}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 984 | 457 | 138 | 916 | 174 | 359 | |
| Adj No. of Lanes | 2 | 0 | 2 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 1269 | 579 | 209 | 2279 | 452 | 403 | |
| Arrive On Green | 0.54 | 0.54 | 0.06 | 0.65 | 0.26 | 0.26 | |
| Sat Flow, veh/h | 2433 | 1068 | 3408 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 732 | 709 | 138 | 916 | 174 | 359 | |
| Grip Sat Flow(s), veh/h | 1752 | 1656 | 1704 | 1752 | 1757 | 1568 | |
| Q Serve(g, s) | 28.3 | 29.5 | 3.4 | 10.7 | 7.0 | 19.0 | |
| Cycle Q Clear(g, c), s | 28.3 | 29.5 | 3.4 | 10.7 | 7.0 | 19.0 | |
| Prop In Lane | 0.64 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grip Cap(c), veh/h | 950 | 898 | 209 | 2279 | 452 | 403 | |
| V/C Ratio(X) | 0.77 | 0.79 | 0.66 | 0.40 | 0.39 | 0.89 | |
| Avail Cap(c.a), veh/h | 1057 | 999 | 316 | 2602 | 571 | 509 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 15.5 | 15.8 | 39.6 | 7.1 | 26.4 | 30.9 | |
| Incr Delay (d2), s/veh | 3.2 | 3.9 | 3.5 | 0.1 | 0.5 | 15.0 | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/h | 14.5 | 14.4 | 1.7 | 5.1 | 3.5 | 9.9 | |
| LnGrp Delay(d), s/veh | 18.7 | 19.7 | 43.1 | 7.3 | 26.9 | 45.9 | |
| LnGrp LOS | B | B | D | A | C | D | |
| Approach Vol, veh/h | 1441 | | 1054 | | 533 | | |
| Approach Delay, s/veh | 19.2 | | 11.9 | | 39.7 | | |
| Approach LOS | B | | B | | D | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 8 |
| Assigned Phs | 2 | 3 | 4 | | | | 8 |
| Phs Duration (G+Y+Rc), s | 26.2 | 9.3 | 50.8 | | | | 60.1 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | 4.0 |
| Max Green Setting (Gmax), s | 28.0 | 8.0 | 52.0 | | | | 64.0 |
| Max Q Clear Time (g, c+H1), s | 21.0 | 5.4 | 31.5 | | | | 12.7 |
| Green Ext Time (p, c), s | 1.1 | 0.1 | 15.2 | | | | 27.7 |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | | | 20.3 | | | | |
| HCM 2010 LOS | | | C | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Syncho 8 Report

HCM 2010 Signalized Intersection Summary
11: Slatten Ranch Road & Laurel Road

10/27/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 183 | 1066 | 632 | 263 | 783 | 355 | 417 | 120 | 123 | 180 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbT}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 199 | 1159 | 344 | 286 | 851 | 386 | 453 | 226 | 130 | 134 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 0 | 2 | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 237 | 1716 | 534 | 327 | 1330 | 601 | 543 | 408 | 226 | 169 |
| Arrive On Green | 0.14 | 0.34 | 0.34 | 0.19 | 0.39 | 0.39 | 0.16 | 0.19 | 0.19 | 0.12 |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 3396 | 1535 | 3408 | 2178 | 1206 | 1757 |
| Grip Volume(v), veh/h | 199 | 1159 | 344 | 286 | 841 | 396 | 453 | 180 | 176 | 134 |
| Grip Sat Flow(s), veh/h | 1757 | 1679 | 1568 | 1757 | 1679 | 1574 | 1704 | 1752 | 1632 | 1757 |
| Q Serve(g, s) | 9.3 | 16.6 | 15.6 | 13.3 | 17.2 | 17.2 | 10.9 | 7.9 | 8.3 | 6.3 |
| Cycle Q Clear(g, c), s | 9.3 | 16.6 | 15.6 | 13.3 | 17.2 | 17.2 | 10.9 | 7.9 | 8.3 | 6.3 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 0.74 | 1.00 | 0.42 |
| Lane Grip Cap(c), veh/h | 237 | 1716 | 534 | 327 | 1315 | 617 | 543 | 328 | 306 | 169 |
| V/C Ratio(X) | 0.84 | 0.68 | 0.64 | 0.87 | 0.64 | 0.64 | 0.83 | 0.55 | 0.57 | 0.79 |
| Avail Cap(c.a), veh/h | 312 | 1791 | 558 | 417 | 1393 | 653 | 395 | 368 | 312 | 374 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 35.6 | 23.8 | 23.5 | 33.4 | 20.8 | 20.8 | 34.4 | 31.0 | 31.2 | 37.3 |
| Incr Delay (d2), s/veh | 14.2 | 1.0 | 2.4 | 15.3 | 0.9 | 2.0 | 8.0 | 1.4 | 1.7 | 8.2 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 5.5 | 7.9 | 7.1 | 7.8 | 8.1 | 7.8 | 5.7 | 3.9 | 3.9 | 3.4 |
| LnGrp Delay(d), s/veh | 49.8 | 24.8 | 25.9 | 48.7 | 21.7 | 22.8 | 42.4 | 32.5 | 32.9 | 45.5 |
| LnGrp LOS | D | C | C | D | C | C | D | C | D | D |
| Approach Vol, veh/h | 1702 | | 1523 | | 809 | | | | | 383 |
| Approach Delay, s/veh | 27.9 | | 27.1 | | 38.1 | | | | | 40.2 |
| Approach LOS | C | | C | | D | | | | | D |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | |
| Phs Duration (G+Y+Rc), s | 12.1 | 19.8 | 19.7 | 32.7 | 17.4 | 14.5 | 15.4 | 37.0 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 15.0 | 19.0 | 20.0 | 30.0 | 16.0 | 18.0 | 15.0 | 35.0 | | |
| Max Q Clear Time (g, c+H1), s | 8.3 | 10.3 | 15.3 | 18.6 | 12.9 | 7.8 | 11.3 | 19.2 | | |
| Green Ext Time (p, c), s | 0.2 | 2.4 | 0.4 | 10.1 | 0.6 | 2.6 | 0.2 | 13.6 | | |
| Intersection Summary | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 30.6 | | | | | | | |
| HCM 2010 LOS | | | C | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Conditions Alt Access 1

Syncho 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|-------|------|------|-------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 312 | 0 | 1197 | 0 | 0 | 0 | 0 | 553 | 571 | 328 | 967 | 0 |
| Number | 7 | 4 | 14 | 0 | 0 | 0 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 328 | 0 | 1260 | 0 | 0 | 0 | 582 | 601 | 345 | 1018 | 0 | 0 |
| Adj No. of Lanes | 2 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 2 | 2 | 0 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | 1601 | 0 | 1429 | 0 | 0 | 0 | 966 | 451 | 422 | 1597 | 0 | 0 |
| Arrive On Green | 0.46 | 0.00 | 0.46 | 0.00 | 0.29 | 0.29 | 0.12 | 0.46 | 0.00 | 0.00 | 0.00 | 0.00 |
| Sat Flow, veh/h | 3514 | 0 | 3136 | 0 | 0 | 0 | 3523 | 1568 | 3408 | 3597 | 0 | 0 |
| Grip Volume(v), veh/h | 328 | 0 | 1260 | 0 | 0 | 0 | 582 | 601 | 345 | 1018 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 0 | 1568 | 0 | 0 | 0 | 1679 | 1568 | 1704 | 1752 | 0 | 0 |
| Q Serve(g, s) | 5.1 | 0.0 | 33.0 | 0.0 | 13.5 | 26.0 | 8.9 | 20.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 5.1 | 0.0 | 33.0 | 0.0 | 13.5 | 26.0 | 8.9 | 20.1 | 0.0 | 0.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Lane Grip Cap(c), veh/h | 1601 | 0 | 1429 | 0 | 0 | 0 | 966 | 451 | 422 | 1597 | 0 | 0 |
| V/C Ratio(X) | 0.20 | 0.00 | 0.88 | 0.00 | 0.60 | 1.33 | 0.82 | 0.64 | 0.00 | 0.00 | 0.00 | 0.00 |
| Avail Cap(c,a), veh/h | 1905 | 0 | 1700 | 0 | 0 | 0 | 966 | 451 | 490 | 1688 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 14.8 | 0.0 | 22.4 | 0.0 | 27.7 | 32.2 | 38.6 | 18.9 | 0.0 | 0.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 5.1 | 0.0 | 1.1 | 164.1 | 9.2 | 0.8 | 0.0 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 2.5 | 0.0 | 15.2 | 0.0 | 6.4 | 31.7 | 4.8 | 9.8 | 0.0 | 0.0 | 0.0 | 0.0 |
| LnGrp Delay(d), s/veh | 14.8 | 0.0 | 27.5 | 0.0 | 28.8 | 196.3 | 47.8 | 19.6 | 0.0 | 0.0 | 0.0 | 0.0 |
| LnGrp LOS | B | C | C | C | F | D | B | D | B | C | C | C |
| Approach Vol, veh/h | 1588 | 0 | 1183 | 0 | 0 | 0 | 1363 | 0 | 0 | 0 | 0 | 0 |
| Approach Delay, s/veh | 24.9 | 0 | 113.9 | 0 | 0 | 0 | 26.8 | 0 | 0 | 0 | 0 | 0 |
| Approach LOS | C | C | F | C | F | D | C | C | C | C | C | C |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|------|------|
| Assigned Phs | 1 | 2 | 4 | 4 | 6 | 6 | 6 | 6 |
| Phs Duration (G+Y+Rc), s | 15.2 | 30.0 | 45.2 | 45.2 | 45.2 | 45.2 | 45.2 | 45.2 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 13.0 | 26.0 | 49.0 | 49.0 | 43.0 | 43.0 | 43.0 | 43.0 |
| Max Q Clear Time (g, c+H1), s | 10.9 | 28.0 | 35.0 | 35.0 | 22.1 | 22.1 | 22.1 | 22.1 |
| Green Ext Time (p, c), s | 0.3 | 0.0 | 6.1 | 6.1 | 15.3 | 15.3 | 15.3 | 15.3 |

| Intersection Summary | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| HCM 2010 Ctrl Delay | 51.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| HCM 2010 LOS | D | C | C | C | F | D | B | D | B | C | C | C |

User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|-------|-------|------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 208 | 115 | 157 | 487 | 307 | 285 | 120 | 140.5 | 400 | 327 | 1111 | 288 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 219 | 121 | 165 | 513 | 323 | 153 | 126 | 1479 | 0 | 344 | 1169 | 303 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 297 | 269 | 367 | 344 | 701 | 596 | 123 | 1332 | 0 | 211 | 1188 | 305 |
| Arrive On Green | 0.38 | 0.38 | 0.38 | 0.38 | 0.38 | 0.38 | 0.07 | 0.38 | 0.00 | 0.12 | 0.43 | 0.43 |
| Sat Flow, veh/h | 906 | 708 | 966 | 1078 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 2764 | 708 |
| Grip Volume(v), veh/h | 219 | 0 | 286 | 513 | 323 | 153 | 126 | 1479 | 0 | 344 | 736 | 305 |
| Grip Sat Flow(s), veh/h/ln | 906 | 0 | 1674 | 1078 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1720 |
| Q Serve(g, s) | 24.0 | 0.0 | 12.8 | 25.2 | 13.2 | 6.7 | 7.0 | 38.0 | 0.0 | 12.0 | 41.3 | 42.6 |
| Cycle Q Clear(g, c), s | 37.1 | 0.0 | 12.8 | 38.0 | 13.2 | 6.7 | 7.0 | 38.0 | 0.0 | 12.0 | 41.3 | 42.6 |
| Prop In Lane | 1.00 | 1.00 | 0.58 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.41 |
| Lane Grip Cap(c), veh/h | 297 | 0 | 636 | 344 | 701 | 596 | 123 | 1332 | 0 | 211 | 754 | 739 |
| V/C Ratio(X) | 0.74 | 0.00 | 0.45 | 1.49 | 0.46 | 0.26 | 1.02 | 1.11 | 0.00 | 1.63 | 0.98 | 0.99 |
| Avail Cap(c,a), veh/h | 297 | 0 | 636 | 344 | 701 | 596 | 123 | 1332 | 0 | 211 | 754 | 739 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 37.3 | 0.0 | 23.2 | 40.0 | 23.3 | 21.3 | 46.5 | 31.0 | 0.0 | 44.0 | 28.0 | 28.4 |
| Incr Delay (d2), s/veh | 9.3 | 0.0 | 0.5 | 236.0 | 0.5 | 0.2 | 87.9 | 60.8 | 0.0 | 304.8 | 27.1 | 31.7 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 6.7 | 0.0 | 6.0 | 32.0 | 6.7 | 2.9 | 6.4 | 29.6 | 0.0 | 23.6 | 25.5 | 26.5 |
| LnGrp Delay(d), s/veh | 46.5 | 0.0 | 23.7 | 276.0 | 23.8 | 21.5 | 134.7 | 91.8 | 0.0 | 348.8 | 55.1 | 60.1 |
| LnGrp LOS | D | C | C | F | C | C | F | F | F | F | E | E |
| Approach Vol, veh/h | 505 | 0 | 989 | 0 | 0 | 0 | 1605 | 0 | 0 | 0 | 1816 | 0 |
| Approach Delay, s/veh | 33.6 | 0 | 154.3 | 0 | 0 | 0 | 95.2 | 0 | 0 | 0 | 112.8 | 0 |
| Approach LOS | C | C | F | C | F | F | F | F | F | F | F | F |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|------|------|
| Assigned Phs | 1 | 2 | 4 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 16.0 | 42.0 | 42.0 | 42.0 | 11.0 | 47.0 | 42.0 | 42.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 12.0 | 38.0 | 38.0 | 38.0 | 7.0 | 43.0 | 38.0 | 38.0 |
| Max Q Clear Time (g, c+H1), s | 14.0 | 40.0 | 39.1 | 39.1 | 9.0 | 44.6 | 40.0 | 40.0 |
| Green Ext Time (p, c), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Intersection Summary | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| HCM 2010 Ctrl Delay | 107.3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| HCM 2010 LOS | F | C | C | F | C | C | F | F | F | F | F | F |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/27/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
|------------------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | |
| Volume (veh/h) | 663 | 216 | 687 | 946 | 66 | 395 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 742 | 235 | 747 | 1028 | 72 | 215 | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap, veh/h | 746 | 236 | 768 | 2672 | 274 | 245 | |
| Arrive On Green | 0.28 | 0.28 | 0.44 | 0.76 | 0.16 | 0.16 | |
| Sat Flow, veh/h | 2713 | 830 | 1757 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 496 | 481 | 747 | 1028 | 72 | 215 | |
| Grip Sat Flow(s),veh/h/ln | 1752 | 1698 | 1757 | 1752 | 1757 | 1568 | |
| Q Serve(g, s) | 27.8 | 27.8 | 41.0 | 9.7 | 3.5 | 13.2 | |
| Cycle Q Clear(g, c), s | 27.8 | 27.8 | 41.0 | 9.7 | 3.5 | 13.2 | |
| Prop In Lane | 0.49 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 499 | 484 | 768 | 2672 | 274 | 245 | |
| V/C Ratio(X) | 0.99 | 0.99 | 0.97 | 0.38 | 0.26 | 0.88 | |
| Avail Cap(c,a), veh/h | 499 | 484 | 768 | 2673 | 304 | 271 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 35.1 | 35.1 | 27.1 | 3.9 | 36.5 | 40.6 | |
| Incr Delay (d2), s/veh | 38.7 | 39.4 | 25.8 | 0.1 | 0.5 | 24.6 | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | 18.7 | 18.2 | 25.2 | 4.6 | 1.8 | 7.4 | |
| LnGrp Delay(d),s/veh | 73.8 | 74.4 | 53.0 | 4.0 | 37.0 | 65.2 | |
| LnGrp LOS | E | E | D | A | D | E | |
| Approach Vol, veh/h | 977 | | | 1775 | 287 | | |
| Approach Delay, s/veh | 74.1 | | | 24.6 | 58.1 | | |
| Approach LOS | E | | | C | E | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 8 |
| Assigned Phs | | 2 | 3 | 4 | | | 8 |
| Phs Duration (G+Y+Rc), s | | 19.4 | 47.0 | 32.0 | | | 79.0 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Max Green Setting (Gmax), s | | 17.0 | 43.0 | 28.0 | | | 75.0 |
| Max Q Clear Time (g_c+H1), s | | 15.2 | 43.0 | 29.8 | | | 11.7 |
| Green Ext Time (p_c), s | | 0.2 | 0.0 | 0.0 | | | 25.2 |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | | | 43.7 | | | | |
| HCM 2010 LOS | | | D | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|--|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1277 | 40 | 0 | 1127 | 20 | 0 | 0 | 0 | 712 | 0 | 566 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 0 | 0 | 0 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1388 | 43 | 0 | 1225 | 0 | 0 | 0 | 0 | 774 | 0 | 615 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | 0 | 0 | 0 | 3 | 3 | 3 |
| Cap, veh/h | 0 | 1657 | 51 | 0 | 1674 | 0 | 0 | 0 | 0 | 1530 | 0 | 683 |
| Arrive On Green | 0.00 | 0.48 | 0.48 | 0.00 | 0.48 | 0.00 | 0.48 | 0.00 | 0.48 | 0.44 | 0.00 | 0.44 |
| Sat Flow, veh/h | 0 | 3563 | 107 | 0 | 3689 | 0 | 0 | 0 | 0 | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 700 | 731 | 0 | 1225 | 0 | 0 | 0 | 0 | 774 | 0 | 615 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1826 | 0 | 1752 | 0 | 0 | 0 | 0 | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 32.0 | 32.1 | 0.0 | 25.8 | 0.0 | 0.0 | 0.0 | 0.0 | 14.7 | 0.0 | 33.5 |
| Cycle Q Clear(g, c), s | 0.0 | 32.0 | 32.1 | 0.0 | 25.8 | 0.0 | 0.0 | 0.0 | 0.0 | 14.7 | 0.0 | 33.5 |
| Prop In Lane | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 837 | 872 | 0 | 1674 | 0 | 0 | 0 | 0 | 1530 | 0 | 683 |
| V/C Ratio(X) | 0.00 | 0.84 | 0.84 | 0.00 | 0.73 | 0.00 | 0.00 | 0.00 | 0.00 | 0.51 | 0.00 | 0.90 |
| Avail Cap(c,a), veh/h | 0 | 857 | 892 | 0 | 1713 | 0 | 0 | 0 | 0 | 1794 | 0 | 801 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 20.9 | 21.0 | 0.0 | 19.3 | 0.0 | 0.0 | 0.0 | 0.0 | 18.8 | 0.0 | 24.1 |
| Incr Delay (d2), s/veh | 0.0 | 7.2 | 7.0 | 0.0 | 1.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 12.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 17.0 | 17.7 | 0.0 | 12.8 | 0.0 | 0.0 | 0.0 | 0.0 | 7.2 | 0.0 | 16.6 |
| LnGrp Delay(d),s/veh | 0.0 | 28.1 | 28.0 | 0.0 | 20.9 | 0.0 | 0.0 | 0.0 | 0.0 | 19.1 | 0.0 | 36.1 |
| LnGrp LOS | | C | C | | C | | | | | B | | D |
| Approach Vol, veh/h | | 1431 | | | 1225 | | | | | 1389 | | |
| Approach Delay, s/veh | | 28.0 | | | 20.9 | | | | | 26.6 | | |
| Approach LOS | | C | | | C | | | | | C | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | | | 48.0 | | 44.1 | | 48.0 | | | | |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 | | | | |
| Max Green Setting (Gmax), s | | | | 45.0 | | 47.0 | | 45.0 | | | | |
| Max Q Clear Time (g_c+H1), s | | | | 34.1 | | 35.5 | | 27.8 | | | | |
| Green Ext Time (p_c), s | | | | 9.8 | | 4.6 | | 14.9 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 25.4 | | | | | | | | | |
| HCM 2010 LOS | | | C | | | | | | | | | |
| Notes | | | | | | | | | | | | |
| User approved volume balancing among the lanes for turning movement. | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|-----|-----|-----|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 229 | 1460 | 0 | 0 | 1043 | 736 | 168 | 0 | 339 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | | | |
| Adj Flow Rate, veh/h | 249 | 1587 | 0 | 0 | 1134 | 0 | 183 | 0 | 368 | | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | | | |
| Cap. veh/h | 290 | 2231 | 0 | 0 | 1489 | 666 | 474 | 0 | 423 | | | |
| Arrive On Green | 0.16 | 0.64 | 0.00 | 0.00 | 0.42 | 0.00 | 0.27 | 0.00 | 0.27 | | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | | |
| Grip Volume(v), veh/h | 249 | 1587 | 0 | 0 | 1134 | 0 | 183 | 0 | 368 | | | |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | | |
| Q Serve(g, s) | 11.8 | 25.6 | 0.0 | 0.0 | 23.4 | 0.0 | 7.2 | 0.0 | 19.1 | | | |
| Cycle Q Clear(g, c), s | 11.8 | 25.6 | 0.0 | 0.0 | 23.4 | 0.0 | 7.2 | 0.0 | 19.1 | | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 290 | 2231 | 0 | 0 | 1489 | 666 | 474 | 0 | 423 | | | |
| V/C Ratio(X) | 0.86 | 0.71 | 0.00 | 0.00 | 0.76 | 0.00 | 0.39 | 0.00 | 0.87 | | | |
| Avail Cap(c,a), veh/h | 392 | 2468 | 0 | 0 | 1522 | 681 | 660 | 0 | 589 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 34.6 | 10.3 | 0.0 | 0.0 | 20.8 | 0.0 | 25.4 | 0.0 | 29.7 | | | |
| Incr Delay (d2), s/veh | 13.5 | 0.9 | 0.0 | 0.0 | 2.3 | 0.0 | 0.5 | 0.0 | 10.1 | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%), veh/ln | 6.8 | 12.4 | 0.0 | 0.0 | 11.8 | 0.0 | 3.6 | 0.0 | 9.5 | | | |
| LnGrp Delay(d), s/veh | 48.1 | 11.2 | 0.0 | 0.0 | 23.1 | 0.0 | 25.9 | 0.0 | 39.8 | | | |
| LnGrp LOS | D | B | | | C | | C | | D | | | |
| Approach Vol, veh/h | 1836 | | | 1134 | | | 551 | | | | | |
| Approach Delay, s/veh | 16.2 | | | 23.1 | | | 35.2 | | | | | |
| Approach LOS | B | | | C | | | D | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 2 | | | 4 | | | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 27.0 | | | 58.2 | | | 18.0 | 40.2 | | | | |
| Change Period (Y+Rc), s | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 32.0 | | | 60.0 | | | 19.0 | 37.0 | | | | |
| Max Q Clear Time (g, c+H1), s | 21.1 | | | 27.6 | | | 13.8 | 25.4 | | | | |
| Green Ext Time (p, c), s | 1.9 | | | 26.6 | | | 0.3 | 10.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 21.4 | | | C | | | | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|-----|------|------|-------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1563 | 851 | 282 | 1689 | 0 | 0 | 0 | 0 | 921 | 0 | 601 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 0 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1645 | 896 | 297 | 1778 | 0 | | | | 977 | 0 | 633 |
| Adj No. of Lanes | 0 | 2 | 2 | 2 | 3 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | | | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1507 | 1187 | 307 | 2820 | 0 | | | | 1265 | 0 | 564 |
| Arrive On Green | 0.00 | 0.43 | 0.43 | 0.09 | 0.56 | 0.00 | | | | 0.36 | 0.00 | 0.36 |
| Sat Flow, veh/h | 0 | 3597 | 2760 | 3408 | 5202 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1645 | 896 | 297 | 1778 | 0 | | | | 977 | 0 | 633 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1752 | 1380 | 1704 | 1679 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 43.0 | 27.4 | 8.7 | 24.0 | 0.0 | | | | 24.6 | 0.0 | 36.0 |
| Cycle Q Clear(g, c), s | 0.0 | 43.0 | 27.4 | 8.7 | 24.0 | 0.0 | | | | 24.6 | 0.0 | 36.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 1507 | 1187 | 307 | 2820 | 0 | | | | 1265 | 0 | 564 |
| V/C Ratio(X) | 0.00 | 1.09 | 0.76 | 0.97 | 0.63 | 0.00 | | | | 0.77 | 0.00 | 1.12 |
| Avail Cap(c,a), veh/h | 0 | 1507 | 1187 | 307 | 2820 | 0 | | | | 1265 | 0 | 564 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 28.5 | 24.1 | 45.4 | 15.0 | 0.0 | | | | 28.4 | 0.0 | 32.0 |
| Incr Delay (d2), s/veh | 0.0 | 52.4 | 2.8 | 42.7 | 0.5 | 0.0 | | | | 3.0 | 0.0 | 75.9 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 31.7 | 10.8 | 5.9 | 11.1 | 0.0 | | | | 12.5 | 0.0 | 27.4 |
| LnGrp Delay(d), s/veh | 0.0 | 80.9 | 26.9 | 88.0 | 15.4 | 0.0 | | | | 31.4 | 0.0 | 107.9 |
| LnGrp LOS | | F | C | F | B | | | | | C | | F |
| Approach Vol, veh/h | 2541 | | | 2075 | | | 1610 | | | | | |
| Approach Delay, s/veh | 61.8 | | | 25.8 | | | 61.4 | | | | | |
| Approach LOS | E | | | C | | | E | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | | 3 | 4 | | 6 | | | | | | |
| Phs Duration (G+Y+Rc), s | | | 13.0 | 47.0 | | 40.0 | | 60.0 | | | | |
| Change Period (Y+Rc), s | | | 4.0 | 4.0 | | 4.0 | | 4.0 | | | | |
| Max Green Setting (Gmax), s | | | 9.0 | 43.0 | | 36.0 | | 56.0 | | | | |
| Max Q Clear Time (g, c+H1), s | | | 10.7 | 45.0 | | 38.0 | | 26.0 | | | | |
| Green Ext Time (p, c), s | | | 0.0 | 0.0 | | 0.0 | | 29.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 49.7 | | | D | | | | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|--|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1990 | 566 | 20 | 38 | 1411 | 580 | 609 | 32 | 481 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 2095 | 385 | 40 | 1485 | 611 | 665 | 0 | 480 | 0 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2526 | 786 | 50 | 2884 | 898 | 1203 | 0 | 537 | 0 | 0 |
| Arrive On Green | 0.00 | 0.50 | 0.50 | 0.03 | 0.57 | 0.57 | 0.34 | 0.00 | 0.34 | 0.00 | 0.34 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 2095 | 385 | 40 | 1485 | 611 | 665 | 0 | 480 | 0 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 33.4 | 15.2 | 2.1 | 16.8 | 25.6 | 14.4 | 0.0 | 27.3 | 0.0 | 27.3 |
| Cycle Q Clear(g, c), s | 0.0 | 33.4 | 15.2 | 2.1 | 16.8 | 25.6 | 14.4 | 0.0 | 27.3 | 0.0 | 27.3 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2526 | 786 | 50 | 2884 | 898 | 1203 | 0 | 537 | 0 | 537 |
| V/C Ratio(X) | 0.00 | 0.83 | 0.49 | 0.80 | 0.51 | 0.68 | 0.55 | 0.00 | 0.89 | 0.00 | 0.89 |
| Avail Cap(c,a), veh/h | 0 | 2526 | 786 | 75 | 2947 | 918 | 1383 | 0 | 617 | 0 | 617 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 20.0 | 15.5 | 45.4 | 12.2 | 14.1 | 25.1 | 0.0 | 29.3 | 0.0 | 29.3 |
| Incr Delay (d2), s/veh | 0.0 | 2.5 | 0.5 | 29.4 | 0.1 | 2.0 | 0.4 | 0.0 | 14.2 | 0.0 | 14.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 15.9 | 6.6 | 1.4 | 7.7 | 11.5 | 7.1 | 0.0 | 13.8 | 0.0 | 13.8 |
| LnGrp Delay(d),s/veh | 0.0 | 22.4 | 15.9 | 74.8 | 12.3 | 16.1 | 25.5 | 0.0 | 43.5 | 0.0 | 43.5 |
| LnGrp LOS | C | B | B | E | B | B | C | C | D | D | D |
| Approach Vol, veh/h | 2480 | | | 2136 | | | 1145 | | | | |
| Approach Delay, s/veh | 21.4 | | | 14.6 | | | 33.0 | | | | |
| Approach LOS | C | | | B | | | C | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 2 | 3 | 4 | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 36.2 | 6.7 | 51.1 | | | | 57.8 | | | | |
| Change Period(Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | 4.0 | | | | |
| Max Green Setting (Gmax), s | 37.0 | 4.0 | 47.0 | | | | 55.0 | | | | |
| Max Q Clear Time (g_c+H1), s | 29.3 | 4.1 | 35.4 | | | | 27.6 | | | | |
| Green Ext Time (p_c), s | 2.9 | 0.0 | 11.4 | | | | 26.2 | | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 21.2 | | | | | | | |
| HCM 2010 LOS | | | | C | | | | | | | |
| Notes | | | | | | | | | | | |
| User approved volume balancing among the lanes for turning movement. | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/27/2015













| Movement | SBT |
|--|------|
| Lane Configurations | 0 |
| Volume (veh/h) | 0 |
| Number | 0 |
| Initial Q (Qb), veh | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |
| Parking Bus, Adj | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 |
| Adj Flow Rate, veh/h | 0 |
| Adj No. of Lanes | 0 |
| Peak Hour Factor | 0.95 |
| Percent Heavy Veh. % | 0 |
| Cap. veh/h | 0 |
| Arrive On Green | 0.00 |
| Sat Flow, veh/h | 0 |
| Grip Volume(v), veh/h | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 |
| Q Serve(g, s), s | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 |
| Prop In Lane | 0.00 |
| Lane Grp Cap(c), veh/h | 0 |
| V/C Ratio(X) | 0.00 |
| Avail Cap(c,a), veh/h | 0 |
| HCM Platoon Ratio | 1.00 |
| Upstream Filter(I) | 0.00 |
| Uniform Delay (d), s/veh | 0.0 |
| Incr Delay (d2), s/veh | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 |
| LnGrp LOS | D |
| Approach Vol, veh/h | 0 |
| Approach Delay, s/veh | 0 |
| Approach LOS | D |
| Timer | |
| User approved ignoring U-Turning movement. | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/27/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU | |
| Lane Configurations | 5 | 5 | AAA | AAA | 5 | AAA | AAA | 5 | AAA | 5 | AAA | |
| Volume (veh/h) | 101 | 273 | 1712 | 131 | 226 | 1389 | 180 | 16 | 195 | 97 | 178 | |
| Number | 7 | 4 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 59 | |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 297 | 1861 | 120 | 246 | 1510 | 148 | 212 | 105 | 168 | 168 | 168 | |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 1 | 3 | 1 | 2 | 1 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 336 | 2335 | 727 | 284 | 2186 | 681 | 285 | 295 | 251 | 251 | 251 | |
| Arrive On Green | 0.19 | 0.46 | 0.46 | 0.16 | 0.43 | 0.43 | 0.08 | 0.16 | 0.16 | 0.16 | 0.16 | |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | 3408 | 1845 | 1568 | 1568 | 1568 | |
| Gp Volume(v), veh/h | 297 | 1861 | 120 | 246 | 1510 | 148 | 212 | 105 | 168 | 168 | 168 | |
| Gp Sat Flow(s), veh/h/ln | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | 1704 | 1845 | 1568 | 1568 | 1568 | |
| Q Serve(Q_s), s | 14.4 | 27.4 | 3.9 | 11.9 | 21.2 | 5.2 | 5.3 | 4.4 | 8.8 | 8.8 | 8.8 | |
| Cycle Q Clear(q_c), s | 14.4 | 27.4 | 3.9 | 11.9 | 21.2 | 5.2 | 5.3 | 4.4 | 8.8 | 8.8 | 8.8 | |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 336 | 2335 | 727 | 284 | 2186 | 681 | 285 | 295 | 251 | 251 | 251 | |
| V/C Ratio(X) | 0.88 | 0.80 | 0.17 | 0.86 | 0.69 | 0.22 | 0.74 | 0.36 | 0.67 | 0.67 | 0.67 | |
| Avail Cap(c_a), veh/h | 422 | 2364 | 736 | 362 | 2191 | 682 | 312 | 444 | 377 | 377 | 377 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 34.3 | 19.9 | 13.6 | 35.7 | 20.0 | 15.4 | 39.1 | 32.7 | 34.5 | 34.5 | 34.5 | |
| Incr Delay (d2), s/veh | 16.4 | 2.0 | 0.1 | 16.0 | 0.9 | 0.2 | 8.4 | 0.7 | 3.1 | 3.1 | 3.1 | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | 8.5 | 13.0 | 1.7 | 7.0 | 10.0 | 2.3 | 2.8 | 2.3 | 4.0 | 4.0 | 4.0 | |
| LnGrp Delay(d), s/veh | 50.8 | 21.9 | 13.7 | 51.6 | 20.9 | 15.6 | 47.5 | 33.4 | 37.6 | 37.6 | 37.6 | |
| LnGrp LOS | D | C | B | D | C | B | D | C | D | C | D | |
| Approach Vol, veh/h | 2278 | | | 1904 | | | 485 | | | | | |
| Approach Delay, s/veh | 25.2 | | | 24.5 | | | 41.0 | | | | | |
| Approach LOS | C | | | C | | | D | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 6.7 | 18.0 | 18.1 | 44.5 | 11.3 | 13.4 | 20.7 | 41.9 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 4.0 | 21.0 | 18.0 | 41.0 | 8.0 | 17.0 | 21.0 | 38.0 | | | | |
| Max Q Clear Time (g_c+H1), s | 3.2 | 10.8 | 13.9 | 29.4 | 7.3 | 7.7 | 16.4 | 23.2 | | | | |
| Green Ext Time (p_c), s | 0.0 | 1.8 | 0.3 | 11.0 | 0.0 | 1.7 | 0.4 | 14.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 27.4 | | | | | | | | | | | |
| HCM 2010 LOS | C | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/27/2015

| Movement | SBL | SBT | SBR |
|----------------------------|------|------|------|
| Lane Configurations | 5 | 4 | 4 |
| Volume (veh/h) | 43 | 149 | 60 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 47 | 162 | 65 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 106 | 266 | 103 |
| Arrive On Green | 0.03 | 0.11 | 0.11 |
| Sat Flow, veh/h | 3408 | 2474 | 955 |
| Grip Volume(v), veh/h | 47 | 113 | 114 |
| Grip Sat Flow(s), veh/h/ln | 1704 | 1752 | 1676 |
| Q Serve(g, s), s | 1.2 | 5.4 | 5.7 |
| Cycle Q Clear(g, c), s | 1.2 | 5.4 | 5.7 |
| Prop In Lane | 1.00 | 1.00 | 0.57 |
| Lane Grp Cap(c), veh/h | 106 | 188 | 180 |
| V/C Ratio(X) | 0.44 | 0.60 | 0.63 |
| Avail Cap(c,a), veh/h | 156 | 341 | 326 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.6 | 37.2 | 37.3 |
| Incr Delay (d2), s/veh | 2.9 | 3.0 | 3.7 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.6 | 2.8 | 2.8 |
| LnGrp Delay(d), s/veh | 44.4 | 40.2 | 41.0 |
| LnGrp LOS | D | D | D |
| Approach Vol, veh/h | 274 | | |
| Approach Delay, s/veh | 41.3 | | |
| Approach LOS | D | | |
| Timer | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Country Hills Road & Laurel Road

10/27/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
|------------------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | |
| Volume (veh/h) | 960 | 120 | 402 | 1371 | 90 | 170 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 1043 | 130 | 437 | 1490 | 98 | 185 | |
| Adj No. of Lanes | 2 | 0 | 2 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 1677 | 209 | 556 | 2627 | 258 | 230 | |
| Arrive On Green | 0.53 | 0.53 | 0.16 | 0.75 | 0.15 | 0.15 | |
| Sat Flow, veh/h | 3230 | 391 | 3408 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 582 | 591 | 437 | 1490 | 98 | 185 | |
| Grip Sat Flow(s),veh/h/ln | 1752 | 1776 | 1704 | 1752 | 1757 | 1568 | |
| Q Serve(g, s) | 17.9 | 17.9 | 9.5 | 14.3 | 3.9 | 8.8 | |
| Cycle Q Clear(g, c), s | 17.9 | 17.9 | 9.5 | 14.3 | 3.9 | 8.8 | |
| Prop In Lane | 0.22 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 937 | 949 | 556 | 2627 | 258 | 230 | |
| V/C Ratio(X) | 0.62 | 0.62 | 0.79 | 0.57 | 0.38 | 0.80 | |
| Avail Cap(c,a), veh/h | 1089 | 1103 | 926 | 3311 | 432 | 386 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 12.5 | 12.5 | 31.0 | 4.2 | 29.8 | 31.9 | |
| Incr Delay (d2), s/veh | 0.8 | 0.8 | 2.5 | 0.2 | 0.9 | 6.4 | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | 8.8 | 8.9 | 4.7 | 6.9 | 1.9 | 4.2 | |
| LnGrp Delay(d),s/veh | 13.4 | 13.4 | 33.5 | 4.4 | 30.7 | 38.3 | |
| LnGrp LOS | B | B | C | A | C | D | |
| Approach Vol, veh/h | 1173 | | 1927 | 283 | | | |
| Approach Delay, s/veh | 13.4 | | 11.0 | 35.7 | | | |
| Approach LOS | B | | B | D | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 8 |
| Assigned Phs | 2 | 3 | 4 | | | | 8 |
| Phs Duration (G+Y+Rc), s | 15.4 | 16.6 | 45.3 | | | | 61.9 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | 4.0 |
| Max Green Setting (Gmax), s | 19.0 | 21.0 | 48.0 | | | | 73.0 |
| Max Q Clear Time (g_c+H1), s | 10.8 | 11.5 | 19.9 | | | | 16.3 |
| Green Ext Time (p_c), s | 0.6 | 1.1 | 21.4 | | | | 34.6 |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | | | 13.9 | | | | |
| HCM 2010 LOS | | | B | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
11: Slatten Ranch Road & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 113 | 1378 | 230 | 260 | 1048 | 230 | 612 | 301 | 230 | 410 | 110 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 123 | 1498 | 157 | 283 | 1139 | 250 | 665 | 295 | 327 | 250 | 446 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 0 | 2 | 2 | 0 | 1 | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 151 | 1511 | 470 | 299 | 1587 | 348 | 682 | 367 | 328 | 282 | 465 |
| Arrive On Green | 0.09 | 0.30 | 0.30 | 0.17 | 0.38 | 0.20 | 0.21 | 0.21 | 0.16 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 4134 | 907 | 3408 | 1752 | 1568 | 1757 | 2737 |
| Grip Volume(v), veh/h | 123 | 1498 | 157 | 283 | 925 | 464 | 665 | 295 | 327 | 250 | 284 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 1679 | 1568 | 1757 | 1679 | 1685 | 1704 | 1752 | 1568 | 1757 | 1752 |
| Q Serve(g, s) | 6.9 | 29.6 | 7.8 | 15.9 | 23.4 | 23.4 | 19.4 | 16.0 | 20.8 | 13.9 | 16.1 |
| Cycle Q Clear(g, c), s | 6.9 | 29.6 | 7.8 | 15.9 | 23.4 | 23.4 | 19.4 | 16.0 | 20.8 | 13.9 | 16.1 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.54 | 1.00 | 1.00 | 1.00 | 1.00 | 0.43 |
| Lane Grp Cap(c), veh/h | 151 | 1511 | 470 | 299 | 1289 | 647 | 682 | 367 | 328 | 282 | 298 |
| V/C Ratio(X) | 0.81 | 0.99 | 0.33 | 0.95 | 0.72 | 0.72 | 0.98 | 0.80 | 1.00 | 0.89 | 0.95 |
| Avail Cap(c,a), veh/h | 176 | 1511 | 470 | 299 | 1289 | 647 | 682 | 367 | 328 | 316 | 298 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.9 | 34.9 | 27.2 | 41.1 | 26.2 | 26.2 | 39.8 | 37.6 | 39.5 | 41.1 | 41.2 |
| Incr Delay (d2), s/veh | 21.7 | 21.1 | 0.4 | 38.2 | 1.9 | 3.8 | 28.3 | 12.3 | 46.6 | 22.9 | 39.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 4.3 | 16.7 | 3.4 | 10.9 | 11.1 | 11.5 | 11.8 | 9.0 | 13.4 | 8.5 | 11.0 |
| LnGrp Delay(d),s/veh | 66.6 | 56.0 | 27.6 | 79.2 | 28.2 | 30.0 | 68.1 | 49.8 | 88.1 | 64.0 | 80.9 |
| LnGrp LOS | E | E | C | E | C | C | E | D | F | E | F |
| Approach Vol, veh/h | | 1778 | | | 1672 | | | 1287 | | | 816 |
| Approach Delay, s/veh | | 54.2 | | | 37.3 | | | 69.0 | | | 77.0 |
| Approach LOS | | D | | | D | | | E | | | E |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Phs Duration (G+Y+Rc), s | 20.1 | 24.9 | 21.0 | 34.0 | 24.0 | 21.0 | 12.6 | 42.4 | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Max Green Setting (Gmax), s | 18.0 | 19.0 | 17.0 | 30.0 | 20.0 | 17.0 | 10.0 | 37.0 | | | |
| Max Q Clear Time (g_c+H1), s | 15.9 | 22.8 | 17.9 | 31.6 | 21.4 | 18.3 | 8.9 | 25.4 | | | |
| Green Ext Time (p_c), s | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.8 | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | 55.9 | | | | | | |
| HCM 2010 LOS | | | | | E | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative Conditions Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
1: Hillcrest Ave & SR4 WB Ramps

10/26/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------------|-----|------|------|------|------|-------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 655 | 646 | 816 | 124 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 712 | 702 | 887 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 988 | 1686 | 1888 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 712 | 702 | 887 | 0 |
| Grip Sat Flow(s),veh/h/ln | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.7 | 2.5 | 7.3 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.7 | 2.5 | 7.3 | 0.0 |
| Prop In Lane | | | 1.00 | | | |
| Lane Grp Cap(c), veh/h | | | 988 | 1686 | 1888 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.42 | 0.47 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2851 | 3798 | 3984 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 14.9 | 0.3 | 6.6 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.2 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 4.2 | 1.1 | 3.5 | 0.0 |
| LnGrp Delay(d),s/veh | | | 15.9 | 0.4 | 6.8 | 0.0 |
| LnGrp LOS | | | B | A | A | |
| Approach Vol, veh/h | | | | 1414 | 887 | |
| Approach Delay, s/veh | | | | 8.2 | 6.8 | |
| Approach LOS | | | | A | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 7 8 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.6 | | | 17.5 | 29.1 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 39.0 | 53.0 |
| Max Q Clear Time (g, c+H1), s | | 4.5 | | | 10.7 | 9.3 |
| Green Ext Time (p, c), s | | 17.9 | | | 2.8 | 15.8 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 7.7 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 142 | 1 | 687 | 0 | 0 | 0 | 0 | 1157 | 395 | 168 | 636 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1900 | 1845 | 1845 | | | | 0 | 1845 | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 154 | 1 | 747 | | | | 0 | 1258 | 429 | 183 | 691 | 0 |
| Adj No. of Lanes | 0 | 1 | 2 | | | | 0 | 3 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | | | | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | 511 | 3 | 807 | | | | 0 | 1664 | 566 | 221 | 2166 | 0 |
| Arrive On Green | 0.29 | 0.29 | 0.29 | | | | 0.00 | 0.45 | 0.45 | 0.13 | 0.82 | 0.00 |
| Sat Flow, veh/h | 1746 | 11 | 2760 | | | | 0 | 3881 | 1264 | 1757 | 3597 | 0 |
| Grip Volume(v), veh/h | 155 | 0 | 747 | | | | 0 | 1136 | 551 | 183 | 691 | 0 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 0 | 1380 | | | | 0 | 1679 | 1622 | 1757 | 1752 | 0 |
| Q Serve(g, s), s | 6.1 | 0.0 | 23.5 | | | | 0.0 | 25.3 | 25.4 | 9.1 | 8.4 | 0.0 |
| Cycle Q Clear(g, c), s | 6.1 | 0.0 | 23.5 | | | | 0.0 | 25.3 | 25.4 | 9.1 | 8.4 | 0.0 |
| Prop In Lane | 0.99 | | 1.00 | | | | 0.00 | | 0.78 | 1.00 | 0.00 | |
| Lane Grp Cap(c), veh/h | 514 | 0 | 807 | | | | 0 | 1504 | 726 | 221 | 2166 | 0 |
| V/C Ratio(X) | 0.30 | 0.00 | 0.93 | | | | 0.00 | 0.76 | 0.76 | 0.83 | 0.32 | 0.00 |
| Avail Cap(c,a), veh/h | 530 | 0 | 832 | | | | 0 | 1612 | 779 | 353 | 2544 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | | | | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 24.6 | 0.0 | 30.7 | | | | 0.0 | 20.6 | 20.7 | 38.2 | 8.1 | 0.0 |
| Incr Delay (d2), s/veh | 0.3 | 0.0 | 15.8 | | | | 0.0 | 2.0 | 4.0 | 8.7 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 3.0 | 0.0 | 10.7 | | | | 0.0 | 12.1 | 12.1 | 5.0 | 4.1 | 0.0 |
| LnGrp Delay(d),s/veh | 24.9 | 0.0 | 46.5 | | | | 0.0 | 22.6 | 24.7 | 46.9 | 8.2 | 0.0 |
| LnGrp LOS | C | D | D | | | | C | C | C | D | A | |
| Approach Vol, veh/h | | | 902 | | | | | 1887 | | | 874 | |
| Approach Delay, s/veh | | | 42.8 | | | | | 23.3 | | | 16.3 | |
| Approach LOS | | | D | | | | | C | | | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 15.2 | 44.1 | | 30.2 | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | | | | | | | |
| Max Green Setting (Gmax), s | 18.0 | 43.0 | | 27.0 | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 11.1 | 27.4 | | 25.5 | | | | | | | | |
| Green Ext Time (p, c), s | 0.3 | 12.7 | | 0.7 | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 26.6 | | | | | | | | |
| HCM 2010 LOS | | | | C | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBL | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 79 | 59 | 55 | 174 | 40 | 196 | 64 | 331 | 142 | 183 | 327 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 86 | 64 | 60 | 189 | 43 | 106 | 70 | 360 | 0 | 199 | 355 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 513 | 258 | 242 | 472 | 543 | 462 | 94 | 927 | 0 | 267 | 1001 |
| Arrive On Green | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | 0.05 | 0.26 | 0.00 | 0.15 | 0.36 |
| Sat Flow, veh/h | 1222 | 877 | 822 | 1250 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 2758 |
| Grip Volume(v), veh/h | 86 | 0 | 124 | 189 | 43 | 106 | 70 | 360 | 0 | 199 | 224 |
| Grip Sat Flow(s), veh/h | 1222 | 0 | 1700 | 1250 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 |
| Q Serve(g, s) | 2.3 | 0.0 | 2.3 | 5.6 | 0.7 | 2.1 | 1.6 | 3.5 | 0.0 | 4.5 | 3.9 |
| Cycle Q Clear(g, c), s | 3.0 | 0.0 | 2.3 | 7.9 | 0.7 | 2.1 | 1.6 | 3.5 | 0.0 | 4.5 | 3.9 |
| Prop In Lane | 1.00 | 0.48 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.42 |
| Lane Grp Cap(c), veh/h | 513 | 0 | 500 | 472 | 543 | 462 | 94 | 927 | 0 | 267 | 636 |
| V/C Ratio(X) | 0.17 | 0.00 | 0.25 | 0.40 | 0.08 | 0.23 | 0.75 | 0.39 | 0.00 | 0.75 | 0.35 |
| Avail Cap(c,a), veh/h | 1125 | 0 | 1352 | 1098 | 1488 | 1247 | 551 | 2535 | 0 | 1059 | 1774 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 11.6 | 0.0 | 11.1 | 14.2 | 10.6 | 11.1 | 19.4 | 12.5 | 0.0 | 16.8 | 9.6 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 0.3 | 0.5 | 0.1 | 0.3 | 11.1 | 0.3 | 0.0 | 4.1 | 0.3 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.8 | 0.0 | 1.1 | 2.0 | 0.4 | 1.0 | 1.1 | 1.7 | 0.0 | 2.5 | 1.9 |
| LnGrp Delay(d), s/veh | 11.8 | 0.0 | 11.4 | 14.7 | 10.6 | 11.3 | 30.5 | 12.8 | 0.0 | 21.0 | 10.0 |
| LnGrp LOS | B | B | B | B | B | B | C | B | C | A | B |
| Approach Vol, veh/h | 210 | | | 338 | | | 430 | | | 647 | |
| Approach Delay, s/veh | 11.6 | | | 13.1 | | | 15.6 | | | 13.4 | |
| Approach LOS | B | | | B | | | B | | | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | |
| Phs Duration (G+Y+Rc), s | 10.3 | 15.0 | | 16.2 | 6.2 | 19.1 | | 16.2 | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | | | |
| Max Green Setting (Gmax), s | 25.0 | 30.0 | | 33.0 | 13.0 | 42.0 | | 33.0 | | | |
| Max Q Clear Time (g, c+H1), s | 6.5 | 5.5 | | 5.0 | 3.6 | 6.0 | | 9.9 | | | |
| Green Ext Time (p, c), s | 0.5 | 5.5 | | 2.4 | 0.1 | 5.9 | | 2.3 | | | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 13.7 | | | | | | | |
| HCM 2010 LOS | | | | B | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/26/2015

| Movement | EBT | EBL | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|-----|-----|-----|-----|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 463 | 66 | 179 | 510 | 113 | 195 | | | | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Adj Sat Flow, veh/h | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | | | | |
| Adj Flow Rate, veh/h | 525 | 72 | 195 | 554 | 123 | 107 | | | | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | | | | |
| Cap. veh/h | 1256 | 172 | 264 | 2322 | 219 | 195 | | | | |
| Arrive On Green | 0.41 | 0.41 | 0.15 | 0.66 | 0.12 | 0.12 | | | | |
| Sat Flow, veh/h | 3191 | 424 | 1757 | 3597 | 1757 | 1568 | | | | |
| Grip Volume(v), veh/h | 296 | 301 | 195 | 554 | 123 | 107 | | | | |
| Grip Sat Flow(s), veh/h | 1752 | 1770 | 1757 | 1752 | 1757 | 1568 | | | | |
| Q Serve(g, s) | 4.5 | 4.6 | 4.0 | 2.4 | 2.5 | 2.4 | | | | |
| Cycle Q Clear(g, c), s | 4.5 | 4.6 | 4.0 | 2.4 | 2.5 | 2.4 | | | | |
| Prop In Lane | 0.24 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Lane Grp Cap(c), veh/h | 710 | 717 | 264 | 2322 | 219 | 195 | | | | |
| V/C Ratio(X) | 0.42 | 0.42 | 0.74 | 0.24 | 0.56 | 0.55 | | | | |
| Avail Cap(c,a), veh/h | 1588 | 1604 | 1264 | 6072 | 1264 | 1128 | | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | |
| Uniform Delay (d), s/veh | 8.0 | 8.0 | 15.2 | 2.5 | 15.5 | 15.4 | | | | |
| Incr Delay (d2), s/veh | 0.4 | 0.4 | 4.0 | 0.1 | 2.3 | 2.4 | | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | |
| %ile BackOfQ(50%), veh/h | 2.2 | 2.3 | 2.2 | 1.1 | 1.3 | 1.2 | | | | |
| LnGrp Delay(d), s/veh | 8.4 | 8.4 | 19.2 | 2.6 | 17.7 | 17.8 | | | | |
| LnGrp LOS | A | A | B | A | B | B | | | | |
| Approach Vol, veh/h | 597 | | | 749 | | 230 | | | | |
| Approach Delay, s/veh | 8.4 | | | 6.9 | | 17.8 | | | | |
| Approach LOS | A | | | A | | B | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | |
| Assigned Phs | 2 | | 3 | 4 | | | | | | |
| Phs Duration (G+Y+Rc), s | 8.7 | 9.6 | 19.2 | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | | | | |
| Max Green Setting (Gmax), s | 27.0 | 27.0 | 34.0 | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 4.5 | 6.0 | 6.6 | | | | | | | |
| Green Ext Time (p, c), s | 0.7 | 0.5 | 8.6 | | | | | | | |
| Intersection Summary | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 9.1 | | | | | | |
| HCM 2010 LOS | | | | A | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 697 | 75 | 0 | 616 | 487 | 0 | 0 | 0 | 450 | 1 | 160 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 758 | 82 | 0 | 670 | 0 | | | | 490 | 0 | 174 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1791 | 194 | 0 | 1967 | 0 | | | | 831 | 0 | 371 |
| Arrive On Green | 0.00 | 0.56 | 0.56 | 0.00 | 0.56 | 0.00 | | | | 0.24 | 0.00 | 0.24 |
| Sat Flow, veh/h | 0 | 3283 | 345 | 0 | 3689 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 416 | 424 | 0 | 670 | 0 | | | | 490 | 0 | 174 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1784 | 0 | 1752 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 5.4 | 5.4 | 0.0 | 4.1 | 0.0 | | | | 4.9 | 0.0 | 3.8 |
| Cycle Q Clear(g, c), s | 0.0 | 5.4 | 5.4 | 0.0 | 4.1 | 0.0 | | | | 4.9 | 0.0 | 3.8 |
| Prop In Lane | 0.00 | 0.19 | 0.00 | 0.00 | 0.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 983 | 1001 | 0 | 1967 | 0 | | | | 831 | 0 | 371 |
| V/C Ratio(X) | 0.00 | 0.42 | 0.42 | 0.00 | 0.34 | 0.00 | | | | 0.59 | 0.00 | 0.47 |
| Avail Cap(c,a), veh/h | 0 | 2570 | 2616 | 0 | 5139 | 0 | | | | 3020 | 0 | 1348 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 5.0 | 5.0 | 0.0 | 4.7 | 0.0 | | | | 13.4 | 0.0 | 13.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.3 | 0.3 | 0.0 | 0.1 | 0.0 | | | | 0.7 | 0.0 | 0.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 2.6 | 2.7 | 0.0 | 2.0 | 0.0 | | | | 2.4 | 0.0 | 1.7 |
| LnGrp Delay(d),s/veh | 0.0 | 5.3 | 5.3 | 0.0 | 4.8 | 0.0 | | | | 14.1 | 0.0 | 13.9 |
| LnGrp LOS | | A | A | | A | | | | | B | | B |
| Approach Vol, veh/h | | 840 | | | 670 | | | | | | 664 | |
| Approach Delay, s/veh | | 5.3 | | | 4.8 | | | | | | 14.0 | |
| Approach LOS | | A | | | A | | | | | | B | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--|---|---|---|------|---|------|---|------|
| Assigned Phs | | | | 4 | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 26.2 | | 13.4 | | 26.2 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 58.0 | | 34.0 | | 58.0 |
| Max Q Clear Time (g_c+H1), s | | | | 7.4 | | 6.9 | | 6.1 |
| Green Ext Time (p_c), s | | | | 14.8 | | 2.5 | | 14.9 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 7.8 | | | | |
| HCM 2010 LOS | | | | A | | | | |
| Notes | | | | | | | | |
| User approved volume balancing among the lanes for turning movement. | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 227 | 921 | 0 | 0 | 1092 | 725 | 26 | 0 | 318 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 247 | 1001 | 0 | 0 | 1187 | 0 | | | | 28 | 0 | 346 |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | | | | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 289 | 2293 | 0 | 0 | 1547 | 692 | | | | 438 | 0 | 391 |
| Arrive On Green | 0.16 | 0.65 | 0.00 | 0.00 | 0.44 | 0.00 | | | | 0.25 | 0.00 | 0.25 |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | | | | 1757 | 0 | 1568 |
| Grip Volume(v), veh/h | 247 | 1001 | 0 | 0 | 1187 | 0 | | | | 28 | 0 | 346 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 11.3 | 11.4 | 0.0 | 0.0 | 23.7 | 0.0 | | | | 1.0 | 0.0 | 17.6 |
| Cycle Q Clear(g, c), s | 11.3 | 11.4 | 0.0 | 0.0 | 23.7 | 0.0 | | | | 1.0 | 0.0 | 17.6 |
| Prop In Lane | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 289 | 2293 | 0 | 0 | 1547 | 692 | | | | 438 | 0 | 391 |
| V/C Ratio(X) | 0.85 | 0.44 | 0.00 | 0.00 | 0.77 | 0.00 | | | | 0.06 | 0.00 | 0.89 |
| Avail Cap(c,a), veh/h | 403 | 2624 | 0 | 0 | 1651 | 739 | | | | 637 | 0 | 588 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 33.6 | 6.9 | 0.0 | 0.0 | 19.5 | 0.0 | | | | 23.7 | 0.0 | 30.0 |
| Incr Delay (d2), s/veh | 12.1 | 0.1 | 0.0 | 0.0 | 2.1 | 0.0 | | | | 0.1 | 0.0 | 11.3 |
| Initial Q Delay(d3),s/veh | 6.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 6.5 | 5.5 | 0.0 | 0.0 | 11.8 | 0.0 | | | | 0.5 | 0.0 | 8.8 |
| LnGrp Delay(d),s/veh | 45.8 | 7.1 | 0.0 | 0.0 | 21.6 | 0.0 | | | | 23.8 | 0.0 | 41.3 |
| LnGrp LOS | | D | A | | C | C | | | | D | | D |
| Approach Vol, veh/h | | 1248 | | | 1187 | | | | | 374 | | |
| Approach Delay, s/veh | | 14.7 | | | 21.6 | | | | | 40.0 | | |
| Approach LOS | | B | | | C | | | | | D | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|------|------|------|---|------|------|---|
| Assigned Phs | | 2 | | 4 | | 5 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | | 24.6 | | 58.2 | | 17.6 | 40.5 | |
| Change Period (Y+Rc), s | | 4.0 | | 4.0 | | 4.0 | 4.0 | |
| Max Green Setting (Gmax), s | | 30.0 | | 62.0 | | 19.0 | 39.0 | |
| Max Q Clear Time (g_c+H1), s | | 19.6 | | 13.4 | | 13.4 | 25.7 | |
| Green Ext Time (p_c), s | | 1.0 | | 27.8 | | 0.4 | 10.9 | |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 21.0 | | | | | |
| HCM 2010 LOS | | | C | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 783 | 424 | 95 | 1180 | 0 | 0 | 0 | 0 | 318 | 1 | 353 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 851 | 472 | 103 | 1283 | 0 | 347 | 0 | 427 | 0 | 427 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | 2 | 0 | 2 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2276 | 709 | 174 | 2823 | 0 | 1139 | 0 | 508 | 0 | 508 | 0 |
| Arrive On Green | 0.00 | 0.45 | 0.45 | 0.05 | 0.56 | 0.00 | 0.32 | 0.00 | 0.32 | 0.00 | 0.32 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 851 | 472 | 103 | 1283 | 0 | 347 | 0 | 427 | 0 | 427 | 0 |
| Grip Sat Flow(s),veh/h | 0 | 1679 | 1568 | 1704 | 1679 | 0 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s) | 0.0 | 7.7 | 16.4 | 2.1 | 10.4 | 0.0 | 5.1 | 0.0 | 17.6 | 0.0 | 17.6 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 7.7 | 16.4 | 2.1 | 10.4 | 0.0 | 5.1 | 0.0 | 17.6 | 0.0 | 17.6 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2276 | 709 | 174 | 2823 | 0 | 1139 | 0 | 508 | 0 | 508 | 0 |
| V/C Ratio(X) | 0.00 | 0.37 | 0.67 | 0.59 | 0.45 | 0.00 | 0.30 | 0.00 | 0.84 | 0.00 | 0.84 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 2463 | 767 | 343 | 3280 | 0 | 2376 | 0 | 1060 | 0 | 1060 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 12.6 | 14.9 | 32.3 | 9.0 | 0.0 | 17.6 | 0.0 | 21.8 | 0.0 | 21.8 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 2.0 | 3.2 | 0.1 | 0.0 | 0.1 | 0.0 | 3.8 | 0.0 | 3.8 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 3.6 | 7.5 | 1.0 | 4.8 | 0.0 | 2.5 | 0.0 | 8.1 | 0.0 | 8.1 | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 | 12.7 | 16.9 | 35.4 | 9.1 | 0.0 | 17.8 | 0.0 | 25.6 | 0.0 | 25.6 | 0.0 |
| LnGrp LOS | B | B | B | D | A | B | B | B | C | B | C | C |
| Approach Vol, veh/h | 1323 | | | | 1386 | | | | | | | 774 |
| Approach Delay, s/veh | 14.2 | | | | 11.1 | | | | | | | 22.1 |
| Approach LOS | B | | | | B | | | | | | | C |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|-----|------|---|---|------|---|------|
| Assigned Phs | | 3 | 4 | | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | 7.6 | 35.4 | | | 26.5 | | 43.0 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | 7.0 | 34.0 | | | 47.0 | | 45.0 |
| Max Q Clear Time (g_c+H1), s | | 4.1 | 18.4 | | | 19.6 | | 12.4 |
| Green Ext Time (p_c), s | | 0.1 | 13.0 | | | 3.0 | | 23.4 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 14.7 |
| HCM 2010 LOS | B |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 956 | 166 | 8 | 3 | 850 | 311 | 429 | 19 | 138 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1039 | 90 | 3 | 924 | 338 | 481 | 0 | 150 | 0 | 150 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2783 | 867 | 6 | 3197 | 995 | 728 | 0 | 325 | 0 | 325 | 0 |
| Arrive On Green | 0.00 | 0.55 | 0.55 | 0.00 | 0.63 | 0.63 | 0.21 | 0.00 | 0.21 | 0.00 | 0.21 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 1039 | 90 | 3 | 924 | 338 | 481 | 0 | 150 | 0 | 150 | 0 |
| Grip Sat Flow(s),veh/h | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s) | 0.0 | 5.9 | 1.4 | 0.1 | 4.2 | 5.1 | 6.4 | 0.0 | 4.2 | 0.0 | 4.2 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 5.9 | 1.4 | 0.1 | 4.2 | 5.1 | 6.4 | 0.0 | 4.2 | 0.0 | 4.2 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2783 | 867 | 6 | 3197 | 995 | 728 | 0 | 325 | 0 | 325 | 0 |
| V/C Ratio(X) | 0.00 | 0.37 | 0.10 | 0.52 | 0.29 | 0.34 | 0.66 | 0.00 | 0.46 | 0.00 | 0.46 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 2783 | 867 | 1214 | 6561 | 2043 | 1803 | 0 | 805 | 0 | 805 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 6.4 | 5.4 | 25.2 | 4.1 | 4.3 | 18.4 | 0.0 | 17.6 | 0.0 | 17.6 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 0.1 | 38.5 | 0.0 | 0.2 | 1.0 | 0.0 | 1.0 | 0.0 | 1.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 2.7 | 0.6 | 0.1 | 1.9 | 2.2 | 3.2 | 0.0 | 1.9 | 0.0 | 1.9 | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 | 6.5 | 5.4 | 83.7 | 4.2 | 4.5 | 19.5 | 0.0 | 18.6 | 0.0 | 18.6 | 0.0 |
| LnGrp LOS | A | A | A | F | A | A | B | B | B | B | B | B |
| Approach Vol, veh/h | 1129 | | | | 1265 | | | | 631 | | | |
| Approach Delay, s/veh | 6.4 | | | | 4.5 | | | | 19.3 | | | |
| Approach LOS | A | | | | A | | | | B | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|------|------|------|---|---|---|------|
| Assigned Phs | | 2 | 3 | 4 | | | | 8 |
| Phs Duration (G+Y+Rc), s | | 14.5 | 4.2 | 32.0 | | | | 36.2 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | | 4.0 |
| Max Green Setting (Gmax), s | | 26.0 | 35.0 | 27.0 | | | | 66.0 |
| Max Q Clear Time (g_c+H1), s | | 8.4 | 2.1 | 7.9 | | | | 7.1 |
| Green Ext Time (p_c), s | | 2.1 | 0.0 | 13.6 | | | | 25.1 |

| Intersection Summary | |
|----------------------|-----|
| HCM 2010 Ctrl Delay | 8.3 |
| HCM 2010 LOS | A |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/26/2015

| Movement | SBR |
|------------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus Adj | |
| Adj Sat Flow, veh/h/in | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s),veh/h/in | |
| Q Serve(g, s) | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grip Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c,a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(I) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/in | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |
| Timer | |
| Assigned Phs | |
| Phs Duration (G+Y+Rc), s | |
| Change Period (Y+Rc), s | |
| Max Green Setting (Gmax), s | |
| Max Q Clear Time (g_c+11), s | |
| Green Ext Time (p_c), s | |

User approved ignoring U-Turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 43 | 131 | 470 | 41 | 61 | 610 | 92 | 15 | 107 | 88 | 47 | 25 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | 5 | 2 | 12 | | |
| Initial Q (Qb), veh | | | | | | | | | | | | |
| Ped-Bike Adj(A_pbT) | | | | | | | | | | | | |
| Parking Bus Adj | | | | | | | | | | | | |
| Adj Sat Flow, veh/h/in | | | | | | | | | | | | |
| Adj Flow Rate, veh/h | | | | | | | | | | | | |
| Adj No. of Lanes | | | | | | | | | | | | |
| Peak Hour Factor | | | | | | | | | | | | |
| Percent Heavy Veh. % | | | | | | | | | | | | |
| Cap. veh/h | | | | | | | | | | | | |
| Arrive On Green | | | | | | | | | | | | |
| Sat Flow, veh/h | | | | | | | | | | | | |
| Grip Volume(v), veh/h | | | | | | | | | | | | |
| Grip Sat Flow(s),veh/h/in | | | | | | | | | | | | |
| Q Serve(g, s) | | | | | | | | | | | | |
| Cycle Q Clear(g, c), s | | | | | | | | | | | | |
| Prop In Lane | | | | | | | | | | | | |
| Lane Grip Cap(c), veh/h | | | | | | | | | | | | |
| V/C Ratio(X) | | | | | | | | | | | | |
| Avail Cap(c,a), veh/h | | | | | | | | | | | | |
| HCM Platoon Ratio | | | | | | | | | | | | |
| Upstream Filter(I) | | | | | | | | | | | | |
| Uniform Delay (d), s/veh | | | | | | | | | | | | |
| Incr Delay (d2), s/veh | | | | | | | | | | | | |
| Initial Q Delay(d3),s/veh | | | | | | | | | | | | |
| %ile BackOfQ(50%), veh/in | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | | | | | | | | | |
| LnGrp LOS | | | | | | | | | | | | |
| Approach Vol, veh/h | | | | | | | | | | | | |
| Approach Delay, s/veh | | | | | | | | | | | | |
| Approach LOS | | | | | | | | | | | | |
| Timer | | | | | | | | | | | | |
| Assigned Phs | | | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | | | | | | | | | | | | |
| Change Period (Y+Rc), s | | | | | | | | | | | | |
| Max Green Setting (Gmax), s | | | | | | | | | | | | |
| Max Q Clear Time (g_c+11), s | | | | | | | | | | | | |
| Green Ext Time (p_c), s | | | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | | | | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |
| User approved ignoring U-Turning movement. | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | SBL | SBT | SBR |
|----------------------------|------|------|------|
| Lane Configurations | SBT | SBT | SBT |
| Volume (veh/h) | 120 | 126 | 119 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 130 | 137 | 129 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 250 | 283 | 246 |
| Arrive On Green | 0.07 | 0.16 | 0.16 |
| Sat Flow, veh/h | 3408 | 1778 | 1546 |
| Grip Volume(v), veh/h | 130 | 135 | 131 |
| Grip Sat Flow(s), veh/h/ln | 1704 | 1752 | 1572 |
| Q Serve(g, s), s | 1.6 | 3.0 | 3.3 |
| Cycle Q Clear(g, c), s | 1.6 | 3.0 | 3.3 |
| Prop In Lane | 1.00 | 0.98 | |
| Lane Grip Cap(c), veh/h | 250 | 279 | 250 |
| V/C Ratio(X) | 0.52 | 0.48 | 0.52 |
| Avail Cap(c,a), veh/h | 318 | 653 | 586 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.2 | 16.4 | 16.6 |
| Incr Delay (d2), s/veh | 1.7 | 1.3 | 1.7 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.8 | 1.6 | 1.5 |
| LnGrp Delay(d), s/veh | 20.8 | 17.7 | 18.3 |
| LnGrp LOS | C | B | B |
| Approach Vol, veh/h | | 396 | |
| Approach Delay, s/veh | | 18.9 | |
| Approach LOS | | B | |
| Timer | 1 | 2 | 3 |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Laurel Road & Country Hills Road

10/26/2015

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | WBT | WBR | SBL | SBR |
| Volume (veh/h) | 9 | 669 | 675 | 27 | 79 | 11 |
| Number | 7 | 4 | 8 | 18 | 1 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 10 | 727 | 734 | 29 | 86 | 12 |
| Adj No. of Lanes | 1 | 2 | 2 | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 19 | 2465 | 1991 | 79 | 123 | 110 |
| Arrive On Green | 0.01 | 0.70 | 0.58 | 0.58 | 0.07 | 0.07 |
| Sat Flow, veh/h | 1757 | 3597 | 3530 | 136 | 1757 | 1568 |
| Grip Volume(v), veh/h | 10 | 727 | 374 | 389 | 86 | 12 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 1752 | 1821 | 1757 | 1568 |
| Q Serve(g, s), s | 0.2 | 2.7 | 4.0 | 4.0 | 1.7 | 0.3 |
| Cycle Q Clear(g, c), s | 0.2 | 2.7 | 4.0 | 4.0 | 1.7 | 0.3 |
| Prop In Lane | 1.00 | | | 0.07 | 1.00 | 1.00 |
| Lane Grip Cap(c), veh/h | 19 | 2465 | 1015 | 1055 | 123 | 110 |
| V/C Ratio(X) | 0.54 | 0.29 | 0.37 | 0.37 | 0.70 | 0.11 |
| Avail Cap(c,a), veh/h | 398 | 6756 | 2782 | 2890 | 1195 | 1067 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 17.4 | 2.0 | 4.0 | 4.0 | 16.0 | 15.4 |
| Incr Delay (d2), s/veh | 22.0 | 0.1 | 0.2 | 0.2 | 7.0 | 0.4 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.2 | 1.2 | 1.9 | 2.0 | 1.1 | 0.2 |
| LnGrp Delay(d), s/veh | 39.4 | 2.0 | 4.2 | 4.2 | 23.0 | 15.8 |
| LnGrp LOS | D | A | A | A | C | B |
| Approach Vol, veh/h | | 737 | 763 | | 98 | |
| Approach Delay, s/veh | | 2.5 | 4.2 | | 22.2 | |
| Approach LOS | | A | A | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| Assigned Phs | | | | 4 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 28.8 | | 6.5 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 68.0 | | 24.0 |
| Max Q Clear Time (g_c+11), s | | | | 4.7 | | 3.7 |
| Green Ext Time (p_c), s | | | | 15.0 | | 0.2 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 4.5 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Project Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
1: Hillcrest Ave & SR4 WB Ramps

10/26/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|------------------------------|-----|------|------|------|------|-------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 648 | 555 | 876 | 141 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | 1.00 | | | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 704 | 603 | 952 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 977 | 1686 | 1898 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 704 | 603 | 952 | 0 |
| Grip Sat Flow(s),veh/h/ln | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.7 | 1.9 | 8.0 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.7 | 1.9 | 8.0 | 0.0 |
| Prop In Lane | | | 1.00 | | | 0.00 |
| Lane Grp Cap(c), veh/h | | | 977 | 1686 | 1898 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.36 | 0.50 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2705 | 3799 | 4136 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 14.9 | 0.3 | 6.7 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.1 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 4.1 | 0.9 | 3.9 | 0.0 |
| LnGrp Delay(d),s/veh | | | 16.0 | 0.4 | 6.9 | 0.0 |
| LnGrp LOS | | | B | A | A | A |
| Approach Vol, veh/h | | | | 1307 | 952 | |
| Approach Delay, s/veh | | | | 8.8 | 6.9 | |
| Approach LOS | | | | A | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 7 8 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.6 | | | 17.4 | 29.2 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 37.0 | 55.0 |
| Max Q Clear Time (g_c+H1), s | | 3.9 | | | 10.7 | 10.0 |
| Green Ext Time (p_c), s | | 17.0 | | | 2.7 | 15.3 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 8.0 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EBRamps/SR 4 EB Ramps

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------------|-----|------|------|-----|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 122 | 0 | 730 | 0 | 0 | 0 | 0 | 1083 | 398 | 182 | 688 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | | | | | 1.00 | | | | | 1.00 |
| Parking Bus, Adj | | | | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | | | | | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 |
| Adj Flow Rate, veh/h | | | | | | | 128 | 0 | 768 | 0 | 1140 | 724 |
| Adj No. of Lanes | | | | | | | 0 | 1 | 2 | 0 | 3 | 2 |
| Peak Hour Factor | | | | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | | | | | | | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | | | | | 540 | 0 | 848 | 0 | 1539 | 2107 |
| Arrive On Green | | | | | | | 0.31 | 0.00 | 0.31 | 0.00 | 0.42 | 0.13 |
| Sat Flow, veh/h | | | | | | | 1757 | 0 | 2760 | 0 | 3798 | 3597 |
| Grip Volume(v), veh/h | | | | | | | 128 | 0 | 768 | 0 | 1054 | 505 |
| Grip Sat Flow(s),veh/h/ln | | | | | | | 1757 | 0 | 1380 | 0 | 1679 | 1752 |
| Q Serve(g, s), s | | | | | | | 4.8 | 0.0 | 23.3 | 0.0 | 23.0 | 9.3 |
| Cycle Q Clear(g, c), s | | | | | | | 4.8 | 0.0 | 23.3 | 0.0 | 23.0 | 9.3 |
| Prop In Lane | | | | | | | 1.00 | | 1.00 | 0.83 | 1.00 | 0.00 |
| Lane Grp Cap(c), veh/h | | | | | | | 540 | 0 | 848 | 0 | 1422 | 682 |
| V/C Ratio(X) | | | | | | | 0.24 | 0.00 | 0.91 | 0.00 | 0.74 | 0.74 |
| Avail Cap(c,a), veh/h | | | | | | | 584 | 0 | 917 | 0 | 1539 | 738 |
| HCM Platoon Ratio | | | | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | | | | | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | | | | | | | 22.6 | 0.0 | 29.0 | 0.0 | 21.1 | 21.1 |
| Incr Delay (d2), s/veh | | | | | | | 0.2 | 0.0 | 11.9 | 0.0 | 1.8 | 3.7 |
| Initial Q Delay(d3),s/veh | | | | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | | | | | 2.3 | 0.0 | 10.3 | 0.0 | 10.9 | 10.8 |
| LnGrp Delay(d),s/veh | | | | | | | 22.8 | 0.0 | 40.9 | 0.0 | 22.9 | 24.8 |
| LnGrp LOS | | | | | | | C | D | D | C | D | A |
| Approach Vol, veh/h | | | | | | | | 896 | | 1559 | | 916 |
| Approach Delay, s/veh | | | | | | | | 38.3 | | 23.5 | | 16.3 |
| Approach LOS | | | | | | | | D | | C | | B |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | 1 | 2 | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | | 15.5 | 41.0 | | | | | | | | | |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | | | | | | | | | |
| Max Green Setting (Gmax), s | | 19.0 | 40.0 | | | | | | | | | |
| Max Q Clear Time (g_c+H1), s | | 11.3 | 25.0 | | | | | | | | | |
| Green Ext Time (p_c), s | | 0.3 | 11.9 | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | | | | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 27 | 15 | 21 | 229 | 138 | 131 | 27 | 373 | 119 | 189 | 454 | 38 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 28 | 16 | 22 | 241 | 145 | 70 | 28 | 393 | 0 | 199 | 478 | 40 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 419 | 195 | 268 | 523 | 510 | 434 | 47 | 999 | 0 | 266 | 1342 | 112 |
| Arrive On Green | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.03 | 0.28 | 0.00 | 0.15 | 0.41 | 0.41 |
| Sat Flow, veh/h | 1150 | 705 | 969 | 1351 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 3276 | 273 |
| Grip Volume(v), veh/h | 28 | 0 | 38 | 241 | 145 | 70 | 28 | 393 | 0 | 199 | 255 | 263 |
| Grip Sat Flow(s), veh/h/ln | 1150 | 0 | 1674 | 1351 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1796 |
| Q Serve(g, s) | 0.8 | 0.0 | 0.7 | 6.7 | 2.6 | 1.4 | 0.7 | 3.8 | 0.0 | 4.5 | 4.2 | 4.2 |
| Cycle Q Clear(g, c), s | 3.4 | 0.0 | 0.7 | 7.4 | 2.6 | 1.4 | 0.7 | 3.8 | 0.0 | 4.5 | 4.2 | 4.2 |
| Prop In Lane | 1.00 | 0.58 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.15 | 0.15 |
| Lane Grp Cap(c), veh/h | 419 | 0 | 463 | 523 | 510 | 434 | 47 | 999 | 0 | 266 | 718 | 736 |
| V/C Ratio(X) | 0.07 | 0.00 | 0.08 | 0.46 | 0.28 | 0.16 | 0.60 | 0.39 | 0.00 | 0.75 | 0.36 | 0.36 |
| Avail Cap(c,a), veh/h | 1064 | 0 | 1401 | 1280 | 1544 | 1312 | 294 | 2431 | 0 | 1008 | 1928 | 1976 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 13.2 | 0.0 | 11.2 | 13.9 | 11.9 | 11.5 | 20.1 | 12.0 | 0.0 | 17.0 | 8.5 | 8.5 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 0.1 | 0.6 | 0.3 | 0.2 | 11.7 | 0.3 | 0.0 | 4.2 | 0.3 | 0.3 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.3 | 0.0 | 0.3 | 2.6 | 1.3 | 0.6 | 0.5 | 1.8 | 0.0 | 2.5 | 2.0 | 2.1 |
| LnGrp Delay(d), s/veh | 13.3 | 0.0 | 11.3 | 14.6 | 12.2 | 11.6 | 31.9 | 12.3 | 0.0 | 21.2 | 8.8 | 8.8 |
| LnGrp LOS | B | B | B | B | B | B | C | B | C | C | A | A |
| Approach Vol, veh/h | 66 | | | | | 456 | | 421 | | | | 717 |
| Approach Delay, s/veh | 12.1 | | | | | 13.4 | | 13.6 | | | | 12.2 |
| Approach LOS | B | | | | | B | | B | | | | B |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.3 | 15.9 | | 15.6 | 5.1 | 21.1 | | 15.6 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | | 4.0 | | | | |
| Max Green Setting (Gmax), s | 24.0 | 29.0 | | 35.0 | 7.0 | 46.0 | | 35.0 | | | | |
| Max Q Clear Time (g_c+H1), s | 6.5 | 5.8 | | 5.4 | 2.7 | 6.2 | | 9.4 | | | | |
| Green Ext Time (p_c), s | 0.5 | 6.1 | | 2.2 | 0.0 | 6.9 | | 2.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | | 12.9 | | | | | | |
| HCM 2010 LOS | | | | | | B | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/26/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 423 | 48 | 153 | 600 | 102 | 189 |
| Number | 4 | 14 | 3 | 8 | 5 | 12 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 460 | 52 | 166 | 652 | 111 | 103 |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 1296 | 146 | 225 | 2281 | 211 | 188 |
| Arrive On Green | 0.41 | 0.41 | 0.13 | 0.65 | 0.12 | 0.12 |
| Sat Flow, veh/h | 3269 | 358 | 1757 | 3597 | 1757 | 1568 |
| Grip Volume(v), veh/h | 253 | 259 | 166 | 652 | 111 | 103 |
| Grip Sat Flow(s), veh/h/ln | 1752 | 1782 | 1757 | 1752 | 1757 | 1568 |
| Q Serve(g, s) | 3.5 | 3.5 | 3.2 | 2.8 | 2.1 | 2.2 |
| Cycle Q Clear(g, c), s | 3.5 | 3.5 | 3.2 | 2.8 | 2.1 | 2.2 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 715 | 727 | 225 | 2281 | 211 | 188 |
| V/C Ratio(X) | 0.35 | 0.36 | 0.74 | 0.29 | 0.53 | 0.55 |
| Avail Cap(c,a), veh/h | 1606 | 1633 | 1308 | 6224 | 1510 | 1347 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 7.1 | 7.2 | 14.6 | 2.6 | 14.4 | 14.5 |
| Incr Delay (d2), s/veh | 0.3 | 0.3 | 4.6 | 0.1 | 2.0 | 2.5 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 1.7 | 1.8 | 1.8 | 1.3 | 1.1 | 1.1 |
| LnGrp Delay(d), s/veh | 7.4 | 7.5 | 19.3 | 2.7 | 16.5 | 16.9 |
| LnGrp LOS | A | A | B | A | B | B |
| Approach Vol, veh/h | 512 | | | 818 | 214 | |
| Approach Delay, s/veh | 7.5 | | | 6.1 | 16.7 | |
| Approach LOS | A | | | A | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| Assigned Phs | | 2 | 3 | 4 | | 8 |
| Phs Duration (G+Y+Rc), s | | 8.2 | 8.5 | 18.2 | | 26.7 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | 30.0 | 26.0 | 32.0 | | 62.0 |
| Max Q Clear Time (g_c+H1), s | | 4.2 | 5.2 | 5.5 | | 4.8 |
| Green Ext Time (p_c), s | | 0.6 | 0.4 | 8.7 | | 10.2 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | | 8.0 | | |
| HCM 2010 LOS | | | | A | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 602 | 42 | 0 | 946 | 360 | 0 | 0 | 0 | 896 | 2 | 417 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 654 | 46 | 0 | 1028 | 0 | 0 | 1028 | 0 | 975 | 0 | 453 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1639 | 115 | 0 | 1729 | 0 | 0 | 1729 | 0 | 1340 | 0 | 598 |
| Arrive On Green | 0.00 | 0.49 | 0.49 | 0.00 | 0.49 | 0.00 | 0.00 | 0.49 | 0.00 | 0.38 | 0.00 | 0.38 |
| Sat Flow, veh/h | 0 | 3415 | 233 | 0 | 3689 | 0 | 0 | 3689 | 0 | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 345 | 355 | 0 | 1028 | 0 | 0 | 1028 | 0 | 975 | 0 | 453 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1803 | 0 | 1752 | 0 | 0 | 1752 | 0 | 1568 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 7.9 | 7.9 | 0.0 | 13.4 | 0.0 | 0.0 | 13.4 | 0.0 | 15.2 | 0.0 | 16.0 |
| Cycle Q Clear(g, c), s | 0.0 | 7.9 | 7.9 | 0.0 | 13.4 | 0.0 | 0.0 | 13.4 | 0.0 | 15.2 | 0.0 | 16.0 |
| Prop In Lane | 0.00 | 0.13 | 0.00 | 0.00 | 0.13 | 0.00 | 0.00 | 0.13 | 0.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 864 | 890 | 0 | 1729 | 0 | 0 | 1729 | 0 | 1340 | 0 | 598 |
| V/C Ratio(X) | 0.00 | 0.40 | 0.40 | 0.00 | 0.59 | 0.00 | 0.00 | 0.59 | 0.00 | 0.73 | 0.00 | 0.76 |
| Avail Cap(c,a), veh/h | 0 | 1346 | 1385 | 0 | 2692 | 0 | 0 | 2692 | 0 | 2369 | 0 | 1057 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 10.2 | 10.2 | 0.0 | 11.6 | 0.0 | 0.0 | 11.6 | 0.0 | 16.9 | 0.0 | 17.2 |
| Incr Delay (d2), s/veh | 0.0 | 0.3 | 0.3 | 0.0 | 0.3 | 0.0 | 0.0 | 0.3 | 0.0 | 0.8 | 0.0 | 2.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 3.9 | 4.0 | 0.0 | 6.5 | 0.0 | 0.0 | 6.5 | 0.0 | 7.5 | 0.0 | 7.3 |
| LnGrp Delay(d),s/veh | 0.0 | 10.5 | 10.5 | 0.0 | 11.9 | 0.0 | 0.0 | 11.9 | 0.0 | 17.7 | 0.0 | 19.2 |
| LnGrp LOS | B | B | B | B | B | B | B | B | B | B | B | B |
| Approach Vol, veh/h | 700 | | | 1028 | | | 1428 | | | 181 | | |
| Approach Delay, s/veh | 10.5 | | | 11.9 | | | 18.1 | | | B | | |
| Approach LOS | B | | | B | | | B | | | B | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|---|---|------|---|------|---|------|
| Assigned Phs | | | | 4 | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 35.5 | | 28.3 | | 35.5 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 49.0 | | 43.0 | | 49.0 |
| Max Q Clear Time (g_c+H1), s | | | | 9.9 | | 18.0 | | 15.4 |
| Green Ext Time (p_c), s | | | | 17.1 | | 6.3 | | 16.0 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 14.4 | | | | | | | |
| HCM 2010 LOS | B | | | | | | | |
| Notes | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 98 | 1399 | 0 | 0 | 1265 | 465 | 128 | 0 | 497 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 107 | 1521 | 0 | 0 | 1375 | 0 | 139 | 0 | 540 | | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 128 | 1924 | 0 | 0 | 1524 | 682 | 646 | 0 | 577 | | | |
| Arrive On Green | 0.07 | 0.55 | 0.00 | 0.00 | 0.43 | 0.00 | 0.37 | 0.00 | 0.37 | | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | | |
| Grip Volume(v), veh/h | 107 | 1521 | 0 | 0 | 1375 | 0 | 139 | 0 | 540 | | | |
| Grip Sat Flow(s),veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | | |
| Q Serve(g, s) | 5.8 | 33.3 | 0.0 | 0.0 | 35.1 | 0.0 | 5.2 | 0.0 | 31.9 | | | |
| Cycle Q Clear(g, c), s | 5.8 | 33.3 | 0.0 | 0.0 | 35.1 | 0.0 | 5.2 | 0.0 | 31.9 | | | |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 128 | 1924 | 0 | 0 | 1524 | 682 | 646 | 0 | 577 | | | |
| V/C Ratio(X) | 0.84 | 0.79 | 0.00 | 0.00 | 0.90 | 0.00 | 0.22 | 0.00 | 0.94 | | | |
| Avail Cap(c,a), veh/h | 128 | 1931 | 0 | 0 | 1530 | 685 | 712 | 0 | 636 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 44.0 | 17.3 | 0.0 | 0.0 | 25.3 | 0.0 | 20.9 | 0.0 | 29.3 | | | |
| Incr Delay (d2), s/veh | 36.1 | 2.3 | 0.0 | 0.0 | 7.8 | 0.0 | 0.2 | 0.0 | 20.5 | | | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%), veh/ln | 4.1 | 16.5 | 0.0 | 0.0 | 18.5 | 0.0 | 2.6 | 0.0 | 17.1 | | | |
| LnGrp Delay(d),s/veh | 80.1 | 19.6 | 0.0 | 0.0 | 33.1 | 0.0 | 21.0 | 0.0 | 49.8 | | | |
| LnGrp LOS | F | B | B | B | C | C | C | C | D | | | |
| Approach Vol, veh/h | 1628 | | | 1375 | | | 679 | | | | | |
| Approach Delay, s/veh | 23.6 | | | 33.1 | | | 43.9 | | | | | |
| Approach LOS | C | | | C | | | D | | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|---|------|---|------|---|------|
| Assigned Phs | | 2 | | 4 | | 7 | | 8 |
| Phs Duration (G+Y+Rc), s | | 39.4 | | 56.8 | | 11.0 | | 45.8 |
| Change Period (Y+Rc), s | | 4.0 | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | 39.0 | | 53.0 | | 7.0 | | 42.0 |
| Max Q Clear Time (g_c+H1), s | | 33.9 | | 35.3 | | 7.8 | | 37.1 |
| Green Ext Time (p_c), s | | 1.4 | | 16.2 | | 0.0 | | 4.7 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 30.9 | | | | | | | |
| HCM 2010 LOS | C | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1415 | 497 | 120 | 1383 | 0 | 0 | 0 | 0 | 461 | 2 | 374 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1489 | 523 | 126 | 1456 | 0 | 1489 | 523 | 126 | 1456 | 0 | 394 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | 3 | 1 | 2 | 3 | 0 | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2467 | 789 | 200 | 3016 | 0 | 2467 | 789 | 200 | 3016 | 0 | 471 |
| Arrive On Green | 0.00 | 0.49 | 0.49 | 0.06 | 0.60 | 0.00 | 0.49 | 0.49 | 0.06 | 0.60 | 0.00 | 0.30 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | 5202 | 1568 | 3408 | 5202 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1489 | 523 | 126 | 1456 | 0 | 1489 | 523 | 126 | 1456 | 0 | 394 |
| Grip Sat Flow(s), veh/h | 0 | 1679 | 1568 | 1704 | 1679 | 0 | 1679 | 1568 | 1704 | 1679 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 17.0 | 20.3 | 2.9 | 13.0 | 0.0 | 17.0 | 20.3 | 2.9 | 13.0 | 0.0 | 18.7 |
| Cycle Q Clear(g, c), s | 0.0 | 17.0 | 20.3 | 2.9 | 13.0 | 0.0 | 17.0 | 20.3 | 2.9 | 13.0 | 0.0 | 18.7 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2467 | 789 | 200 | 3016 | 0 | 2467 | 789 | 200 | 3016 | 0 | 471 |
| V/C Ratio(X) | 0.00 | 0.60 | 0.68 | 0.63 | 0.48 | 0.00 | 0.60 | 0.68 | 0.63 | 0.48 | 0.00 | 0.84 |
| Avail Cap(c.a), veh/h | 0 | 2534 | 789 | 343 | 3294 | 0 | 2534 | 789 | 343 | 3294 | 0 | 789 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 14.7 | 15.5 | 36.6 | 9.0 | 0.0 | 14.7 | 15.5 | 36.6 | 9.0 | 0.0 | 26.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.4 | 2.3 | 3.3 | 0.1 | 0.0 | 0.4 | 2.3 | 3.3 | 0.1 | 0.0 | 4.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 7.9 | 9.2 | 1.4 | 6.0 | 0.0 | 7.9 | 9.2 | 1.4 | 6.0 | 0.0 | 8.6 |
| LnGrp Delay(d), s/veh | 0.0 | 15.1 | 17.8 | 39.8 | 9.1 | 0.0 | 15.1 | 17.8 | 39.8 | 9.1 | 0.0 | 30.0 |
| LnGrp LOS | B | B | B | D | A | B | B | B | B | D | C | C |
| Approach Vol, veh/h | 2012 | | | 1582 | | | 880 | | | 880 | | |
| Approach Delay, s/veh | 15.8 | | | 11.6 | | | 26.1 | | | 26.1 | | |
| Approach LOS | B | | | B | | | C | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|-----|------|------|------|------|------|------|------|
| Assigned Phs | 3 | 4 | 4 | 4 | 6 | 6 | 8 | 8 |
| Phs Duration (G+Y+Rc), s | 8.7 | 42.9 | 27.9 | 27.9 | 51.6 | 51.6 | 51.6 | 51.6 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 8.0 | 40.0 | 40.0 | 40.0 | 52.0 | 52.0 | 52.0 | 52.0 |
| Max Q Clear Time (g_c+H1), s | 4.9 | 22.3 | 20.7 | 20.7 | 15.0 | 15.0 | 15.0 | 15.0 |
| Green Ext Time (p_c), s | 0.1 | 16.6 | 3.2 | 3.2 | 32.6 | 32.6 | 32.6 | 32.6 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 16.3 |
| HCM 2010 LOS | B |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1611 | 265 | 20 | 5 | 982 | 384 | 539 | 29 | 189 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1696 | 153 | 5 | 1034 | 404 | 589 | 0 | 199 | 0 | 199 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 3028 | 943 | 9 | 3343 | 1041 | 780 | 0 | 348 | 0 | 348 | 0 |
| Arrive On Green | 0.00 | 0.60 | 0.60 | 0.01 | 0.66 | 0.66 | 0.22 | 0.00 | 0.22 | 0.00 | 0.22 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 1696 | 153 | 5 | 1034 | 404 | 589 | 0 | 199 | 0 | 199 | 0 |
| Grip Sat Flow(s), veh/h | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s), s | 0.0 | 14.2 | 3.0 | 0.2 | 6.1 | 8.2 | 11.0 | 0.0 | 7.9 | 0.0 | 7.9 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 14.2 | 3.0 | 0.2 | 6.1 | 8.2 | 11.0 | 0.0 | 7.9 | 0.0 | 7.9 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 3028 | 943 | 9 | 3343 | 1041 | 780 | 0 | 348 | 0 | 348 | 0 |
| V/C Ratio(X) | 0.00 | 0.56 | 0.16 | 0.54 | 0.31 | 0.39 | 0.76 | 0.00 | 0.57 | 0.00 | 0.57 | 0.00 |
| Avail Cap(c.a), veh/h | 0 | 3028 | 943 | 552 | 4679 | 1457 | 1356 | 0 | 605 | 0 | 605 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 8.4 | 6.2 | 34.7 | 5.0 | 5.3 | 25.4 | 0.0 | 24.3 | 0.0 | 24.3 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.1 | 40.7 | 0.1 | 0.2 | 1.5 | 0.0 | 1.5 | 0.0 | 1.5 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 6.5 | 1.3 | 0.2 | 2.8 | 3.5 | 5.5 | 0.0 | 3.5 | 0.0 | 3.5 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 8.6 | 6.2 | 75.4 | 5.0 | 5.6 | 27.0 | 0.0 | 25.7 | 0.0 | 25.7 | 0.0 |
| LnGrp LOS | A | A | A | E | A | A | C | C | C | C | C | C |
| Approach Vol, veh/h | 1849 | | | 1443 | | | 788 | | | 788 | | |
| Approach Delay, s/veh | 8.4 | | | 5.4 | | | 26.7 | | | 26.7 | | |
| Approach LOS | A | | | A | | | C | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|------|------|------|------|------|------|
| Assigned Phs | 2 | 3 | 4 | 4 | 4 | 4 | 8 | 8 |
| Phs Duration (G+Y+Rc), s | 19.5 | 4.4 | 46.1 | 46.1 | 50.4 | 50.4 | 50.4 | 50.4 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 27.0 | 22.0 | 39.0 | 39.0 | 65.0 | 65.0 | 65.0 | 65.0 |
| Max Q Clear Time (g_c+H1), s | 13.0 | 2.2 | 16.2 | 16.2 | 10.2 | 10.2 | 10.2 | 10.2 |
| Green Ext Time (p_c), s | 2.6 | 0.0 | 19.8 | 19.8 | 36.3 | 36.3 | 36.3 | 36.3 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 10.9 |
| HCM 2010 LOS | B |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/26/2015

| Movement | SBR |
|------------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s), veh/h/ln | |
| Q Serve(g, s) | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grip Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c,a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(l) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |
| Timer | |
| Assigned Phs | |
| Phs Duration (G+Y+Rc), s | |
| Change Period (Y+Rc), s | |
| Max Green Setting (Gmax), s | |
| Max Q Clear Time (g_c+H1), s | |
| Green Ext Time (p_c), s | |

User approved ignoring U-Turning movement.

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 101 | 240 | 810 | 95 | 90 | 749 | 157 | 16 | 94 | 94 | 37 | 59 |
| Number | | 7 | 4 | 14 | 3 | 8 | 18 | | 5 | 2 | 12 | |
| Initial Q (Qb), veh | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | | 253 | 853 | 52 | 95 | 788 | 86 | | 99 | 99 | 20 | |
| Adj No. of Lanes | | 1 | 3 | 1 | 1 | 3 | 1 | | 2 | 1 | 1 | 1 |
| Peak Hour Factor | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | | 3 | 3 | 3 | 3 | 3 | 3 | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | 320 | 2079 | 647 | 123 | 1514 | 471 | | 191 | 235 | 200 | |
| Arrive On Green | | 0.18 | 0.41 | 0.07 | 0.30 | 0.30 | 0.30 | | 0.06 | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | | 3408 | 1845 | 1568 | 1568 |
| Gp Volume(v), veh/h | | 253 | 853 | 52 | 95 | 788 | 86 | | 99 | 99 | 20 | |
| Gp Sat Flow(s),veh/h/ln | | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | | 1704 | 1845 | 1568 | 1568 |
| Q Served, s | | 7.7 | 6.7 | 1.1 | 3.0 | 7.3 | 2.3 | | 1.6 | 2.8 | 0.6 | |
| Cycle Q Clear(g_c), s | | 7.7 | 6.7 | 1.1 | 3.0 | 7.3 | 2.3 | | 1.6 | 2.8 | 0.6 | |
| Prop In Lane | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | | 320 | 2079 | 647 | 123 | 1514 | 471 | | 191 | 235 | 200 | |
| V/C Ratio(X) | | 0.79 | 0.41 | 0.08 | 0.77 | 0.52 | 0.18 | | 0.52 | 0.42 | 0.10 | |
| Avail Cap(c,a), veh/h | | 1378 | 4308 | 1341 | 376 | 1514 | 471 | | 364 | 559 | 475 | |
| HCM Platoon Ratio | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | | 21.9 | 11.6 | 10.0 | 25.7 | 16.3 | 14.5 | | 25.7 | 22.6 | 21.6 | |
| Incr Delay (d2), s/veh | | 4.4 | 0.1 | 0.1 | 9.8 | 0.3 | 0.2 | | 2.2 | 1.2 | 0.2 | |
| Initial Q Delay(d3),s/veh | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | | 4.1 | 3.1 | 0.5 | 1.8 | 3.4 | 1.0 | | 0.8 | 1.5 | 0.3 | |
| LnGrp Delay(d),s/veh | | 26.3 | 11.8 | 10.1 | 35.5 | 16.6 | 14.7 | | 27.9 | 23.8 | 21.9 | |
| LnGrp LOS | | C | B | B | D | B | B | | C | C | C | C |
| Approach Vol, veh/h | | 1158 | | | 969 | | | 218 | | | | |
| Approach Delay, s/veh | | 14.9 | | | 18.3 | | | 25.5 | | | | |
| Approach LOS | | B | | | B | | | C | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 9.9 | 11.1 | 7.9 | 27.2 | 7.1 | 13.9 | 14.2 | 20.9 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 7.0 | 17.0 | 12.0 | 48.0 | 6.0 | 18.0 | 44.0 | 16.0 | | | | |
| Max Q Clear Time (g_c+H1), s | 5.9 | 4.8 | 5.0 | 8.7 | 3.6 | 7.9 | 9.7 | 9.3 | | | | |
| Green Ext Time (p_c), s | 0.1 | 2.2 | 0.1 | 14.5 | 0.1 | 2.0 | 0.7 | 5.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 18.9 | | | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | SBL | SBT | SBR |
|----------------------------|------|------|------|
| Lane Configurations | SB | TT | |
| Volume (veh/h) | 234 | 194 | 155 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 246 | 204 | 163 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 357 | 334 | 254 |
| Arrive On Green | 0.10 | 0.18 | 0.18 |
| Sat Flow, veh/h | 3408 | 1900 | 1443 |
| Grip Volume(v), veh/h | 246 | 187 | 180 |
| Grip Sat Flow(s), veh/h/ln | 1704 | 1752 | 1590 |
| Q Serve(g, s), s | 3.9 | 5.5 | 5.9 |
| Cycle Q Clear(g, c), s | 3.9 | 5.5 | 5.9 |
| Prop In Lane | 1.00 | | 0.91 |
| Lane Grp Cap(c), veh/h | 357 | 308 | 280 |
| V/C Ratio(X) | 0.69 | 0.61 | 0.64 |
| Avail Cap(c.a), veh/h | 425 | 562 | 510 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 24.2 | 21.3 | 21.5 |
| Incr Delay (d2), s/veh | 3.7 | 1.9 | 2.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 2.0 | 2.8 | 2.8 |
| LnGrp Delay(d),s/veh | 27.9 | 23.3 | 23.9 |
| LnGrp LOS | C | C | C |
| Approach Vol, veh/h | | 613 | |
| Approach Delay, s/veh | | 25.3 | |
| Approach LOS | | C | |
| Timer | 1 | 2 | 3 |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Laurel Road & Country Hills Road

10/26/2015

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|----------------------------|------|------|------|------|------|------|
| Lane Configurations | TT | TT | TT | TT | TT | TT |
| Volume (veh/h) | 24 | 589 | 1141 | 94 | 55 | 7 |
| Number | 7 | 4 | 8 | 18 | 1 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 26 | 640 | 1240 | 102 | 60 | 8 |
| Adj No. of Lanes | 1 | 2 | 2 | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 42 | 2793 | 2281 | 187 | 85 | 76 |
| Arrive On Green | 0.02 | 0.80 | 0.70 | 0.70 | 0.05 | 0.05 |
| Sat Flow, veh/h | 1757 | 3597 | 3373 | 269 | 1757 | 1568 |
| Grip Volume(v), veh/h | 26 | 640 | 661 | 681 | 60 | 8 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 1752 | 1797 | 1757 | 1568 |
| Q Serve(g, s), s | 0.8 | 2.3 | 9.5 | 9.6 | 1.7 | 0.3 |
| Cycle Q Clear(g, c), s | 0.8 | 2.3 | 9.5 | 9.6 | 1.7 | 0.3 |
| Prop In Lane | 1.00 | | | 0.15 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 42 | 2793 | 1219 | 1250 | 85 | 76 |
| V/C Ratio(X) | 0.61 | 0.23 | 0.54 | 0.54 | 0.71 | 0.11 |
| Avail Cap(c.a), veh/h | 238 | 5224 | 2239 | 2296 | 510 | 455 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 25.0 | 1.3 | 3.9 | 3.9 | 24.2 | 23.5 |
| Incr Delay (d2), s/veh | 13.5 | 0.0 | 0.4 | 0.4 | 10.3 | 0.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.5 | 1.1 | 4.5 | 4.7 | 1.1 | 0.2 |
| LnGrp Delay(d),s/veh | 38.5 | 1.3 | 4.2 | 4.2 | 34.5 | 24.1 |
| LnGrp LOS | D | A | A | A | C | C |
| Approach Vol, veh/h | | 666 | 1342 | | 68 | |
| Approach Delay, s/veh | | 2.8 | 4.2 | | 33.3 | |
| Approach LOS | | A | A | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 |

Laurel Ranch Traffic Impact Analysis
PM Existing Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

1: Hillcrest Ave & SR4 Ramps

10/26/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------------|-----|------|------|------|------|-------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 655 | 650 | 817 | 124 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 712 | 707 | 888 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 987 | 1687 | 1891 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 712 | 707 | 888 | 0 |
| Grip Sat Flow(s),veh/h/ln | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.8 | 2.5 | 7.3 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.8 | 2.5 | 7.3 | 0.0 |
| Prop In Lane | | | 1.00 | | | |
| Lane Grp Cap(c), veh/h | | | 987 | 1687 | 1891 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.42 | 0.47 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2841 | 3785 | 3970 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 14.9 | 0.3 | 6.6 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.2 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 4.2 | 1.1 | 3.5 | 0.0 |
| LnGrp Delay(d),s/veh | | | 15.9 | 0.4 | 6.8 | 0.0 |
| LnGrp LOS | | | B | A | A | |
| Approach Vol, veh/h | | | | 1419 | 888 | |
| Approach Delay, s/veh | | | | 8.2 | 6.8 | |
| Approach LOS | | | | A | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 7 8 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.8 | | | 17.5 | 29.2 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 39.0 | 53.0 |
| Max Q Clear Time (g, c+H1), s | | 4.5 | | | 10.8 | 9.3 |
| Green Ext Time (p, c), s | | 18.1 | | | 2.8 | 15.9 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 7.7 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

2: Hillcrest Ave & SR 4 Ramps

10/26/2015











| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 142 | 1 | 687 | 0 | 0 | 0 | 0 | 1161 | 395 | 168 | 637 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1900 | | | | 1845 | | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | | | 154 | | | | 1747 | | 1262 | 429 | 183 | 692 |
| Adj No. of Lanes | | | 0 | | | | 1 | | 3 | 0 | 1 | 2 |
| Peak Hour Factor | | | 0.92 | | | | 0.92 | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | | | | 0 | | 3 | 3 | 3 | 0 |
| Cap. veh/h | | | 510 | | | | 3 | | 1666 | 565 | 221 | 2167 |
| Arrive On Green | | | 0.29 | | | | 0.29 | | 0.00 | 0.45 | 0.13 | 0.82 |
| Sat Flow, veh/h | | | 1746 | | | | 11 | | 3885 | 1261 | 1757 | 3597 |
| Grip Volume(v), veh/h | | | 155 | | | | 0 | | 1139 | 552 | 183 | 692 |
| Grip Sat Flow(s),veh/h/ln | | | 1757 | | | | 0 | | 1679 | 1622 | 1757 | 1752 |
| Q Serve(g, s), s | | | 6.1 | | | | 0.0 | | 25.4 | 25.5 | 9.1 | 8.4 |
| Cycle Q Clear(g, c), s | | | 6.1 | | | | 0.0 | | 25.4 | 25.5 | 9.1 | 8.4 |
| Prop In Lane | | | 0.99 | | | | 1.00 | | 0.00 | 0.78 | 1.00 | 0.00 |
| Lane Grp Cap(c), veh/h | | | 514 | | | | 0 | | 1504 | 727 | 221 | 2167 |
| V/C Ratio(X) | | | 0.30 | | | | 0.00 | | 0.76 | 0.76 | 0.83 | 0.32 |
| Avail Cap(c,a), veh/h | | | 530 | | | | 0 | | 1611 | 779 | 353 | 2543 |
| HCM Platoon Ratio | | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | | | | 0.00 | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 24.6 | | | | 0.0 | | 20.6 | 20.7 | 38.2 | 8.1 |
| Incr Delay (d2), s/veh | | | 0.3 | | | | 0.0 | | 2.0 | 4.1 | 8.7 | 0.1 |
| Initial Q Delay(d3),s/veh | | | 0.0 | | | | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 3.0 | | | | 0.0 | | 12.1 | 12.2 | 5.0 | 4.1 |
| LnGrp Delay(d),s/veh | | | 24.9 | | | | 0.0 | | 22.6 | 24.8 | 47.0 | 8.2 |
| LnGrp LOS | | | C | | | | D | | C | C | D | A |
| Approach Vol, veh/h | | | | | | | 902 | | 1891 | | | 875 |
| Approach Delay, s/veh | | | | | | | 42.9 | | 23.3 | | | 16.3 |
| Approach LOS | | | | | | | D | | C | | | B |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 15.2 | 44.1 | | 30.2 | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | | | | | | | |
| Max Green Setting (Gmax), s | 18.0 | 43.0 | | 27.0 | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 11.1 | 27.5 | | 25.5 | | | | | | | | |
| Green Ext Time (p, c), s | 0.3 | 12.6 | | 0.7 | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 26.6 | | | | | | | | |
| HCM 2010 LOS | | | | C | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/26/2015

| Movement | EBL | EBT | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------------|---|---|---|---|---|---|---|---|---|---|
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |
| Volume (veh/h) | 79 | 59 | 55 | 174 | 40 | 196 | 64 | 334 | 142 | 183 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 86 | 64 | 60 | 189 | 43 | 133 | 70 | 363 | 0 | 199 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 2 | 0 | 1 | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 501 | 258 | 242 | 468 | 542 | 461 | 93 | 954 | 0 | 263 |
| Arrive On Green | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | 0.05 | 0.27 | 0.00 | 0.15 |
| Sat Flow, veh/h | 1192 | 877 | 822 | 1250 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 |
| Grp Volume(v), veh/h | 86 | 0 | 124 | 189 | 43 | 133 | 70 | 363 | 0 | 199 |
| Grp Sat Flow(s), veh/h/ln | 1192 | 0 | 1700 | 1250 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 |
| Q Serve(g, s), s | 2.4 | 0.0 | 2.3 | 5.7 | 0.7 | 2.8 | 1.7 | 3.5 | 0.0 | 4.6 |
| Cycle Q Clear(g, c), s | 3.1 | 0.0 | 2.3 | 8.1 | 0.7 | 2.8 | 1.7 | 3.5 | 0.0 | 4.6 |
| Prop In Lane | 1.00 | 0.48 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.41 |
| Lane Grp Cap(c), veh/h | 501 | 0 | 499 | 468 | 542 | 461 | 93 | 954 | 0 | 263 |
| V/C Ratio(X) | 0.17 | 0.00 | 0.25 | 0.40 | 0.08 | 0.29 | 0.75 | 0.38 | 0.00 | 0.76 |
| Avail Cap(c, a), veh/h | 998 | 0 | 1208 | 989 | 1311 | 1115 | 708 | 3322 | 0 | 749 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 11.9 | 0.0 | 11.4 | 14.4 | 10.8 | 11.5 | 19.7 | 12.5 | 0.0 | 17.2 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 0.3 | 0.6 | 0.1 | 0.3 | 11.4 | 0.3 | 0.0 | 4.4 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.8 | 0.0 | 1.1 | 2.0 | 0.4 | 1.2 | 1.1 | 1.7 | 0.0 | 2.5 |
| LnGrp Delay(d), s/veh | 12.0 | 0.0 | 11.6 | 15.0 | 10.8 | 11.8 | 31.1 | 12.7 | 0.0 | 21.6 |
| LnGrp LOS | B | B | B | B | B | C | B | C | A | B |
| Approach Vol, veh/h | 210 | | 365 | | 433 | | 649 | | 649 | |
| Approach Delay, s/veh | 11.8 | | 13.4 | | 15.7 | | 13.6 | | 13.6 | |
| Approach LOS | B | | B | | B | | B | | B | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | |
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 6 | 8 | | | |
| Phs Duration (G+Y+Rc), s | 10.3 | 15.5 | 16.4 | 6.2 | 19.6 | 16.4 | 16.4 | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Max Green Setting (Gmax), s | 18.0 | 40.0 | 30.0 | 17.0 | 41.0 | 30.0 | 30.0 | | | |
| Max Q Clear Time (g_c+H1), s | 6.6 | 5.5 | 5.1 | 3.7 | 6.0 | 10.1 | 10.1 | | | |
| Green Ext Time (p_c), s | 0.4 | 5.9 | 2.4 | 0.1 | 6.0 | 2.3 | 2.3 | | | |
| Intersection Summary | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 13.8 | | | | | | | | | |
| HCM 2010 LOS | B | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/26/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
|-----------------------------|------|------|-----------|------|------|------|------|
| Lane Configurations | ↖↗ | ↖ | ↖ | ↖↗ | ↖ | ↖ | ↖↗ |
| Volume (veh/h) | 483 | 66 | 194 | 510 | 113 | 240 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Ob), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | | | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 525 | 72 | 211 | 554 | 123 | 131 | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 1206 | 165 | 284 | 2293 | 246 | 219 | |
| Arrive On Green | 0.39 | 0.39 | 0.16 | 0.65 | 0.14 | 0.14 | |
| Sat Flow, veh/h | 3191 | 424 | 1757 | 3597 | 1757 | 1568 | |
| Gp Volume(v), veh/h | 296 | 301 | 211 | 554 | 123 | 131 | |
| Gp Sat Flow(s),veh/h/ln | 1752 | 1770 | 1757 | 1752 | 1757 | 1568 | |
| Q Serve(g,s), s | 4.8 | 4.9 | 4.4 | 2.5 | 2.5 | 3.0 | |
| Cycle Q Clear(g, c), s | 4.8 | 4.9 | 4.4 | 2.5 | 2.5 | 3.0 | |
| Prop In Lane | 0.24 | 1.00 | | | | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 682 | 689 | 284 | 2293 | 246 | 219 | |
| V/C Ratio(X) | 0.43 | 0.44 | 0.74 | 0.24 | 0.50 | 0.60 | |
| Avail Cap(c,a), veh/h | 1399 | 1413 | 1221 | 5595 | 1357 | 1211 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 8.7 | 8.7 | 15.5 | 2.8 | 15.4 | 15.7 | |
| Incr Delay (d2), s/veh | 0.4 | 0.4 | 3.8 | 0.1 | 1.6 | 2.6 | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%),veh/ln | 2.4 | 2.4 | 2.4 | 1.2 | 1.3 | 1.4 | |
| LnGrp Delay(d),s/veh | 9.2 | 9.2 | 19.3 | 2.8 | 17.0 | 18.3 | |
| LnGrp LOS | A | A | B | A | B | B | |
| Approach Vol, veh/h | 597 | | 765 | | 254 | | |
| Approach Delay, s/veh | 9.2 | | 7.4 | | 17.7 | | |
| Approach LOS | A | | A | | B | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 8 |
| Assigned Phs | 2 | | 3 4 | | 8 | | |
| Phs Duration (G+Y+Rc), s | 9.4 | | 10.3 19.1 | | 29.4 | | |
| Change Period (Y+Rc), s | 4.0 | | 4.0 4.0 | | 4.0 | | |
| Max Green Setting (Gmax), s | 30.0 | | 27.0 31.0 | | 62.0 | | |
| Max Q Clear Time (g_c+1), s | 5.0 | | 6.4 6.9 | | 4.5 | | |
| Green Ext Time (p_c), s | 0.8 | | 0.6 8.3 | | 9.9 | | |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | 9.6 | | | | | | |
| HCM 2010 LOS | A | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

5: SR 4 On-Ramps/SR 4 Off-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 732 | 85 | 0 | 623 | 487 | 0 | 0 | 0 | 450 | 1 | 168 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 0 | 1845 | 1900 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 796 | 92 | 0 | 677 | 0 | 0 | 677 | 0 | 490 | 0 | 183 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1812 | 209 | 0 | 2005 | 0 | 0 | 2005 | 0 | 821 | 0 | 366 |
| Arrive On Green | 0.00 | 0.57 | 0.00 | 0.00 | 0.57 | 0.00 | 0.00 | 0.57 | 0.00 | 0.23 | 0.00 | 0.23 |
| Sat Flow, veh/h | 0 | 3259 | 366 | 0 | 3689 | 0 | 0 | 3689 | 0 | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 440 | 448 | 0 | 677 | 0 | 0 | 677 | 0 | 490 | 0 | 183 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1752 | 1780 | 0 | 1752 | 0 | 0 | 1752 | 0 | 1757 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 5.9 | 5.9 | 0.0 | 4.2 | 0.0 | 0.0 | 4.2 | 0.0 | 5.1 | 0.0 | 4.2 |
| Cycle Q Clear(g, c), s | 0.0 | 5.9 | 5.9 | 0.0 | 4.2 | 0.0 | 0.0 | 4.2 | 0.0 | 5.1 | 0.0 | 4.2 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 1003 | 1018 | 0 | 2005 | 0 | 0 | 2005 | 0 | 821 | 0 | 366 |
| V/C Ratio(X) | 0.00 | 0.44 | 0.44 | 0.00 | 0.34 | 0.00 | 0.00 | 0.34 | 0.00 | 0.60 | 0.00 | 0.50 |
| Avail Cap(c,a), veh/h | 0 | 2469 | 2508 | 0 | 4937 | 0 | 0 | 4937 | 0 | 2901 | 0 | 1295 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 5.0 | 5.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.7 | 0.0 | 14.1 | 0.0 | 13.7 |
| Incr Delay (d2), s/veh | 0.0 | 0.3 | 0.3 | 0.0 | 0.1 | 0.0 | 0.0 | 0.1 | 0.0 | 0.7 | 0.0 | 1.1 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 2.9 | 2.9 | 0.0 | 2.0 | 0.0 | 0.0 | 2.0 | 0.0 | 2.5 | 0.0 | 1.9 |
| LnGrp Delay(d), s/veh | 0.0 | 5.3 | 5.3 | 0.0 | 4.8 | 0.0 | 0.0 | 4.8 | 0.0 | 14.8 | 0.0 | 14.7 |
| LnGrp LOS | A | A | A | A | A | A | A | A | A | B | B | B |
| Approach Vol, veh/h | 888 | | | 677 | | | 673 | | | 673 | | |
| Approach Delay, s/veh | 5.3 | | | 4.8 | | | 4.8 | | | 14.8 | | |
| Approach LOS | A | | | A | | | A | | | B | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|-----|---|---|------|---|------|---|------|
| Assigned Phs | | | | 4 | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 27.6 | | 13.6 | | 27.6 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 58.0 | | 34.0 | | 58.0 |
| Max Q Clear Time (g_c+H1), s | | | | 7.9 | | 7.1 | | 6.2 |
| Green Ext Time (p_c), s | | | | 15.6 | | 2.5 | | 15.8 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 8.0 | | | | | | | |
| HCM 2010 LOS | A | | | | | | | |
| Notes | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 Off-Ramps/SR 4 On-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 251 | 931 | 0 | 0 | 1096 | 725 | 29 | 0 | 318 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 273 | 1012 | 0 | 0 | 1191 | 0 | 32 | 0 | 346 | | | |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 315 | 2300 | 0 | 0 | 1506 | 674 | 437 | 0 | 390 | | | |
| Arrive On Green | 0.18 | 0.66 | 0.00 | 0.00 | 0.43 | 0.00 | 0.25 | 0.00 | 0.25 | | | |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | | | |
| Grip Volume(v), veh/h | 273 | 1012 | 0 | 0 | 1191 | 0 | 32 | 0 | 346 | | | |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | | | |
| Q Serve(g, s), s | 12.7 | 11.7 | 0.0 | 0.0 | 24.7 | 0.0 | 1.2 | 0.0 | 17.9 | | | |
| Cycle Q Clear(g, c), s | 12.7 | 11.7 | 0.0 | 0.0 | 24.7 | 0.0 | 1.2 | 0.0 | 17.9 | | | |
| Prop In Lane | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 315 | 2300 | 0 | 0 | 1506 | 674 | 437 | 0 | 390 | | | |
| V/C Ratio(X) | 0.87 | 0.44 | 0.00 | 0.00 | 0.79 | 0.00 | 0.07 | 0.00 | 0.89 | | | |
| Avail Cap(c,a), veh/h | 417 | 2582 | 0 | 0 | 1582 | 708 | 626 | 0 | 559 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 33.6 | 7.0 | 0.0 | 0.0 | 20.7 | 0.0 | 24.2 | 0.0 | 30.5 | | | |
| Incr Delay (d2), s/veh | 13.9 | 0.1 | 0.0 | 0.0 | 2.7 | 0.0 | 0.1 | 0.0 | 11.9 | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%), veh/ln | 7.4 | 5.7 | 0.0 | 0.0 | 12.5 | 0.0 | 0.6 | 0.0 | 9.0 | | | |
| LnGrp Delay(d), s/veh | 47.5 | 7.1 | 0.0 | 0.0 | 23.4 | 0.0 | 24.3 | 0.0 | 42.3 | | | |
| LnGrp LOS | D | A | A | A | C | C | C | D | D | | | |
| Approach Vol, veh/h | 1285 | | | 1191 | | | 378 | | | D | | |
| Approach Delay, s/veh | 15.7 | | | 23.4 | | | 40.8 | | | D | | |
| Approach LOS | B | | | C | | | D | | | D | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|---|------|---|---|------|------|
| Assigned Phs | | 2 | | 4 | | | 7 | 8 |
| Phs Duration (G+Y+Rc), s | | 24.9 | | 59.2 | | | 19.1 | 40.2 |
| Change Period (Y+Rc), s | | 4.0 | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 30.0 | | 62.0 | | | 20.0 | 38.0 |
| Max Q Clear Time (g_c+H1), s | | 19.9 | | 13.7 | | | 14.7 | 26.7 |
| Green Ext Time (p_c), s | | 1.0 | | 28.0 | | | 0.4 | 9.5 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 22.3 | | | | | | | |
| HCM 2010 LOS | C | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 790 | 424 | 95 | 1182 | 0 | 0 | 0 | 0 | 318 | 1 | 353 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A, pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 859 | 472 | 103 | 1285 | 0 | 347 | 0 | 427 | 0 | 427 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | 2 | 0 | 2 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2276 | 709 | 174 | 2824 | 0 | 1139 | 0 | 508 | 0 | 508 | 0 |
| Arrive On Green | 0.00 | 0.45 | 0.45 | 0.05 | 0.56 | 0.00 | 0.32 | 0.00 | 0.32 | 0.00 | 0.32 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 859 | 472 | 103 | 1285 | 0 | 347 | 0 | 427 | 0 | 427 | 0 |
| Grip Sat Flow(s), veh/h | 0 | 1679 | 1568 | 1704 | 1679 | 0 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s) | 0.0 | 7.8 | 16.4 | 2.1 | 10.5 | 0.0 | 5.2 | 0.0 | 17.6 | 0.0 | 17.6 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 7.8 | 16.4 | 2.1 | 10.5 | 0.0 | 5.2 | 0.0 | 17.6 | 0.0 | 17.6 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2276 | 709 | 174 | 2824 | 0 | 1139 | 0 | 508 | 0 | 508 | 0 |
| V/C Ratio(X) | 0.00 | 0.38 | 0.67 | 0.59 | 0.46 | 0.00 | 0.30 | 0.00 | 0.84 | 0.00 | 0.84 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 2462 | 766 | 343 | 3258 | 0 | 2374 | 0 | 1059 | 0 | 1059 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 12.6 | 14.9 | 32.3 | 9.0 | 0.0 | 17.6 | 0.0 | 21.8 | 0.0 | 21.8 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 2.0 | 3.2 | 0.1 | 0.0 | 0.1 | 0.0 | 3.8 | 0.0 | 3.8 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 3.6 | 7.5 | 1.0 | 4.8 | 0.0 | 2.5 | 0.0 | 8.1 | 0.0 | 8.1 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 12.7 | 16.9 | 35.4 | 9.1 | 0.0 | 17.8 | 0.0 | 25.6 | 0.0 | 25.6 | 0.0 |
| LnGrp LOS | B | B | B | D | A | A | B | B | C | B | C | C |
| Approach Vol, veh/h | 1331 | | | 1388 | | | 774 | | | 774 | | |
| Approach Delay, s/veh | 14.2 | | | 11.1 | | | 22.1 | | | 22.1 | | |
| Approach LOS | B | | | B | | | C | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|-----|------|------|------|------|------|------|------|
| Assigned Phs | 3 | 4 | 4 | 4 | 6 | 6 | 8 | 8 |
| Phs Duration (G+Y+Rc), s | 7.6 | 35.4 | 26.6 | 43.0 | 26.6 | 43.0 | 43.0 | 43.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 7.0 | 34.0 | 47.0 | 45.0 | 47.0 | 45.0 | 45.0 | 45.0 |
| Max Q Clear Time (g, c+H1), s | 4.1 | 18.4 | 19.6 | 12.5 | 19.6 | 12.5 | 12.5 | 12.5 |
| Green Ext Time (p, c), s | 0.1 | 13.0 | 3.0 | 23.5 | 3.0 | 23.5 | 23.5 | 23.5 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 14.7 |
| HCM 2010 LOS | B |
| Notes | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 EB On-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 962 | 166 | 8 | 3 | 852 | 311 | 429 | 19 | 138 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A, pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1046 | 90 | 3 | 926 | 338 | 481 | 0 | 147 | 0 | 147 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2776 | 864 | 6 | 3188 | 993 | 737 | 0 | 329 | 0 | 329 | 0 |
| Arrive On Green | 0.00 | 0.55 | 0.55 | 0.00 | 0.63 | 0.63 | 0.21 | 0.00 | 0.21 | 0.00 | 0.21 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 1046 | 90 | 3 | 926 | 338 | 481 | 0 | 147 | 0 | 147 | 0 |
| Grip Sat Flow(s), veh/h | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s) | 0.0 | 6.0 | 1.4 | 0.1 | 4.2 | 5.1 | 6.4 | 0.0 | 4.2 | 0.0 | 4.2 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 6.0 | 1.4 | 0.1 | 4.2 | 5.1 | 6.4 | 0.0 | 4.2 | 0.0 | 4.2 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2776 | 864 | 6 | 3188 | 993 | 737 | 0 | 329 | 0 | 329 | 0 |
| V/C Ratio(X) | 0.00 | 0.38 | 0.10 | 0.52 | 0.29 | 0.34 | 0.65 | 0.00 | 0.45 | 0.00 | 0.45 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 4152 | 1293 | 207 | 5141 | 1601 | 2759 | 0 | 1231 | 0 | 1231 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 6.5 | 5.4 | 25.3 | 4.2 | 4.4 | 18.4 | 0.0 | 17.5 | 0.0 | 17.5 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.1 | 0.1 | 38.5 | 0.0 | 0.2 | 1.0 | 0.0 | 1.0 | 0.0 | 1.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 2.7 | 0.6 | 0.1 | 1.9 | 2.2 | 3.2 | 0.0 | 1.9 | 0.0 | 1.9 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 6.6 | 5.5 | 83.8 | 4.3 | 4.6 | 19.4 | 0.0 | 18.5 | 0.0 | 18.5 | 0.0 |
| LnGrp LOS | A | A | A | F | A | A | B | B | B | B | B | B |
| Approach Vol, veh/h | 1136 | | | 1267 | | | 628 | | | 628 | | |
| Approach Delay, s/veh | 6.5 | | | 4.5 | | | 19.2 | | | 19.2 | | |
| Approach LOS | A | | | A | | | B | | | B | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|-----|------|------|------|------|------|------|
| Assigned Phs | 2 | 3 | 4 | 4 | 4 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 14.7 | 4.2 | 32.1 | 32.1 | 32.1 | 36.2 | 36.2 | 36.2 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 40.0 | 6.0 | 42.0 | 42.0 | 42.0 | 52.0 | 52.0 | 52.0 |
| Max Q Clear Time (g, c+H1), s | 8.4 | 2.1 | 8.0 | 8.0 | 8.0 | 7.1 | 7.1 | 7.1 |
| Green Ext Time (p, c), s | 2.3 | 0.0 | 20.1 | 20.1 | 20.1 | 23.3 | 23.3 | 23.3 |

| Intersection Summary | |
|----------------------|-----|
| HCM 2010 Ctrl Delay | 8.3 |
| HCM 2010 LOS | A |
| Notes | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 EB On-Ramps & Lone Tree Way

10/26/2015

| Movement | SBR |
|-----------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s), veh/h/ln | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g_c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c_a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(I) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |
| Timer | |
| Assigned Phs | |
| Phs Duration (G+Y+Rc), s | |
| Change Period (Y+Rc), s | |
| Max Green Setting (Gmax), s | |
| Max Q Clear Time (g_c+H), s | |
| Green Ext Time (p_c), s | |

User approved ignoring U-Turning movement.

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 43 | 131 | 476 | 41 | 61 | 612 | 92 | 15 | 107 | 88 | 47 | 25 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | 5 | 2 | 12 | | |
| Initial Q (Qb), veh | | | | | | | | | | | | |
| Ped-Bike Adj(A_pbT) | | | | | | | | | | | | |
| Parking Bus, Adj | | | | | | | | | | | | |
| Adj Sat Flow, veh/h/ln | | | | | | | | | | | | |
| Adj Flow Rate, veh/h | | | | | | | | | | | | |
| Adj No. of Lanes | | | | | | | | | | | | |
| Peak Hour Factor | | | | | | | | | | | | |
| Percent Heavy Veh. % | | | | | | | | | | | | |
| Cap. veh/h | | | | | | | | | | | | |
| Arrive On Green | | | | | | | | | | | | |
| Sat Flow, veh/h | | | | | | | | | | | | |
| Grip Volume(v), veh/h | | | | | | | | | | | | |
| Grip Sat Flow(s), veh/h/ln | | | | | | | | | | | | |
| Q Serve(g, s), s | | | | | | | | | | | | |
| Cycle Q Clear(g_c), s | | | | | | | | | | | | |
| Prop In Lane | | | | | | | | | | | | |
| Lane Grp Cap(c), veh/h | | | | | | | | | | | | |
| V/C Ratio(X) | | | | | | | | | | | | |
| Avail Cap(c_a), veh/h | | | | | | | | | | | | |
| HCM Platoon Ratio | | | | | | | | | | | | |
| Upstream Filter(I) | | | | | | | | | | | | |
| Uniform Delay (d), s/veh | | | | | | | | | | | | |
| Incr Delay (d2), s/veh | | | | | | | | | | | | |
| Initial Q Delay(d3),s/veh | | | | | | | | | | | | |
| %ile BackOfQ(50%), veh/ln | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | | | | | | | | | |
| LnGrp LOS | | | | | | | | | | | | |
| Approach Vol, veh/h | | | | | | | | | | | | |
| Approach Delay, s/veh | | | | | | | | | | | | |
| Approach LOS | | | | | | | | | | | | |
| Timer | | | | | | | | | | | | |
| Assigned Phs | | | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | | | | | | | | | | | | |
| Change Period (Y+Rc), s | | | | | | | | | | | | |
| Max Green Setting (Gmax), s | | | | | | | | | | | | |
| Max Q Clear Time (g_c+H), s | | | | | | | | | | | | |
| Green Ext Time (p_c), s | | | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | | | | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |
| User approved ignoring U-Turning movement. | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | SBL | SBT | SBR |
|-----------------------------|------|------|------|
| Lane Configurations | SB | LT | RT |
| Volume (veh/h) | 120 | 126 | 119 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 130 | 137 | 129 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 241 | 291 | 253 |
| Arrive On Green | 0.07 | 0.16 | 0.16 |
| Sat Flow, veh/h | 3408 | 1778 | 1546 |
| Grip Volume(v), veh/h | 130 | 135 | 131 |
| Grip Sat Flow(s), veh/h/ln | 1704 | 1752 | 1572 |
| Q Serve(g, s), s | 1.7 | 3.2 | 3.5 |
| Cycle Q Clear(g, c), s | 1.7 | 3.2 | 3.5 |
| Prop In Lane | 1.00 | 0.98 | |
| Lane Grp Cap(c), veh/h | 241 | 286 | 257 |
| V/C Ratio(X) | 0.54 | 0.47 | 0.51 |
| Avail Cap(c,a), veh/h | 895 | 921 | 826 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 20.5 | 17.3 | 17.4 |
| Incr Delay (d2), s/veh | 1.9 | 1.2 | 1.6 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.9 | 1.6 | 1.6 |
| LnGrp Delay(d), s/veh | 22.4 | 18.5 | 19.0 |
| LnGrp LOS | C | B | B |
| Approach Vol, veh/h | | 396 | |
| Approach Delay, s/veh | | 19.9 | |
| Approach LOS | | B | |
| Timer | | | |
| 1 | 2 | 3 | 4 |
| Assigned Phs | | | |
| Phs Duration (G+Y+Rc), s | | | |
| Change Period (Y+Rc), s | | | |
| Max Green Setting (Gmax), s | | | |
| Max Q Clear Time (g_c+H), s | | | |
| Green Ext Time (p_c), s | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Laurel Road & Country Hills Road

10/26/2015

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------|------|------|------|------|------|------|
| Lane Configurations | LT | RT | LT | RT | LT | RT |
| Volume (veh/h) | 9 | 714 | 680 | 27 | 79 | 11 |
| Number | 7 | 4 | 8 | 18 | 1 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 10 | 776 | 750 | 29 | 86 | 12 |
| Adj No. of Lanes | 1 | 2 | 2 | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 19 | 2495 | 2035 | 79 | 121 | 108 |
| Arrive On Green | 0.01 | 0.71 | 0.59 | 0.59 | 0.07 | 0.07 |
| Sat Flow, veh/h | 1757 | 3597 | 3533 | 133 | 1757 | 1568 |
| Grip Volume(v), veh/h | 10 | 776 | 382 | 397 | 86 | 12 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 1752 | 1821 | 1757 | 1568 |
| Q Serve(g, s), s | 0.2 | 3.0 | 4.2 | 4.2 | 1.7 | 0.3 |
| Cycle Q Clear(g, c), s | 0.2 | 3.0 | 4.2 | 4.2 | 1.7 | 0.3 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 19 | 2495 | 1037 | 1077 | 121 | 108 |
| V/C Ratio(X) | 0.54 | 0.31 | 0.37 | 0.37 | 0.71 | 0.11 |
| Avail Cap(c,a), veh/h | 385 | 6530 | 2689 | 2795 | 1155 | 1031 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 18.0 | 1.9 | 3.9 | 3.9 | 16.6 | 15.9 |
| Incr Delay (d2), s/veh | 22.1 | 0.1 | 0.2 | 0.2 | 7.4 | 0.4 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.2 | 1.4 | 2.0 | 2.0 | 1.1 | 0.2 |
| LnGrp Delay(d), s/veh | 40.1 | 2.0 | 4.1 | 4.1 | 24.0 | 16.4 |
| LnGrp LOS | D | A | A | A | C | B |
| Approach Vol, veh/h | | 786 | 779 | | 98 | |
| Approach Delay, s/veh | | 2.5 | 4.1 | | 23.1 | |
| Approach LOS | | A | A | | C | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| Assigned Phs | | | | | | |
| Phs Duration (G+Y+Rc), s | | | | | | |
| Change Period (Y+Rc), s | | | | | | |
| Max Green Setting (Gmax), s | | | | | | |
| Max Q Clear Time (g_c+H), s | | | | | | |
| Green Ext Time (p_c), s | | | | | | |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 4.5 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
AM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
1: Hillcrest Ave & SR4 WB Ramps

10/26/2015

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------------|-----|------|------|------|------|-------|
| Lane Configurations | | | | | | |
| Volume (veh/h) | 0 | 0 | 648 | 558 | 880 | 141 |
| Number | | | 5 | 2 | 6 | 16 |
| Initial Q (Qb), veh | | | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | | | 704 | 607 | 957 | 0 |
| Adj No. of Lanes | | | 2 | 1 | 2 | 0 |
| Peak Hour Factor | | | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | | 976 | 1687 | 1904 | 0 |
| Arrive On Green | | | 0.29 | 0.91 | 0.54 | 0.00 |
| Sat Flow, veh/h | | | 3408 | 1845 | 3689 | 0 |
| Grip Volume(v), veh/h | | | 704 | 607 | 957 | 0 |
| Grip Sat Flow(s),veh/h/ln | | | 1704 | 1845 | 1752 | 0 |
| Q Serve(g, s), s | | | 8.7 | 2.0 | 8.0 | 0.0 |
| Cycle Q Clear(g, c), s | | | 8.7 | 2.0 | 8.0 | 0.0 |
| Prop In Lane | | | 1.00 | | | |
| Lane Grp Cap(c), veh/h | | | 976 | 1687 | 1904 | 0 |
| V/C Ratio(X) | | | 0.72 | 0.36 | 0.50 | 0.00 |
| Avail Cap(c,a), veh/h | | | 2690 | 3777 | 4112 | 0 |
| HCM Platoon Ratio | | | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | | | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | | | 15.1 | 0.3 | 6.7 | 0.0 |
| Incr Delay (d2), s/veh | | | 1.0 | 0.1 | 0.2 | 0.0 |
| Initial Q Delay(d3),s/veh | | | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | | | 4.1 | 0.9 | 3.9 | 0.0 |
| LnGrp Delay(d),s/veh | | | 16.1 | 0.4 | 6.9 | 0.0 |
| LnGrp LOS | | | B | A | A | |
| Approach Vol, veh/h | | | 1311 | | 957 | |
| Approach Delay, s/veh | | | 8.8 | | 6.9 | |
| Approach LOS | | | A | | A | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 7 8 |
| Assigned Phs | | 2 | | | 5 | 6 |
| Phs Duration (G+Y+Rc), s | | 46.9 | | | 17.4 | 29.5 |
| Change Period (Y+Rc), s | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 96.0 | | | 37.0 | 55.0 |
| Max Q Clear Time (g, c+H1), s | | 4.0 | | | 10.7 | 10.0 |
| Green Ext Time (p, c), s | | 17.2 | | | 2.7 | 15.4 |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 8.0 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 122 | 0 | 730 | 0 | 0 | 0 | 0 | 1086 | 398 | 182 | 692 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1900 | 1845 | 1845 | | | | 0 | 1845 | 1900 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 128 | 0 | 768 | | | | 0 | 1143 | 419 | 192 | 728 | 0 |
| Adj No. of Lanes | 0 | 1 | 2 | | | | 0 | 3 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | | | | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | 533 | 0 | 837 | | | | 0 | 1558 | 571 | 231 | 2123 | 0 |
| Arrive On Green | 0.30 | 0.00 | 0.30 | | | | 0.00 | 0.43 | 0.43 | 0.13 | 0.61 | 0.00 |
| Sat Flow, veh/h | 1757 | 0 | 2760 | | | | 0 | 3801 | 1332 | 1757 | 3597 | 0 |
| Grip Volume(v), veh/h | 128 | 0 | 768 | | | | 0 | 1056 | 506 | 192 | 728 | 0 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 0 | 1380 | | | | 0 | 1679 | 1610 | 1757 | 1752 | 0 |
| Q Serve(g, s), s | 4.8 | 0.0 | 23.6 | | | | 0.0 | 23.0 | 23.0 | 9.4 | 9.1 | 0.0 |
| Cycle Q Clear(g, c), s | 4.8 | 0.0 | 23.6 | | | | 0.0 | 23.0 | 23.0 | 9.4 | 9.1 | 0.0 |
| Prop In Lane | 1.00 | | 1.00 | | | | 0.00 | | 0.83 | 1.00 | 0.00 | |
| Lane Grp Cap(c), veh/h | 533 | 0 | 837 | | | | 0 | 1439 | 690 | 231 | 2123 | 0 |
| V/C Ratio(X) | 0.24 | 0.00 | 0.92 | | | | 0.00 | 0.73 | 0.73 | 0.83 | 0.34 | 0.00 |
| Avail Cap(c,a), veh/h | 560 | 0 | 880 | | | | 0 | 1567 | 751 | 380 | 2553 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | | | | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 23.0 | 0.0 | 29.5 | | | | 0.0 | 20.9 | 20.9 | 37.2 | 8.6 | 0.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 14.0 | | | | 0.0 | 1.7 | 3.4 | 7.8 | 0.1 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 2.4 | 0.0 | 10.6 | | | | 0.0 | 10.9 | 10.8 | 5.0 | 4.4 | 0.0 |
| LnGrp Delay(d),s/veh | 23.2 | 0.0 | 43.5 | | | | 0.0 | 22.6 | 24.3 | 45.0 | 8.7 | 0.0 |
| LnGrp LOS | C | | D | | | | C | C | C | D | A | |
| Approach Vol, veh/h | | | 896 | | | | 1562 | | | | | |
| Approach Delay, s/veh | | | 40.6 | | | | 23.1 | | | | | |
| Approach LOS | | | D | | | | C | | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | | | | | | | | |
| Phs Duration (G+Y+Rc), s | 15.6 | 41.7 | | 30.6 | | | | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | | | | | | | |
| Max Green Setting (Gmax), s | 19.0 | 41.0 | | 28.0 | | | | | | | | |
| Max Q Clear Time (g, c+H1), s | 11.4 | 25.0 | | 25.6 | | | | | | | | |
| Green Ext Time (p, c), s | 0.3 | 12.6 | | 1.0 | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 25.9 | | | | C | | | | | |
| HCM 2010 LOS | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBL | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | EBL | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | 27 | 15 | 21 | 229 | 138 | 131 | 27 | 375 | 119 | 189 | 458 | 38 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 28 | 16 | 22 | 241 | 145 | 79 | 28 | 395 | 0 | 199 | 482 | 40 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 405 | 189 | 260 | 510 | 495 | 421 | 47 | 1041 | 0 | 266 | 1383 | 114 |
| Arrive On Green | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | 0.03 | 0.30 | 0.00 | 0.15 | 0.42 | 0.42 |
| Sat Flow, veh/h | 1141 | 705 | 969 | 1351 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 3278 | 271 |
| Grip Volume(v), veh/h | 28 | 0 | 38 | 241 | 145 | 79 | 28 | 395 | 0 | 199 | 257 | 265 |
| Grip Sat Flow(s), veh/h | 1141 | 0 | 1674 | 1351 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1797 |
| Q Serve(g, s) | 0.8 | 0.0 | 0.7 | 6.9 | 2.6 | 1.6 | 0.7 | 3.8 | 0.0 | 4.6 | 4.2 | 4.2 |
| Cycle Q Clear(g, c), s | 3.5 | 0.0 | 0.7 | 7.6 | 2.6 | 1.6 | 0.7 | 3.8 | 0.0 | 4.6 | 4.2 | 4.2 |
| Prop In Lane | 1.00 | 0.58 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.15 | 0.15 |
| Lane Grp Cap(c), veh/h | 405 | 0 | 449 | 510 | 495 | 421 | 47 | 1041 | 0 | 266 | 740 | 758 |
| V/C Ratio(X) | 0.07 | 0.00 | 0.08 | 0.47 | 0.29 | 0.19 | 0.60 | 0.38 | 0.00 | 0.75 | 0.35 | 0.35 |
| Avail Cap(c,a), veh/h | 690 | 0 | 888 | 848 | 957 | 813 | 414 | 3306 | 0 | 1077 | 2314 | 2373 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 13.7 | 0.0 | 11.6 | 14.5 | 12.3 | 11.9 | 20.4 | 11.8 | 0.0 | 17.2 | 8.3 | 8.3 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 0.1 | 0.7 | 0.3 | 0.2 | 11.8 | 0.2 | 0.0 | 4.2 | 0.3 | 0.3 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.3 | 0.0 | 0.3 | 2.6 | 1.4 | 0.7 | 0.5 | 1.8 | 0.0 | 2.5 | 2.1 | 2.1 |
| LnGrp Delay(d), s/veh | 13.8 | 0.0 | 11.7 | 15.1 | 12.6 | 12.2 | 32.2 | 12.0 | 0.0 | 21.4 | 8.6 | 8.6 |
| LnGrp LOS | B | B | B | B | B | B | C | B | C | C | A | A |
| Approach Vol, veh/h | 66 | | | 465 | | | 423 | | | 721 | | |
| Approach Delay, s/veh | 12.6 | | | 13.9 | | | 13.4 | | | 12.1 | | |
| Approach LOS | B | | | B | | | B | | | B | | |

| | | | | | | | | |
|------------------------------|------|------|------|------|------|------|---|---|
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 | | |
| Phs Duration (G+Y+Rc), s | 10.4 | 16.6 | 15.4 | 5.1 | 21.9 | 15.4 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 26.0 | 40.0 | 22.0 | 10.0 | 56.0 | 22.0 | | |
| Max Q Clear Time (g_c+H1), s | 6.6 | 5.8 | 5.5 | 2.7 | 6.2 | 9.6 | | |
| Green Ext Time (p_c), s | 0.5 | 6.8 | 2.0 | 0.0 | 7.1 | 1.8 | | |

| | |
|----------------------|------|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 12.9 |
| HCM 2010 LOS | B |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/26/2015

| Movement | EBT | EBL | WBL | WBT | NBL | NBT | NBR |
|----------------------------|------|------|------|------|------|------|-----|
| Lane Configurations | EBT | EBL | WBL | WBT | NBL | NBT | NBR |
| Volume (veh/h) | 423 | 48 | 203 | 600 | 102 | 219 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 460 | 52 | 221 | 652 | 111 | 120 | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 1223 | 138 | 298 | 2312 | 229 | 204 | |
| Arrive On Green | 0.39 | 0.39 | 0.17 | 0.66 | 0.13 | 0.13 | |
| Sat Flow, veh/h | 3269 | 358 | 1757 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 253 | 259 | 221 | 652 | 111 | 120 | |
| Grip Sat Flow(s), veh/h | 1752 | 1782 | 1757 | 1752 | 1757 | 1568 | |
| Q Serve(g, s) | 3.9 | 4.0 | 4.5 | 3.0 | 2.2 | 2.7 | |
| Cycle Q Clear(g, c), s | 3.9 | 4.0 | 4.5 | 3.0 | 2.2 | 2.7 | |
| Prop In Lane | 0.20 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 675 | 686 | 298 | 2312 | 229 | 204 | |
| V/C Ratio(X) | 0.37 | 0.38 | 0.74 | 0.28 | 0.49 | 0.59 | |
| Avail Cap(c,a), veh/h | 1473 | 1498 | 1200 | 5710 | 1385 | 1236 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 8.4 | 8.4 | 15.0 | 2.7 | 15.4 | 15.6 | |
| Incr Delay (d2), s/veh | 0.3 | 0.3 | 3.7 | 0.1 | 1.6 | 2.7 | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/h | 2.0 | 2.0 | 2.5 | 1.4 | 1.2 | 1.3 | |
| LnGrp Delay(d), s/veh | 8.8 | 8.8 | 18.7 | 2.8 | 17.0 | 18.3 | |
| LnGrp LOS | A | A | B | A | B | B | |
| Approach Vol, veh/h | 512 | | | 873 | | | |
| Approach Delay, s/veh | 8.8 | | | 6.8 | | | |
| Approach LOS | A | | | B | | | |

| | | | | | | | | |
|------------------------------|------|------|------|---|---|---|---|---|
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 2 | 3 | 4 | | | | | |
| Phs Duration (G+Y+Rc), s | 9.0 | 10.4 | 18.7 | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | | | | | |
| Max Green Setting (Gmax), s | 30.0 | 26.0 | 32.0 | | | | | |
| Max Q Clear Time (g_c+H1), s | 4.7 | 6.5 | 6.0 | | | | | |
| Green Ext Time (p_c), s | 0.7 | 0.6 | 8.7 | | | | | |

| | |
|----------------------|-----|
| Intersection Summary | |
| HCM 2010 Ctrl Delay | 9.0 |
| HCM 2010 LOS | A |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 625 | 49 | 0 | 969 | 360 | 0 | 0 | 0 | 896 | 2 | 444 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 679 | 53 | 0 | 1053 | 0 | | | | 975 | 0 | 483 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1619 | 126 | 0 | 1722 | 0 | | | | 1375 | 0 | 614 |
| Arrive On Green | 0.00 | 0.49 | 0.49 | 0.00 | 0.49 | 0.00 | | | | 0.39 | 0.00 | 0.39 |
| Sat Flow, veh/h | 0 | 3387 | 257 | 0 | 3689 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 361 | 371 | 0 | 1053 | 0 | | | | 975 | 0 | 483 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1799 | 0 | 1752 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 9.0 | 9.0 | 0.0 | 14.9 | 0.0 | | | | 16.0 | 0.0 | 18.5 |
| Cycle Q Clear(g, c), s | 0.0 | 9.0 | 9.0 | 0.0 | 14.9 | 0.0 | | | | 16.0 | 0.0 | 18.5 |
| Prop In Lane | 0.00 | 0.14 | 0.00 | 0.00 | 0.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 861 | 884 | 0 | 1722 | 0 | | | | 1375 | 0 | 614 |
| V/C Ratio(X) | 0.00 | 0.42 | 0.42 | 0.00 | 0.61 | 0.00 | | | | 0.71 | 0.00 | 0.79 |
| Avail Cap(c,a), veh/h | 0 | 1284 | 1318 | 0 | 2588 | 0 | | | | 2162 | 0 | 965 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 11.1 | 11.1 | 0.0 | 12.6 | 0.0 | | | | 17.5 | 0.0 | 18.3 |
| Incr Delay (d2), s/veh | 0.0 | 0.3 | 0.3 | 0.0 | 0.4 | 0.0 | | | | 0.7 | 0.0 | 2.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 4.4 | 4.5 | 0.0 | 7.3 | 0.0 | | | | 7.8 | 0.0 | 8.3 |
| LnGrp Delay(d),s/veh | 0.0 | 11.4 | 11.4 | 0.0 | 13.0 | 0.0 | | | | 18.2 | 0.0 | 20.6 |
| LnGrp LOS | | B | B | | B | | | | | B | | C |
| Approach Vol, veh/h | | 732 | | | 1053 | | | | | | | 1458 |
| Approach Delay, s/veh | | 11.4 | | | 13.0 | | | | | | | 19.0 |
| Approach LOS | | B | | | B | | | | | | | B |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--|---|---|---|------|---|------|---|------|
| Assigned Phs | | | | 4 | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 37.5 | | 30.7 | | 37.5 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 50.0 | | 42.0 | | 50.0 |
| Max Q Clear Time (g_c+H1), s | | | | 11.0 | | 20.5 | | 16.9 |
| Green Ext Time (p_c), s | | | | 17.9 | | 6.2 | | 16.6 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 15.3 | | | | |
| HCM 2010 LOS | | | | B | | | | |
| Notes | | | | | | | | |
| User approved volume balancing among the lanes for turning movement. | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 114 | 1406 | 0 | 0 | 1276 | 465 | 140 | 0 | 497 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 124 | 1528 | 0 | 0 | 1387 | 0 | | | | 152 | 0 | 540 |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | | | | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 146 | 1924 | 0 | 0 | 1488 | 666 | | | | 646 | 0 | 577 |
| Arrive On Green | 0.08 | 0.55 | 0.00 | 0.00 | 0.42 | 0.00 | | | | 0.37 | 0.00 | 0.37 |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | | | | 1757 | 0 | 1568 |
| Grip Volume(v), veh/h | 124 | 1528 | 0 | 0 | 1387 | 0 | | | | 152 | 0 | 540 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s), s | 6.7 | 33.6 | 0.0 | 0.0 | 36.3 | 0.0 | | | | 5.8 | 0.0 | 32.0 |
| Cycle Q Clear(g, c), s | 6.7 | 33.6 | 0.0 | 0.0 | 36.3 | 0.0 | | | | 5.8 | 0.0 | 32.0 |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 146 | 1924 | 0 | 0 | 1488 | 666 | | | | 646 | 0 | 577 |
| V/C Ratio(X) | 0.85 | 0.79 | 0.00 | 0.00 | 0.93 | 0.00 | | | | 0.24 | 0.00 | 0.94 |
| Avail Cap(c,a), veh/h | 146 | 1927 | 0 | 0 | 1491 | 667 | | | | 711 | 0 | 634 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 43.6 | 17.4 | 0.0 | 0.0 | 26.4 | 0.0 | | | | 21.1 | 0.0 | 29.4 |
| Incr Delay (d2), s/veh | 35.3 | 2.4 | 0.0 | 0.0 | 10.9 | 0.0 | | | | 0.2 | 0.0 | 20.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 4.7 | 16.8 | 0.0 | 0.0 | 19.8 | 0.0 | | | | 2.8 | 0.0 | 17.1 |
| LnGrp Delay(d),s/veh | 78.9 | 19.7 | 0.0 | 0.0 | 37.3 | 0.0 | | | | 21.3 | 0.0 | 49.8 |
| LnGrp LOS | | E | B | | D | C | | | | D | | D |
| Approach Vol, veh/h | | 1652 | | | 1387 | | | | | 692 | | |
| Approach Delay, s/veh | | 24.2 | | | 37.3 | | | | | 43.6 | | |
| Approach LOS | | C | | | D | | | | | D | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|------|---|------|---|---|------|------|
| Assigned Phs | | 2 | | 4 | | | 7 | 8 |
| Phs Duration (G+Y+Rc), s | | 39.5 | | 56.9 | | | 12.0 | 44.9 |
| Change Period (Y+Rc), s | | 4.0 | | 4.0 | | | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | | 39.0 | | 53.0 | | | 8.0 | 41.0 |
| Max Q Clear Time (g_c+H1), s | | 34.0 | | 35.6 | | | 8.7 | 38.3 |
| Green Ext Time (p_c), s | | 1.5 | | 15.9 | | | 0.0 | 2.6 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 32.7 | | | | |
| HCM 2010 LOS | | | | C | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1420 | 497 | 120 | 1391 | 0 | 0 | 0 | 0 | 461 | 2 | 374 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1495 | 523 | 126 | 1464 | 0 | 1495 | 523 | 126 | 1464 | 0 | 394 |
| Adj No. of Lanes | 0 | 3 | 1 | 2 | 3 | 0 | 3 | 1 | 2 | 3 | 0 | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2469 | 769 | 200 | 3017 | 0 | 2469 | 769 | 200 | 3017 | 0 | 471 |
| Arrive On Green | 0.00 | 0.49 | 0.49 | 0.06 | 0.60 | 0.00 | 0.49 | 0.49 | 0.06 | 0.60 | 0.00 | 0.30 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 3408 | 5202 | 0 | 5202 | 1568 | 3408 | 5202 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 1495 | 523 | 126 | 1464 | 0 | 1495 | 523 | 126 | 1464 | 0 | 394 |
| Grip Sat Flow(s), veh/h | 0 | 1679 | 1568 | 1704 | 1679 | 0 | 1679 | 1568 | 1704 | 1679 | 0 | 1568 |
| Q Serve(g, s), s | 0.0 | 17.1 | 20.3 | 2.9 | 13.1 | 0.0 | 17.1 | 20.3 | 2.9 | 13.1 | 0.0 | 18.7 |
| Cycle Q Clear(g, c), s | 0.0 | 17.1 | 20.3 | 2.9 | 13.1 | 0.0 | 17.1 | 20.3 | 2.9 | 13.1 | 0.0 | 18.7 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2469 | 769 | 200 | 3017 | 0 | 2469 | 769 | 200 | 3017 | 0 | 471 |
| V/C Ratio(X) | 0.00 | 0.61 | 0.68 | 0.63 | 0.49 | 0.00 | 0.61 | 0.68 | 0.63 | 0.49 | 0.00 | 0.84 |
| Avail Cap(c,a), veh/h | 0 | 2529 | 788 | 342 | 3288 | 0 | 2529 | 788 | 342 | 3288 | 0 | 788 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 14.7 | 15.5 | 36.6 | 9.0 | 0.0 | 14.7 | 15.5 | 36.6 | 9.0 | 0.0 | 26.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.4 | 2.3 | 3.3 | 0.1 | 0.0 | 0.4 | 2.3 | 3.3 | 0.1 | 0.0 | 4.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 8.0 | 9.2 | 1.4 | 6.0 | 0.0 | 8.0 | 9.2 | 1.4 | 6.0 | 0.0 | 8.6 |
| LnGrp Delay(d), s/veh | 0.0 | 15.1 | 17.8 | 39.9 | 9.1 | 0.0 | 15.1 | 17.8 | 39.9 | 9.1 | 0.0 | 30.0 |
| LnGrp LOS | B | B | B | D | A | C | B | B | B | D | C | C |
| Approach Vol, veh/h | 2018 | | | 1590 | | | 880 | | | 26.1 | | |
| Approach Delay, s/veh | 15.8 | | | 11.6 | | | B | | | C | | |
| Approach LOS | B | | | B | | | B | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|-----|------|------|------|------|------|------|------|
| Assigned Phs | 3 | 4 | 4 | 4 | 6 | 6 | 8 | 8 |
| Phs Duration (G+Y+Rc), s | 8.7 | 43.0 | 27.9 | 43.0 | 27.9 | 43.0 | 51.7 | 51.7 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 8.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 52.0 | 52.0 |
| Max Q Clear Time (g_c+H1), s | 4.9 | 22.3 | 20.7 | 22.3 | 20.7 | 20.7 | 15.1 | 15.1 |
| Green Ext Time (p_c), s | 0.1 | 16.6 | 3.2 | 16.6 | 3.2 | 3.2 | 32.6 | 32.6 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 16.3 |
| HCM 2010 LOS | B |
| Notes | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/26/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA | AAA |
| Volume (veh/h) | 0 | 1616 | 265 | 20 | 5 | 990 | 384 | 539 | 29 | 189 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1701 | 153 | 5 | 1042 | 404 | 589 | 0 | 197 | 0 | 197 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 3027 | 943 | 9 | 3338 | 1039 | 788 | 0 | 352 | 0 | 352 | 0 |
| Arrive On Green | 0.00 | 0.60 | 0.60 | 0.01 | 0.66 | 0.66 | 0.22 | 0.00 | 0.22 | 0.00 | 0.22 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 1701 | 153 | 5 | 1042 | 404 | 589 | 0 | 197 | 0 | 197 | 0 |
| Grip Sat Flow(s), veh/h | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s), s | 0.0 | 14.4 | 3.1 | 0.2 | 6.2 | 8.3 | 11.1 | 0.0 | 7.9 | 0.0 | 7.9 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 14.4 | 3.1 | 0.2 | 6.2 | 8.3 | 11.1 | 0.0 | 7.9 | 0.0 | 7.9 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 3027 | 943 | 9 | 3338 | 1039 | 788 | 0 | 352 | 0 | 352 | 0 |
| V/C Ratio(X) | 0.00 | 0.56 | 0.16 | 0.54 | 0.31 | 0.39 | 0.75 | 0.00 | 0.56 | 0.00 | 0.56 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 3408 | 1061 | 149 | 4117 | 1282 | 1884 | 0 | 752 | 0 | 752 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 8.5 | 6.3 | 35.2 | 5.1 | 5.4 | 25.6 | 0.0 | 24.4 | 0.0 | 24.4 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.1 | 40.7 | 0.1 | 0.2 | 1.4 | 0.0 | 1.4 | 0.0 | 1.4 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/h | 0.0 | 6.7 | 1.3 | 0.2 | 2.9 | 3.5 | 5.5 | 0.0 | 3.5 | 0.0 | 3.5 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 8.7 | 6.3 | 75.9 | 5.1 | 5.7 | 27.1 | 0.0 | 25.8 | 0.0 | 25.8 | 0.0 |
| LnGrp LOS | A | A | A | E | A | A | C | C | C | C | C | C |
| Approach Vol, veh/h | 1854 | | | 1451 | | | 786 | | | 26.8 | | |
| Approach Delay, s/veh | 8.5 | | | 5.5 | | | A | | | C | | |
| Approach LOS | A | | | A | | | A | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|-----|------|------|-----|-----|------|------|
| Assigned Phs | 2 | 3 | 4 | 4 | 6 | 6 | 8 | 8 |
| Phs Duration (G+Y+Rc), s | 19.9 | 4.4 | 46.6 | 46.6 | 4.4 | 4.4 | 51.0 | 51.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 34.0 | 6.0 | 48.0 | 48.0 | 6.0 | 6.0 | 58.0 | 58.0 |
| Max Q Clear Time (g_c+H1), s | 13.1 | 2.2 | 16.4 | 16.4 | 2.2 | 2.2 | 10.3 | 10.3 |
| Green Ext Time (p_c), s | 2.8 | 0.0 | 26.2 | 26.2 | 0.0 | 0.0 | 36.5 | 36.5 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 10.9 |
| HCM 2010 LOS | B |
| Notes | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/26/2015

| Movement | SBR |
|------------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s),veh/h/ln | |
| Q Serve(g, s) | |
| Cycle Q Clear(g, c), s | |
| Prop In Lane | |
| Lane Grp Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c,a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(I) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |
| Timer | |
| Assigned Phs | |
| Phs Duration (G+Y+Rc), s | |
| Change Period (Y+Rc), s | |
| Max Green Setting (Gmax), s | |
| Max Q Clear Time (g_c+H1), s | |
| Green Ext Time (p_c), s | |













Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

9: Empire Avenue & Lone Tree Way

10/26/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |
|------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 101 | 240 | 815 | 95 | 90 | 757 | 157 | 16 | 94 | 94 | 37 | 59 |
| Number | | 7 | 4 | 14 | 3 | 8 | 18 | | 5 | 2 | 12 | |
| Initial Q (Ob), veh | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | | 253 | 858 | 58 | 95 | 797 | 112 | | 99 | 99 | 22 | |
| Adj No. of Lanes | | 1 | 3 | 1 | 1 | 3 | 1 | | 2 | 1 | 1 | 1 |
| Peak Hour Factor | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | | 3 | 3 | 3 | 3 | 3 | 3 | | 3 | 3 | 3 | 3 |
| Cap. veh/h | | 318 | 2076 | 646 | 123 | 1517 | 472 | | 189 | 236 | 201 | |
| Arrive On Green | | 0.18 | 0.41 | 0.41 | 0.07 | 0.30 | 0.30 | | 0.06 | 0.13 | 0.13 | 0.13 |
| Sat. Flow, veh/h | | 1757 | 5036 | 1568 | 1568 | 1757 | 5036 | | 1568 | 1845 | 1568 | |
| Gp Volume(v), veh/h | | 253 | 858 | 58 | 95 | 797 | 112 | | 99 | 99 | 22 | |
| Gp Sat Flow(s),veh/h/ln | | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | | 1704 | 1845 | 1568 | |
| Q Serve(g, s), s | | 7.9 | 6.9 | 1.3 | 3.0 | 7.5 | 3.1 | | 1.6 | 2.8 | 0.7 | |
| Cycle Q Clear(g, c), s | | 7.9 | 6.9 | 1.3 | 3.0 | 7.5 | 3.1 | | 1.6 | 2.8 | 0.7 | |
| Prop In Lane | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | | 318 | 2076 | 646 | 123 | 1517 | 472 | | 189 | 236 | 201 | |
| V/C Ratio(X) | | 0.80 | 0.41 | 0.09 | 0.77 | 0.53 | 0.24 | | 0.52 | 0.42 | 0.11 | |
| Avail Cap(c,a), veh/h | | 950 | 3515 | 1094 | 368 | 1845 | 575 | | 416 | 579 | 492 | |
| HCM Platoon Ratio | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | | 22.5 | 11.9 | 10.3 | 26.2 | 16.6 | 15.1 | | 26.3 | 23.0 | 22.1 | |
| Incr Delay (d2), s/veh | | 4.5 | 0.1 | 0.1 | 9.8 | 0.3 | 0.3 | | 2.3 | 1.2 | 0.2 | |
| Initial Q Delay(d3),s/veh | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | | 4.2 | 3.2 | 0.6 | 1.8 | 3.5 | 1.4 | | 0.8 | 1.5 | 0.3 | |
| LnGrp Delay(d),s/veh | | 27.0 | 12.1 | 10.3 | 36.0 | 16.9 | 15.3 | | 28.6 | 24.2 | 22.3 | |
| LnGrp LOS | | C | B | B | D | B | B | | C | C | C | |
| Approach Vol, veh/h | 1169 | | | 1004 | | | 220 | | | 260 | | |
| Approach Delay, s/veh | 15.2 | | | 18.5 | | | B | | | C | | |
| Approach LOS | B | | | B | | | C | | | C | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.3 | 11.3 | 8.0 | 27.6 | 7.2 | 14.5 | 14.4 | 21.3 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 14.0 | 18.0 | 12.0 | 40.0 | 7.0 | 25.0 | 31.0 | 21.0 | | | | |
| Max Q Clear Time (g_c+H1), s | 6.0 | 4.8 | 5.0 | 8.9 | 3.6 | 8.0 | 9.9 | 9.5 | | | | |
| Green Ext Time (p_c), s | 0.5 | 2.3 | 0.1 | 14.3 | 0.1 | 2.5 | 0.7 | 7.7 | | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/26/2015

| Movement | SBL | SBT | SBR |
|------------------------------|------|------|------|
| Lane Configurations | SBT | SBT | SBR |
| Volume (veh/h) | 234 | 194 | 155 |
| Number | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 246 | 204 | 163 |
| Adj No. of Lanes | 2 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 |
| Cap. veh/h | 377 | 348 | 264 |
| Arrive On Green | 0.11 | 0.18 | 0.18 |
| Sat Flow, veh/h | 3408 | 1900 | 1443 |
| Grip Volume(v), veh/h | 246 | 187 | 180 |
| Grip Sat Flow(s), veh/h/ln | 1704 | 1752 | 1590 |
| Q Serve(g, s), s | 4.0 | 5.6 | 6.0 |
| Cycle Q Clear(g, c), s | 4.0 | 5.6 | 6.0 |
| Prop In Lane | 1.00 | 0.91 | |
| Lane Grp Cap(c), veh/h | 377 | 321 | 291 |
| V/C Ratio(X) | 0.65 | 0.58 | 0.62 |
| Avail Cap(c,a), veh/h | 833 | 764 | 694 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 24.4 | 21.4 | 21.5 |
| Incr Delay (d2), s/veh | 1.9 | 1.7 | 2.1 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 1.9 | 2.9 | 2.8 |
| LnGrp Delay(d), s/veh | 26.4 | 23.1 | 23.7 |
| LnGrp LOS | C | C | C |
| Approach Vol, veh/h | | 613 | |
| Approach Delay, s/veh | | 24.6 | |
| Approach LOS | | C | |
| Timer | | | |
| Assigned Phs | | | |
| Phs Duration (G+Y+Rc), s | | | |
| Change Period (Y+Rc), s | | | |
| Max Green Setting (Gmax), s | | | |
| Max Q Clear Time (g_c+H1), s | | | |
| Green Ext Time (p_c), s | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Laurel Road & Country Hills Road

10/26/2015

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|------------------------------|------|------|------|------|------|------|
| Lane Configurations | EBL | EBT | WBT | WBR | SBL | SBR |
| Volume (veh/h) | 24 | 619 | 1191 | 94 | 55 | 7 |
| Number | 7 | 4 | 8 | 18 | 1 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 26 | 673 | 1295 | 102 | 60 | 8 |
| Adj No. of Lanes | 1 | 2 | 2 | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 42 | 2822 | 2330 | 183 | 83 | 74 |
| Arrive On Green | 0.02 | 0.81 | 0.71 | 0.71 | 0.05 | 0.05 |
| Sat Flow, veh/h | 1757 | 3597 | 3385 | 259 | 1757 | 1568 |
| Grip Volume(v), veh/h | 26 | 673 | 688 | 709 | 60 | 8 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 1752 | 1799 | 1757 | 1568 |
| Q Serve(g, s), s | 0.8 | 2.5 | 10.2 | 10.3 | 1.8 | 0.3 |
| Cycle Q Clear(g, c), s | 0.8 | 2.5 | 10.2 | 10.3 | 1.8 | 0.3 |
| Prop In Lane | 1.00 | | | 0.14 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 42 | 2822 | 1240 | 1273 | 83 | 74 |
| V/C Ratio(X) | 0.62 | 0.24 | 0.55 | 0.56 | 0.72 | 0.11 |
| Avail Cap(c,a), veh/h | 227 | 4974 | 2132 | 2188 | 486 | 433 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 26.2 | 1.3 | 3.8 | 3.8 | 25.5 | 24.8 |
| Incr Delay (d2), s/veh | 13.9 | 0.0 | 0.4 | 0.4 | 11.2 | 0.6 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.5 | 1.1 | 4.9 | 5.1 | 1.1 | 0.2 |
| LnGrp Delay(d), s/veh | 40.2 | 1.3 | 4.2 | 4.2 | 36.7 | 25.4 |
| LnGrp LOS | D | A | A | A | D | C |
| Approach Vol, veh/h | | 699 | 1397 | | 68 | |
| Approach Delay, s/veh | | 2.8 | 4.2 | | 35.4 | |
| Approach LOS | | A | A | | D | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| Assigned Phs | | | | | | |
| Phs Duration (G+Y+Rc), s | | | | | | |
| Change Period (Y+Rc), s | | | | | | |
| Max Green Setting (Gmax), s | | | | | | |
| Max Q Clear Time (g_c+H1), s | | | | | | |
| Green Ext Time (p_c), s | | | | | | |
| Intersection Summary | | | | | | |
| HCM 2010 Ctrl Delay | | | 4.7 | | | |
| HCM 2010 LOS | | | A | | | |

Laurel Ranch Traffic Impact Analysis
PM Existing Plus Prj Plus Nearby Prj Conditions

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 32 | 0 | 137 | 0 | 0 | 0 | 0 | 1806 | 503 | 294 | 569 | 0 |
| Number | 7 | 4 | 14 | 0 | 0 | 0 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 35 | 0 | 149 | 0 | 0 | 0 | 1963 | 547 | 320 | 618 | 0 | 0 |
| Adj No. of Lanes | 2 | 0 | 2 | 0 | 0 | 0 | 3 | 0 | 2 | 2 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 0 |
| Cap, veh/h | 259 | 0 | 231 | 0 | 0 | 0 | 2636 | 702 | 406 | 2915 | 0 | 0 |
| Arrive On Green | 0.07 | 0.00 | 0.07 | 0.00 | 0.00 | 0.00 | 0.67 | 0.67 | 0.12 | 0.83 | 0.00 | 0.00 |
| Sat Flow, veh/h | 3514 | 0 | 3136 | 0 | 0 | 0 | 4127 | 1055 | 3408 | 3597 | 0 | 0 |
| Grip Volume(v), veh/h | 35 | 0 | 149 | 0 | 0 | 0 | 1650 | 860 | 320 | 618 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 0 | 1568 | 0 | 0 | 0 | 1679 | 1659 | 1704 | 1752 | 0 | 0 |
| Q Serve(g, s) | 0.8 | 0.0 | 3.9 | 0.0 | 0.0 | 0.0 | 27.4 | 30.5 | 7.7 | 3.0 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.8 | 0.0 | 3.9 | 0.0 | 0.0 | 0.0 | 27.4 | 30.5 | 7.7 | 3.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.64 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Lane Grp Cap(c), veh/h | 259 | 0 | 231 | 0 | 0 | 0 | 2234 | 1104 | 406 | 2915 | 0 | 0 |
| V/C Ratio(X) | 0.14 | 0.00 | 0.64 | 0.00 | 0.00 | 0.00 | 0.74 | 0.78 | 0.79 | 0.21 | 0.00 | 0.00 |
| Avail Cap(c.a), veh/h | 664 | 0 | 593 | 0 | 0 | 0 | 2339 | 1156 | 523 | 3146 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 36.7 | 0.0 | 38.1 | 0.0 | 0.0 | 0.0 | 9.3 | 9.8 | 36.3 | 1.5 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 3.0 | 0.0 | 0.0 | 0.0 | 1.2 | 3.3 | 6.1 | 0.0 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.4 | 0.0 | 1.8 | 0.0 | 0.0 | 0.0 | 12.8 | 14.6 | 4.0 | 1.5 | 0.0 | 0.0 |
| LnGrp Delay(d), s/veh | 36.9 | 0.0 | 41.1 | 0.0 | 0.0 | 0.0 | 10.5 | 13.2 | 42.3 | 1.5 | 0.0 | 0.0 |
| LnGrp LOS | D | D | D | D | D | D | B | B | D | A | A | A |
| Approach Vol, veh/h | 184 | | | 2510 | | | 938 | | | | | |
| Approach Delay, s/veh | 40.3 | | | 11.4 | | | 15.4 | | | | | |
| Approach LOS | D | | | B | | | B | | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|---|------|---|------|---|---|
| Assigned Phs | 1 | 2 | | 4 | | 6 | | |
| Phs Duration (G+Y+Rc), s | 14.1 | 60.3 | | 10.2 | | 74.4 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | 4.0 | | |
| Max Green Setting (Gmax), s | 13.0 | 59.0 | | 16.0 | | 76.0 | | |
| Max Q Clear Time (g, c+1), s | 9.7 | 32.5 | | 5.9 | | 5.0 | | |
| Green Ext Time (p, c), s | 0.4 | 23.8 | | 0.4 | | 54.9 | | |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 13.9 | | | | | | | |
| HCM 2010 LOS | B | | | | | | | |
| Notes | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|----------------------------|------|------|------|-------|------|------|------|------|------|-------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 121 | 90 | 85 | 366 | 80 | 252 | 98 | 1191 | 531 | 436 | 1094 | 145 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 132 | 98 | 92 | 398 | 87 | 138 | 107 | 1295 | 0 | 474 | 1189 | 158 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 354 | 248 | 232 | 299 | 521 | 443 | 134 | 1419 | 0 | 337 | 1619 | 214 |
| Arrive On Green | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.08 | 0.40 | 0.00 | 0.19 | 0.52 | 0.52 |
| Sat Flow, veh/h | 1140 | 877 | 823 | 1177 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 3112 | 412 |
| Grip Volume(v), veh/h | 132 | 0 | 190 | 398 | 87 | 138 | 107 | 1295 | 0 | 474 | 688 | 679 |
| Grip Sat Flow(s), veh/h/ln | 1140 | 0 | 1699 | 1177 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1772 |
| Q Serve(g, s) | 9.8 | 0.0 | 9.0 | 19.0 | 3.5 | 6.9 | 5.9 | 34.6 | 0.0 | 19.0 | 29.3 | 29.6 |
| Cycle Q Clear(g, c), s | 13.3 | 0.0 | 9.0 | 28.0 | 3.5 | 6.9 | 5.9 | 34.6 | 0.0 | 19.0 | 29.3 | 29.6 |
| Prop In Lane | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.23 |
| Lane Grp Cap(c), veh/h | 354 | 0 | 480 | 299 | 521 | 443 | 134 | 1419 | 0 | 337 | 912 | 922 |
| V/C Ratio(X) | 0.37 | 0.00 | 0.40 | 1.33 | 0.17 | 0.31 | 0.80 | 0.91 | 0.00 | 1.41 | 0.73 | 0.74 |
| Avail Cap(c.a), veh/h | 354 | 0 | 480 | 299 | 521 | 443 | 160 | 1450 | 0 | 337 | 912 | 922 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 31.8 | 0.0 | 28.7 | 42.4 | 26.8 | 28.0 | 45.0 | 27.8 | 0.0 | 40.1 | 18.4 | 18.5 |
| Incr Delay (d2), s/veh | 0.7 | 0.0 | 0.5 | 170.6 | 0.1 | 0.4 | 21.1 | 9.0 | 0.0 | 200.3 | 3.1 | 3.1 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 3.1 | 0.0 | 4.3 | 22.3 | 1.8 | 3.0 | 3.7 | 18.3 | 0.0 | 27.9 | 14.9 | 15.1 |
| LnGrp Delay(d), s/veh | 32.4 | 0.0 | 29.3 | 212.9 | 26.9 | 28.4 | 66.2 | 36.9 | 0.0 | 240.3 | 21.5 | 21.6 |
| LnGrp LOS | C | C | C | F | C | C | E | D | F | C | C | C |
| Approach Vol, veh/h | 322 | | | 623 | | | 1402 | | | 1821 | | |
| Approach Delay, s/veh | 30.6 | | | 146.1 | | | 39.1 | | | 78.5 | | |
| Approach LOS | C | | | F | | | D | | | E | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|------|------|
| Assigned Phs | 1 | 2 | 4 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 23.0 | 44.1 | 32.0 | 11.5 | 55.6 | 32.0 | 32.0 | 32.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 19.0 | 41.0 | 28.0 | 9.0 | 51.0 | 28.0 | 28.0 | 28.0 |
| Max Q Clear Time (g, c+H1), s | 21.0 | 36.6 | 15.3 | 7.9 | 31.6 | 30.0 | 30.0 | 30.0 |
| Green Ext Time (p, c), s | 0.0 | 3.5 | 3.7 | 0.0 | 16.6 | 0.0 | 0.0 | 0.0 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 71.6 | | | | | | | |
| HCM 2010 LOS | E | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/27/2015

| Movement | EBT | EBR | WBL | WBT | NBL | NBR | |
|-------------------------------|------|------|------|------|------|------|------|
| Lane Configurations | ↔↔ | ↔↔ | ↔↔ | ↔↔ | ↔↔ | ↔↔ | |
| Volume (veh/h) | 1041 | 117 | 314 | 782 | 154 | 369 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h/ln | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 1132 | 127 | 341 | 850 | 167 | 201 | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 1488 | 167 | 389 | 2594 | 280 | 250 | |
| Arrive On Green | 0.47 | 0.47 | 0.22 | 0.74 | 0.16 | 0.16 | |
| Sat Flow, veh/h | 3271 | 356 | 1757 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 623 | 636 | 341 | 850 | 167 | 201 | |
| Grip Sat Flow(s),veh/h/ln | 1752 | 1782 | 1757 | 1752 | 1757 | 1568 | |
| Q Serve(g, s) | 23.3 | 23.4 | 14.9 | 6.6 | 7.0 | 9.8 | |
| Cycle Q Clear(g, c), s | 23.3 | 23.4 | 14.9 | 6.6 | 7.0 | 9.8 | |
| Prop In Lane | 0.20 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 820 | 834 | 389 | 2594 | 280 | 250 | |
| V/C Ratio(X) | 0.76 | 0.76 | 0.88 | 0.33 | 0.60 | 0.81 | |
| Avail Cap(c,a), veh/h | 904 | 920 | 575 | 3133 | 484 | 415 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 17.4 | 17.5 | 29.9 | 3.5 | 31.0 | 32.2 | |
| Incr Delay (d2), s/veh | 3.4 | 3.5 | 10.0 | 0.1 | 2.0 | 6.0 | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/ln | 12.0 | 12.3 | 8.3 | 3.2 | 3.5 | 4.6 | |
| LnGrp Delay(d),s/veh | 20.9 | 20.9 | 39.9 | 3.6 | 33.1 | 38.2 | |
| LnGrp LOS | C | C | D | A | C | D | |
| Approach Vol, veh/h | 1259 | | 1191 | | 368 | | |
| Approach Delay, s/veh | 20.9 | | 14.0 | | 35.9 | | |
| Approach LOS | C | | B | | D | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 8 |
| Assigned Phs | | 2 | 3 | 4 | | | 8 |
| Phs Duration (G+Y+Rc), s | | 16.6 | 21.6 | 41.2 | | | 62.8 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Max Green Setting (Gmax), s | | 21.0 | 26.0 | 41.0 | | | 71.0 |
| Max Q Clear Time (g, c+H1), s | | 11.8 | 16.9 | 25.4 | | | 8.6 |
| Green Ext Time (p, c), s | | 0.8 | 0.7 | 11.8 | | | 27.5 |
| Intersection Summary | | | | | | | |
| HCM 2010 Ctrl Delay | | | 19.9 | | | | |
| HCM 2010 LOS | | | B | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|-----|------|-----|------|------|------|
| Lane Configurations | | ↔↔ | ↔↔ | ↔↔ | ↔↔ | ↔↔ | | | | ↔↔ | ↔↔ | ↔↔ |
| Volume (veh/h) | 0 | 1363 | 122 | 0 | 575 | 100 | 0 | 0 | 0 | 830 | 0 | 342 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1482 | 133 | 0 | 625 | 0 | | | | 902 | 0 | 372 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1888 | 168 | 0 | 2033 | 0 | | | | 1129 | 0 | 504 |
| Arrive On Green | 0.00 | 0.58 | 0.58 | 0.00 | 0.58 | 0.00 | | | | 0.32 | 0.00 | 0.32 |
| Sat Flow, veh/h | 0 | 3348 | 290 | 0 | 3689 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 793 | 822 | 0 | 625 | 0 | | | | 902 | 0 | 372 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1793 | 0 | 1752 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 28.2 | 28.8 | 0.0 | 7.4 | 0.0 | | | | 19.0 | 0.0 | 17.1 |
| Cycle Q Clear(g, c), s | 0.0 | 28.2 | 28.8 | 0.0 | 7.4 | 0.0 | | | | 19.0 | 0.0 | 17.1 |
| Prop In Lane | 0.00 | 0.16 | 0.00 | 0.00 | 0.00 | 0.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 1016 | 1040 | 0 | 2033 | 0 | | | | 1129 | 0 | 504 |
| V/C Ratio(X) | 0.00 | 0.78 | 0.79 | 0.00 | 0.31 | 0.00 | | | | 0.80 | 0.00 | 0.74 |
| Avail Cap(c,a), veh/h | 0 | 1124 | 1150 | 0 | 2248 | 0 | | | | 1733 | 0 | 774 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 13.1 | 13.2 | 0.0 | 8.7 | 0.0 | | | | 25.1 | 0.0 | 24.5 |
| Incr Delay (d2), s/veh | 0.0 | 3.3 | 3.5 | 0.0 | 0.1 | 0.0 | | | | 1.5 | 0.0 | 2.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 14.4 | 15.2 | 0.0 | 3.6 | 0.0 | | | | 9.4 | 0.0 | 7.6 |
| LnGrp Delay(d),s/veh | 0.0 | 16.4 | 16.7 | 0.0 | 8.8 | 0.0 | | | | 26.7 | 0.0 | 26.6 |
| LnGrp LOS | | B | B | | A | | | | | C | | C |
| Approach Vol, veh/h | | 1615 | | | 625 | | | | | | 1274 | |
| Approach Delay, s/veh | | 16.5 | | | 8.8 | | | | | | 26.6 | |
| Approach LOS | | B | | | A | | | | | C | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | | | 4 | | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | | | 51.0 | | 30.1 | | 51.0 | | | | |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 | | | | |
| Max Green Setting (Gmax), s | | | | 52.0 | | 40.0 | | 52.0 | | | | |
| Max Q Clear Time (g, c+H1), s | | | | 30.8 | | 21.0 | | 30.8 | | | | |
| Green Ext Time (p, c), s | | | | 16.2 | | 5.1 | | 26.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 18.8 | | | | | | | | |
| HCM 2010 LOS | | | | B | | | | | | | | |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 654 | 1475 | 0 | 0 | 728 | 310 | 38 | 0 | 109 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 0 | 0 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 711 | 1603 | 0 | 0 | 791 | 0 | 41 | 0 | 118 | 0 | 0 |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 1 | 0 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 766 | 2806 | 0 | 0 | 1103 | 494 | 175 | 0 | 156 | 0 | 0 |
| Arrive On Green | 0.44 | 0.80 | 0.00 | 0.00 | 0.31 | 0.00 | 0.10 | 0.00 | 0.10 | 0.00 | 0.00 |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | 1757 | 0 | 1568 | 0 | 0 |
| Grip Volume(v), veh/h | 711 | 1603 | 0 | 0 | 791 | 0 | 41 | 0 | 118 | 0 | 0 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | 1757 | 0 | 1568 | 0 | 0 |
| Q Serve(g, s) | 30.7 | 13.5 | 0.0 | 0.0 | 16.0 | 0.0 | 1.7 | 0.0 | 5.9 | 0.0 | 0.0 |
| Cycle Q Clear(g, c), s | 30.7 | 13.5 | 0.0 | 0.0 | 16.0 | 0.0 | 1.7 | 0.0 | 5.9 | 0.0 | 0.0 |
| Prop In Lane | 1.00 | 0.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 766 | 2806 | 0 | 0 | 1103 | 494 | 175 | 0 | 156 | 0 | 0 |
| V/C Ratio(X) | 0.93 | 0.57 | 0.00 | 0.00 | 0.72 | 0.00 | 0.23 | 0.00 | 0.76 | 0.00 | 0.00 |
| Avail Cap(c,a), veh/h | 987 | 3281 | 0 | 0 | 1137 | 509 | 373 | 0 | 333 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 21.4 | 2.9 | 0.0 | 0.0 | 24.3 | 0.0 | 33.3 | 0.0 | 35.1 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 12.4 | 0.2 | 0.0 | 0.0 | 2.1 | 0.0 | 0.7 | 0.0 | 7.2 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 17.4 | 6.3 | 0.0 | 0.0 | 8.0 | 0.0 | 0.9 | 0.0 | 2.8 | 0.0 | 0.0 |
| LnGrp Delay(d), s/veh | 33.8 | 3.1 | 0.0 | 0.0 | 26.4 | 0.0 | 33.9 | 0.0 | 42.4 | 0.0 | 0.0 |
| LnGrp LOS | C | A | | | C | | C | | D | | |
| Approach Vol, veh/h | 2314 | | | 791 | | | 159 | | | 1351 | |
| Approach Delay, s/veh | 12.5 | | | 26.4 | | | 40.2 | | | 37.7 | |
| Approach LOS | B | | | C | | | D | | | D | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|------|------|
| Assigned Phs | 2 | 2 | 3 | 4 | 4 | 5 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 12.0 | 68.1 | 38.9 | 29.2 | 38.8 | 60.0 | 60.0 | 60.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 17.0 | 75.0 | 45.0 | 26.0 | 44.0 | 36.0 | 56.0 | 56.0 |
| Max Q Clear Time (g, c+H1), s | 7.9 | 15.5 | 32.7 | 18.0 | 33.2 | 25.6 | 33.2 | 25.6 |
| Green Ext Time (p, c), s | 0.3 | 36.5 | 2.2 | 7.2 | 1.6 | 28.5 | 1.6 | 28.5 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 17.3 |
| HCM 2010 LOS | B |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBT | SBR |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1336 | 469 | 242 | 1648 | 0 | 0 | 0 | 0 | 762 | 12 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 0 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1452 | 510 | 263 | 1791 | 0 | 514 | 514 | 837 | 0 | 514 |
| Adj No. of Lanes | 0 | 2 | 2 | 2 | 3 | 0 | 2 | 2 | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1560 | 1228 | 276 | 2854 | 0 | 1238 | 1238 | 0 | 552 | 0 |
| Arrive On Green | 0.00 | 0.45 | 0.45 | 0.08 | 0.57 | 0.00 | 0.35 | 0.00 | 0.35 | 0.00 | 0.35 |
| Sat Flow, veh/h | 0 | 3597 | 2760 | 3408 | 5202 | 0 | 3514 | 3514 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 1452 | 510 | 263 | 1791 | 0 | 837 | 837 | 0 | 514 | 0 |
| Grip Sat Flow(s), veh/h/ln | 0 | 1752 | 1380 | 1704 | 1679 | 0 | 1757 | 1757 | 0 | 1568 | 0 |
| Q Serve(g, s) | 0.0 | 38.8 | 12.4 | 7.6 | 23.6 | 0.0 | 20.0 | 20.0 | 0.0 | 31.2 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 38.8 | 12.4 | 7.6 | 23.6 | 0.0 | 20.0 | 20.0 | 0.0 | 31.2 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Lane Grp Cap(c), veh/h | 0 | 1560 | 1228 | 276 | 2854 | 0 | 1238 | 1238 | 0 | 552 | 0 |
| V/C Ratio(X) | 0.00 | 0.93 | 0.42 | 0.95 | 0.63 | 0.00 | 0.68 | 0.00 | 0.93 | 0.00 | 0.93 |
| Avail Cap(c,a), veh/h | 0 | 1562 | 1230 | 276 | 2856 | 0 | 1281 | 1281 | 0 | 572 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 26.0 | 18.6 | 45.2 | 14.4 | 0.0 | 27.2 | 27.2 | 0.0 | 30.8 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 10.3 | 0.2 | 41.3 | 0.4 | 0.0 | 1.4 | 1.4 | 0.0 | 21.7 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 20.8 | 4.7 | 5.1 | 10.9 | 0.0 | 9.9 | 9.9 | 0.0 | 16.7 | 0.0 |
| LnGrp Delay(d), s/veh | 0.0 | 36.3 | 18.9 | 86.5 | 14.8 | 0.0 | 28.6 | 28.6 | 0.0 | 52.5 | 0.0 |
| LnGrp LOS | D | D | B | F | B | | C | C | | D | |
| Approach Vol, veh/h | 1962 | | | 2054 | | | 1351 | | | 37.7 | |
| Approach Delay, s/veh | 31.8 | | | 24.0 | | | 37.7 | | | D | |
| Approach LOS | C | | | C | | | D | | | D | |













| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|------|------|------|------|
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 12.0 | 48.0 | 38.8 | 60.0 | 38.8 | 60.0 | 60.0 | 60.0 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 8.0 | 44.0 | 36.0 | 56.0 | 44.0 | 36.0 | 56.0 | 56.0 |
| Max Q Clear Time (g, c+H1), s | 9.6 | 40.8 | 33.2 | 25.6 | 40.8 | 33.2 | 25.6 | 25.6 |
| Green Ext Time (p, c), s | 0.0 | 3.2 | 1.6 | 28.5 | 1.6 | 28.5 | 1.6 | 28.5 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 30.3 |
| HCM 2010 LOS | C |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

| | | | | | | | | | | | | |
|--|---|---|---|---|---|---|---|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ←←← | ←←← | ← | ← | ←←← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 0 | 1483 | 607 | 42 | 1531 | 356 | 355 | 27 | 322 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Ped-Bike Adj(A, pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | | | |
| Adj Flow Rate, veh/h | 0 | 1612 | 443 | 46 | 1664 | 387 | 407 | 0 | 323 | | | |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | | |
| Cap. veh/h | 0 | 2959 | 921 | 59 | 3382 | 1053 | 797 | 0 | 356 | | | |
| Arrive On Green | 0.00 | 0.59 | 0.59 | 0.03 | 0.67 | 0.67 | 0.23 | 0.00 | 0.23 | | | |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | | | |
| Grip Volume(v), veh/h | 0 | 1612 | 443 | 46 | 1664 | 387 | 407 | 0 | 323 | | | |
| Grip Sat Flow(s),veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | | | |
| Q Serve(g, s), s | 0.0 | 15.3 | 12.8 | 2.0 | 12.8 | 8.5 | 8.0 | 0.0 | 15.8 | | | |
| Cycle Q Clear(g, c), s | 0.0 | 15.3 | 12.8 | 2.0 | 12.8 | 8.5 | 8.0 | 0.0 | 15.8 | | | |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Lane Grp Cap(c), veh/h | 0 | 2959 | 921 | 59 | 3382 | 1053 | 797 | 0 | 356 | | | |
| V/C Ratio(X) | 0.00 | 0.54 | 0.48 | 0.79 | 0.49 | 0.37 | 0.51 | 0.00 | 0.91 | | | |
| Avail Cap(c,a), veh/h | 0 | 2959 | 921 | 825 | 4728 | 1472 | 802 | 0 | 358 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 0.0 | 9.9 | 9.3 | 37.8 | 6.3 | 5.6 | 26.6 | 0.0 | 29.7 | | | |
| Incr Delay (d2), s/veh | 0.0 | 0.2 | 0.4 | 20.1 | 0.1 | 0.2 | 0.5 | 0.0 | 26.0 | | | |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%) veh/ln | 0.0 | 7.1 | 5.6 | 1.3 | 5.9 | 3.7 | 3.9 | 0.0 | 9.4 | | | |
| LnGrp Delay(d),s/veh | 0.0 | 10.1 | 9.7 | 57.9 | 6.5 | 5.9 | 27.2 | 0.0 | 55.7 | | | |
| LnGrp LOS | | B | A | E | A | A | C | | E | | | |
| Approach Vol, veh/h | | 2055 | | | 2097 | | | 730 | | | | |
| Approach Delay, s/veh | | 10.0 | | | 7.5 | | | 39.8 | | | | |
| Approach LOS | | A | | | A | | | D | | | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | | 2 | 3 | 4 | | | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | | 21.9 | 6.6 | 50.3 | | | | 56.9 | | | | |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | | 4.0 | | | | |
| Max Green Setting (Gmax), s | | 18.0 | 37.0 | 33.0 | | | | 74.0 | | | | |
| Max Q Clear Time (g, c+H1), s | | 17.8 | 4.0 | 17.3 | | | | 14.8 | | | | |
| Green Ext Time (p, c), s | | 0.1 | 0.1 | 15.0 | | | | 38.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | | 13.4 | | | | | | | |
| HCM 2010 LOS | | | | | B | | | | | | | |
| Notes | | | | | | | | | | | | |
| User approved volume balancing among the lanes for turning movement. | | | | | | | | | | | | |

User approved ignoring U-Turning movement.

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 120 | 1095 | 77 | 207 | 1511 | 144 | 164 | 92 | 128 | 37 | 81 | 87 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbt}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 130 | 1190 | 48 | 225 | 1642 | 117 | 178 | 100 | 114 | 40 | 88 | 95 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 2 | 1 | 1 | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 172 | 2012 | 627 | 279 | 2320 | 722 | 267 | 292 | 249 | 109 | 196 | 175 |
| Arrive On Green | 0.10 | 0.40 | 0.40 | 0.16 | 0.46 | 0.46 | 0.08 | 0.16 | 0.16 | 0.03 | 0.11 | 0.11 |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 5036 | 1568 | 1704 | 1845 | 1568 | 3408 | 1752 | 1568 |
| Grip Volume(v), veh/h | 130 | 1190 | 48 | 225 | 1642 | 117 | 178 | 100 | 114 | 40 | 88 | 95 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1679 | 1568 | 1757 | 1679 | 1568 | 1704 | 1845 | 1568 | 1704 | 1752 | 1568 |
| Q Serve(g, s) | 4.6 | 11.8 | 1.2 | 7.9 | 16.6 | 2.8 | 3.2 | 3.1 | 4.2 | 0.7 | 3.0 | 3.6 |
| Cycle Q Clear(g, c), s | 4.6 | 11.8 | 1.2 | 7.9 | 16.6 | 2.8 | 3.2 | 3.1 | 4.2 | 0.7 | 3.0 | 3.6 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grip Cap(c), veh/h | 172 | 2012 | 627 | 279 | 2320 | 722 | 267 | 292 | 249 | 109 | 196 | 175 |
| V/C Ratio(X) | 0.76 | 0.59 | 0.08 | 0.81 | 0.71 | 0.16 | 0.67 | 0.34 | 0.46 | 0.37 | 0.45 | 0.54 |
| Avail Cap(c,a), veh/h | 1103 | 3240 | 1009 | 579 | 2320 | 722 | 267 | 521 | 443 | 214 | 467 | 418 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 28.0 | 15.0 | 11.8 | 25.9 | 13.8 | 10.0 | 28.5 | 23.9 | 24.3 | 30.2 | 26.5 | 26.7 |
| Incr Delay (d2), s/veh | 6.6 | 0.3 | 0.1 | 5.4 | 1.0 | 0.1 | 6.1 | 0.7 | 1.3 | 2.1 | 1.6 | 2.6 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 2.6 | 5.5 | 0.5 | 4.2 | 7.8 | 1.2 | 1.7 | 1.6 | 1.9 | 0.4 | 1.5 | 1.7 |
| LnGrp Delay(d), s/veh | 34.6 | 15.3 | 11.9 | 31.3 | 14.8 | 10.1 | 34.7 | 24.5 | 25.6 | 32.3 | 28.1 | 29.3 |
| LnGrp LOS | C | B | B | C | B | B | C | C | C | C | C | C |
| Approach Vol, veh/h | 1368 | | | 1984 | | | 392 | | | 223 | | |
| Approach Delay, s/veh | 17.0 | | | 16.4 | | | 29.5 | | | 29.4 | | |
| Approach LOS | B | | | B | | | C | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|------|------|-----|------|------|------|
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 6.0 | 14.1 | 14.1 | 29.5 | 9.0 | 11.1 | 10.2 | 33.4 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 4.0 | 18.0 | 21.0 | 41.0 | 5.0 | 17.0 | 40.0 | 22.0 |
| Max Q Clear Time (g, c+1), s | 2.7 | 6.2 | 9.9 | 13.8 | 5.2 | 5.6 | 6.6 | 18.6 |
| Green Ext Time (p, c), s | 0.0 | 1.5 | 0.4 | 11.6 | 0.0 | 1.5 | 0.3 | 3.2 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 18.6 | | | | | | | |
| HCM 2010 LOS | B | | | | | | | |
| Notes | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Country Hills Road & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 7 | 905 | 420 | 127 | 843 | 29 | 160 | 0 | 330 | 84 | 0 | 8 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbt}) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 8 | 984 | 457 | 138 | 916 | 32 | 174 | 0 | 359 | 91 | 0 | 9 |
| Adj No. of Lanes | 1 | 2 | 0 | 2 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 14 | 1073 | 489 | 202 | 1760 | 61 | 207 | 0 | 390 | 115 | 0 | 308 |
| Arrive On Green | 0.01 | 0.46 | 0.46 | 0.06 | 0.51 | 0.51 | 0.12 | 0.00 | 0.25 | 0.07 | 0.00 | 0.20 |
| Sat Flow, veh/h | 1757 | 2341 | 1068 | 3408 | 3455 | 121 | 1757 | 0 | 1568 | 1757 | 0 | 1568 |
| Grip Volume(v), veh/h | 8 | 732 | 709 | 138 | 465 | 483 | 174 | 0 | 359 | 91 | 0 | 9 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 1656 | 1704 | 1752 | 1823 | 1757 | 0 | 1568 | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.4 | 37.0 | 38.6 | 3.8 | 16.8 | 16.8 | 9.2 | 0.0 | 21.2 | 4.9 | 0.0 | 0.4 |
| Cycle Q Clear(g, c), s | 0.4 | 37.0 | 38.6 | 3.8 | 16.8 | 16.8 | 9.2 | 0.0 | 21.2 | 4.9 | 0.0 | 0.4 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grip Cap(c), veh/h | 14 | 803 | 759 | 202 | 893 | 929 | 207 | 0 | 390 | 115 | 0 | 308 |
| V/C Ratio(X) | 0.57 | 0.91 | 0.93 | 0.68 | 0.52 | 0.52 | 0.84 | 0.00 | 0.92 | 0.79 | 0.00 | 0.03 |
| Avail Cap(c,a), veh/h | 74 | 829 | 783 | 215 | 893 | 929 | 240 | 0 | 412 | 148 | 0 | 330 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 47.0 | 24.0 | 24.4 | 43.9 | 15.6 | 15.6 | 41.1 | 0.0 | 34.8 | 43.8 | 0.0 | 30.9 |
| Incr Delay (d2), s/veh | 31.3 | 14.0 | 17.8 | 8.0 | 0.5 | 0.5 | 20.5 | 0.0 | 25.2 | 19.2 | 0.0 | 0.0 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.3 | 20.8 | 21.3 | 2.0 | 8.3 | 8.6 | 5.7 | 0.0 | 11.9 | 3.0 | 0.0 | 0.2 |
| LnGrp Delay(d), s/veh | 78.4 | 38.0 | 42.2 | 51.9 | 16.1 | 16.1 | 61.6 | 0.0 | 60.0 | 63.0 | 0.0 | 30.9 |
| LnGrp LOS | E | D | D | D | B | B | E | E | E | E | E | C |
| Approach Vol, veh/h | 1449 | | | 1086 | | | 533 | | | 100 | | |
| Approach Delay, s/veh | 40.3 | | | 20.7 | | | 60.5 | | | 60.1 | | |
| Approach LOS | D | | | C | | | E | | | E | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|-----|------|------|------|-----|------|
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 10.3 | 27.7 | 9.6 | 47.6 | 15.2 | 22.7 | 4.8 | 52.5 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 8.0 | 25.0 | 6.0 | 45.0 | 13.0 | 20.0 | 4.0 | 47.0 |
| Max Q Clear Time (g, c+H1), s | 6.9 | 23.2 | 5.8 | 40.6 | 11.2 | 2.4 | 2.4 | 18.8 |
| Green Ext Time (p, c), s | 0.0 | 0.4 | 0.0 | 3.0 | 0.1 | 2.3 | 0.0 | 18.9 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 37.6 | | | | | | | |
| HCM 2010 LOS | D | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
11: Slatten Ranch Road & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ←←← | → | ← | ←←← | ← | ←← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 188 | 1071 | 643 | 263 | 785 | 355 | 421 | 208 | 120 | 123 | 180 | 51 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 204 | 1164 | 356 | 286 | 853 | 386 | 458 | 226 | 130 | 134 | 196 | 55 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 0 | 2 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 242 | 1713 | 533 | 327 | 1320 | 595 | 547 | 412 | 228 | 169 | 339 | 93 |
| Arrive On Green | 0.14 | 0.34 | 0.34 | 0.19 | 0.39 | 0.39 | 0.16 | 0.19 | 0.19 | 0.10 | 0.12 | 0.12 |
| Sat Flow, veh/h | 1757 | 5036 | 1568 | 1757 | 3393 | 1533 | 3408 | 2178 | 1206 | 1757 | 2721 | 744 |
| Grip Volume(v), veh/h | 204 | 1164 | 356 | 286 | 843 | 396 | 458 | 180 | 176 | 134 | 124 | 127 |
| Grip Sat Flow(s),veh/h | 1757 | 1679 | 1568 | 1757 | 1679 | 1574 | 1704 | 1752 | 1632 | 1757 | 1752 | 1713 |
| Q Serve(g, s) | 9.6 | 16.8 | 16.4 | 13.4 | 17.4 | 17.4 | 11.0 | 7.9 | 8.3 | 6.3 | 5.7 | 5.9 |
| Cycle Q Clear(g, c), s | 9.6 | 16.8 | 16.4 | 13.4 | 17.4 | 17.4 | 11.0 | 7.9 | 8.3 | 6.3 | 5.7 | 5.9 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 0.74 | 1.00 | 1.00 | 0.43 | 0.43 |
| Lane Grp Cap(c), veh/h | 242 | 1713 | 533 | 327 | 1303 | 611 | 547 | 331 | 308 | 169 | 218 | 214 |
| V/C Ratio(X) | 0.84 | 0.68 | 0.67 | 0.88 | 0.65 | 0.65 | 0.84 | 0.54 | 0.57 | 0.80 | 0.57 | 0.56 |
| Avail Cap(c, a), veh/h | 311 | 1784 | 555 | 415 | 1387 | 651 | 644 | 393 | 366 | 311 | 372 | 364 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 35.6 | 24.0 | 23.9 | 33.5 | 21.2 | 21.2 | 34.5 | 31.0 | 31.2 | 37.5 | 34.9 | 35.0 |
| Incr Delay (d2), s/veh | 15.1 | 1.0 | 2.9 | 15.5 | 1.0 | 2.1 | 8.4 | 1.4 | 1.7 | 8.2 | 2.3 | 2.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/h | 5.7 | 7.9 | 7.5 | 7.9 | 8.1 | 8.0 | 5.9 | 3.9 | 3.9 | 3.4 | 2.9 | 3.0 |
| LnGrp Delay(d),s/veh | 50.7 | 25.0 | 26.8 | 49.0 | 22.1 | 23.3 | 42.9 | 32.4 | 32.9 | 45.7 | 37.3 | 37.7 |
| LnGrp LOS | D | C | C | D | C | C | D | C | C | D | D | D |
| Approach Vol, veh/h | 1724 | | | 1525 | | | 814 | | | 385 | | |
| Approach Delay, s/veh | 28.4 | | | 27.5 | | | 38.4 | | | 40.3 | | |
| Approach LOS | C | | | C | | | D | | | D | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.1 | 20.0 | 19.8 | 32.8 | 17.6 | 14.6 | 15.7 | 36.9 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 15.0 | 19.0 | 20.0 | 30.0 | 16.0 | 18.0 | 15.0 | 35.0 | | | | |
| Max Q Clear Time (g, c+H1), s | 8.3 | 10.3 | 15.4 | 18.8 | 13.0 | 7.9 | 11.6 | 19.4 | | | | |
| Green Ext Time (p, c), s | 0.2 | 2.4 | 0.4 | 10.0 | 0.5 | 2.6 | 0.2 | 13.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 30.9 | | | | | | | | | | | |
| HCM 2010 LOS | C | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
AM Cumulative Plus Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
2: Hillcrest Ave & SR 4 EB Ramps

10/27/2015

| | ↖ | → | ↗ | ↖ | ← | ↗ | ↖ | ↗ | ↖ | ↗ | ↖ | ↗ |
|-------------------------------|------|------|------|------|-----|------|-------|------|-------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ↖ | ↖ | ↖ | | | | | ↖ | ↖ | ↖ | ↖ | ↖ |
| Volume (veh/h) | 312 | 0 | 1197 | 0 | 0 | 0 | 0 | 553 | 571 | 328 | 967 | 0 |
| Number | 7 | 4 | 14 | | | | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | | | | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/hIn | 1845 | 1845 | 1845 | | | | 1845 | 1900 | 1845 | 1845 | 1845 | 0 |
| Adj Flow Rate, veh/h | 328 | 0 | 1260 | | | | 0 | 582 | 601 | 345 | 1018 | 0 |
| Adj No. of Lanes | 2 | 0 | 2 | | | | 0 | 3 | 0 | 2 | 2 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | | | | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 3 | 3 | 3 | | | | 0 | 3 | 3 | 3 | 3 | 0 |
| Cap. veh/h | 1601 | 0 | 1429 | | | | 0 | 966 | 451 | 422 | 1597 | 0 |
| Arrive On Green | 0.46 | 0.00 | 0.46 | | | | 0.00 | 0.29 | 0.29 | 0.12 | 0.46 | 0.00 |
| Sat Flow, veh/h | 3514 | 0 | 3136 | | | | 0 | 3523 | 1568 | 3408 | 3597 | 0 |
| Gp Volume(v), veh/h | 328 | 0 | 1260 | | | | 0 | 582 | 601 | 345 | 1018 | 0 |
| Gp Sat Flow(s)/veh/hIn | 1757 | 0 | 1588 | | | | 0 | 1679 | 1588 | 1704 | 1752 | 0 |
| Q Serve(g, s), s | 5.1 | 0.0 | 33.0 | | | | 0.0 | 13.5 | 26.0 | 8.9 | 20.1 | 0.0 |
| Cycle Q Clear(g, c), s | 5.1 | 0.0 | 33.0 | | | | 0.0 | 13.5 | 26.0 | 8.9 | 20.1 | 0.0 |
| Prop In Lane | 1.00 | | 1.00 | | | | 0.00 | | 1.00 | 1.00 | | 0.00 |
| Lane Grp Cap(c), veh/h | 1601 | 0 | 1429 | | | | 0 | 966 | 451 | 422 | 1597 | 0 |
| V/C Ratio(X) | 0.20 | 0.00 | 0.88 | | | | 0.00 | 0.60 | 1.33 | 0.82 | 0.64 | 0.00 |
| Avail Cap(c,a), veh/h | 1905 | 0 | 1700 | | | | 0 | 966 | 451 | 490 | 1668 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | | | | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 14.8 | 0.0 | 22.4 | | | | 0.0 | 27.7 | 32.2 | 38.6 | 18.9 | 0.0 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 5.1 | | | | 0.0 | 1.1 | 164.1 | 9.2 | 0.8 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/hIn | 2.5 | 0.0 | 15.2 | | | | 0.0 | 6.4 | 31.7 | 4.8 | 9.8 | 0.0 |
| LnGrp Delay(d),s/veh | 14.8 | 0.0 | 27.5 | | | | 0.0 | 28.8 | 196.3 | 47.8 | 19.6 | 0.0 |
| LnGrp LOS | B | C | C | | | | C | F | D | D | B | |
| Approach Vol, veh/h | 1588 | | | | | | 1183 | | | 1363 | | |
| Approach Delay, s/veh | 24.9 | | | | | | 113.9 | | | 26.8 | | |
| Approach LOS | C | | | | | | F | | | C | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 15.2 | 30.0 | | 45.2 | | 45.2 | | | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | | 4.0 | | 4.0 | | | | | | |
| Max Green Setting (Gmax), s | 13.0 | 26.0 | | 49.0 | | 43.0 | | | | | | |
| Max Q Clear Time (g, c+H1), s | 10.9 | 28.0 | | 35.0 | | 22.1 | | | | | | |
| Green Ext Time (p, c), s | 0.3 | 0.0 | | 6.1 | | 15.3 | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 51.0 | | | | | | | | | | | |
| HCM 2010 LOS | D | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
3: Hillcrest Ave & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBL | EBR | WBL | WBT | WBL | NBL | NBT | NBL | NBR | SBL | SBT | SBL | SBR |
|----------------------------|------|------|-------|-------|------|------|-------|------|------|-------|------|------|-----|-----|-----|
| Lane Configurations | EBL | EBT | EBL | EBR | WBL | WBT | WBL | NBL | NBT | NBL | NBR | SBL | SBT | SBL | SBR |
| Volume (veh/h) | 208 | 115 | 157 | 497 | 307 | 285 | 120 | 1405 | 418 | 327 | 1111 | 288 | | | |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Adj Sat Flow, veh/h | 1845 | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | | | |
| Adj Flow Rate, veh/h | 219 | 121 | 165 | 523 | 323 | 153 | 126 | 1479 | 0 | 344 | 1169 | 303 | | | |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 2 | 0 | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | | |
| Cap. veh/h | 297 | 269 | 367 | 344 | 701 | 596 | 123 | 1332 | 0 | 211 | 1188 | 305 | | | |
| Arrive On Green | 0.38 | 0.38 | 0.38 | 0.38 | 0.38 | 0.38 | 0.07 | 0.38 | 0.00 | 0.12 | 0.43 | 0.43 | | | |
| Sat Flow, veh/h | 906 | 708 | 966 | 1078 | 1845 | 1568 | 1757 | 3597 | 0 | 1757 | 2764 | 708 | | | |
| Grip Volume(v), veh/h | 219 | 0 | 286 | 523 | 323 | 153 | 126 | 1479 | 0 | 344 | 736 | 736 | | | |
| Grip Sat Flow(s), veh/h | 906 | 0 | 1674 | 1078 | 1845 | 1568 | 1757 | 1752 | 0 | 1757 | 1752 | 1720 | | | |
| Q Serve(g, s) | 24.0 | 0.0 | 12.8 | 25.2 | 13.2 | 6.7 | 7.0 | 38.0 | 0.0 | 12.0 | 41.3 | 42.6 | | | |
| Cycle Q Clear(g, c), s | 37.1 | 0.0 | 12.8 | 38.0 | 13.2 | 6.7 | 7.0 | 38.0 | 0.0 | 12.0 | 41.3 | 42.6 | | | |
| Prop In Lane | 1.00 | 0.58 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.41 | | | |
| Lane Grp Cap(c), veh/h | 297 | 0 | 636 | 344 | 701 | 596 | 123 | 1332 | 0 | 211 | 754 | 739 | | | |
| V/C Ratio(X) | 0.74 | 0.00 | 0.45 | 1.52 | 0.46 | 0.26 | 1.02 | 1.11 | 0.00 | 1.63 | 0.98 | 0.99 | | | |
| Avail Cap(c.a), veh/h | 297 | 0 | 636 | 344 | 701 | 596 | 123 | 1332 | 0 | 211 | 754 | 739 | | | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | | | |
| Uniform Delay (d), s/veh | 37.3 | 0.0 | 23.2 | 40.0 | 23.3 | 21.3 | 46.5 | 31.0 | 0.0 | 44.0 | 28.0 | 28.4 | | | |
| Incr Delay (d2), s/veh | 9.3 | 0.0 | 0.5 | 248.6 | 0.5 | 0.2 | 87.9 | 60.8 | 0.0 | 304.8 | 27.1 | 31.7 | | | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | |
| %ile BackOfQ(50%), veh/h | 6.7 | 0.0 | 6.0 | 33.2 | 6.7 | 2.9 | 6.4 | 29.6 | 0.0 | 23.6 | 25.5 | 26.5 | | | |
| LnGrp Delay(d), s/veh | 46.5 | 0.0 | 23.7 | 288.6 | 23.8 | 21.5 | 134.7 | 91.8 | 0.0 | 348.8 | 55.1 | 60.1 | | | |
| LnGrp LOS | D | | C | F | C | C | F | F | F | F | F | E | | | |
| Approach Vol, veh/h | 505 | | 999 | | 1605 | | | | | 1816 | | | | | |
| Approach Delay, s/veh | 33.6 | | 162.1 | | 95.2 | | | | | 112.8 | | | | | |
| Approach LOS | C | | F | | F | | | | | F | | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|-------|------|------|------|---|---|
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 | | |
| Phs Duration (G+Y+Rc), s | 16.0 | 42.0 | 42.0 | 11.0 | 47.0 | 42.0 | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Max Green Setting (Gmax), s | 12.0 | 38.0 | 38.0 | 7.0 | 43.0 | 38.0 | | |
| Max Q Clear Time (g, c+H1), s | 14.0 | 40.0 | 39.1 | 9.0 | 44.6 | 40.0 | | |
| Green Ext Time (p, c), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 108.9 | | | | | |
| HCM 2010 LOS | | | F | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
4: Canada Valley Road & Laurel Road

10/27/2015

| Movement | EBT | EBL | EBR | WBL | WBT | NBL | NBR |
|----------------------------|------|------|------|------|------|------|-----|
| Lane Configurations | EBT | EBL | EBR | WBL | WBT | NBL | NBR |
| Volume (veh/h) | 701 | 216 | 687 | 956 | 66 | 395 | |
| Number | 4 | 14 | 3 | 8 | 5 | 12 | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Adj Sat Flow, veh/h | 1845 | 1900 | 1845 | 1845 | 1845 | 1845 | |
| Adj Flow Rate, veh/h | 762 | 235 | 747 | 1039 | 72 | 215 | |
| Adj No. of Lanes | 2 | 0 | 1 | 2 | 1 | 1 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | |
| Cap. veh/h | 752 | 232 | 768 | 2672 | 274 | 245 | |
| Arrive On Green | 0.28 | 0.28 | 0.44 | 0.76 | 0.16 | 0.16 | |
| Sat Flow, veh/h | 2732 | 814 | 1757 | 3597 | 1757 | 1568 | |
| Grip Volume(v), veh/h | 506 | 491 | 747 | 1039 | 72 | 215 | |
| Grip Sat Flow(s), veh/h | 1752 | 1701 | 1757 | 1752 | 1757 | 1568 | |
| Q Serve(g, s) | 28.0 | 28.0 | 41.0 | 9.8 | 3.5 | 13.2 | |
| Cycle Q Clear(g, c), s | 28.0 | 28.0 | 41.0 | 9.8 | 3.5 | 13.2 | |
| Prop In Lane | 0.48 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Lane Grp Cap(c), veh/h | 499 | 484 | 768 | 2672 | 274 | 245 | |
| V/C Ratio(X) | 1.01 | 1.01 | 0.97 | 0.39 | 0.26 | 0.88 | |
| Avail Cap(c.a), veh/h | 499 | 484 | 768 | 2673 | 304 | 271 | |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Uniform Delay (d), s/veh | 35.2 | 35.2 | 27.1 | 3.9 | 36.5 | 40.6 | |
| Incr Delay (d2), s/veh | 43.8 | 44.4 | 25.8 | 0.1 | 0.5 | 24.6 | |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| %ile BackOfQ(50%), veh/h | 19.5 | 19.0 | 25.2 | 4.7 | 1.8 | 7.4 | |
| LnGrp Delay(d), s/veh | 79.0 | 79.6 | 53.0 | 4.0 | 37.0 | 65.2 | |
| LnGrp LOS | F | F | D | A | D | E | |
| Approach Vol, veh/h | 997 | | 1786 | | 287 | | |
| Approach Delay, s/veh | 79.3 | | 24.5 | | 58.1 | | |
| Approach LOS | E | | C | | E | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------------------------------|------|------|------|------|---|---|---|---|
| Assigned Phs | 1 | 2 | 3 | 4 | | | | |
| Phs Duration (G+Y+Rc), s | 19.4 | 47.0 | 32.0 | 79.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 17.0 | 43.0 | 28.0 | 75.0 | | | | |
| Max Q Clear Time (g, c+H1), s | 15.2 | 43.0 | 30.0 | 11.8 | | | | |
| Green Ext Time (p, c), s | 0.2 | 0.0 | 0.0 | 25.9 | | | | |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | | | 45.4 | | | | | |
| HCM 2010 LOS | | | D | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

5: SR 4 EB On-Ramps/SR 4 EB Off-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 0 | 1312 | 64 | 0 | 1192 | 20 | 0 | 0 | 0 | 712 | 0 | 601 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | | | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1900 | 0 | 1845 | 1900 | | | | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1426 | 70 | 0 | 1296 | 0 | | | | 774 | 0 | 653 |
| Adj No. of Lanes | 0 | 2 | 0 | 0 | 2 | 0 | | | | 2 | 0 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1570 | 77 | 0 | 1618 | 0 | | | | 1596 | 0 | 712 |
| Arrive On Green | 0.00 | 0.46 | 0.00 | 0.46 | 0.00 | 0.00 | | | | 0.45 | 0.00 | 0.45 |
| Sat Flow, veh/h | 0 | 3493 | 167 | 0 | 3689 | 0 | | | | 3514 | 0 | 1568 |
| Grip Volume(v), veh/h | 0 | 733 | 763 | 0 | 1296 | 0 | | | | 774 | 0 | 653 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1815 | 0 | 1752 | 0 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 0.0 | 36.7 | 37.0 | 0.0 | 30.0 | 0.0 | | | | 14.6 | 0.0 | 36.9 |
| Cycle Q Clear(g, c), s | 0.0 | 36.7 | 37.0 | 0.0 | 30.0 | 0.0 | | | | 14.6 | 0.0 | 36.9 |
| Prop In Lane | 0.00 | 0.09 | 0.00 | 0.00 | 0.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 809 | 838 | 0 | 1618 | 0 | | | | 1596 | 0 | 712 |
| V/C Ratio(X) | 0.00 | 0.91 | 0.91 | 0.00 | 0.80 | 0.00 | | | | 0.49 | 0.00 | 0.92 |
| Avail Cap(c,a), veh/h | 0 | 813 | 842 | 0 | 1626 | 0 | | | | 1779 | 0 | 794 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 23.6 | 23.7 | 0.0 | 21.8 | 0.0 | | | | 18.1 | 0.0 | 24.2 |
| Incr Delay (d2), s/veh | 0.0 | 13.7 | 13.9 | 0.0 | 3.0 | 0.0 | | | | 0.2 | 0.0 | 14.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 20.8 | 21.7 | 0.0 | 15.1 | 0.0 | | | | 7.1 | 0.0 | 18.8 |
| LnGrp Delay(d),s/veh | 0.0 | 37.4 | 37.6 | 0.0 | 24.8 | 0.0 | | | | 18.3 | 0.0 | 38.7 |
| LnGrp LOS | D | D | D | C | C | C | | | | B | D | D |
| Approach Vol, veh/h | 1496 | | | 1296 | | | | | | 1427 | | |
| Approach Delay, s/veh | 37.5 | | | 24.8 | | | | | | 27.7 | | |
| Approach LOS | D | | | C | | | | | | C | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|---|---|------|---|------|---|------|
| Assigned Phs | | | | 4 | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | | | 47.8 | | 47.1 | | 47.8 |
| Change Period (Y+Rc), s | | | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | | | 44.0 | | 48.0 | | 44.0 |
| Max Q Clear Time (g_c+H1), s | | | | 39.0 | | 38.9 | | 32.0 |
| Green Ext Time (p_c), s | | | | 4.7 | | 4.1 | | 11.0 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 30.3 | | | | | | | |
| HCM 2010 LOS | C | | | | | | | |
| Notes | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

6: SR 4 WB Off-Ramps/SR 4 WB On-Ramps & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|-----|-----|-----|------|------|------|
| Lane Configurations | | ↔ | ↔ | ↔ | ↔ | ↔ | | | | ↔ | ↔ | ↔ |
| Volume (veh/h) | 250 | 1474 | 0 | 0 | 1067 | 736 | 209 | 0 | 339 | 0 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | | | | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 0 | 0 | 1845 | 1845 | | | | 1900 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 272 | 1602 | 0 | 0 | 1160 | 0 | | | | 227 | 0 | 368 |
| Adj No. of Lanes | 1 | 2 | 0 | 0 | 2 | 1 | | | | 0 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 0 | 0 | 3 | 3 | | | | 3 | 3 | 3 |
| Cap. veh/h | 311 | 2237 | 0 | 0 | 1457 | 652 | | | | 475 | 0 | 424 |
| Arrive On Green | 0.18 | 0.64 | 0.00 | 0.00 | 0.42 | 0.00 | | | | 0.27 | 0.00 | 0.27 |
| Sat Flow, veh/h | 1757 | 3597 | 0 | 0 | 3597 | 1568 | | | | 1757 | 0 | 1568 |
| Grip Volume(v), veh/h | 272 | 1602 | 0 | 0 | 1160 | 0 | | | | 227 | 0 | 368 |
| Grip Sat Flow(s),veh/h/ln | 1757 | 1752 | 0 | 0 | 1752 | 1568 | | | | 1757 | 0 | 1568 |
| Q Serve(g, s) | 13.2 | 26.6 | 0.0 | 0.0 | 25.3 | 0.0 | | | | 9.5 | 0.0 | 19.6 |
| Cycle Q Clear(g, c), s | 13.2 | 26.6 | 0.0 | 0.0 | 25.3 | 0.0 | | | | 9.5 | 0.0 | 19.6 |
| Prop In Lane | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 311 | 2237 | 0 | 0 | 1457 | 652 | | | | 475 | 0 | 424 |
| V/C Ratio(X) | 0.88 | 0.72 | 0.00 | 0.00 | 0.80 | 0.00 | | | | 0.48 | 0.00 | 0.87 |
| Avail Cap(c,a), veh/h | 382 | 2406 | 0 | 0 | 1484 | 664 | | | | 574 | 0 | 574 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | | | | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 35.0 | 10.5 | 0.0 | 0.0 | 22.3 | 0.0 | | | | 26.7 | 0.0 | 30.4 |
| Incr Delay (d2), s/veh | 17.1 | 1.0 | 0.0 | 0.0 | 3.1 | 0.0 | | | | 0.7 | 0.0 | 10.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 7.9 | 13.0 | 0.0 | 0.0 | 12.7 | 0.0 | | | | 4.7 | 0.0 | 9.7 |
| LnGrp Delay(d),s/veh | 52.2 | 11.5 | 0.0 | 0.0 | 25.4 | 0.0 | | | | 27.5 | 0.0 | 40.8 |
| LnGrp LOS | D | B | C | C | C | C | | | | D | D | D |
| Approach Vol, veh/h | 1874 | | | 1160 | | | | | | 595 | | |
| Approach Delay, s/veh | 17.4 | | | 25.4 | | | | | | 35.7 | | |
| Approach LOS | B | | | C | | | | | | D | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|------|------|---|------|---|------|---|------|
| Assigned Phs | | 2 | | 4 | | 7 | | 8 |
| Phs Duration (G+Y+Rc), s | | 27.6 | | 59.8 | | 19.5 | | 40.3 |
| Change Period (Y+Rc), s | | 4.0 | | 4.0 | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | 32.0 | | 60.0 | | 19.0 | | 37.0 |
| Max Q Clear Time (g_c+H1), s | | 21.6 | | 28.6 | | 15.2 | | 27.3 |
| Green Ext Time (p_c), s | | 2.1 | | 26.2 | | 0.3 | | 9.1 |
| Intersection Summary | | | | | | | | |
| HCM 2010 Ctrl Delay | 23.0 | | | | | | | |
| HCM 2010 LOS | C | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

7: SR 4 EB On-ramps/SR 4 EB Off-Ramps & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|-------|------|
| Lane Configurations | → | → | → | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 0 | 1563 | 851 | 282 | 1689 | 0 | 0 | 0 | 0 | 928 | 10 | 601 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 0 | 0 | 0 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 1645 | 896 | 297 | 1778 | 0 | 985 | 0 | 985 | 0 | 633 | 0 |
| Adj No. of Lanes | 0 | 2 | 2 | 2 | 3 | 0 | 2 | 0 | 2 | 0 | 1 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 0 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 1507 | 1187 | 307 | 2820 | 0 | 1265 | 0 | 1265 | 0 | 564 | 0 |
| Arrive On Green | 0.00 | 0.43 | 0.43 | 0.09 | 0.56 | 0.00 | 0.36 | 0.00 | 0.36 | 0.00 | 0.36 | 0.00 |
| Sat Flow, veh/h | 0 | 3597 | 2760 | 3408 | 5202 | 0 | 3514 | 0 | 3514 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 1645 | 896 | 297 | 1778 | 0 | 985 | 0 | 985 | 0 | 633 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1752 | 1380 | 1704 | 1679 | 0 | 1757 | 0 | 1757 | 0 | 1568 | 0 |
| Q Serve(g, s), s | 0.0 | 43.0 | 27.4 | 8.7 | 24.0 | 0.0 | 24.9 | 0.0 | 24.9 | 0.0 | 36.0 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 43.0 | 27.4 | 8.7 | 24.0 | 0.0 | 24.9 | 0.0 | 24.9 | 0.0 | 36.0 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 1507 | 1187 | 307 | 2820 | 0 | 1265 | 0 | 1265 | 0 | 564 | 0 |
| V/C Ratio(X) | 0.00 | 1.09 | 0.76 | 0.97 | 0.63 | 0.00 | 0.78 | 0.00 | 0.78 | 0.00 | 1.12 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 1507 | 1187 | 307 | 2820 | 0 | 1265 | 0 | 1265 | 0 | 564 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 28.5 | 24.1 | 45.4 | 15.0 | 0.0 | 28.5 | 0.0 | 28.5 | 0.0 | 32.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 52.4 | 2.8 | 42.7 | 0.5 | 0.0 | 3.2 | 0.0 | 3.2 | 0.0 | 75.9 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 31.7 | 10.8 | 5.9 | 11.1 | 0.0 | 12.6 | 0.0 | 12.6 | 0.0 | 27.4 | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 | 80.9 | 26.9 | 88.0 | 15.4 | 0.0 | 31.6 | 0.0 | 31.6 | 0.0 | 107.9 | 0.0 |
| LnGrp LOS | F | C | C | F | B | C | C | C | C | C | F | F |
| Approach Vol, veh/h | 2541 | | | 2075 | | | | | | | 1618 | |
| Approach Delay, s/veh | 61.8 | | | 25.8 | | | | | | | 61.4 | |
| Approach LOS | E | | | C | | | | | | | E | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|------|------|---|---|------|---|------|
| Assigned Phs | | 3 | 4 | | | 6 | | 8 |
| Phs Duration (G+Y+Rc), s | | 13.0 | 47.0 | | | 40.0 | | 60.0 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | | | 4.0 | | 4.0 |
| Max Green Setting (Gmax), s | | 9.0 | 43.0 | | | 36.0 | | 56.0 |
| Max Q Clear Time (g_c+H1), s | | 10.7 | 45.0 | | | 38.0 | | 26.0 |
| Green Ext Time (p_c), s | | 0.0 | 0.0 | | | 0.0 | | 29.0 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 49.7 |
| HCM 2010 LOS | D |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | → | → | → | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 0 | 1997 | 566 | 20 | 38 | 1411 | 592 | 609 | 32 | 481 | 0 | 0 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | | | |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 | 1845 |
| Adj Flow Rate, veh/h | 0 | 2102 | 385 | 40 | 1485 | 623 | 665 | 0 | 480 | 0 | 480 | 0 |
| Adj No. of Lanes | 0 | 3 | 1 | 1 | 3 | 1 | 2 | 0 | 1 | 0 | 1 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh. % | 0 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 0 | 2527 | 787 | 50 | 2884 | 898 | 1202 | 0 | 537 | 0 | 537 | 0 |
| Arrive On Green | 0.00 | 0.50 | 0.50 | 0.03 | 0.57 | 0.57 | 0.34 | 0.00 | 0.34 | 0.00 | 0.34 | 0.00 |
| Sat Flow, veh/h | 0 | 5202 | 1568 | 1757 | 5036 | 1568 | 3514 | 0 | 1568 | 0 | 1568 | 0 |
| Grip Volume(v), veh/h | 0 | 2102 | 385 | 40 | 1485 | 623 | 665 | 0 | 480 | 0 | 480 | 0 |
| Grip Sat Flow(s),veh/h/ln | 0 | 1679 | 1568 | 1757 | 1679 | 1568 | 1757 | 0 | 1568 | 0 | 1568 | 0 |
| Q Serve(g, s), s | 0.0 | 33.6 | 15.3 | 2.1 | 16.8 | 26.5 | 14.4 | 0.0 | 27.3 | 0.0 | 27.3 | 0.0 |
| Cycle Q Clear(g, c), s | 0.0 | 33.6 | 15.3 | 2.1 | 16.8 | 26.5 | 14.4 | 0.0 | 27.3 | 0.0 | 27.3 | 0.0 |
| Prop In Lane | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 2527 | 787 | 50 | 2884 | 898 | 1202 | 0 | 537 | 0 | 537 | 0 |
| V/C Ratio(X) | 0.00 | 0.83 | 0.49 | 0.80 | 0.51 | 0.69 | 0.55 | 0.00 | 0.89 | 0.00 | 0.89 | 0.00 |
| Avail Cap(c,a), veh/h | 0 | 2527 | 787 | 75 | 2945 | 917 | 1382 | 0 | 617 | 0 | 617 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 0.00 |
| Uniform Delay (d), s/veh | 0.0 | 20.0 | 15.5 | 45.4 | 12.2 | 14.2 | 25.1 | 0.0 | 29.3 | 0.0 | 29.3 | 0.0 |
| Incr Delay (d2), s/veh | 0.0 | 2.5 | 0.5 | 29.4 | 0.1 | 2.2 | 0.4 | 0.0 | 14.3 | 0.0 | 14.3 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.0 | 16.0 | 6.6 | 1.4 | 7.7 | 12.0 | 7.1 | 0.0 | 13.8 | 0.0 | 13.8 | 0.0 |
| LnGrp Delay(d),s/veh | 0.0 | 22.6 | 15.9 | 74.9 | 12.3 | 16.5 | 25.5 | 0.0 | 43.6 | 0.0 | 43.6 | 0.0 |
| LnGrp LOS | C | C | B | E | B | B | C | C | D | | D | |
| Approach Vol, veh/h | 2487 | | | 2148 | | | 1145 | | | | | |
| Approach Delay, s/veh | 21.5 | | | 14.7 | | | 33.1 | | | | | |
| Approach LOS | C | | | B | | | C | | | | | |

| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------------------|---|------|-----|------|---|---|---|------|
| Assigned Phs | | 2 | 3 | 4 | | | | 8 |
| Phs Duration (G+Y+Rc), s | | 36.2 | 6.7 | 51.2 | | | | 57.9 |
| Change Period (Y+Rc), s | | 4.0 | 4.0 | 4.0 | | | | 4.0 |
| Max Green Setting (Gmax), s | | 37.0 | 4.0 | 47.0 | | | | 55.0 |
| Max Q Clear Time (g_c+H1), s | | 29.3 | 4.1 | 35.6 | | | | 28.5 |
| Green Ext Time (p_c), s | | 2.9 | 0.0 | 11.2 | | | | 25.4 |

| Intersection Summary | |
|----------------------|------|
| HCM 2010 Ctrl Delay | 21.3 |
| HCM 2010 LOS | C |

Notes
User approved volume balancing among the lanes for turning movement.

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

8: Jefferey Way /SR 4 WB On-Ramps & Lone Tree Way

10/27/2015

| Movement | SBR |
|------------------------------|-----|
| Lane Configurations | |
| Volume (veh/h) | 0 |
| Number | |
| Initial Q (Qb), veh | |
| Ped-Bike Adj(A_pbT) | |
| Parking Bus, Adj | |
| Adj Sat Flow, veh/h/ln | |
| Adj Flow Rate, veh/h | |
| Adj No. of Lanes | |
| Peak Hour Factor | |
| Percent Heavy Veh. % | |
| Cap. veh/h | |
| Arrive On Green | |
| Sat Flow, veh/h | |
| Grip Volume(v), veh/h | |
| Grip Sat Flow(s), veh/h/ln | |
| Q Serve(g, s), s | |
| Cycle Q Clear(g_c), s | |
| Prop In Lane | |
| Lane Grip Cap(c), veh/h | |
| V/C Ratio(X) | |
| Avail Cap(c_a), veh/h | |
| HCM Platoon Ratio | |
| Upstream Filter(l) | |
| Uniform Delay (d), s/veh | |
| Incr Delay (d2), s/veh | |
| Initial Q Delay(d3),s/veh | |
| %ile BackOfQ(50%), veh/ln | |
| LnGrp Delay(d),s/veh | |
| LnGrp LOS | |
| Approach Vol, veh/h | |
| Approach Delay, s/veh | |
| Approach LOS | |
| Timer | |
| Assigned Phs | |
| Phs Duration (G+Y+Rc), s | |
| Change Period (Y+Rc), s | |
| Max Green Setting (Gmax), s | |
| Max Q Clear Time (g_c+H1), s | |
| Green Ext Time (p_c), s | |

User approved ignoring U-Turning movement.

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary

9: Empire Avenue & Lone Tree Way

10/27/2015

| Movement | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|------------------------------|-----|-----|------|-----|-----|------|-----|-----|-----|-----|-----|-----|
| Lane Configurations | | | | | | | | | | | | |
| Volume (veh/h) | 101 | 273 | 1726 | 131 | 226 | 1413 | 180 | 16 | 195 | 97 | 178 | 59 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | | 5 | 2 | 12 | | |
| Initial Q (Qb), veh | | | | | | | | | | | | |
| Ped-Bike Adj(A_pbT) | | | | | | | | | | | | |
| Parking Bus, Adj | | | | | | | | | | | | |
| Adj Sat Flow, veh/h/ln | | | | | | | | | | | | |
| Adj Flow Rate, veh/h | | | | | | | | | | | | |
| Adj No. of Lanes | | | | | | | | | | | | |
| Peak Hour Factor | | | | | | | | | | | | |
| Percent Heavy Veh. % | | | | | | | | | | | | |
| Cap. veh/h | | | | | | | | | | | | |
| Arrive On Green | | | | | | | | | | | | |
| Sat Flow, veh/h | | | | | | | | | | | | |
| Grip Volume(v), veh/h | | | | | | | | | | | | |
| Grip Sat Flow(s), veh/h/ln | | | | | | | | | | | | |
| Q Serve(g, s), s | | | | | | | | | | | | |
| Cycle Q Clear(g_c), s | | | | | | | | | | | | |
| Prop In Lane | | | | | | | | | | | | |
| Lane Grip Cap(c), veh/h | | | | | | | | | | | | |
| V/C Ratio(X) | | | | | | | | | | | | |
| Avail Cap(c_a), veh/h | | | | | | | | | | | | |
| HCM Platoon Ratio | | | | | | | | | | | | |
| Upstream Filter(l) | | | | | | | | | | | | |
| Uniform Delay (d), s/veh | | | | | | | | | | | | |
| Incr Delay (d2), s/veh | | | | | | | | | | | | |
| Initial Q Delay(d3),s/veh | | | | | | | | | | | | |
| %ile BackOfQ(50%), veh/ln | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | | | | | | | | | | | | |
| LnGrp LOS | | | | | | | | | | | | |
| Approach Vol, veh/h | | | | | | | | | | | | |
| Approach Delay, s/veh | | | | | | | | | | | | |
| Approach LOS | | | | | | | | | | | | |
| Timer | | | | | | | | | | | | |
| Assigned Phs | | | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s | | | | | | | | | | | | |
| Change Period (Y+Rc), s | | | | | | | | | | | | |
| Max Green Setting (Gmax), s | | | | | | | | | | | | |
| Max Q Clear Time (g_c+H1), s | | | | | | | | | | | | |
| Green Ext Time (p_c), s | | | | | | | | | | | | |

User approved ignoring U-Turning movement.

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
9: Empire Avenue & Lone Tree Way

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 16 |
| Volume (veh/h) | 43 | 149 | 60 | 149 | 60 | 149 | 60 | 149 | 60 | 43 | 149 | 60 |
| Number | 1 | 6 | 16 | 1 | 6 | 16 | 1 | 6 | 16 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 47 | 162 | 65 | 47 | 162 | 65 | 47 | 162 | 65 | 47 | 162 | 65 |
| Adj No. of Lanes | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 0 | 2 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 106 | 266 | 102 | 106 | 266 | 102 | 106 | 266 | 102 | 106 | 266 | 102 |
| Arrive On Green | 0.03 | 0.11 | 0.11 | 0.03 | 0.11 | 0.11 | 0.03 | 0.11 | 0.11 | 0.03 | 0.11 | 0.11 |
| Sat Flow, veh/h | 3408 | 2474 | 955 | 3408 | 2474 | 955 | 3408 | 2474 | 955 | 3408 | 2474 | 955 |
| Grip Volume(v), veh/h | 47 | 113 | 114 | 47 | 113 | 114 | 47 | 113 | 114 | 47 | 113 | 114 |
| Grip Sat Flow(s), veh/h/ln | 1704 | 1752 | 1676 | 1704 | 1752 | 1676 | 1704 | 1752 | 1676 | 1704 | 1752 | 1676 |
| Q Serve(g, s), s | 1.2 | 5.4 | 5.7 | 1.2 | 5.4 | 5.7 | 1.2 | 5.4 | 5.7 | 1.2 | 5.4 | 5.7 |
| Cycle Q Clear(g, c), s | 1.2 | 5.4 | 5.7 | 1.2 | 5.4 | 5.7 | 1.2 | 5.4 | 5.7 | 1.2 | 5.4 | 5.7 |
| Prop In Lane | 1.00 | 0.57 | 0.57 | 1.00 | 0.57 | 0.57 | 1.00 | 0.57 | 0.57 | 1.00 | 0.57 | 0.57 |
| Lane Grp Cap(c), veh/h | 106 | 188 | 180 | 106 | 188 | 180 | 106 | 188 | 180 | 106 | 188 | 180 |
| V/C Ratio(X) | 0.44 | 0.60 | 0.63 | 0.44 | 0.60 | 0.63 | 0.44 | 0.60 | 0.63 | 0.44 | 0.60 | 0.63 |
| Avail Cap(c,a), veh/h | 156 | 341 | 326 | 156 | 341 | 326 | 156 | 341 | 326 | 156 | 341 | 326 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.6 | 37.2 | 37.4 | 41.6 | 37.2 | 37.4 | 41.6 | 37.2 | 37.4 | 41.6 | 37.2 | 37.4 |
| Incr Delay (d2), s/veh | 2.9 | 3.1 | 3.7 | 2.9 | 3.1 | 3.7 | 2.9 | 3.1 | 3.7 | 2.9 | 3.1 | 3.7 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.6 | 2.8 | 2.8 | 0.6 | 2.8 | 2.8 | 0.6 | 2.8 | 2.8 | 0.6 | 2.8 | 2.8 |
| LnGrp Delay(d), s/veh | 44.5 | 40.3 | 41.0 | 44.5 | 40.3 | 41.0 | 44.5 | 40.3 | 41.0 | 44.5 | 40.3 | 41.0 |
| LnGrp LOS | D | D | D | D | D | D | D | D | D | D | D | D |
| Approach Vol, veh/h | 274 | | | 274 | | | 274 | | | 274 | | |
| Approach Delay, s/veh | 41.3 | | | 41.3 | | | 41.3 | | | 41.3 | | |
| Approach LOS | D | | | D | | | D | | | D | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Phs Duration (G+Y+Rc), s | 7.8 | 16.0 | 16.9 | 41.7 | 9.9 | 13.9 | 5.5 | 53.1 | 7.8 | 16.0 | 16.9 | 41.7 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 9.0 | 18.0 | 17.0 | 40.0 | 10.0 | 17.0 | 4.0 | 53.0 | 9.0 | 18.0 | 17.0 | 40.0 |
| Max Q Clear Time (g_c+H1), s | 5.0 | 11.4 | 12.2 | 24.3 | 6.5 | 2.2 | 2.9 | 29.4 | 5.0 | 11.4 | 12.2 | 24.3 |
| Green Ext Time (p_c), s | 0.0 | 0.5 | 0.7 | 13.4 | 0.1 | 0.9 | 0.0 | 18.9 | 0.0 | 0.5 | 0.7 | 13.4 |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 23.2 | | | | | | | | | | | |
| HCM 2010 LOS | C | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
10: Country Hills Road & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 16 |
| Volume (veh/h) | 18 | 960 | 120 | 402 | 1371 | 100 | 90 | 0 | 170 | 59 | 0 | 5 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 20 | 1043 | 130 | 437 | 1490 | 109 | 98 | 0 | 185 | 64 | 0 | 5 |
| Adj No. of Lanes | 1 | 2 | 0 | 2 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap. veh/h | 31 | 1434 | 179 | 535 | 1976 | 144 | 125 | 0 | 227 | 82 | 0 | 189 |
| Arrive On Green | 0.02 | 0.46 | 0.46 | 0.16 | 0.60 | 0.60 | 0.07 | 0.00 | 0.15 | 0.05 | 0.00 | 0.12 |
| Sat Flow, veh/h | 1757 | 3137 | 391 | 3408 | 3313 | 241 | 1757 | 0 | 1568 | 1757 | 0 | 1568 |
| Grip Volume(v), veh/h | 20 | 582 | 591 | 437 | 784 | 815 | 98 | 0 | 185 | 64 | 0 | 5 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1752 | 1776 | 1704 | 1752 | 1802 | 1757 | 0 | 1568 | 1757 | 0 | 1568 |
| Q Serve(g, s), s | 0.9 | 22.3 | 22.3 | 10.2 | 27.0 | 27.4 | 4.5 | 0.0 | 9.4 | 3.0 | 0.0 | 0.2 |
| Cycle Q Clear(g, c), s | 0.9 | 22.3 | 22.3 | 10.2 | 27.0 | 27.4 | 4.5 | 0.0 | 9.4 | 3.0 | 0.0 | 0.2 |
| Prop In Lane | 1.00 | 0.22 | 0.22 | 1.00 | 0.13 | 0.13 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 31 | 801 | 812 | 535 | 1045 | 1075 | 125 | 0 | 227 | 82 | 0 | 189 |
| V/C Ratio(X) | 0.64 | 0.73 | 0.73 | 0.82 | 0.75 | 0.76 | 0.78 | 0.00 | 0.81 | 0.78 | 0.00 | 0.03 |
| Avail Cap(c,a), veh/h | 85 | 851 | 862 | 703 | 1127 | 1159 | 213 | 0 | 342 | 192 | 0 | 323 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 40.2 | 18.2 | 18.2 | 33.6 | 12.2 | 12.3 | 37.6 | 0.0 | 34.1 | 38.9 | 0.0 | 32.0 |
| Incr Delay (d2), s/veh | 19.6 | 2.9 | 2.9 | 5.7 | 2.7 | 2.7 | 10.1 | 0.0 | 8.7 | 14.6 | 0.0 | 0.1 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 0.6 | 11.3 | 11.5 | 5.2 | 13.6 | 14.2 | 2.6 | 0.0 | 4.6 | 1.8 | 0.0 | 0.1 |
| LnGrp Delay(d), s/veh | 59.8 | 21.1 | 21.1 | 39.3 | 14.8 | 15.0 | 47.7 | 0.0 | 42.9 | 53.5 | 0.0 | 32.0 |
| LnGrp LOS | E | C | C | D | B | B | D | D | D | D | D | C |
| Approach Vol, veh/h | 1193 | | | 2036 | | | 283 | | | 69 | | |
| Approach Delay, s/veh | 21.8 | | | 20.1 | | | 44.5 | | | 52.0 | | |
| Approach LOS | C | | | C | | | D | | | D | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Phs Duration (G+Y+Rc), s | 7.8 | 16.0 | 16.9 | 41.7 | 9.9 | 13.9 | 5.5 | 53.1 | 7.8 | 16.0 | 16.9 | 41.7 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 9.0 | 18.0 | 17.0 | 40.0 | 10.0 | 17.0 | 4.0 | 53.0 | 9.0 | 18.0 | 17.0 | 40.0 |
| Max Q Clear Time (g_c+H1), s | 5.0 | 11.4 | 12.2 | 24.3 | 6.5 | 2.2 | 2.9 | 29.4 | 5.0 | 11.4 | 12.2 | 24.3 |
| Green Ext Time (p_c), s | 0.0 | 0.5 | 0.7 | 13.4 | 0.1 | 0.9 | 0.0 | 18.9 | 0.0 | 0.5 | 0.7 | 13.4 |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 23.2 | | | | | | | | | | | |
| HCM 2010 LOS | C | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Prj Cond Alt Access 1

Synchro 8 Report

HCM 2010 Signalized Intersection Summary
11: Slatten Ranch Road & Laurel Road

10/27/2015

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← | ← |
| Volume (veh/h) | 116 | 1381 | 297 | 260 | 1054 | 230 | 624 | 271 | 301 | 230 | 410 | 116 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A, pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1845 | 1845 | 1845 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 | 1845 | 1845 | 1900 |
| Adj Flow Rate, veh/h | 126 | 1501 | 165 | 283 | 1146 | 250 | 678 | 295 | 327 | 250 | 446 | 126 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 0 | 2 | 2 | 0 | 1 | 2 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh. % | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| Cap, veh/h | 155 | 1511 | 470 | 299 | 1581 | 345 | 682 | 367 | 328 | 282 | 460 | 129 |
| Arrive On Green | 0.09 | 0.30 | 0.30 | 0.17 | 0.38 | 0.38 | 0.20 | 0.21 | 0.21 | 0.16 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1757 | 5036 | 1588 | 1757 | 4140 | 903 | 3408 | 1752 | 1568 | 1757 | 2705 | 758 |
| Grip Volume(v), veh/h | 126 | 1501 | 165 | 283 | 929 | 467 | 678 | 295 | 327 | 250 | 288 | 284 |
| Grip Sat Flow(s), veh/h/ln | 1757 | 1679 | 1588 | 1757 | 1679 | 1685 | 1704 | 1752 | 1568 | 1757 | 1752 | 1711 |
| Q Serve(g, s) | 7.0 | 29.7 | 8.2 | 15.9 | 23.7 | 23.7 | 19.9 | 16.0 | 20.8 | 13.9 | 16.3 | 16.5 |
| Cycle Q Clear(g, c), s | 7.0 | 29.7 | 8.2 | 15.9 | 23.7 | 23.7 | 19.9 | 16.0 | 20.8 | 13.9 | 16.3 | 16.5 |
| Prop In Lane | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.54 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.44 |
| Lane Grp Cap(c), veh/h | 155 | 1511 | 470 | 299 | 1283 | 644 | 682 | 367 | 328 | 282 | 298 | 291 |
| V/C Ratio(X) | 0.82 | 0.99 | 0.35 | 0.95 | 0.72 | 0.72 | 0.99 | 0.80 | 1.00 | 0.89 | 0.97 | 0.98 |
| Avail Cap(c,a), veh/h | 176 | 1511 | 470 | 299 | 1283 | 644 | 682 | 367 | 328 | 316 | 298 | 291 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.8 | 34.9 | 27.4 | 41.1 | 26.4 | 26.4 | 39.9 | 37.6 | 39.5 | 41.1 | 41.2 | 41.3 |
| Incr Delay (d2), s/veh | 22.5 | 21.6 | 0.4 | 38.2 | 2.1 | 4.1 | 33.1 | 12.3 | 46.6 | 22.9 | 42.7 | 46.5 |
| Initial Q Delay(d3), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/ln | 4.4 | 16.8 | 3.6 | 10.9 | 11.3 | 11.7 | 12.5 | 9.0 | 13.4 | 8.5 | 11.4 | 11.6 |
| LnGrp Delay(d), s/veh | 67.3 | 56.5 | 27.8 | 79.2 | 28.5 | 30.5 | 73.0 | 49.8 | 88.1 | 64.0 | 83.9 | 87.8 |
| LnGrp LOS | E | E | C | E | C | C | E | D | F | E | F | F |
| Approach Vol, veh/h | 1792 | | | 1679 | | | 1300 | | | 822 | | |
| Approach Delay, s/veh | 54.6 | | | 37.6 | | | 71.5 | | | 79.2 | | |
| Approach LOS | D | | | D | | | E | | | E | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 20.1 | 24.9 | 21.0 | 34.0 | 24.0 | 21.0 | 12.8 | 42.2 | | | | |
| Change Period(Y+Rc), s | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | |
| Max Green Setting (Gmax), s | 18.0 | 19.0 | 17.0 | 30.0 | 20.0 | 17.0 | 10.0 | 37.0 | | | | |
| Max Q Clear Time (g, c+H1), s | 15.9 | 22.8 | 17.9 | 31.7 | 21.9 | 18.5 | 9.0 | 25.7 | | | | |
| Green Ext Time (p, c), s | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 10.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 57.0 | | | | | | | | | | | |
| HCM 2010 LOS | E | | | | | | | | | | | |

Laurel Ranch Traffic Impact Analysis
PM Cumulative + Proj Cond Alt Access 1

Synchro 8 Report

Appendix C

Project Driveway Queuing Calculations

| Intersection: 10: Country Hills Road & Laurel Road | | | | | | | | | | | | |
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|----|----|
| Movement | EB | EB | WB | WB | WB | WB | WB | NB | NB | WB | WB | NB |
| Directions Served | T | TR | L | L | L | T | T | L | R | | | |
| Maximum Queue (ft) | 246 | 275 | 54 | 84 | 106 | 115 | 115 | 136 | 154 | | | |
| Average Queue (ft) | 143 | 200 | 34 | 54 | 54 | 61 | 61 | 85 | 96 | | | |
| 95th Queue (ft) | 267 | 321 | 61 | 94 | 111 | 125 | 125 | 147 | 175 | | | |
| Link Distance (ft) | 561 | 561 | | | | 889 | 889 | | 331 | | | |
| Upstream Blk Time (%) | | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | | |
| Storage Bay Dist (ft) | | | 200 | 200 | | | | | 250 | | | |
| Storage Blk Time (%) | | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | | |

| Intersection: 10: Country Hills Road & Laurel Road | | | | | | | | | | | | |
|--|-----|-----|-----|-----|-----|-----|-----|----|-----|----|----|----|
| Movement | EB | EB | WB | WB | WB | WB | WB | NB | NB | WB | WB | NB |
| Directions Served | T | TR | L | L | L | T | T | L | R | | | |
| Maximum Queue (ft) | 151 | 166 | 92 | 116 | 116 | 109 | 109 | 72 | 76 | | | |
| Average Queue (ft) | 91 | 107 | 62 | 86 | 86 | 71 | 53 | 49 | 50 | | | |
| 95th Queue (ft) | 160 | 181 | 116 | 127 | 144 | 116 | 81 | 81 | 87 | | | |
| Link Distance (ft) | 561 | 561 | | | | 889 | 889 | | 331 | | | |
| Upstream Blk Time (%) | | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | | |
| Storage Bay Dist (ft) | | | 200 | 200 | | | | | 250 | | | |
| Storage Blk Time (%) | | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | | |

| Intersection: 16: D Lane & Laurel Road | |
|--|-----|
| Movement | NB |
| Directions Served | R |
| Maximum Queue (ft) | 85 |
| Average Queue (ft) | 45 |
| 95th Queue (ft) | 88 |
| Link Distance (ft) | 212 |
| Upstream Blk Time (%) | |
| Queuing Penalty (veh) | |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

| Intersection: 16: D Lane & Laurel Road | |
|--|-----|
| Movement | NB |
| Directions Served | R |
| Maximum Queue (ft) | 40 |
| Average Queue (ft) | 25 |
| 95th Queue (ft) | 52 |
| Link Distance (ft) | 212 |
| Upstream Blk Time (%) | |
| Queuing Penalty (veh) | |
| Storage Bay Dist (ft) | |
| Storage Blk Time (%) | |
| Queuing Penalty (veh) | |

Intersection: 10: Country Hills Road & Laurel Road

| Movement | EB | EB | EB | WB | WB | WB | WB | WB | NB | NB | NB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|----|
| | L | T | TR | L | T | TR | L | T | L | TR | L | TR | TR |
| Directions Served | 22 | 191 | 238 | 61 | 75 | 108 | 112 | 138 | 174 | 61 | 11 | | |
| Maximum Queue (ft) | 6 | 136 | 175 | 24 | 47 | 58 | 64 | 89 | 104 | 39 | 3 | | |
| Average Queue (ft) | 25 | 209 | 268 | 61 | 82 | 121 | 125 | 154 | 188 | 76 | 14 | | |
| 95th Queue (ft) | | | | | | | | | | | | | |
| Link Distance (ft) | 560 | 560 | | | | | 863 | 863 | | 331 | | 350 | |
| Upstream Blk Time (%) | | | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | | | |
| Storage Bay Dist (ft) | 215 | | | 200 | 200 | | 250 | | | 100 | | | |
| Storage Blk Time (%) | 0 | | | | | | | | 0 | 0 | | | |
| Queuing Penalty (veh) | 0 | | | | | | | | 0 | 0 | | | |

Intersection: 10: Country Hills Road & Laurel Road

| Movement | EB | EB | EB | WB | WB | WB | WB | WB | NB | NB | NB | SB | SB |
|-----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|-----|----|
| | L | T | TR | L | T | TR | L | T | L | TR | L | TR | TR |
| Directions Served | 20 | 183 | 203 | 95 | 128 | 159 | 168 | 79 | 103 | 56 | 15 | | |
| Maximum Queue (ft) | 9 | 109 | 128 | 59 | 96 | 90 | 91 | 54 | 64 | 29 | 3 | | |
| Average Queue (ft) | 28 | 201 | 229 | 106 | 165 | 191 | 187 | 96 | 116 | 64 | 15 | | |
| 95th Queue (ft) | | | | | | | | | | | | | |
| Link Distance (ft) | 560 | 560 | | | | | 863 | 863 | | 331 | | 350 | |
| Upstream Blk Time (%) | | | | | | | | | | | | | |
| Queuing Penalty (veh) | | | | | | | | | | | | | |
| Storage Bay Dist (ft) | 215 | | | 200 | 200 | | 250 | | | 100 | | | |
| Storage Blk Time (%) | 1 | | | | | | 0 | | | 0 | | | |
| Queuing Penalty (veh) | 0 | | | | | | 2 | | | 0 | | | |

| Intersection: 16: D Lane & Laurel Road | | | |
|--|-----|-----|--|
| Movement | NB | SB | |
| Directions Served | R | R | |
| Maximum Queue (ft) | 50 | 35 | |
| Average Queue (ft) | 34 | 15 | |
| 95th Queue (ft) | 59 | 42 | |
| Link Distance (ft) | 212 | 239 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

| Intersection: 16: D Lane & Laurel Road | | | |
|--|-----|-----|--|
| Movement | NB | SB | |
| Directions Served | R | R | |
| Maximum Queue (ft) | 47 | 18 | |
| Average Queue (ft) | 28 | 4 | |
| 95th Queue (ft) | 54 | 20 | |
| Link Distance (ft) | 212 | 239 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Appendix D

Alternative Access Queuing Calculations

| Intersection: 16: D Lane & Laurel Road | | | |
|--|-----|-----|--|
| Movement | WB | NB | |
| Directions Served | L | R | |
| Maximum Queue (ft) | 30 | 75 | |
| Average Queue (ft) | 13 | 44 | |
| 95th Queue (ft) | 36 | 78 | |
| Link Distance (ft) | | 212 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | 200 | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

| Intersection: 16: D Lane & Laurel Road | | | |
|--|-----|-----|--|
| Movement | WB | NB | |
| Directions Served | L | R | |
| Maximum Queue (ft) | 71 | 44 | |
| Average Queue (ft) | 36 | 32 | |
| 95th Queue (ft) | 75 | 51 | |
| Link Distance (ft) | | 212 | |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | 200 | | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

| Intersection: 16: D Lane & Laurel Road | | | | | | |
|--|-----|-----|-----|------|-----|-----|
| Movement | WB | NB | SB | WB | NB | SB |
| Directions Served | L | R | R | L | R | R |
| Maximum Queue (ft) | 44 | 69 | 34 | 56 | 45 | 18 |
| Average Queue (ft) | 18 | 40 | 14 | 2 | 29 | 7 |
| 95th Queue (ft) | 52 | 72 | 41 | 11 | 68 | 27 |
| Link Distance (ft) | | 212 | 239 | 1176 | 212 | 239 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | 200 | | | 200 | | |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

| Intersection: 16: D Lane & Laurel Road | | | | | | |
|--|----|------|-----|-----|----|------|
| Movement | EB | WB | NB | SB | EB | WB |
| Directions Served | TR | L | R | R | TR | L |
| Maximum Queue (ft) | 8 | 56 | 45 | 18 | 8 | 56 |
| Average Queue (ft) | 2 | 29 | 27 | 7 | 2 | 29 |
| 95th Queue (ft) | 11 | 68 | 53 | 27 | 11 | 68 |
| Link Distance (ft) | | 1176 | 212 | 239 | | 1176 |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | 200 | | | | 200 |
| Storage Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |

Appendix E

Sight Distance

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**A.2 - Traffic Technical Memorandum prepared by Fehr & Peers for
2009 Park Ridge Addendum**

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Appendices

Appendix A

Transportation Analysis & Appendices

TECHNICAL MEMORANDUM

Date: November 28, 2008

To: Richard T. Loewke, AICP

From: Sam Tabibnia and Ellen Robinson

Subject: *Antioch Davidon Homes Transportation Analysis*

WC05-2153

This memorandum documents the results of the updated traffic analysis completed for the proposed Davidon Homes project. The proposed development is part of the Future Urbanization Area (FUA) #2 Specific Plan, which was originally analyzed in an EIR certified in 1996. The transportation section of the EIR was based on future growth assumptions developed in the early 1990s. Although the planned development within the specific plan area has not changed drastically since the certification of the EIR in 1996, the planned transportation infrastructure and traffic conditions have changed to require a new analysis. Thus, this study uses more recent traffic counts and forecasts to update the future traffic analyses and determine if the proposed Project would cause any new traffic impacts that were not identified in the 1996 EIR. Note that this updated analysis focuses on traffic impacts and a few specific issues that have been raised; it does not provide a broad analysis of other transportation issues such as bicycle and pedestrian circulation, transit services, or on-site circulation.

Based on the analysis, the Project would cause a significant impact at the Lone Tree Way/Hillcrest Avenue intersection under Cumulative conditions. The impact can be mitigated by restriping the southbound Hillcrest Avenue approach to one exclusive right-turn lane, one through lane, and two exclusive left-turn lanes, and providing an additional left-turn lane on the eastbound Lone Tree Way approach.

In addition, the following improvements are also recommended. These improvements would enhance traffic flow in the study area. However, they are not identified as significant impacts because they do not exceed the significance criteria used in this analysis.

- At the Lone Tree Way/Canada Valley Road intersection, convert the southbound through lane to a shared through/left-turn lane. This will also require implementation of split phasing signal operations in the north/south directions. This modification is needed under Near-Term conditions only and the intersection can be converted back to its current configuration after project access to Laurel Road in the north is completed.

In addition, if the full project is completed under Near-Term Plus Project conditions without any direct connections to Laurel Road, the queues on southbound Canada Valley Road at Lone Tree Way would spill back to the upstream intersection even if the above stated improvements are implemented. Based on our analysis, about 50 percent of the Davidon project, corresponding to about 270 single-family residential units, can be developed before access to Laurel Road would be required.

- At the Canada Valley Road/Vista Grande Drive/Pinnacle View Way, consider strategies that would enhance pedestrian safety and encourage walking between the Davidson Homes project and the existing elementary school and park on Vista Grande Drive. Potential improvement options, such as high-visibility cross-walks, in-crosswalk signage, flashing beacons/signs, in-pavement warning lights, and/or HAWK signals are described in detail starting on page 10 of this memorandum.
- At the Laurel Road/Country Hills Drive intersection, consider providing a second left-turn lane on westbound Laurel Road into southbound Country Hills Drive in order to reduce the likelihood for queue spillover into the through lanes. This will also require providing a second 300-foot receiving lane on southbound Country Hills Drive.

This memorandum includes the following sections:

- **Study Area** – describes the project study area and defines the study intersections.
- **Analysis Methodology** – Describes the methodologies used to analyze project impacts.
- **Existing Conditions** – Describes the current conditions in the vicinity of the proposed project.
- **Near-Term Conditions Analysis** – Provides an analysis of project impacts under Near-Term conditions that accounts for other developments expected to be completed in the next few years.
- **Cumulative Conditions Analysis** – Provides an analysis of project impacts under Cumulative conditions that accounts for buildout of the City's General Plan.
- **CCTA Traffic Service Objectives Analysis** – Provides an analysis of traffic service objectives on routes of regional significance as required by Contra Costa Transportation Authority (CCTA).

STUDY AREA

The proposed Project would consist of 525 dwelling units located on the south side of Laurel Road between Canada Valley Road and Country Hills Drive in the City of Antioch. This analysis focuses on the operations of the following key intersections in the vicinity of the site:

- | | |
|---|---|
| 1. Laurel Road/Canada Valley Road | 10. Lone Tree Way/Northbound SR 4 Bypass Ramps |
| 2. Laurel Road/Country Hills Drive | 11. Lone Tree Way /Slatten Ranch Road |
| 3. Laurel Road/Southbound SR 4 Bypass Ramps | 12. Lone Tree Way/Empire Avenue |
| 4. Laurel Road/Northbound SR 4 Bypass Ramps | 13. Lone Tree Way/Deer Valley Road |
| 5. Laurel Road/Slatten Ranch Road | 14. Lone Tree Way/Hillcrest Avenue |
| 6. Laurel Road/Live Oak Avenue | 15. Lone Tree Way/Vista Grande Drive |
| 7. Laurel Road/Empire Avenue | 16. Country Hills Drive/Hillcrest Avenue |
| 8. Lone Tree Way/Canada Valley Road | 17. Laurel Road/Tree Line Way (With Project only) |
| 9. Lone Tree Way/Southbound SR 4 Bypass Ramps | 18. Laurel Road/Hillcrest Avenue |

The locations of the study intersections are shown on Figure 1. Figure 2 presents the proposed site plan for the Project.

ANALYSIS METHODOLOGY

Study intersection operations were evaluated using Level of Service (LOS) calculations. The analysis method outlined in *Technical Procedures Update* prepared by the Contra Costa Transportation Authority (CCTA) (July, 2006), known as CCTALOS, was utilized. To augment this analysis, the Transportation Research Board's 2000 *Highway Capacity Manual* (HCM) method and Synchro software were also used.

Level of Service Criteria

In order to measure and describe the operation of a local roadway network, traffic engineers and planners commonly use a grading system called level of service (LOS) to describe intersection operations. The LOS grading system qualitatively characterizes traffic conditions associated with varying levels of traffic. These levels range from LOS A, indicating free-flow traffic conditions with little or no delay experienced by motorists, to LOS F, which describes congested conditions where traffic flows exceed design capacity, resulting in long queues and delays.

At each study intersection, traffic conditions were evaluated using the LOS methodologies developed by the CCTA and HCM. The CCTA planning-level analysis uses various intersection characteristics (i.e., traffic volumes, lane geometry, and signal phasing) to estimate the volume-to-capacity (v/c) ratio of an intersection. Table 1 summarizes the relationship between the v/c ratio and LOS. HCM operation analysis uses various intersection characteristics (i.e., traffic volumes, lane geometry, signal timing, and pedestrian activity) to estimate the average delay (measured in seconds per vehicle) experienced by motorists traveling through an intersection. Table 2 summarizes the relationship between delay and LOS for signalized and unsignalized intersections. Typically, the delay and LOS for the worse movement from the side-street is reported for side-street stop-controlled intersections.

| TABLE 1 INTERSECTION LEVEL OF SERVICE DEFINITIONS (CCTA) | | |
|--|--|---|
| Level of Service | Sum of Critical Volume-to-Capacity Ratio | Description |
| A | < 0.60 | Stable Flow: Very slight or no delay. No approach phase is fully utilized by traffic and no vehicle waits longer than one red indication. |
| B | 0.61 - 0.70 | Stable Flow: Slight delay. An occasional approach phase is fully utilized. |
| C | 0.71 - 0.80 | Stable Flow: Acceptable delay. A few drivers arriving at the end of a queue may occasionally have to wait through one signal cycle. |
| D | 0.81 - 0.90 | Approaching Unstable Flow: Tolerable delay. Delays may be substantial during short periods, but excessive back ups do not occur. |
| E | 0.91 - 1.00 | Unstable Flow: Intolerable delay. Delay may extend through several cycle lengths. |
| F | > 1.00 | Forced Flow: Excessive delay. |
| Source: <i>Technical Procedures</i> , Contra Costa Transportation Authority, 1997. | | |

| TABLE 2 INTERSECTION LEVEL OF SERVICE DEFINITIONS (HIGHWAY CAPACITY MANUAL) | | |
|---|---|---------------------------------|
| Level of Service | Description | Average Control Delay (Seconds) |
| Signalized Intersections | | |
| A | Operations with very low delay occurring with favorable progression and/or short cycle length. | ≤ 10.0 |
| B | Operations with low delay occurring with good progression and/or short cycle lengths. | > 10.0 to 20.0 |
| C | Operations with average delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures begin to appear. | > 20.0 to 35.0 |
| D | Operations with longer delays due to a combination of unfavorable progression, long cycle lengths, or high V/C ratios. Many vehicles stop and individual cycle failures are noticeable. | > 35.0 to 55.0 |
| E | Operations with high delay values indicating poor progression, long cycle lengths, and high V/C ratios. Individual cycle failures are frequent occurrences. This is considered to be the limit of acceptable delay. | > 55.0 to 80.0 |
| F | Operation with delays unacceptable to most drivers occurring due to over saturation, poor progression, or very long cycle lengths. | > 80.0 |
| Unsignalized Intersections | | |
| A | Little or no delays | ≤ 10.0 |
| B | Short traffic delays | > 10.0 to 15.0 |
| C | Average traffic delays | > 15.0 to 25.0 |
| D | Long traffic delays | > 25.0 to 35.0 |
| E | Very long traffic delays | > 35.0 to 50.0 |
| F | Extreme traffic delays with intersection capacity exceeded | > 50.0 |
| Source: <i>Highway Capacity Manual</i> , Transportation Research Board, 2000 | | |

The CCTALOS methodology can produce different results than the HCM methodology. The primary reason that the methodologies produce different results is that the CCTALOS methodology analyzes each intersection independently as an isolated intersection and calculates LOS based on the theoretical capacity of each movement at the intersection. LOS in the HCM methodology is based on the delay experienced by each vehicle, which is a function of the physical characteristics of the intersection including signal timing and phasing.

Significance Criteria

The following criteria were used to determine if the proposed Project would have a significant impact on the study intersections:

- A significant impact occurs if any basic route intersection operations within regional commercial areas or within 1,000 feet of a freeway interchange (Intersections 2-5) deteriorate below an acceptable minimum LOS Low level E ($v/c = 0.94$) (GM Policy 3.4.2.1a).
- A significant impact occurs if any basic route intersection operations on other residential or arterial roadways (Intersections 1 and 17) deteriorate below an acceptable minimum LOS Mid-Range D ($v/c = 0.87$) (GM Policy 3.4.2.1c).
- A significant impact occurs if intersection operations on regional routes of significance or basic intersections outside the Antioch Planning Area (Intersections 6-13, 14, 15, 16 and 18) deteriorate below the adopted Action Plan acceptable minimum LOS D or better ($v/c = 0.89$) to an unacceptable level E or F (GM Policy 3.4.1.1).
- A significant impact occurs if the v/c ratio at an intersection operating at an unacceptable level (LOS E or F) increases by more than 0.02 (2003 General Plan EIR).
- A significant impact occurs if the average delay at an intersection operating at an unacceptable level (LOS E or F) increases by more than 5 seconds (2003 General Plan EIR).
- A significant impact occurs at an unsignalized intersection if operations decline from an acceptable level to an unacceptable level (as defined above), and the need occurs for installation of a traffic signal based on the *Manual on Uniform Traffic Control Devices* (MUTCD) Peak Hour Signal Warrant (Warrant 3).
- Operations of a roadway segment to exceed the established traffic service objective (TSO) standard.
- Deterioration in a roadway segment that already exceeds the established TSO standard by increasing the roadway volume by more than one percent.

EXISTING CONDITIONS

City of Antioch provided weekday morning (7:00 to 9:00 AM) and evening (4:00 to 6:00 PM) peak period intersection turning movement counts in May 2008 at the study intersections. The existing traffic counts are provided in Appendix A. For each intersection, the single hour with the highest traffic volumes during each count period was identified. The peak hour volumes are presented on Figure 3. The peak hour data is used as the basis for intersection operations analysis. These counts were collected after Segment 1 of the SR 4 Bypass freeway between SR 4 and Lone Tree Way was opened for public use and account for the resulting changes in local and regional traffic pattern. The existing lane configurations and traffic control at the study intersections are shown on Figure 4.

Intersection operations were analyzed at ten of the study intersections using both the HCM and CCTALOS methodologies. Only these ten intersections were analyzed under Existing and Near-Term conditions because the other intersections either do not exist or the proposed project would not add substantial amount of traffic to them under Existing and Near-Term conditions because of the roadway network that would be completed under Near-Term conditions.

Table 3 summarizes LOS at the study intersection, as calculated using both HCM and CCTALOS methodologies. The detailed intersection LOS calculation sheets are provided in Appendices B and C for both HCM and CCTALOS methodologies, respectively. Using either HCM or CCTALOS methodologies, the ten study intersections currently operate at LOS D or better during both AM and PM peak hours using either the HCM or CCTALOS methodologies.

**TABLE 3
EXISTING CONDITIONS
PEAK HOUR LEVEL OF SERVICE**

| No. | Intersection | Control ¹ | Peak Hour | HCM | | CCTALOS | |
|-----|--|----------------------|-----------|----------|------------------|--------------|------------------|
| | | | | Delay | LOS ² | V/C | LOS ³ |
| 8 | Lone Tree Way/Canada Valley Road | Signal | AM PM | 19 26 | B C | 0.38 0.54 | A A |
| 9 | Lone Tree Way/Southbound SR 4 Bypass Ramps | Signal | AM PM | 20 20 | B B | 0.51 0.59 | A A |
| 10 | Lone Tree Way/Northbound SR 4 Bypass Ramps | Signal | AM PM | 22 14 | C B | 0.31 0.48 | A A |
| 11 | Lone Tree Way/Slatten Ranch Road | Signal | AM PM | 24 30 | C C | 0.46 0.49 | A A |
| 12 | Lone Tree Way/Empire Avenue | Signal | AM PM | 30 30 | C C | 0.48 0.50 | A A |
| 13 | Lone Tree Way/Deer Valley Road | Signal | AM PM | 42 40 | D D | 0.71 0.61 | C B |
| 14 | Lone Tree Way/Hillcrest Avenue | Signal | AM PM | 33 29 | C C | 0.44 0.54 | A A |
| 15 | Lone Tree Way/Vista Grande Drive | Signal | AM PM | 13 13 | B B | 0.32 0.44 | A A |
| 16 | Country Hills Drive/Hillcrest Avenue | Signal | AM PM | 39 27 | D C | 0.44 0.32 | A A |
| 18 | Laurel Road/Hillcrest Avenue | Signal | AM PM | 21 17 | C B | 0.34 0.22 | A A |

Note: **Bold** indicates intersections exceeding LOS standard.

1. Signal = signal controlled intersection; SSS = side street stop controlled intersection.
2. Level of service for intersections based on control delay per vehicle, according to the *Highway Capacity Manual*, Transportation Research Board, 2000.
3. Signalized intersection level of service is based on v/c ratio according to the *Contra Costa Transportation Authority Technical Procedures Manual, 1997(CCTA)*.

Source: Fehr & Peers, 2008.

PROJECT TRIP GENERATION AND DISTRIBUTION

The proposed Davidon Homes project would consist of 525 single-family dwelling units. Vehicle trips generated by the Project were estimated by applying trip generation rates from Institute of Transportation Engineers *Trip Generation* (7th Edition). As summarized in Table 4, the proposed Project is estimated to generate 394 AM peak hour trips and 530 PM peak hour trips.

Project trip distribution takes into account the location, land use, and density of other developments within the study area and the major travel routes that serve the Project area. Trip distribution for the Project is shown on Figure 5. This trip distribution is consistent with the trip distribution presented in the *Traffic Study for the Proposed Laurel Ranch Development* (TJKM, February 2004).

**TABLE 4
PROPOSED PROJECT TRIP GENERATION**

| Land Use | Size | Daily Trips | AM Trips | | | PM Trips | | |
|--|----------|-------------|----------|-----|-------|----------|-----|-------|
| | | | In | Out | Total | In | Out | Total |
| Single Family Residential ¹ | 525 d.u. | 5,024 | 98 | 296 | 394 | 334 | 196 | 530 |

Notes: d.u. = dwelling unit

1. ITE Land Use Category 210 Single Family Detached Housing:

Daily: T = 9.57 (x)

AM: T = 0.75 (x) ; In = 25%, out = 75%

PM: T = 1.01 (x) ; In = 63%, Out = 37%

Source: Fehr & Peers, 2008.

NEAR-TERM CONDITIONS

The analysis of Near-Term No Project and Near-Term With Project conditions are described below.

Near-Term No Project Conditions

The Near-Term conditions represents traffic conditions in the near future. It accounts for traffic that will be generated by projects currently under construction or expected to be completed within the next few years in the vicinity of the proposed project. For this analysis, traffic generated by the following projects was added to the Existing Conditions volumes to estimate traffic volumes under Near-Term No Project conditions:

- Deer Valley Estates (136 single-family dwelling units)
- Hidden Glen (371 single-family dwelling units)
- Sand Creek Ranch (308 single-family dwelling units)
- Tierra Villas (122 single-family dwelling units)
- Lone Tree Landing (33,000 square feet of retail)
- Wal-Mart expansion (33,575 square feet of retail)

Intersection volumes under Near-Term No Project conditions are presented on Figure 5. This analysis assumes that the roadway network and intersection configurations under Near-Term conditions would remain same as the Existing conditions. Tables 4 summarizes peak hour LOS at the study intersection under Near-Term No Project conditions. The detailed intersection LOS calculation sheets are provided in Appendices B and C. All study intersections would continue to operate at LOS D or better under Near-Term No Project conditions using either the HCM or CCTALOS methodologies.

**TABLE 4
NEAR-TERM CONDITIONS
PEAK HOUR LEVEL OF SERVICE**

| No. | Intersection | Control ¹ | Peak Hour | No Project | | | | With Project ⁴ | | | |
|-----|--|----------------------|-----------|------------|------------------|--------------|------------------|---------------------------|------------------|--------------|------------------|
| | | | | HCM | | CCTALOS | | HCM | | CCTALOS | |
| | | | | Delay | LOS ² | V/C | LOS ³ | Delay | LOS ² | V/C | LOS ³ |
| 8 | Lone Tree Way/Canada Valley Road | Signal | AM PM | 21 29 | C C | 0.45 0.65 | A B | 37 47 | D D | 0.59 0.73 | A C |
| 9 | Lone Tree Way/Southbound SR 4 Bypass Ramps | Signal | AM PM | 19 24 | B C | 0.60 0.74 | B C | 21 30 | C C | 0.65 0.81 | B D |
| 10 | Lone Tree Way/Northbound SR 4 Bypass Ramps | Signal | AM PM | 20 15 | B B | 0.34 0.55 | A A | 20 15 | B B | 0.36 0.58 | A A |
| 11 | Lone Tree Way/Slatten Ranch Road | Signal | AM PM | 21 28 | C C | 0.48 0.55 | A A | 22 28 | C C | 0.49 0.57 | A A |
| 12 | Lone Tree Way/Empire Avenue | Signal | AM PM | 31 33 | C C | 0.57 0.64 | A B | 30 35 | C C | 0.62 0.70 | B C |
| 13 | Lone Tree Way/Deer Valley Road | Signal | AM PM | 43 42 | D D | 0.77 0.73 | C C | 44 42 | D D | 0.78 0.75 | C C |
| 14 | Lone Tree Way/Hillcrest Avenue | Signal | AM PM | 36 35 | D C | 0.54 0.63 | A B | 36 35 | D D | 0.55 0.66 | A B |
| 15 | Lone Tree Way/Vista Grande Drive | Signal | AM PM | 11 13 | B B | 0.35 0.49 | A A | 11 13 | B B | 0.37 0.50 | A A |
| 16 | Country Hills Drive/Hillcrest Avenue | Signal | AM PM | 36 23 | D C | 0.50 0.36 | A A | 40 27 | D C | 0.53 0.41 | A A |
| 18 | Laurel Road/Hillcrest Avenue | Signal | AM PM | 19 14 | B B | 0.40 0.29 | A A | 19 14 | B B | 0.41 0.30 | A A |

Note: **Bold** indicates intersections exceeding LOS standard.

1. Signal = signal controlled intersection.
2. Level of service for intersections based on control delay per vehicle, according to the *Highway Capacity Manual*, Transportation Research Board, 2000.
3. Signalized intersection level of service is based on v/c ratio according to the *Contra Costa Transportation Authority Technical Procedures Manual, 1997(CCTA)*.
4. The project analyzed under this scenario includes all phases of the development (i.e., 525 dwelling units).

Source: Fehr & Peers, 2008.

Near-Term With Project Conditions

Trips generated by the proposed Davidon Homes project were added to the Near-Term No Project volumes to estimate the Near-Term With Project Volumes shown on Figure 7. The Near-Term With Project conditions analysis includes all phases of the Davidon Homes development, consisting of 525 dwelling units. This analysis assumes that the roadway network would remain same as the existing roadway network and all study intersections would continue to have the same configuration. Thus, this analysis assumes that Laurel Road would not be extended further west from the SR 4 Bypass and the proposed Davidon Homes project would not connect to Laurel Road. All access for the proposed

Davidon Homes project would be to and from the south through Vista Grande Drive and Canada Valley Road.

Table 4 summarizes LOS results at the study intersections under Near-Term With Project conditions using both HCM and CCTALOS methodologies. The detailed intersection LOS calculation sheets are provided in Appendices B and C. Although delay experienced by vehicles would increase and LOS would deteriorate under Near-Term Plus Project conditions, the study intersections would continue to operate at LOS D or better.

Queuing on Southbound Canada Valley Road at Lone Tree Way

The Lone Tree Way/Canada Valley Road intersection currently operates at LOS B during the AM peak hour and LOS C during the PM peak hour based on the HCM methodology. The intersection would operate at LOS D under Near-Term With Project conditions. Since the intersection would continue to operate at an acceptable LOS, The project would not cause a significant impact at this intersection using the significance criteria described earlier.

However, based on the completed analysis and confirmed by field observations, the queue on southbound left-turn on Canada Valley Road onto eastbound Lone Tree Way currently exceeds the 170-foot left-turn pocket during both AM and PM peak hours. Table 5 presents the 95th percentile queues on the southbound approach of the intersection under Existing and Near-Term conditions. The detailed queuing analysis reports are included in Appendix D. The queue is expected to increase under Near-Term No Project conditions and would be further exacerbated by the addition of traffic generated by the buildout of the proposed Davidon Homes project.

TABLE 5
QUEUE LENGTHS AT LONE TREE WAY/CANADA VALLEY ROAD

| Lane | Storage Length (feet) | Peak Hour | 95 th Percentile Queue Length (feet) ¹ | | | | | | | |
|--------------------|-----------------------|-----------|--|--------------------------------|----------------------|--------------------------------|--|--------------------------------|---|--------------------------------|
| | | | Existing Conditions | | Near-Term No Project | | Near-Term With Full Project ³ | | Near-Term With Partial Project ³ | |
| | | | Existing Phasing | N/S Split Phasing ² | Existing Phasing | N/S Split Phasing ² | Existing Phasing | N/S Split Phasing ² | Existing Phasing | N/S Split Phasing ² |
| Southbound Through | 320 | AM | 50 | 170 | 50 | 170 | 50 | 370 | 50 | 310 |
| | | PM | 70 | 140 | 70 | 140 | 70 | 360 | 70 | 300 |
| Southbound Left | 170 | AM | 250 | 160 | 250 | 160 | 650 | 260 | 550 | 170 |
| | | PM | 250 | 140 | 290 | 140 | 570 | 250 | 510 | 160 |

Note: **Bold** indicates queue exceeding storage length.

1. 95th percentile queue as calculated by Synchro.
2. This includes implementation of split phasing in the north/south direction and converting the southbound through lane to a shared left-turn/through lane.
3. The project analyzed under this scenario includes all phases of the development (i.e., 525 dwelling units).
4. The project analyzed under this scenario includes 270 dwelling units.

Source: Fehr & Peers, 2008.

The current roadway configuration and the adjacent developments do not allow for providing an additional left-turn lane or lengthening the existing left-turn lane. However, the queue spillover can be alleviated by converting the exclusive southbound through-lane to a shared through/left-turn lane. This lane configuration would require the intersection signal operation to be converted to split phasing in the northbound and southbound directions. The pedestrian signal phases on both the east and west sides of the intersection can still be maintained.

As shown in Table 5, the proposed intersection reconfiguration would reduce the 95th percentile queues on southbound Canada Valley Road under Existing and Near-Term No Project conditions to less than the provided storage length. However, the 95th percentile queues under the Near-Term With Project scenario (where development of the full Davidson project is assumed) after the implementation of the proposed improvement, would be longer than the provided capacity on both the exclusive left-turn lane and the shared left-turn/through lane and queues would spill back to the upstream intersection. It is estimated that the proposed Davidson project would need to be reduced by about 50 percent to about 270 units in order to reduce the queues on southbound Canada Valley Road to be accommodated within the provided storage capacity.

The Lone Tree Way/Canada Valley Road intersection would continue to operate at acceptable LOS D or better after conversion of the exclusive through lane to a shared left/through lane and implementation of split phasing in the north/south direction under Existing, Near-Term No Project, and Near-Term With Project conditions during both AM and PM peak hours.

In the long term, new roadways would connect the Davidson Homes project site to the north through Country Hills Drive and Laurel Road. These roadways would allow trips generated by the Davidson project and adjacent developments to use the new roadways to access the SR 4 Bypass freeway. Thus, reducing the amount of traffic turning left from southbound Canada Valley Road onto Lone Tree Way. The Cumulative conditions analysis, presented in the following section, assumes that these roadway connections would be provided. Therefore, when the roadway connections to Laurel Road are completed, the Davidson Homes project can be completed. In addition, the southbound approach of the Lone Tree Way/Canada Valley Road intersection can be reverted back to its current configuration with exclusive left-turn and through lanes and protected left-turn signal operations in the north/south directions.

Pedestrian Crossing at the Vista Grande Drive/Canada Valley Road/Pinnacle View Way intersection

Canada Valley Road is designated as a collector by City of Antioch. The roadway has a design speed of 45 miles per hour (mph) and a posted speed limit of 30 mph, which is currently under consideration for an increase to 35 mph. As a matter of policy, City of Antioch does not install stop signs on collectors in order to maintain efficient traffic flow.

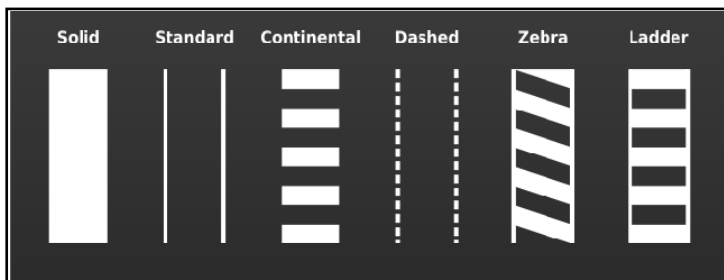
Currently, the Vista Grande Drive/Canada Valley Road/Pinnacle View Way intersection provides three approaches. Only the eastbound Vista Grande Drive approach is stop-controlled. The westbound Pinnacle View Way approach would be completed as part of the Davidson Homes project and would provide access to the project. The Carmen Dragon Elementary School and The Meadow Estates Creek Park are located about one-quarter mile west of the intersection on Vista Grande Drive. Pedestrians must cross Canada Valley Road at this intersection in order to access these uses from the Davidson Homes site. However, the intersection does not currently provide any protected pedestrian crossings and the somewhat high vehicle speeds on Canada Valley Road may deter pedestrians from walking.

Based on traffic volume forecasts developed for this analysis, the intersection is not expected to satisfy MUTCD peak hour intersection volume signal warrants after completion of the Davidson Homes project (See Appendix E). The intersection is also not expected to satisfy the MUTCD pedestrian volume signal

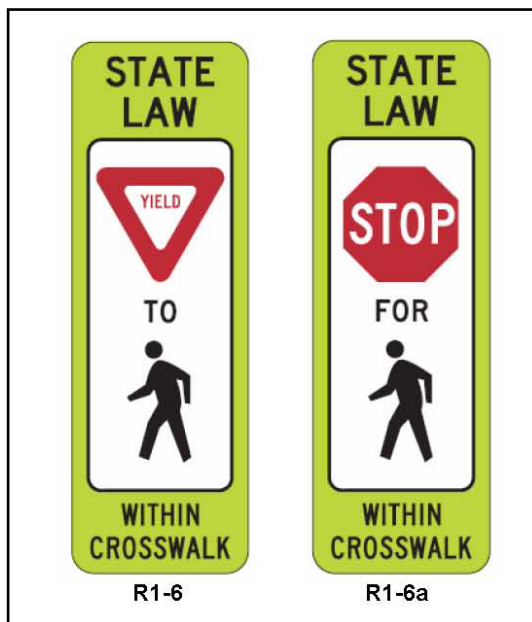
warrant. Thus, conventional signalization of the intersection is not recommended at this time. However, periodic monitoring of vehicular and pedestrian volumes after the completion of the project should be considered to determine if the intersection would satisfy any additional MUTCD signal warrants in the future.

Since conventional signalization or all-way stops are not recommended at this intersection, potential options to improve pedestrian crossing at this intersection are discussed below.

- **High Visibility Crosswalks** – are crosswalks with different striping, patterns, or pavement material that increase the visibility of a crosswalk. They are often accompanied by other enhancements such as in-crosswalk signage, or flashing beacons.



- **In-crosswalk Signage** – (MUTCD Sign R1-6 or R-16a) are typically installed in the roadway median or center striping at unsignalized intersections to remind drivers of pedestrian right-of-way in crosswalk. They are usually manufactured with flexible material to not damage vehicles.



- **Flashing Beacons/Signs** – are overhead or side mounted signs or beacons that are installed at and/or in advance of a crosswalk and are actively or passively activated by pedestrians crossing the roadway. They typically rest on dark and are only activated when pedestrians are present to warn vehicles on the major approach of the roadway. When activated, they regularly flash or stutter amber light to capture driver attention.



- **In-Pavement Warning Lights** – Both sides of a crosswalk are lined with pavement markers, oftentimes containing an amber LED strobe-light. These are manually or passively activated by pedestrians and the strobe-lights provide a dynamic visual cue to drivers. However, their visibility decreases during periods of sunrise/sunset and high congestion. The in-pavement warning lights can be combined with flashing beacons to further increase effectiveness.



- **HAWK Signal** (High Intensity Activated Crosswalks) – Also known as a pedestrian hybrid signal is a special type of pedestrian activated signal used to warn and control traffic at an unsignalized location to assist pedestrian crossing a marked crosswalk. When not activated, the signal is dark. The HAWK signal is activated by a pedestrian push button. The overhead signal begins flashing yellow and then solid yellow, advising drivers to prepare to stop. The signal then displays a solid red and shows pedestrians a “Walk” indication. Finally, an alternating flashing red signal [“wig-wag”] indicates that motorists may proceed when safe, after coming to a full stop. The pedestrian is shown a flashing “Don’t Walk” with a countdown indicating the time left to cross.” The side-street movements would continue to be stop-controlled and are not controlled by the HAWK signal. The figures below show a HAWK signal in operations. These signals have been implemented in Tuscan, Arizona and British Columbia and are effective at enhancing pedestrian safety at locations with high vehicle speeds or volumes where normal signal warrants are not satisfied. Parameters for design and installation of HAWK signals are proposed to be included in the 2009 *Manual on Uniform Traffic Control Devices (MUTCD)*.





Many of the tools discussed above can be used by themselves or in combination with each other to enhance pedestrian safety and encourage walking at the Vista Grande Drive/Canada Valley Road/Pinnacle View Way intersection. Based on the significance criteria presented earlier, the condition at this intersection is not a significant impact; however, it is recommended that City staff select an appropriate improvement strategy at this location in consideration of the City's policies and resources in order to enhance pedestrian safety and encourage walking.

CUMULATIVE CONDITIONS

The analysis of Cumulative No Project and Cumulative With Project conditions are described below.

Cumulative No Project Conditions

The roadway network used for the Cumulative conditions analysis consists of roadway improvements expected to be completed by 2025. These assumptions are consistent with previously completed environmental documents in the area. Major roadway improvements in the vicinity of the Project assumed for this analysis include the following:

- Completion of Segment 2 of the SR 4 Bypass as a four-lane freeway between Lone Tree Way and Balfour Road.
- Extension of Laurel Road from its current terminus just west of the SR 4 Bypass to Hillcrest Avenue.
- Extension of Country Hills Drive north to Laurel Road
- Extension of Slatten Ranch Road from its current terminus just north of Lone Tree Way parallel to SR 4 Bypass.

Lane configurations and traffic control at the study intersections assumed for the Cumulative conditions analysis are presented on Figure 8.

The Cumulative conditions represents the buildout of the City of Antioch General Plan, expected in year 2025. The traffic forecasts used in this analysis were developed based on the CCTA East County Travel Demand Model as modified for the City of Antioch General Plan Update in 2003. Since the Cumulative traffic volume forecasts include the buildout of the proposed Davidson Project, the Cumulative No Project intersection volumes were calculated by subtracting the traffic generated by the proposed Project from the Cumulative intersection turning movement forecasts. The Cumulative No Project intersection volumes are shown on Figure 9.

Tables 6 summarizes peak hour LOS at the study intersections under Cumulative No Project conditions. The detailed intersection LOS calculation sheets are provided in Appendices B and C. The Lone Tree Way/Hillcrest Avenue intersection would operate at LOS E during the PM peak hour using either HCM or CCTALOS methodologies. All other study intersections would continue to operate at LOS D or better under Cumulative No Project conditions using either the HCM or CCTALOS methodologies.

Cumulative With Project Conditions

Trips generated by all phases on the proposed Davidon Homes project (525 units) were added to the Cumulative No Project volumes to estimate the Cumulative With Project Volumes shown on Figure 10. This analysis assumes that the roadway network would remain same as the Cumulative No Project conditions network. In comparison to the Near-Term conditions, the proposed Davidon Homes project would be connected to Laurel Road in the north and trips generated by the project can use the Laurel Road Interchange to access the freeway system.

Table 6 summarizes LOS results at the study intersections under Cumulative With Project conditions using both HCM and CCTALOS methodologies. The detailed intersection LOS calculation sheets are provided in Appendices B and C. Based on both methodologies, all study intersections, except the Laurel Road/Tree Line Way and Lone Tree Way/Hillcrest Avenue intersections, would operate at acceptable LOS D or better during both AM and PM peak hours.

The side-street stop-controlled Laurel Road/Tree Line Way intersection would operate at LOS F during the AM and PM peak hours, based on the HCM methodology. However, the intersection serves low traffic volumes and would not meet the MUTCD peak hour volume signal warrant. Thus, the proposed project would not cause an impact at this intersection because the significance criterion for unsignalized intersections requires the intersection to operate at an unacceptable LOS and satisfy the MUTCD peak hour signal warrant.

Under Cumulative No Project Conditions, the Lone Tree Way/Hillcrest Avenue intersection would operate at LOS D using the HCM methodology and LOS A using the CCTALOS methodology during the AM peak hour. During the PM peak hour, the intersection would operate at unacceptable LOS E using either HCM or CCTALOS methodologies. The addition of Project traffic would add more than 3 seconds of delay using the HCM methodology, therefore constituting a significant impact.

IMPACT 1: The addition of project traffic would contribute to unacceptable LOS E operations at the Lone Tree Way/Hillcrest Avenue intersection during the PM peak hour.

MITIGATION 1: This impact can be mitigated by reconfiguring the southbound Hillcrest Avenue approach (currently one exclusive right-turn lane, one through lane, one shared through and left-turn lane, and one exclusive left-turn lane) to an exclusive right-turn lane, one through lane, and two exclusive left-turn lanes, and providing a second left-turn lane on the eastbound Lone Tree Way approach. The Project should contribute its fair share toward the construction of this mitigation measure.

With implementation of this mitigation, the Lone Tree Way/Hillcrest Avenue intersection would improve to acceptable conditions (LOS C with 31 seconds of delay during the AM peak hour and LOS D with 46 seconds of delay during the PM peak hour using the HCM methodology and LOS A with v/c of 0.60 during the AM peak hour and LOS C with v/c of 0.75 during the PM peak hour using the CCTALOS methodology.)

This improvement was also recommended in the *Arcadia Mixed Use Planned Development EIR* (March 2002).

**TABLE 6
CUMULATIVE CONDITIONS
PEAK HOUR LEVEL OF SERVICE**

| No. | Intersection | Control ¹ | Peak Hour | No Project | | | | With Project ⁴ | | | |
|-----|--|----------------------|-----------|-----------------|------------------|---------------------|------------------|---------------------------|----------------------|---------------------|------------------|
| | | | | HCM | | CCTALOS | | HCM | | CCTALOS | |
| | | | | Delay | LOS ² | V/C | LOS ³ | Delay | LOS ² | V/C | LOS ³ |
| 1 | Laurel Road/Canada Valley Road | Signal | AM PM | 19 18 | B B | 0.51 0.48 | A A | 21 21 | C C | 0.53 0.52 | A A |
| 2 | Laurel Road/Country Hills Drive | Signal | AM PM | 32 26 | C C | 0.56 0.48 | A A | 37 30 | D C | 0.68 0.57 | B A |
| 3 | Laurel Road/Southbound SR 4 Bypass Ramps | Signal | AM PM | 17 16 | B B | 0.52 0.51 | A A | 17 15 | B B | 0.58 0.60 | A A |
| 4 | Laurel Road/Northbound SR 4 Bypass Ramps | Signal | AM PM | 7 10 | A A | 0.53 0.63 | A B | 9 12 | A B | 0.57 0.67 | A B |
| 5 | Laurel Road/Slatten Ranch Road | Signal | AM PM | 29 35 | C D | 0.69 0.75 | A C | 28 35 | C C | 0.69 0.76 | B C |
| 6 | Laurel Road/Live Oak Ave | Signal | AM PM | 16 27 | B C | 0.44 0.42 | A A | 16 24 | B C | 0.44 0.43 | A A |
| 7 | Laurel Road/Empire Ave | Signal | AM PM | 27 32 | C C | 0.55 0.52 | A A | 28 31 | C C | 0.56 0.55 | A A |
| 8 | Lone Tree Way/Canada Valley Road | Signal | AM PM | 25 36 | C D | 0.57 0.72 | A C | 26 38 | C D | 0.60 0.78 | A C |
| 9 | Lone Tree Way/SB SR 4 Bypass Ramps | Signal | AM PM | 23 24 | C C | 0.57 0.79 | A C | 23 24 | C C | 0.58 0.80 | A C |
| 10 | Lone Tree Way/NB SR 4 Bypass Ramps | Signal | AM PM | 9 16 | A B | 0.54 0.71 | A C | 10 16 | A B | 0.54 0.71 | A C |
| 11 | Lone Tree Way/Slatten Ranch Road | Signal | AM PM | 45 39 | D D | 0.72 0.79 | C C | 45 40 | D D | 0.72 0.80 | C C |
| 12 | Lone Tree Way/Empire Avenue | Signal | AM PM | 38 24 | D C | 0.61 0.57 | B A | 38 24 | D C | 0.61 0.57 | B A |
| 13 | Lone Tree Way/Deer Valley Road | Signal | AM PM | 49 53 | D D | 0.84 0.88 | D D | 50 55 | D D | 0.85 0.89 | D D |
| 14 | Lone Tree Way/Hillcrest Avenue | Signal | AM PM | 42 58 | D E | 0.60 0.93 | A E | 45 66 | D E | 0.62 0.94 | B E |
| 15 | Lone Tree Way/Vista Grande Drive | Signal | AM PM | 26 38 | C D | 0.56 0.84 | A D | 26 39 | C D | 0.57 0.85 | A D |
| 16 | Country Hills Drive/Hillcrest Avenue | Signal | AM PM | 19 22 | B C | 0.42 0.53 | A A | 19 22 | B C | 0.42 0.54 | A A |
| 17 | Laurel Road/Tree Line Way | SSS ² | AM PM | N/A N/A | N/A N/A | N/A N/A | N/A N/A | 67 68 | F F | N/A N/A | N/A N/A |
| 18 | Laurel Road/Hillcrest Avenue | Signal | AM PM | 40 52 | D D | 0.85 0.87 | D D | 40 54 | D D | 0.85 0.88 | D D |

Note: **Bold** indicates intersections exceeding LOS standard.

1. Signal = signal controlled intersection.
2. Level of service for intersections based on control delay per vehicle, according to the *Highway Capacity Manual*, Transportation Research Board, 2000.
3. Signalized intersection level of service is based on v/c ratio according to the *Contra Costa Transportation Authority Technical Procedures Manual, 1997(CCTA)*.
4. The project analyzed under this scenario includes all phases of the development (i.e., 525 dwelling units).

Source: Fehr & Peers, 2008.

Queuing on Westbound Laurel Road at Country Hills Drive

The analysis completed for this study assumes that the westbound Laurel Road provides a single left-turn lane into southbound Country Hills Drive. As shown in Table 6, the Laurel Road/Country Hills Drive intersection would operate at acceptable LOS D or better during both AM and PM peak hours under Cumulative Plus Project conditions using either HCM or CCTALOS methodologies. However, it is estimated that the close spacing of the Laurel Road/Southbound SR 4 Bypass Ramps intersection to the east limits the storage space available for the left-turn lane on westbound Laurel Road onto southbound Country Hills Drive to about 250 feet under Cumulative With Project conditions. Based on the completed analysis, the 95th percentile queue would be about 300 feet during the PM peak hour under Cumulative Plus Project conditions. Thus, the queue would occasionally spill out of the left-turn pocket and block traffic in the through lane during the peak hours; however since the intersection would operate at LOS D or better, the queue would clear at the end of each signal cycle.

The queue spillover can be alleviated by constructing a second left-turn lane on westbound Laurel Road. This would also require construction of a second receiving lane on southbound Country Hills Drive. The second lane would need to be about 300 feet. This improvement would reduce the 95th percentile queue to about 150 feet for each of the dual left-turn lane and reduce the likelihood that queues would spillover the left-turn pocket.

CCTA TRAFFIC SERVICE OBJECTIVES ANALYSIS

The *East County Action Plan for Routes of Regional Significance* (CCTA, 2000) establishes traffic service objectives (TSOs) for routes of regional significance in eastern Contra Costa County. These routes consist of freeways and major arterials that provide region wide connectivity.

One TSO used to measure freeway and arterial operations is peak hour Delay Index. Delay Index is defined as the ratio of the peak hour congested travel time to free-flow travel time on each roadway segment. For example, a Delay Index of 2.0 means that it takes twice as long to travel a particular segment during the peak commute hour than during non-commute hours when traffic moves at free-flow speeds. Objectives for relevant routes include a Delay Index of 2.5 for the SR 4 freeway and 2.0 for surface arterials.

Operations along routes of regional significance under Cumulative conditions were evaluated using the Delay Index measure. The Delay Index was calculated using results from the latest CCTA countywide travel demand model. As shown in Table 7, all roadway segments satisfy their TSO under Cumulative conditions.

**TABLE 7
CUMULATIVE CONDITIONS
DELAY INDEX SUMMARY¹**

| Roadway Segment | Peak Hour | TSO | No Project | | With Project | |
|--|-----------|-----|-------------------------|-------------------------|-------------------------|-------------------------|
| | | | Northbound or Eastbound | Southbound or Westbound | Northbound or Eastbound | Southbound or Westbound |
| SR4 between A St. and Hillcrest Ave. | AM | 2.5 | 1.0 | 1.3 | 1.0 | 1.3 |
| | PM | 2.5 | 1.6 | 1.1 | 1.6 | 1.1 |
| SR4 between Hillcrest and SR160 | AM | 2.5 | 1.1 | 1.2 | 1.1 | 1.2 |
| | PM | 2.5 | 1.0 | 1.0 | 1.0 | 1.0 |
| SR4 Bypass between SR160 and Laurel Rd | AM | 2.5 | 1.2 | 1.1 | 1.2 | 1.1 |
| | PM | 2.5 | 1.4 | 1.0 | 1.4 | 1.0 |
| SR4 Bypass between Laurel Rd and Lone Tree Way | AM | 2.5 | 1.0 | 1.3 | 1.0 | 1.3 |
| | PM | 2.5 | 1.2 | 1.0 | 1.2 | 1.0 |
| SR4 Bypass between Lone Tree Way and Sand Creek Rd | AM | 2.5 | 1.0 | 1.3 | 1.0 | 1.3 |
| | PM | 2.5 | 1.2 | 1.0 | 1.2 | 1.0 |
| Hillcrest Ave. between SR 4 and Deer Valley Rd. | AM | 2.0 | 1.1 | 1.0 | 1.1 | 1.0 |
| | PM | 2.0 | 1.0 | 1.3 | 1.0 | 1.4 |
| Hillcrest Ave. between Deer Valley Rd. and Laurel Rd. | AM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| | PM | 2.0 | 1.0 | 1.1 | 1.0 | 1.1 |
| Hillcrest Ave. between SR 4 and Deer Valley Rd. | AM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| | PM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Laurel Rd. between Hillcrest Ave. and SR4 Bypass | AM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| | PM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Laurel Rd. between SR4 Bypass and Main St. | AM | 2.0 | 1.0 | 1.2 | 1.0 | 1.2 |
| | PM | 2.0 | 1.2 | 1.0 | 1.2 | 1.0 |
| Lone Tree Way between Deer Valley Rd. and Hillcrest Ave. | AM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| | PM | 2.0 | 1.0 | 1.0 | 1.1 | 1.0 |
| Lone Tree Way between Hillcrest Ave. and SR4 Bypass | AM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| | PM | 2.0 | 1.1 | 1.0 | 1.1 | 1.0 |
| Lone Tree Way between SR4 Bypass and Fairview Ave | AM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| | PM | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |

Note: **Bold** indicates roadway segments exceeding the TSO.

1. Delay Index defined as ratio of peak hour congested to free-flow travel time and as estimated by the CCTA Countywide Travel Demand.

Source: Fehr & Peers, 2008.

Please contact us with any questions or comments.

Attachments:

Figures

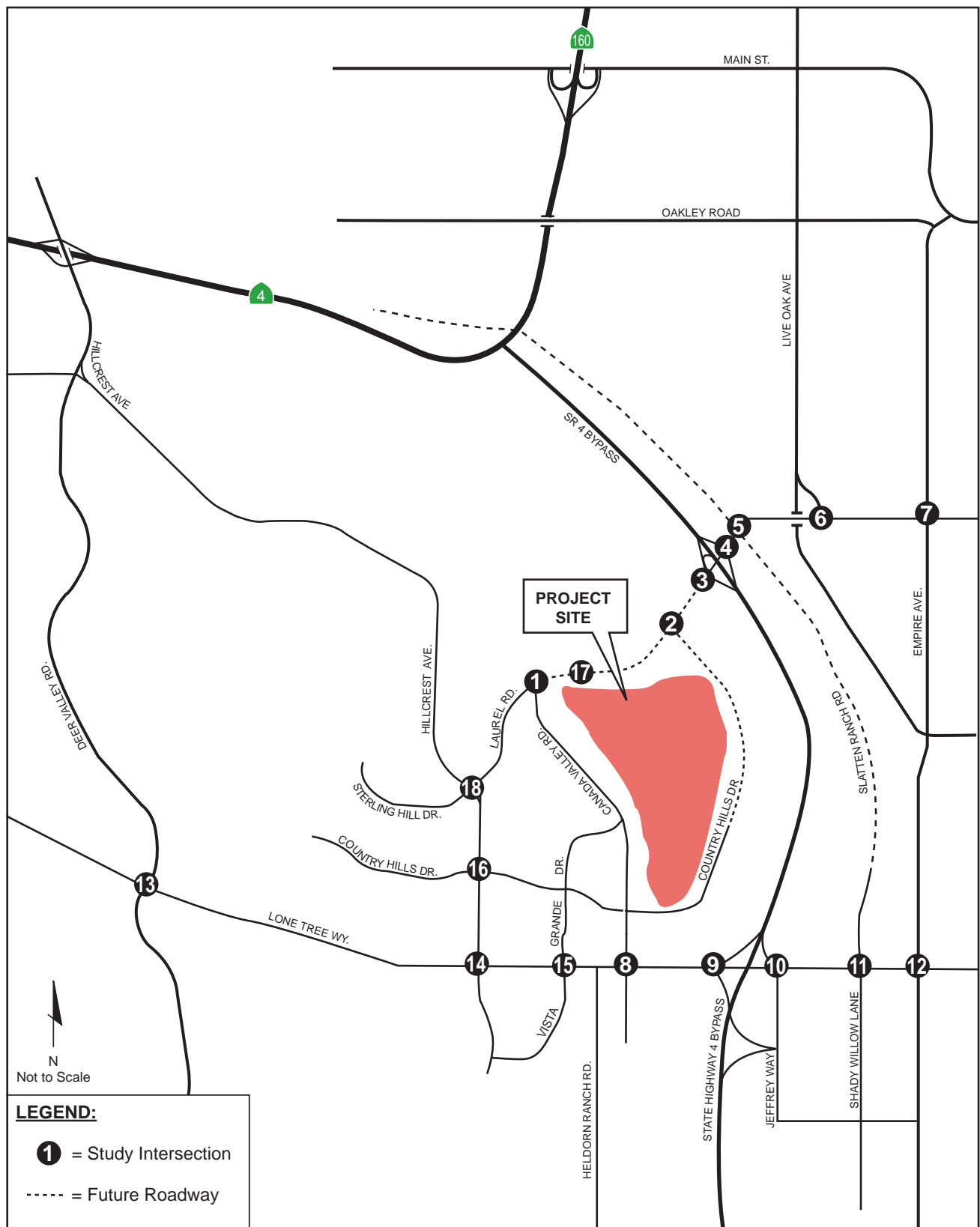
Appendix A: Existing Traffic Counts

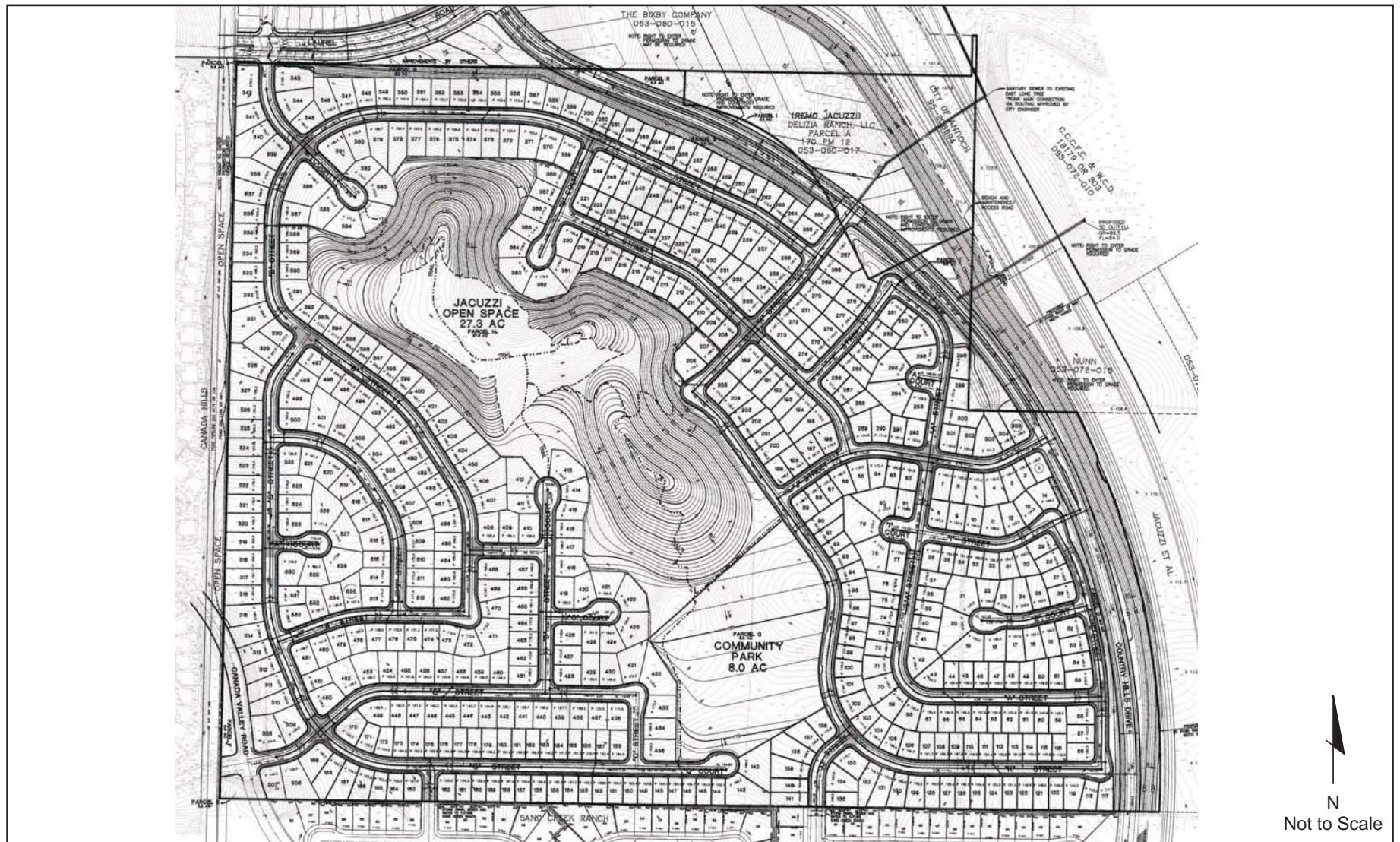
Appendix B: HCM LOS Calculation Worksheets

Appendix C: CCTALOS Calculation Worksheets

Appendix D: Lone Tree Way/Canada Valley Road Queuing Reports (check sheets)

Appendix E: Vista Grande/Canada Valley/Pinnacle View Way Signal Warrant Worksheet



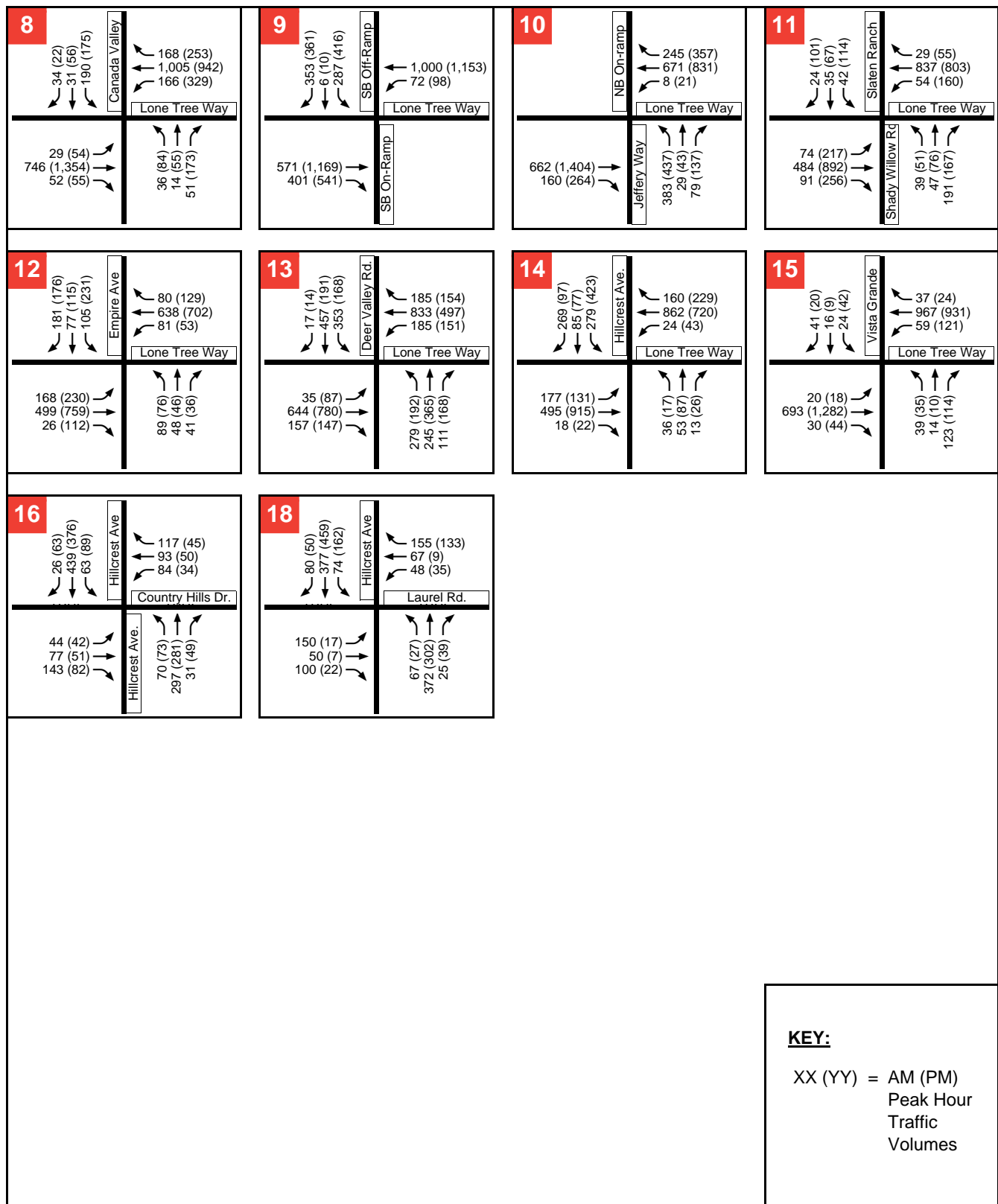


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Davidon Homes Transportation Analysis

SITE PLAN
FIGURE 2



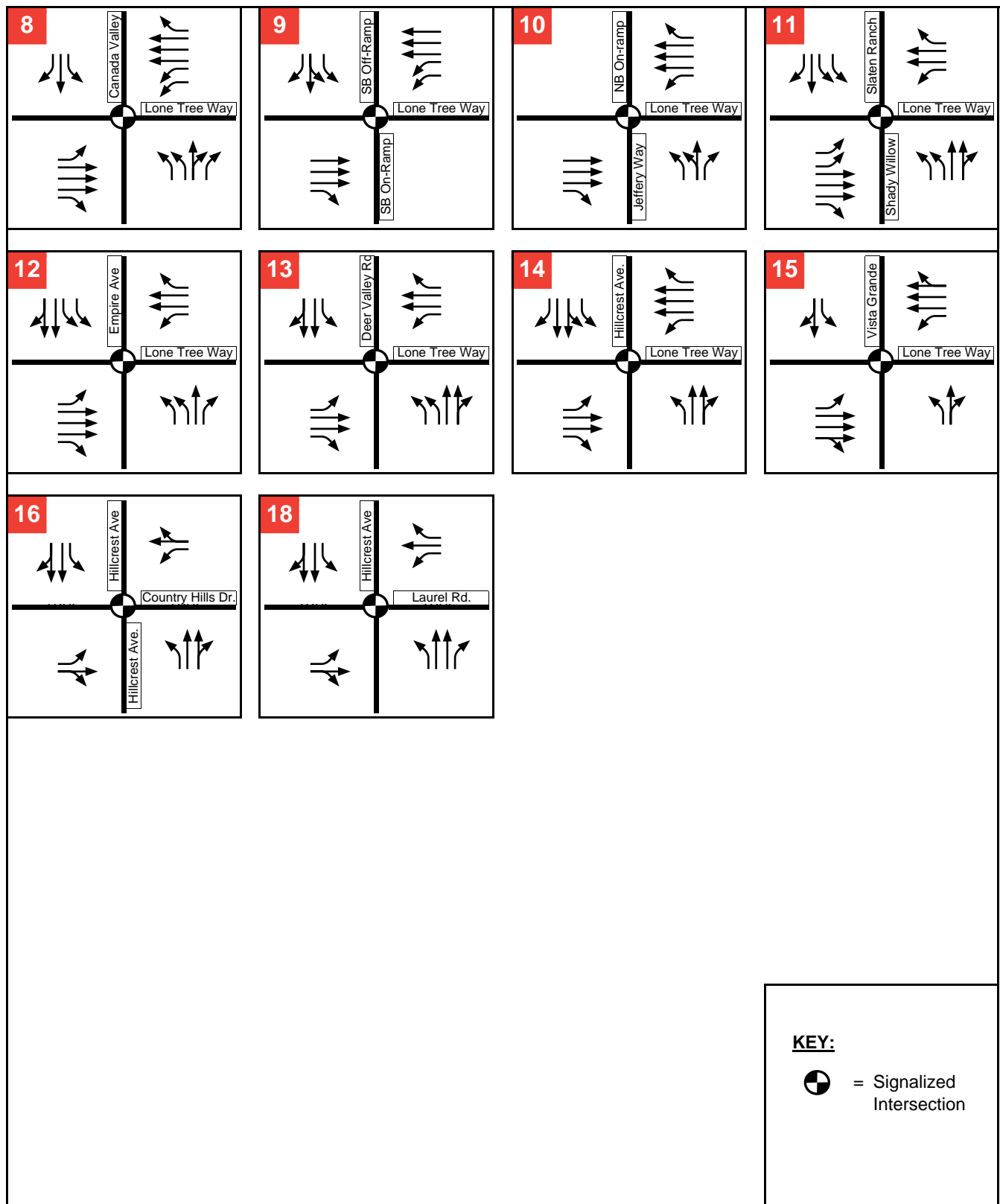
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November 2008
Graphics\Nov08 Update\WC05-2153_3

Davidon Homes Transportation Analysis

EXISTING CONDITIONS PEAK HOUR TURNING MOVEMENTS

FIGURE 3



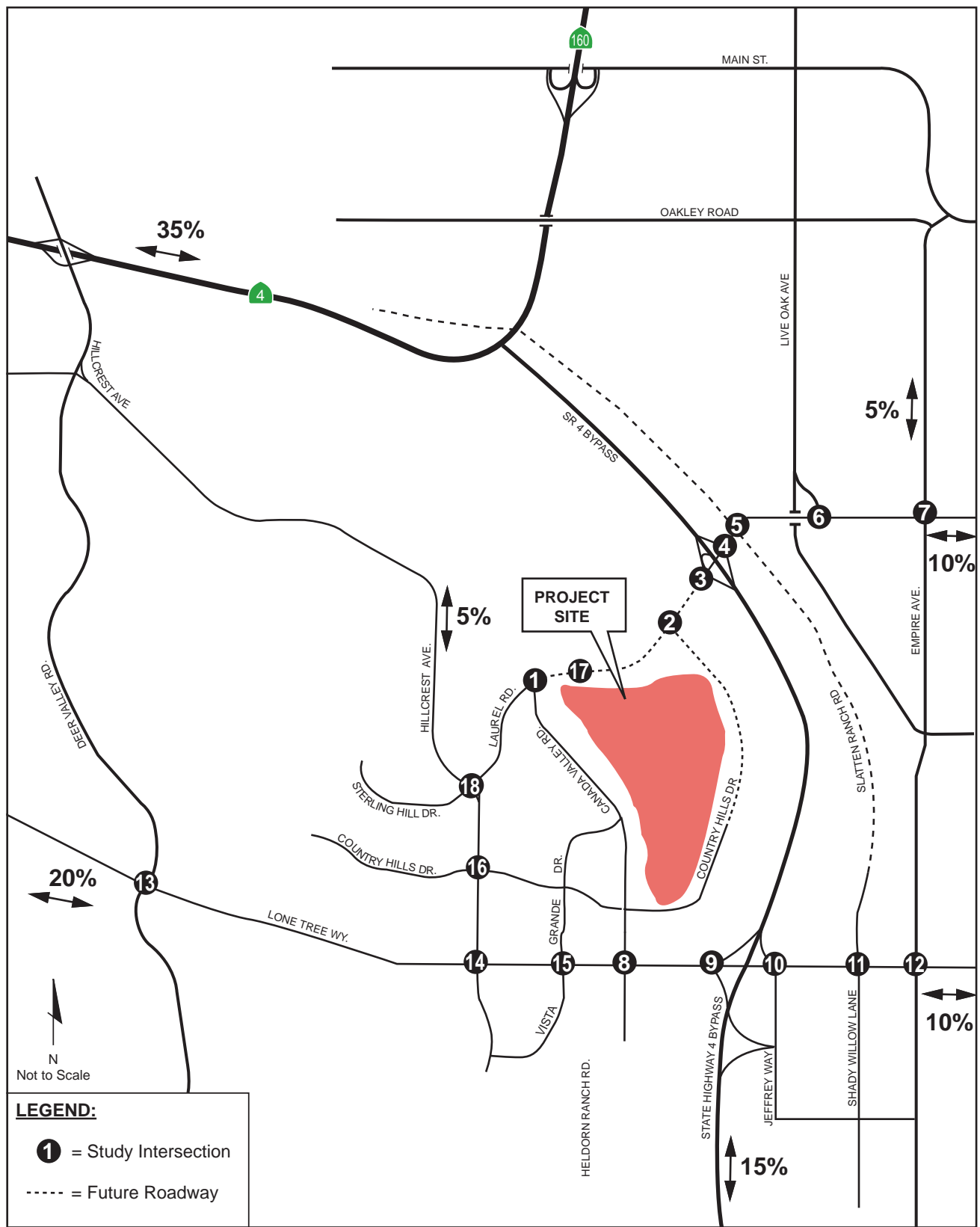
FEHR & PEERS
TRANSPORTATION CONSULTANTS

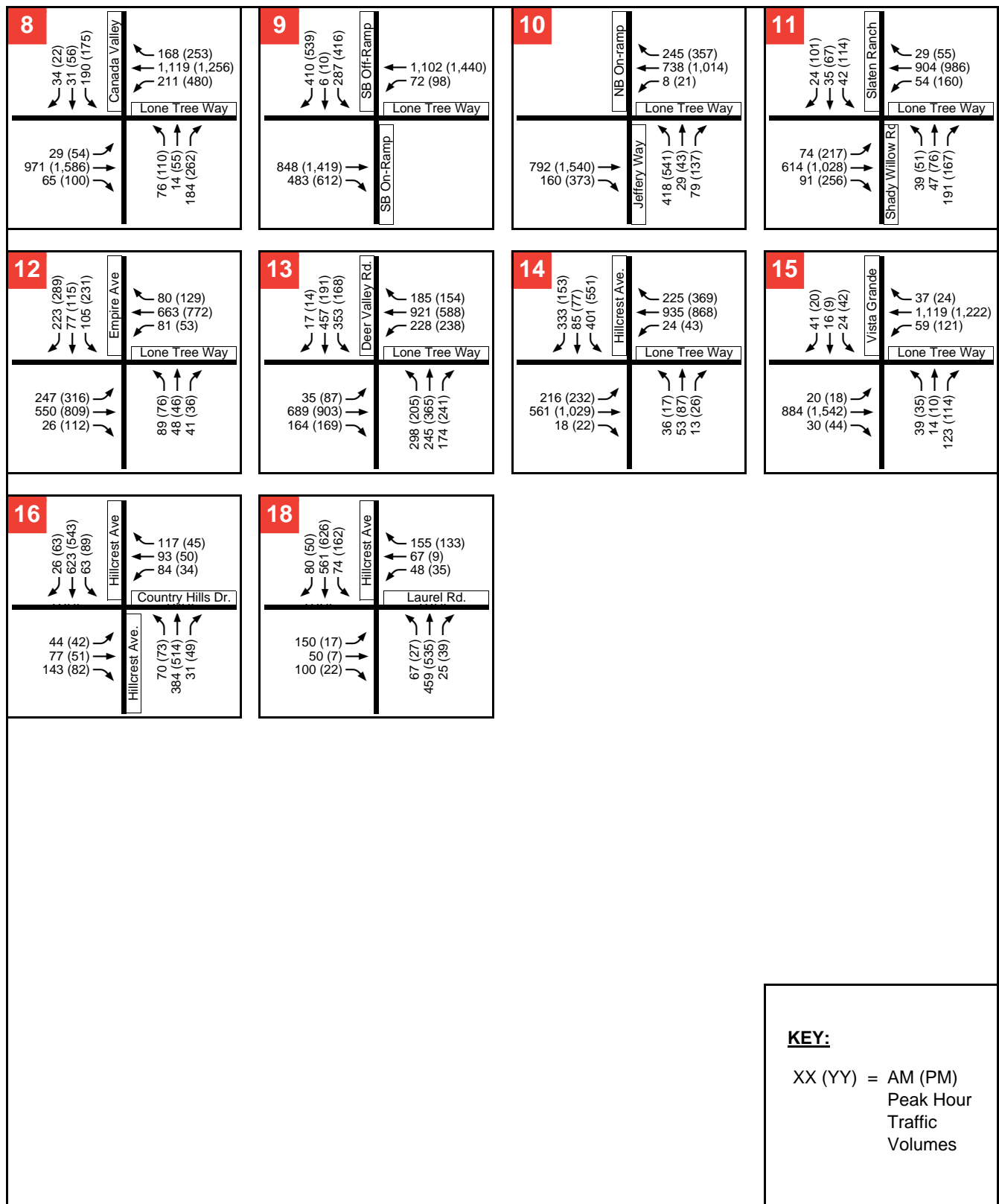
November 2008
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Davidon Homes Transportation Analysis

EXISTING CONDITIONS LANE CONFIGURATIONS AND TRAFFIC CONTROL

FIGURE 4





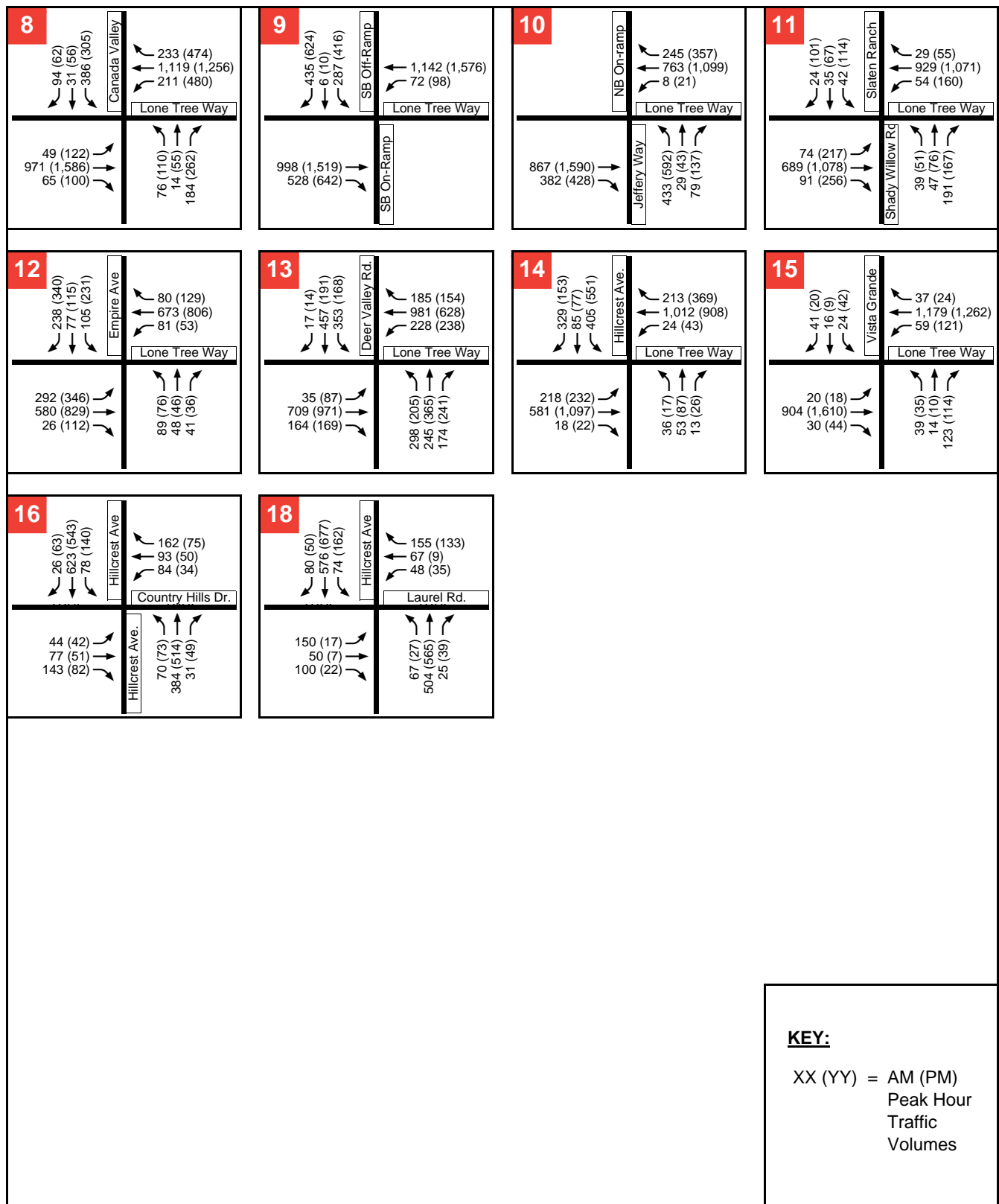
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Davidon Homes Transportation Analysis

NEAR-TERM NO PROJECT PEAK HOUR TURNING MOVEMENTS

FIGURE 6



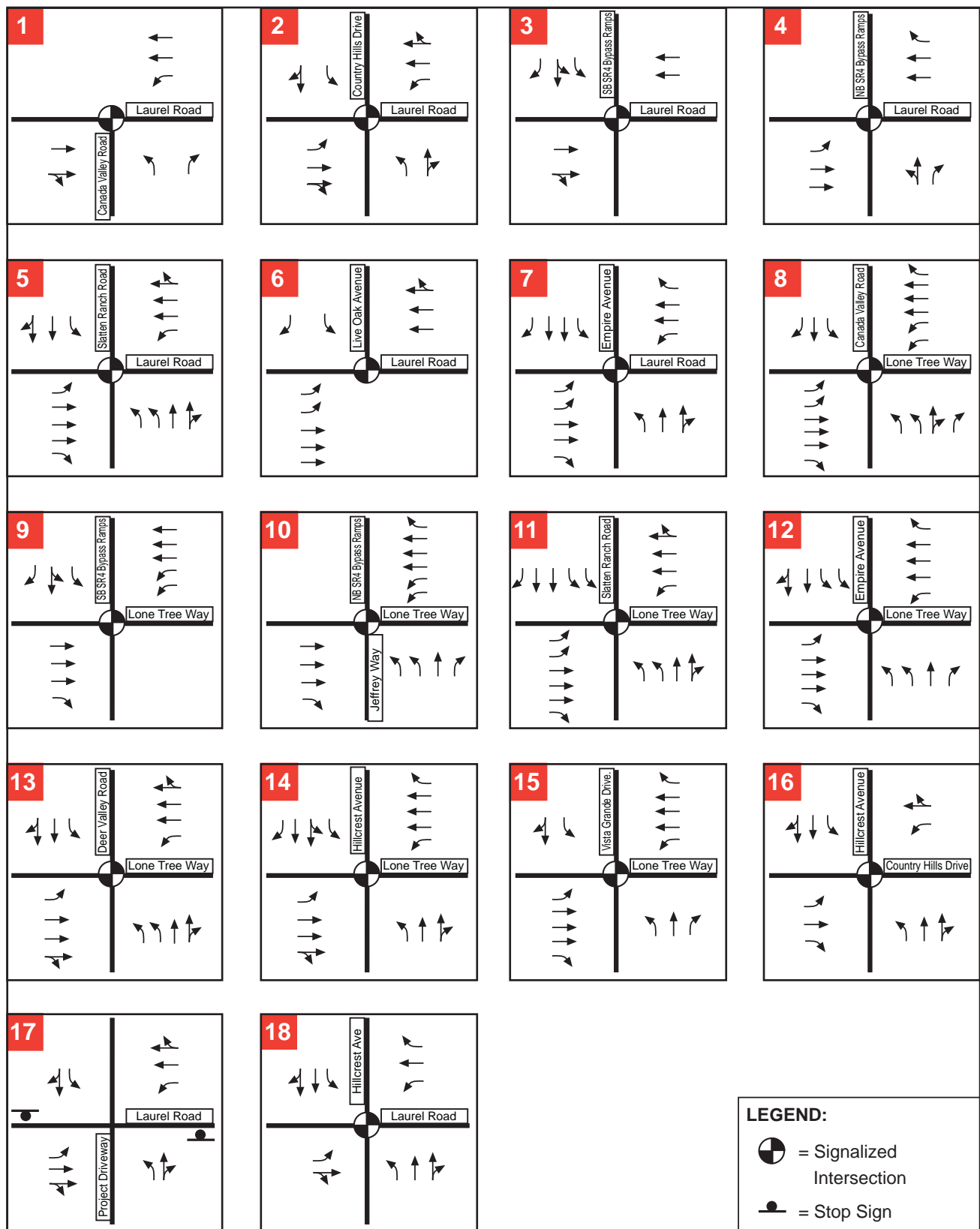
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Davidon Homes Transportation Analysis

NEAR-TERM WITH PROJECT
PEAK HOUR TURNING MOVEMENTS

FIGURE 7



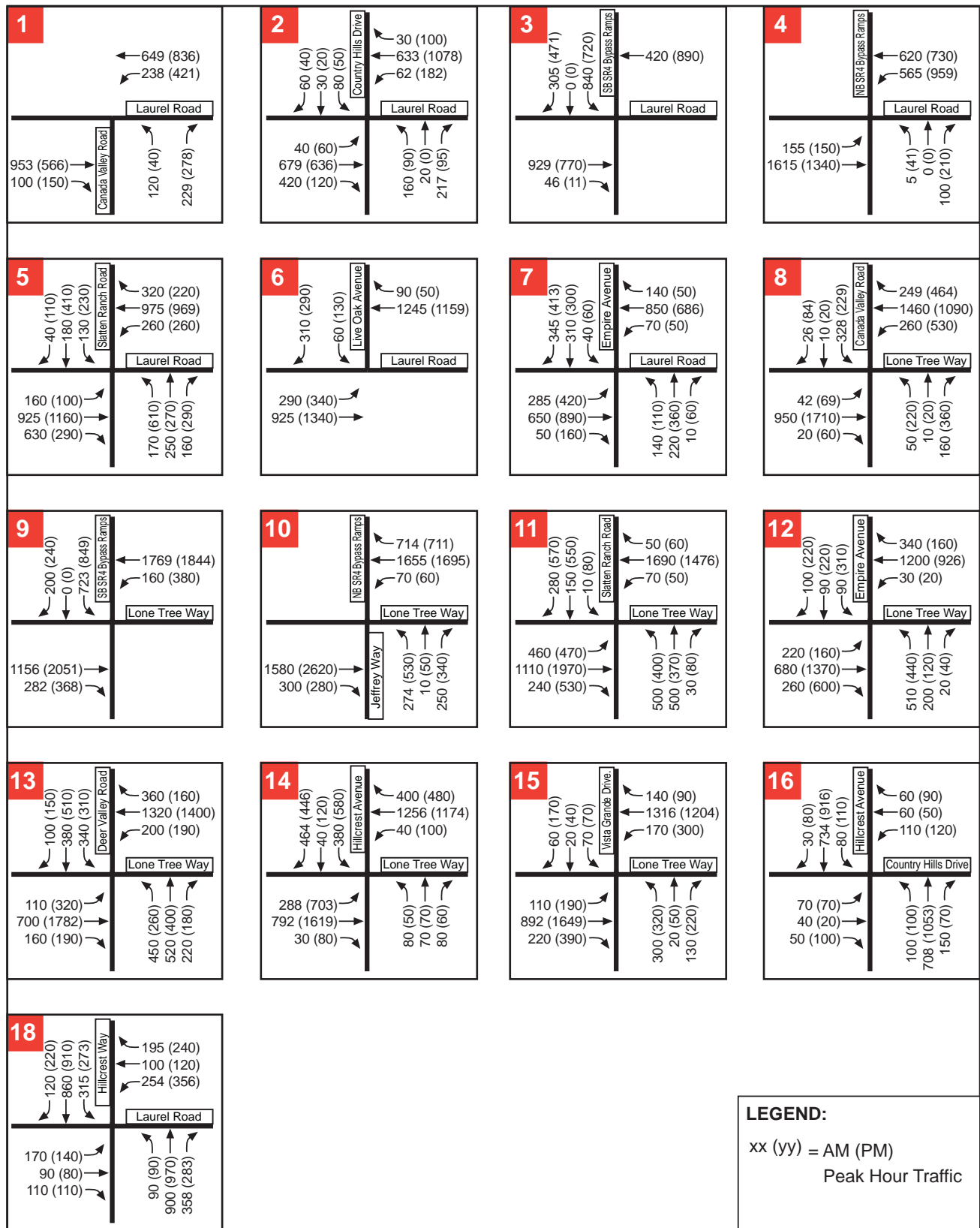
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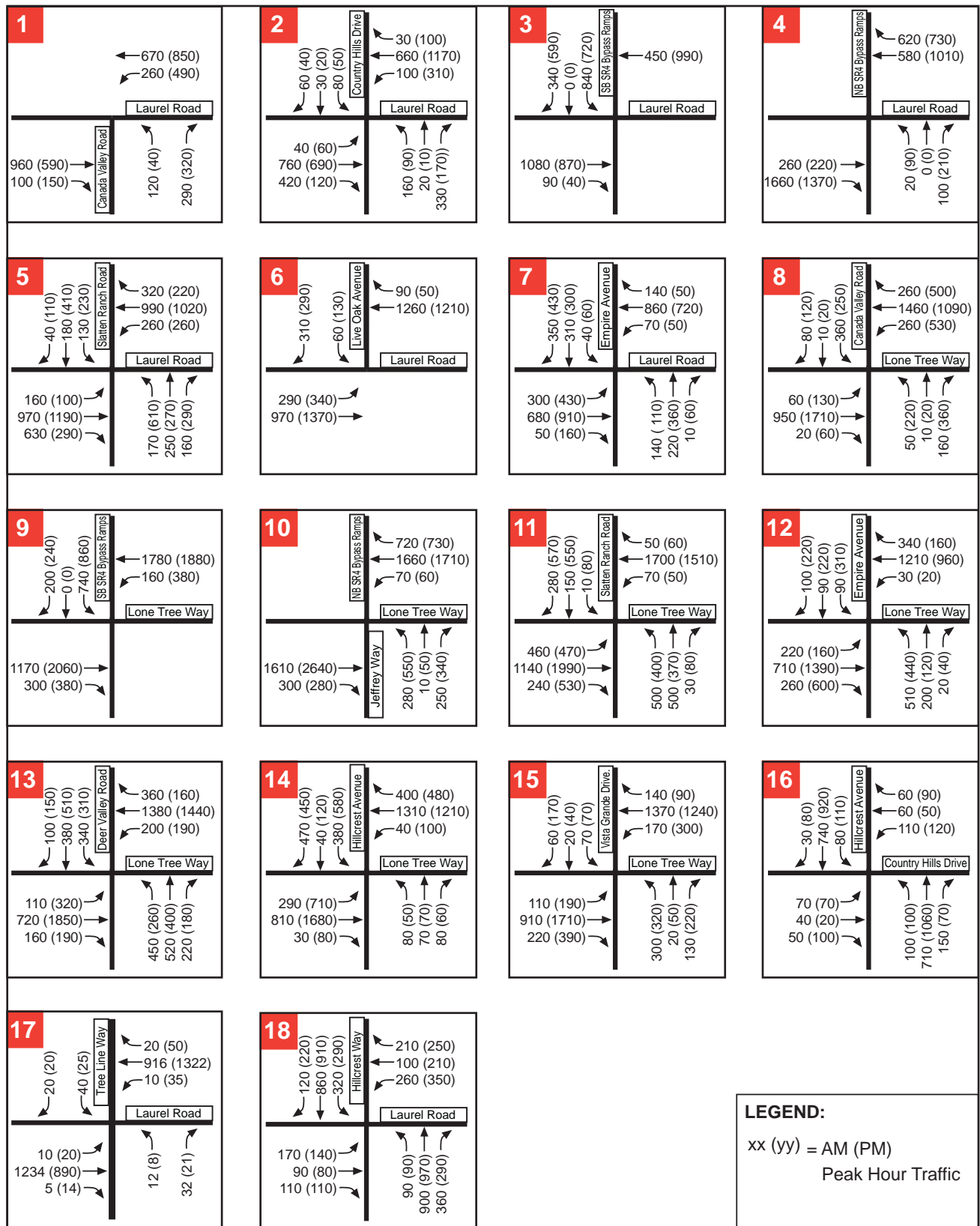
November 2008
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Davidon Homes Transportation Analysis

YEAR 2025 LANE GEOMETRIES AND TRAFFIC CONTROL

FIGURE 8



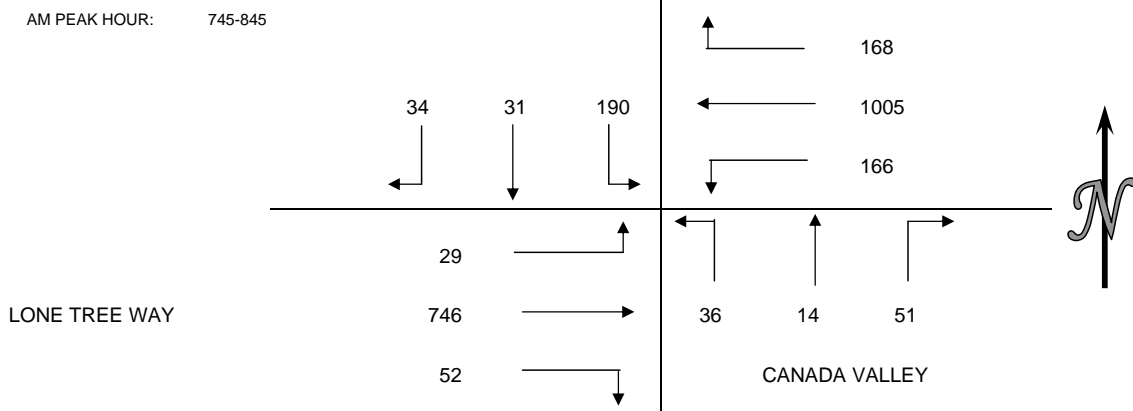


APPENDIX A:
Existing Traffic Counts

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S CANADA VALLEY
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-715 | 14 | 8 | 33 | 30 | 126 | 23 | 5 | 5 | 7 | 7 | 111 | 4 | 373 |
| 715-730 | 8 | 6 | 37 | 27 | 166 | 25 | 8 | 3 | 7 | 6 | 120 | 1 | 414 |
| 730-745 | 10 | 5 | 44 | 33 | 237 | 37 | 5 | 0 | 7 | 9 | 134 | 4 | 525 |
| 745-800 | 10 | 10 | 61 | 55 | 289 | 32 | 14 | 3 | 4 | 13 | 205 | 3 | 699 |
| 800-815 | 11 | 7 | 57 | 50 | 211 | 38 | 12 | 1 | 6 | 10 | 162 | 10 | 575 |
| 815-830 | 5 | 10 | 41 | 39 | 267 | 69 | 11 | 6 | 10 | 13 | 193 | 9 | 673 |
| 830-845 | 8 | 4 | 31 | 24 | 238 | 27 | 14 | 4 | 16 | 16 | 186 | 7 | 575 |
| 845-900 | 5 | 2 | 48 | 21 | 205 | 71 | 11 | 4 | 16 | 10 | 197 | 4 | 594 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-800 | 42 | 29 | 175 | 145 | 818 | 117 | 32 | 11 | 25 | 35 | 570 | 12 | 2011 |
| 715-815 | 39 | 28 | 199 | 165 | 903 | 132 | 39 | 7 | 24 | 38 | 621 | 18 | 2213 |
| 730-830 | 36 | 32 | 203 | 177 | 1004 | 176 | 42 | 10 | 27 | 45 | 694 | 26 | 2472 |
| 745-845 | 34 | 31 | 190 | 168 | 1005 | 166 | 51 | 14 | 36 | 52 | 746 | 29 | 2522 |
| 800-900 | 29 | 23 | 177 | 134 | 921 | 205 | 48 | 15 | 48 | 49 | 738 | 30 | 2417 |



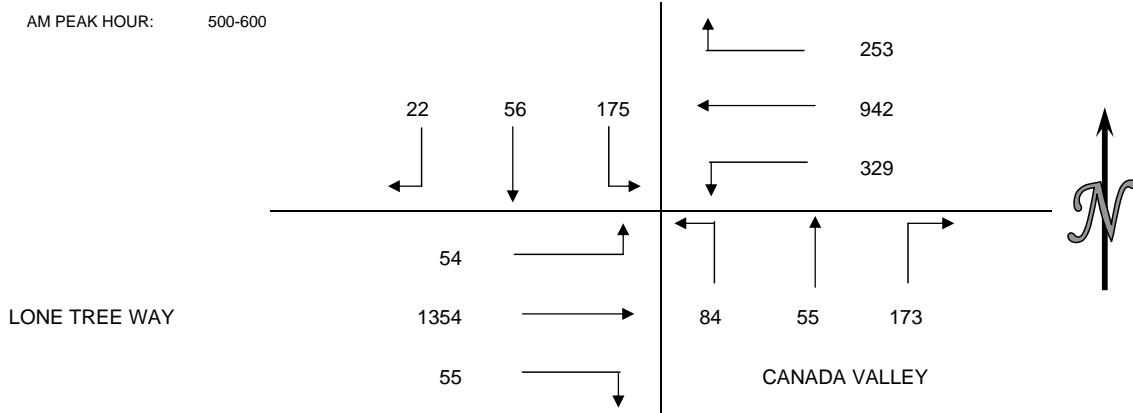
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 3 | 1 | 0 | 4 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 1 | 0 | 0 | 1 |
| 745-800 | 0 | 0 | 0 | 0 | 0 |
| 800-815 | 0 | 0 | 0 | 0 | 0 |
| 815-830 | 1 | 1 | 0 | 0 | 2 |
| 830-845 | 0 | 0 | 1 | 0 | 1 |
| 845-900 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 0 | 4 | 1 | 0 | 5 |
| 715-815 | 0 | 1 | 0 | 0 | 1 |
| 730-830 | 1 | 2 | 0 | 0 | 3 |
| 745-845 | 1 | 1 | 1 | 0 | 3 |
| 800-900 | 1 | 1 | 1 | 0 | 3 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 1 | 0 | 1 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 1 | 0 | 1 | 1 | 3 |
| 800-815 | 1 | 0 | 1 | 0 | 2 |
| 815-830 | 1 | 0 | 1 | 0 | 2 |
| 830-845 | 1 | 1 | 2 | 0 | 4 |
| 845-900 | 1 | 1 | 0 | 0 | 2 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 1 | 0 | 2 | 1 | 4 |
| 715-815 | 2 | 0 | 2 | 1 | 5 |
| 730-830 | 3 | 0 | 3 | 1 | 7 |
| 745-845 | 4 | 1 | 5 | 1 | 11 |
| 800-900 | 4 | 2 | 4 | 0 | 10 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S CANADA VALLEY
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-415 | 9 | 11 | 51 | 58 | 252 | 66 | 41 | 18 | 20 | 14 | 329 | 12 | 881 |
| 415-430 | 9 | 13 | 40 | 41 | 255 | 57 | 29 | 20 | 15 | 10 | 323 | 12 | 824 |
| 430-445 | 11 | 11 | 49 | 42 | 245 | 69 | 34 | 10 | 21 | 10 | 300 | 9 | 811 |
| 445-500 | 9 | 14 | 64 | 55 | 235 | 79 | 50 | 8 | 19 | 20 | 344 | 7 | 904 |
| 500-515 | 7 | 15 | 42 | 52 | 234 | 92 | 22 | 15 | 10 | 14 | 310 | 15 | 828 |
| 515-530 | 6 | 20 | 45 | 76 | 222 | 77 | 55 | 12 | 20 | 16 | 371 | 8 | 928 |
| 530-545 | 4 | 13 | 46 | 49 | 227 | 74 | 36 | 12 | 26 | 15 | 360 | 17 | 879 |
| 545-600 | 5 | 8 | 42 | 76 | 259 | 86 | 60 | 16 | 28 | 10 | 313 | 14 | 917 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-500 | 38 | 49 | 204 | 196 | 987 | 271 | 154 | 56 | 75 | 54 | 1296 | 40 | 3420 |
| 415-515 | 36 | 53 | 195 | 190 | 969 | 297 | 135 | 53 | 65 | 54 | 1277 | 43 | 3367 |
| 430-530 | 33 | 60 | 200 | 225 | 936 | 317 | 161 | 45 | 70 | 60 | 1325 | 39 | 3471 |
| 445-545 | 26 | 62 | 197 | 232 | 918 | 322 | 163 | 47 | 75 | 65 | 1385 | 47 | 3539 |
| 500-600 | 22 | 56 | 175 | 253 | 942 | 329 | 173 | 55 | 84 | 55 | 1354 | 54 | 3552 |



| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 2 | 0 | 0 | 4 | 6 |
| 415-430 | 2 | 0 | 2 | 1 | 5 |
| 430-445 | 0 | 3 | 2 | 0 | 5 |
| 445-500 | 1 | 0 | 0 | 0 | 1 |
| 500-515 | 1 | 2 | 0 | 0 | 3 |
| 515-530 | 0 | 0 | 2 | 1 | 3 |
| 530-545 | 0 | 0 | 2 | 0 | 2 |
| 545-600 | 1 | 0 | 6 | 0 | 7 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 5 | 3 | 4 | 5 | 17 |
| 415-515 | 4 | 5 | 4 | 1 | 14 |
| 430-530 | 2 | 5 | 4 | 1 | 12 |
| 445-545 | 2 | 2 | 4 | 1 | 9 |
| 500-600 | 2 | 2 | 10 | 1 | 15 |

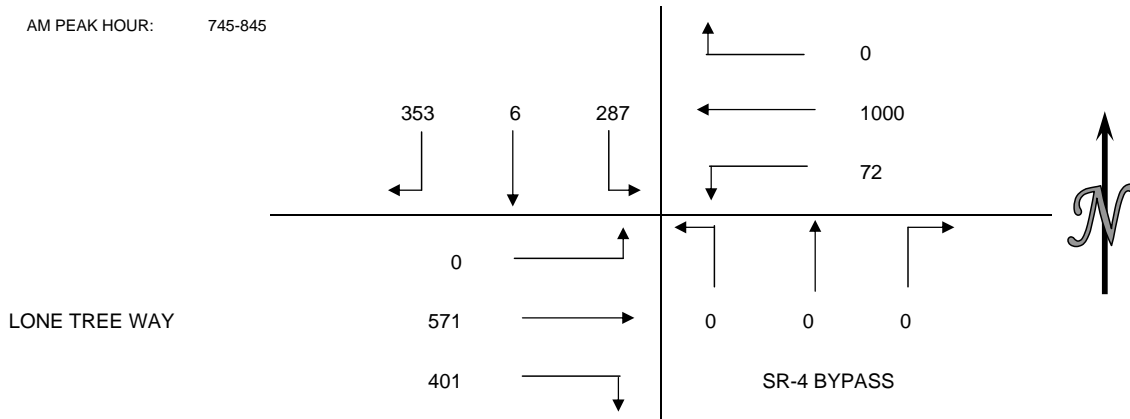
| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 0 | 0 | 0 | 0 |
| 415-430 | 0 | 0 | 0 | 0 | 0 |
| 430-445 | 0 | 0 | 0 | 0 | 0 |
| 445-500 | 0 | 0 | 0 | 1 | 1 |
| 500-515 | 0 | 0 | 2 | 0 | 2 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 0 | 2 | 0 | 2 |
| 545-600 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 0 | 0 | 0 | 1 | 1 |
| 415-515 | 0 | 0 | 2 | 1 | 3 |
| 430-530 | 0 | 0 | 2 | 1 | 3 |
| 445-545 | 0 | 0 | 4 | 1 | 5 |
| 500-600 | 0 | 0 | 4 | 0 | 4 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S SR-4 BYPASS
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-715 | 33 | 1 | 35 | 0 | 131 | 13 | 0 | 0 | 0 | 60 | 56 | 0 | 329 |
| 715-730 | 57 | 1 | 41 | 0 | 187 | 21 | 0 | 0 | 0 | 114 | 84 | 0 | 505 |
| 730-745 | 89 | 1 | 54 | 0 | 202 | 13 | 0 | 0 | 0 | 81 | 101 | 0 | 541 |
| 745-800 | 106 | 3 | 81 | 0 | 261 | 23 | 0 | 0 | 0 | 100 | 170 | 0 | 744 |
| 800-815 | 84 | 0 | 78 | 0 | 255 | 18 | 0 | 0 | 0 | 103 | 152 | 0 | 690 |
| 815-830 | 95 | 1 | 65 | 0 | 267 | 11 | 0 | 0 | 0 | 93 | 111 | 0 | 643 |
| 830-845 | 68 | 2 | 63 | 0 | 217 | 20 | 0 | 0 | 0 | 105 | 138 | 0 | 613 |
| 845-900 | 75 | 0 | 56 | 0 | 237 | 9 | 0 | 0 | 0 | 116 | 136 | 0 | 629 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-800 | 285 | 6 | 211 | 0 | 781 | 70 | 0 | 0 | 0 | 355 | 411 | 0 | 2119 |
| 715-815 | 336 | 5 | 254 | 0 | 905 | 75 | 0 | 0 | 0 | 398 | 507 | 0 | 2480 |
| 730-830 | 374 | 5 | 278 | 0 | 985 | 65 | 0 | 0 | 0 | 377 | 534 | 0 | 2618 |
| 745-845 | 353 | 6 | 287 | 0 | 1000 | 72 | 0 | 0 | 0 | 401 | 571 | 0 | 2690 |
| 800-900 | 322 | 3 | 262 | 0 | 976 | 58 | 0 | 0 | 0 | 417 | 537 | 0 | 2575 |

AM PEAK HOUR: 745-845



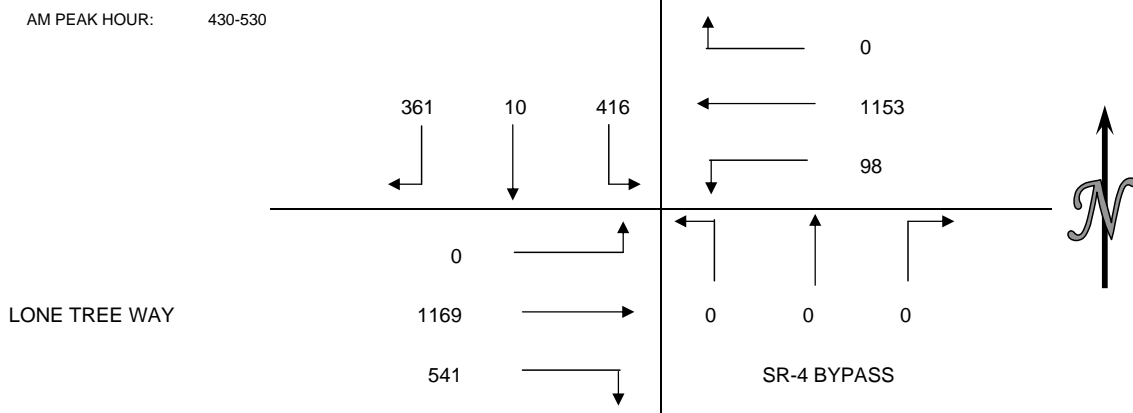
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 1 | 0 | 1 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 0 | 0 | 0 | 0 | 0 |
| 800-815 | 1 | 0 | 0 | 0 | 1 |
| 815-830 | 0 | 0 | 0 | 0 | 0 |
| 830-845 | 1 | 0 | 0 | 0 | 1 |
| 845-900 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 0 | 0 | 1 | 0 | 1 |
| 715-815 | 1 | 0 | 0 | 0 | 1 |
| 730-830 | 1 | 0 | 0 | 0 | 1 |
| 745-845 | 2 | 0 | 0 | 0 | 2 |
| 800-900 | 2 | 0 | 0 | 0 | 2 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 0 | 0 | 0 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 1 | 0 | 0 | 0 | 1 |
| 745-800 | 1 | 0 | 0 | 0 | 1 |
| 800-815 | 1 | 0 | 1 | 0 | 2 |
| 815-830 | 0 | 0 | 1 | 0 | 1 |
| 830-845 | 1 | 0 | 0 | 0 | 1 |
| 845-900 | 2 | 0 | 0 | 0 | 2 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 2 | 0 | 0 | 0 | 2 |
| 715-815 | 3 | 0 | 1 | 0 | 4 |
| 730-830 | 3 | 0 | 2 | 0 | 5 |
| 745-845 | 3 | 0 | 2 | 0 | 5 |
| 800-900 | 4 | 0 | 2 | 0 | 6 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S SR-4 BYPASS
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-415 | 84 | 2 | 80 | 0 | 322 | 35 | 0 | 0 | 0 | 129 | 285 | 0 | 937 |
| 415-430 | 83 | 3 | 125 | 0 | 280 | 35 | 0 | 0 | 0 | 141 | 266 | 0 | 933 |
| 430-445 | 88 | 0 | 109 | 0 | 300 | 33 | 0 | 0 | 0 | 111 | 245 | 0 | 886 |
| 445-500 | 84 | 4 | 102 | 0 | 260 | 18 | 0 | 0 | 0 | 156 | 306 | 0 | 930 |
| 500-515 | 97 | 3 | 122 | 0 | 289 | 22 | 0 | 0 | 0 | 125 | 287 | 0 | 945 |
| 515-530 | 92 | 3 | 83 | 0 | 304 | 25 | 0 | 0 | 0 | 149 | 331 | 0 | 987 |
| 530-545 | 97 | 3 | 93 | 0 | 261 | 35 | 0 | 0 | 0 | 102 | 293 | 0 | 884 |
| 545-600 | 88 | 1 | 113 | 0 | 330 | 31 | 0 | 0 | 0 | 91 | 270 | 0 | 924 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-500 | 339 | 9 | 416 | 0 | 1162 | 121 | 0 | 0 | 0 | 537 | 1102 | 0 | 3686 |
| 415-515 | 352 | 10 | 458 | 0 | 1129 | 108 | 0 | 0 | 0 | 533 | 1104 | 0 | 3694 |
| 430-530 | 361 | 10 | 416 | 0 | 1153 | 98 | 0 | 0 | 0 | 541 | 1169 | 0 | 3748 |
| 445-545 | 370 | 13 | 400 | 0 | 1114 | 100 | 0 | 0 | 0 | 532 | 1217 | 0 | 3746 |
| 500-600 | 374 | 10 | 411 | 0 | 1184 | 113 | 0 | 0 | 0 | 467 | 1181 | 0 | 3740 |



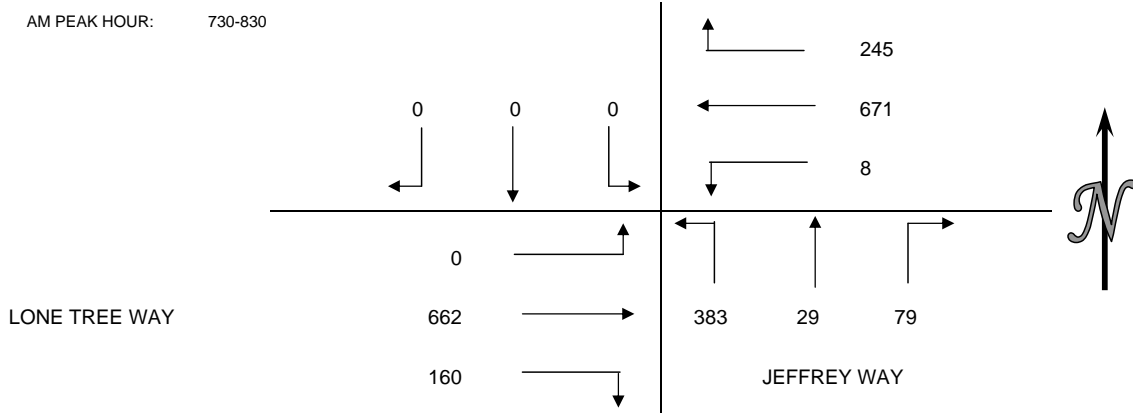
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 4 | 1 | 0 | 0 | 5 |
| 415-430 | 0 | 0 | 0 | 0 | 0 |
| 430-445 | 0 | 0 | 0 | 0 | 0 |
| 445-500 | 2 | 0 | 1 | 0 | 3 |
| 500-515 | 0 | 0 | 0 | 0 | 0 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 4 | 0 | 1 | 0 | 5 |
| 545-600 | 1 | 0 | 1 | 0 | 2 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 6 | 1 | 1 | 0 | 8 |
| 415-515 | 2 | 0 | 1 | 0 | 3 |
| 430-530 | 2 | 0 | 1 | 0 | 3 |
| 445-545 | 6 | 0 | 2 | 0 | 8 |
| 500-600 | 5 | 0 | 2 | 0 | 7 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 0 | 0 | 0 | 0 |
| 415-430 | 0 | 0 | 0 | 0 | 0 |
| 430-445 | 0 | 0 | 0 | 0 | 0 |
| 445-500 | 0 | 0 | 1 | 0 | 1 |
| 500-515 | 0 | 0 | 0 | 0 | 0 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 0 | 2 | 0 | 2 |
| 545-600 | 0 | 0 | 1 | 0 | 1 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 0 | 0 | 1 | 0 | 1 |
| 415-515 | 0 | 0 | 1 | 0 | 1 |
| 430-530 | 0 | 0 | 1 | 0 | 1 |
| 445-545 | 0 | 0 | 3 | 0 | 3 |
| 500-600 | 0 | 0 | 3 | 0 | 3 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: TUESDAY MAY 13, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S JEFFREY WAY
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-715 | 0 | 0 | 0 | 63 | 134 | 4 | 9 | 5 | 64 | 29 | 92 | 0 | 400 |
| 715-730 | 0 | 0 | 0 | 55 | 146 | 1 | 12 | 7 | 84 | 40 | 118 | 0 | 463 |
| 730-745 | 0 | 0 | 0 | 62 | 184 | 2 | 12 | 9 | 94 | 61 | 141 | 0 | 565 |
| 745-800 | 0 | 0 | 0 | 67 | 159 | 2 | 27 | 6 | 97 | 39 | 183 | 0 | 580 |
| 800-815 | 0 | 0 | 0 | 72 | 183 | 2 | 21 | 10 | 107 | 39 | 191 | 0 | 625 |
| 815-830 | 0 | 0 | 0 | 44 | 145 | 2 | 19 | 4 | 85 | 21 | 147 | 0 | 467 |
| 830-845 | 0 | 0 | 0 | 33 | 132 | 2 | 11 | 1 | 69 | 23 | 138 | 0 | 409 |
| 845-900 | 0 | 0 | 0 | 53 | 128 | 2 | 11 | 7 | 89 | 32 | 141 | 0 | 463 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-800 | 0 | 0 | 0 | 247 | 623 | 9 | 60 | 27 | 339 | 169 | 534 | 0 | 2008 |
| 715-815 | 0 | 0 | 0 | 256 | 672 | 7 | 72 | 32 | 382 | 179 | 633 | 0 | 2233 |
| 730-830 | 0 | 0 | 0 | 245 | 671 | 8 | 79 | 29 | 383 | 160 | 662 | 0 | 2237 |
| 745-845 | 0 | 0 | 0 | 216 | 619 | 8 | 78 | 21 | 358 | 122 | 659 | 0 | 2081 |
| 800-900 | 0 | 0 | 0 | 202 | 588 | 8 | 62 | 22 | 350 | 115 | 617 | 0 | 1964 |



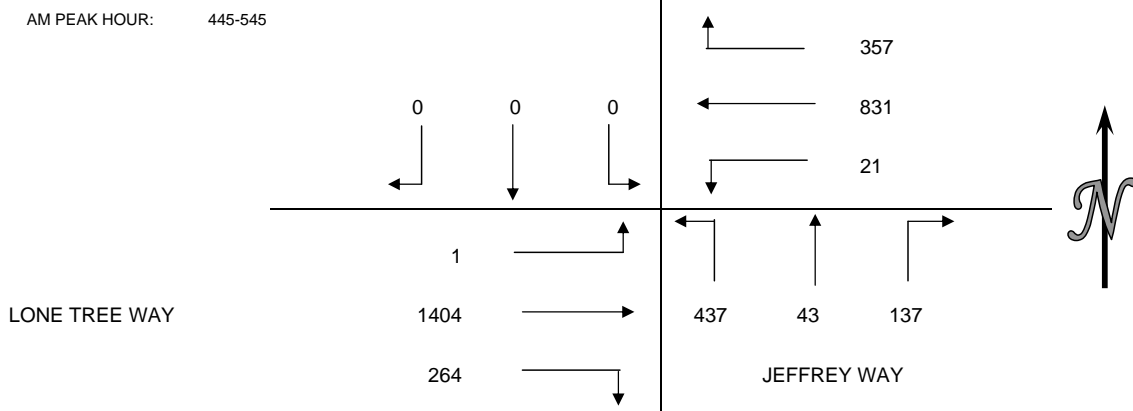
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 0 | 0 | 0 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 0 | 0 | 0 | 0 | 0 |
| 800-815 | 0 | 0 | 0 | 0 | 0 |
| 815-830 | 1 | 0 | 0 | 0 | 1 |
| 830-845 | 1 | 0 | 0 | 0 | 1 |
| 845-900 | 0 | 1 | 0 | 0 | 1 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 0 | 0 | 0 | 0 | 0 |
| 715-815 | 0 | 0 | 0 | 0 | 0 |
| 730-830 | 1 | 0 | 0 | 0 | 1 |
| 745-845 | 2 | 0 | 0 | 0 | 2 |
| 800-900 | 2 | 1 | 0 | 0 | 3 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 1 | 0 | 1 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 1 | 0 | 0 | 0 | 1 |
| 745-800 | 1 | 0 | 0 | 0 | 1 |
| 800-815 | 1 | 0 | 1 | 0 | 2 |
| 815-830 | 1 | 0 | 1 | 0 | 2 |
| 830-845 | 0 | 0 | 0 | 0 | 0 |
| 845-900 | 3 | 0 | 1 | 0 | 4 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 2 | 0 | 1 | 0 | 3 |
| 715-815 | 3 | 0 | 1 | 0 | 4 |
| 730-830 | 4 | 0 | 2 | 0 | 6 |
| 745-845 | 3 | 0 | 2 | 0 | 5 |
| 800-900 | 5 | 0 | 3 | 0 | 8 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: TUESDAY MAY 13, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S JEFFREY WAY
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-415 | 0 | 0 | 0 | 66 | 215 | 4 | 24 | 6 | 125 | 63 | 359 | 0 | 862 |
| 415-430 | 0 | 0 | 0 | 85 | 226 | 9 | 21 | 10 | 116 | 63 | 355 | 1 | 886 |
| 430-445 | 0 | 0 | 0 | 70 | 207 | 9 | 20 | 9 | 87 | 71 | 307 | 0 | 780 |
| 445-500 | 0 | 0 | 0 | 78 | 199 | 6 | 36 | 15 | 104 | 72 | 331 | 0 | 841 |
| 500-515 | 0 | 0 | 0 | 100 | 236 | 3 | 45 | 10 | 135 | 61 | 368 | 0 | 958 |
| 515-530 | 0 | 0 | 0 | 79 | 191 | 8 | 25 | 8 | 96 | 58 | 336 | 1 | 802 |
| 530-545 | 0 | 0 | 0 | 100 | 205 | 4 | 31 | 10 | 102 | 73 | 369 | 0 | 894 |
| 545-600 | 0 | 0 | 0 | 95 | 183 | 6 | 35 | 8 | 108 | 51 | 350 | 0 | 836 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-500 | 0 | 0 | 0 | 299 | 847 | 28 | 101 | 40 | 432 | 269 | 1352 | 1 | 3369 |
| 415-515 | 0 | 0 | 0 | 333 | 868 | 27 | 122 | 44 | 442 | 267 | 1361 | 1 | 3465 |
| 430-530 | 0 | 0 | 0 | 327 | 833 | 26 | 126 | 42 | 422 | 262 | 1342 | 1 | 3381 |
| 445-545 | 0 | 0 | 0 | 357 | 831 | 21 | 137 | 43 | 437 | 264 | 1404 | 1 | 3495 |
| 500-600 | 0 | 0 | 0 | 374 | 815 | 21 | 136 | 36 | 441 | 243 | 1423 | 1 | 3490 |



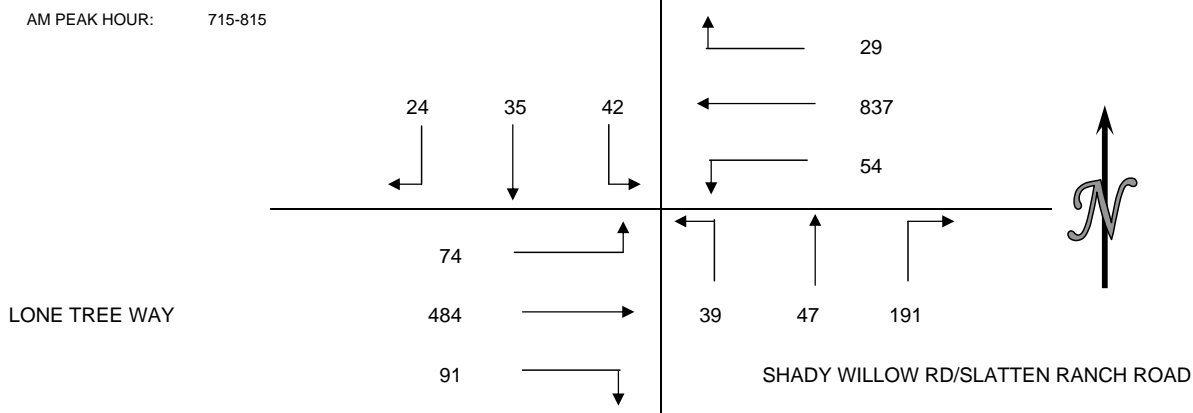
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 3 | 0 | 0 | 0 | 3 |
| 415-430 | 1 | 0 | 0 | 0 | 1 |
| 430-445 | 0 | 0 | 1 | 0 | 1 |
| 445-500 | 1 | 1 | 0 | 0 | 2 |
| 500-515 | 1 | 0 | 0 | 0 | 1 |
| 515-530 | 0 | 0 | 1 | 0 | 1 |
| 530-545 | 0 | 0 | 1 | 0 | 1 |
| 545-600 | 5 | 0 | 0 | 0 | 5 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 5 | 1 | 1 | 0 | 7 |
| 415-515 | 3 | 1 | 1 | 0 | 5 |
| 430-530 | 2 | 1 | 2 | 0 | 5 |
| 445-545 | 2 | 1 | 2 | 0 | 5 |
| 500-600 | 6 | 0 | 2 | 0 | 8 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 0 | 0 | 0 | 0 |
| 415-430 | 0 | 0 | 0 | 0 | 0 |
| 430-445 | 1 | 0 | 0 | 0 | 1 |
| 445-500 | 0 | 0 | 3 | 0 | 3 |
| 500-515 | 0 | 0 | 0 | 0 | 0 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 0 | 0 | 0 | 0 |
| 545-600 | 0 | 0 | 1 | 0 | 1 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 1 | 0 | 3 | 0 | 4 |
| 415-515 | 1 | 0 | 3 | 0 | 4 |
| 430-530 | 1 | 0 | 3 | 0 | 4 |
| 445-545 | 0 | 0 | 3 | 0 | 3 |
| 500-600 | 0 | 0 | 1 | 0 | 1 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 22, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S SHADY WILLOW RD/SLATTEN RANCH ROAD
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-715 | 9 | 5 | 11 | 3 | 200 | 3 | 34 | 5 | 15 | 14 | 90 | 7 | 396 |
| 715-730 | 8 | 3 | 13 | 4 | 194 | 16 | 52 | 13 | 12 | 35 | 133 | 19 | 502 |
| 730-745 | 4 | 8 | 6 | 5 | 199 | 14 | 49 | 10 | 19 | 27 | 111 | 25 | 477 |
| 745-800 | 7 | 14 | 13 | 10 | 231 | 9 | 62 | 17 | 3 | 17 | 137 | 19 | 539 |
| 800-815 | 5 | 10 | 10 | 10 | 213 | 15 | 28 | 7 | 5 | 12 | 103 | 11 | 429 |
| 815-830 | 11 | 5 | 13 | 5 | 167 | 10 | 30 | 5 | 8 | 18 | 122 | 19 | 413 |
| 830-845 | 7 | 3 | 13 | 6 | 158 | 14 | 27 | 16 | 5 | 12 | 95 | 24 | 380 |
| 845-900 | 14 | 3 | 12 | 8 | 207 | 9 | 25 | 11 | 4 | 13 | 106 | 36 | 448 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-800 | 28 | 30 | 43 | 22 | 824 | 42 | 197 | 45 | 49 | 93 | 471 | 70 | 1914 |
| 715-815 | 24 | 35 | 42 | 29 | 837 | 54 | 191 | 47 | 39 | 91 | 484 | 74 | 1947 |
| 730-830 | 27 | 37 | 42 | 30 | 810 | 48 | 169 | 39 | 35 | 74 | 473 | 74 | 1858 |
| 745-845 | 30 | 32 | 49 | 31 | 769 | 48 | 147 | 45 | 21 | 59 | 457 | 73 | 1761 |
| 800-900 | 37 | 21 | 48 | 29 | 745 | 48 | 110 | 39 | 22 | 55 | 426 | 90 | 1670 |



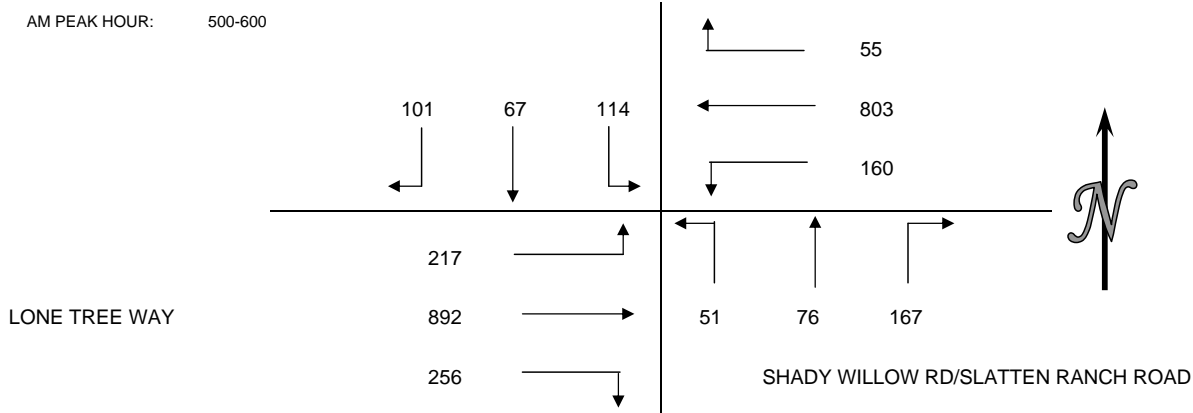
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 0 | 0 | 0 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 0 | 2 | 2 | 0 | 4 |
| 800-815 | 2 | 0 | 0 | 2 | 4 |
| 815-830 | 0 | 0 | 1 | 0 | 1 |
| 830-845 | 0 | 0 | 0 | 0 | 0 |
| 845-900 | 0 | 0 | 1 | 1 | 2 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 0 | 2 | 2 | 0 | 4 |
| 715-815 | 2 | 2 | 2 | 2 | 8 |
| 730-830 | 2 | 2 | 3 | 2 | 9 |
| 745-845 | 2 | 2 | 3 | 2 | 9 |
| 800-900 | 2 | 0 | 2 | 3 | 7 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 1 | 0 | 0 | 0 | 1 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 1 | 0 | 1 |
| 745-800 | 0 | 0 | 0 | 0 | 0 |
| 800-815 | 0 | 0 | 0 | 1 | 1 |
| 815-830 | 0 | 0 | 0 | 0 | 0 |
| 830-845 | 0 | 0 | 2 | 0 | 2 |
| 845-900 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 1 | 0 | 1 | 0 | 2 |
| 715-815 | 0 | 0 | 1 | 1 | 2 |
| 730-830 | 0 | 0 | 1 | 1 | 2 |
| 745-845 | 0 | 0 | 2 | 1 | 3 |
| 800-900 | 0 | 0 | 2 | 1 | 3 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 22, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S SHADY WILLOW RD/SLATTEN RANCH ROAD
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-415 | 34 | 22 | 39 | 3 | 229 | 8 | 36 | 16 | 10 | 71 | 226 | 35 | 729 |
| 415-430 | 21 | 19 | 32 | 6 | 215 | 26 | 41 | 13 | 10 | 48 | 213 | 25 | 669 |
| 430-445 | 28 | 19 | 30 | 6 | 199 | 22 | 38 | 14 | 13 | 38 | 215 | 32 | 654 |
| 445-500 | 32 | 12 | 27 | 4 | 235 | 31 | 46 | 23 | 18 | 63 | 213 | 39 | 743 |
| 500-515 | 26 | 19 | 17 | 5 | 206 | 32 | 44 | 20 | 12 | 80 | 226 | 41 | 728 |
| 515-530 | 29 | 11 | 29 | 15 | 187 | 25 | 46 | 17 | 10 | 55 | 195 | 50 | 669 |
| 530-545 | 27 | 20 | 30 | 15 | 207 | 41 | 44 | 16 | 10 | 60 | 236 | 70 | 776 |
| 545-600 | 19 | 17 | 38 | 20 | 203 | 62 | 33 | 23 | 19 | 61 | 235 | 56 | 786 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-500 | 115 | 72 | 128 | 19 | 878 | 87 | 161 | 66 | 51 | 220 | 867 | 131 | 2795 |
| 415-515 | 107 | 69 | 106 | 21 | 855 | 111 | 169 | 70 | 53 | 229 | 867 | 137 | 2794 |
| 430-530 | 115 | 61 | 103 | 30 | 827 | 110 | 174 | 74 | 53 | 236 | 849 | 162 | 2794 |
| 445-545 | 114 | 62 | 103 | 39 | 835 | 129 | 180 | 76 | 50 | 258 | 870 | 200 | 2916 |
| 500-600 | 101 | 67 | 114 | 55 | 803 | 160 | 167 | 76 | 51 | 256 | 892 | 217 | 2959 |



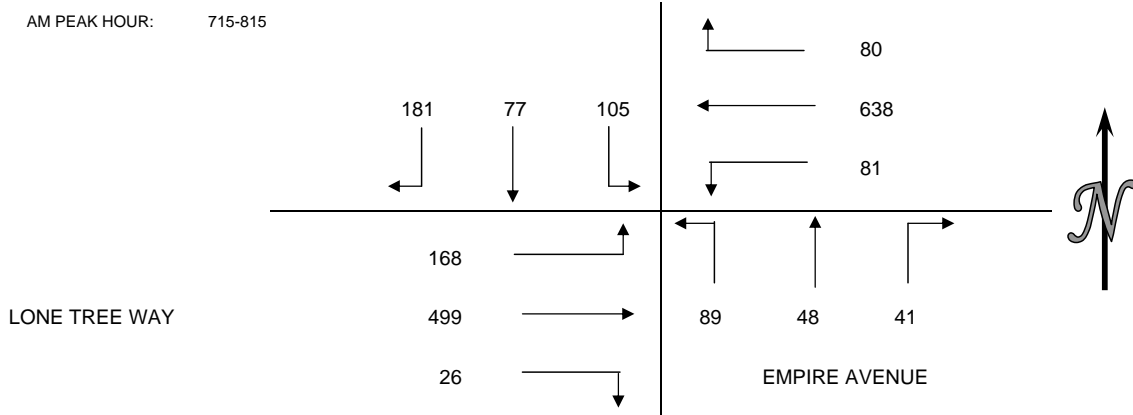
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 0 | 1 | 0 | 1 |
| 415-430 | 0 | 1 | 0 | 0 | 1 |
| 430-445 | 0 | 1 | 3 | 0 | 4 |
| 445-500 | 0 | 1 | 0 | 0 | 1 |
| 500-515 | 0 | 6 | 6 | 3 | 15 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 0 | 1 | 0 | 1 |
| 545-600 | 2 | 5 | 0 | 0 | 7 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 0 | 3 | 4 | 0 | 7 |
| 415-515 | 0 | 9 | 9 | 3 | 21 |
| 430-530 | 0 | 8 | 9 | 3 | 20 |
| 445-545 | 0 | 7 | 7 | 3 | 17 |
| 500-600 | 2 | 11 | 7 | 3 | 23 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 2 | 0 | 0 | 0 | 2 |
| 415-430 | 0 | 1 | 0 | 0 | 1 |
| 430-445 | 0 | 0 | 1 | 0 | 1 |
| 445-500 | 1 | 1 | 0 | 1 | 3 |
| 500-515 | 0 | 0 | 0 | 0 | 0 |
| 515-530 | 0 | 1 | 0 | 1 | 2 |
| 530-545 | 0 | 1 | 0 | 1 | 2 |
| 545-600 | 0 | 0 | 2 | 0 | 2 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 3 | 2 | 1 | 1 | 7 |
| 415-515 | 1 | 2 | 1 | 1 | 5 |
| 430-530 | 1 | 2 | 1 | 2 | 6 |
| 445-545 | 1 | 3 | 0 | 3 | 7 |
| 500-600 | 0 | 2 | 2 | 2 | 6 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 22, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S EMPIRE AVENUE
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-715 | 29 | 16 | 27 | 21 | 128 | 17 | 8 | 8 | 18 | 6 | 102 | 38 | 418 |
| 715-730 | 36 | 21 | 33 | 28 | 168 | 28 | 12 | 16 | 31 | 6 | 123 | 63 | 565 |
| 730-745 | 46 | 19 | 30 | 21 | 149 | 23 | 13 | 13 | 23 | 11 | 145 | 36 | 529 |
| 745-800 | 50 | 18 | 13 | 17 | 168 | 19 | 14 | 14 | 19 | 6 | 125 | 31 | 494 |
| 800-815 | 49 | 19 | 29 | 14 | 153 | 11 | 2 | 5 | 16 | 3 | 106 | 38 | 445 |
| 815-830 | 42 | 15 | 24 | 19 | 139 | 15 | 3 | 12 | 18 | 10 | 120 | 41 | 458 |
| 830-845 | 31 | 27 | 30 | 10 | 122 | 15 | 5 | 9 | 19 | 18 | 112 | 41 | 439 |
| 845-900 | 42 | 23 | 26 | 14 | 134 | 15 | 3 | 4 | 15 | 10 | 99 | 31 | 416 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-800 | 161 | 74 | 103 | 87 | 613 | 87 | 47 | 51 | 91 | 29 | 495 | 168 | 2006 |
| 715-815 | 181 | 77 | 105 | 80 | 638 | 81 | 41 | 48 | 89 | 26 | 499 | 168 | 2033 |
| 730-830 | 187 | 71 | 96 | 71 | 609 | 68 | 32 | 44 | 76 | 30 | 496 | 146 | 1926 |
| 745-845 | 172 | 79 | 96 | 60 | 582 | 60 | 24 | 40 | 72 | 37 | 463 | 151 | 1836 |
| 800-900 | 164 | 84 | 109 | 57 | 548 | 56 | 13 | 30 | 68 | 41 | 437 | 151 | 1758 |



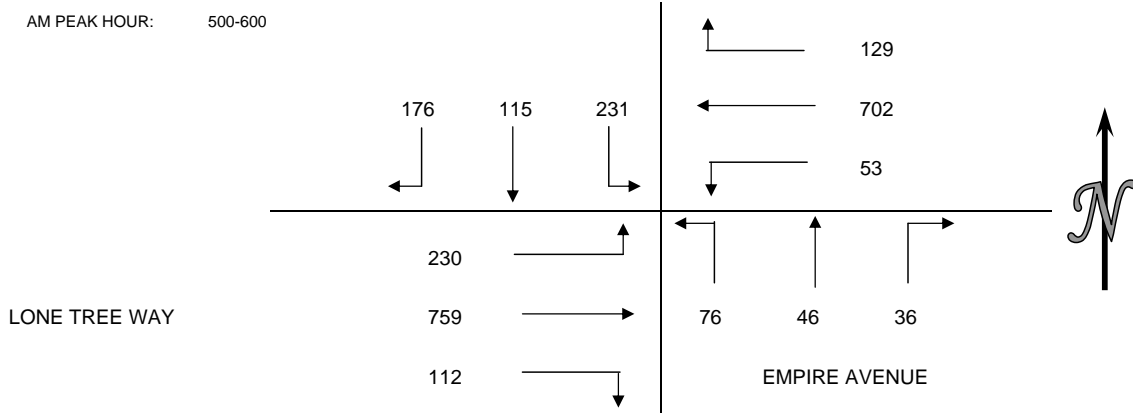
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 1 | 0 | 2 | 0 | 3 |
| 715-730 | 1 | 1 | 1 | 0 | 3 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 0 | 0 | 0 | 0 | 0 |
| 800-815 | 3 | 0 | 2 | 0 | 5 |
| 815-830 | 0 | 0 | 5 | 4 | 9 |
| 830-845 | 0 | 0 | 7 | 3 | 10 |
| 845-900 | 0 | 0 | 0 | 2 | 2 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 2 | 1 | 3 | 0 | 6 |
| 715-815 | 4 | 1 | 3 | 0 | 8 |
| 730-830 | 3 | 0 | 3 | 4 | 7 |
| 745-845 | 3 | 0 | 4 | 7 | 14 |
| 800-900 | 3 | 0 | 4 | 9 | 16 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 1 | 0 | 0 | 0 | 1 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 0 | 0 | 0 | 0 | 0 |
| 800-815 | 2 | 0 | 0 | 0 | 2 |
| 815-830 | 0 | 0 | 0 | 0 | 0 |
| 830-845 | 0 | 0 | 1 | 1 | 2 |
| 845-900 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 1 | 0 | 0 | 0 | 1 |
| 715-815 | 2 | 0 | 0 | 0 | 2 |
| 730-830 | 2 | 0 | 0 | 0 | 2 |
| 745-845 | 2 | 0 | 1 | 1 | 4 |
| 800-900 | 2 | 0 | 1 | 1 | 4 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 22, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S EMPIRE AVENUE
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-415 | 37 | 29 | 44 | 31 | 152 | 20 | 6 | 14 | 18 | 20 | 212 | 78 | 661 |
| 415-430 | 45 | 34 | 62 | 32 | 134 | 16 | 8 | 10 | 18 | 17 | 198 | 63 | 637 |
| 430-445 | 53 | 30 | 71 | 21 | 180 | 21 | 6 | 6 | 14 | 24 | 173 | 63 | 662 |
| 445-500 | 46 | 26 | 43 | 28 | 169 | 21 | 4 | 14 | 26 | 24 | 197 | 63 | 661 |
| 500-515 | 44 | 27 | 57 | 36 | 179 | 15 | 9 | 17 | 22 | 26 | 172 | 75 | 679 |
| 515-530 | 34 | 33 | 63 | 34 | 177 | 11 | 5 | 6 | 17 | 26 | 180 | 50 | 636 |
| 530-545 | 53 | 28 | 57 | 21 | 179 | 14 | 12 | 11 | 18 | 29 | 212 | 45 | 679 |
| 545-600 | 45 | 27 | 54 | 38 | 167 | 13 | 10 | 12 | 19 | 31 | 195 | 60 | 671 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-500 | 181 | 119 | 220 | 112 | 635 | 78 | 24 | 44 | 76 | 85 | 780 | 267 | 2621 |
| 415-515 | 188 | 117 | 233 | 117 | 662 | 73 | 27 | 47 | 80 | 91 | 740 | 264 | 2639 |
| 430-530 | 177 | 116 | 234 | 119 | 705 | 68 | 24 | 43 | 79 | 100 | 722 | 251 | 2638 |
| 445-545 | 177 | 114 | 220 | 119 | 704 | 61 | 30 | 48 | 83 | 105 | 761 | 233 | 2655 |
| 500-600 | 176 | 115 | 231 | 129 | 702 | 53 | 36 | 46 | 76 | 112 | 759 | 230 | 2665 |



| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 0 | 0 | 0 | 0 |
| 415-430 | 1 | 1 | 0 | 0 | 2 |
| 430-445 | 0 | 1 | 0 | 4 | 5 |
| 445-500 | 0 | 4 | 0 | 0 | 4 |
| 500-515 | 0 | 1 | 0 | 0 | 1 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 1 | 0 | 0 | 1 |
| 545-600 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 1 | 6 | 0 | 4 | 11 |
| 415-515 | 1 | 7 | 0 | 4 | 12 |
| 430-530 | 0 | 6 | 0 | 4 | 10 |
| 445-545 | 0 | 6 | 0 | 0 | 6 |
| 500-600 | 0 | 2 | 0 | 0 | 2 |


| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 2 | 0 | 0 | 2 |
| 415-430 | 0 | 1 | 0 | 0 | 1 |
| 430-445 | 0 | 3 | 0 | 0 | 3 |
| 445-500 | 0 | 0 | 0 | 1 | 1 |
| 500-515 | 0 | 0 | 0 | 0 | 0 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 0 | 0 | 0 | 0 |
| 545-600 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 0 | 6 | 0 | 1 | 7 |
| 415-515 | 0 | 4 | 0 | 1 | 5 |
| 430-530 | 0 | 3 | 0 | 1 | 4 |
| 445-545 | 0 | 0 | 0 | 1 | 1 |
| 500-600 | 0 | 0 | 0 | 0 | 0 |

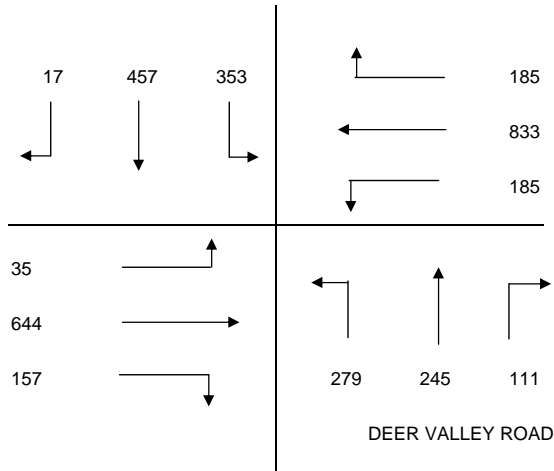
INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S DEER VALLEY ROAD
 E/W LONE TREE WAY

| 15 MIN COUNTS PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTALS |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|
| 700-715 | 5 | 54 | 26 | 6 | 113 | 17 | 2 | 25 | 48 | 25 | 62 | 1 | 384 |
| 715-730 | 1 | 90 | 42 | 12 | 140 | 30 | 4 | 36 | 52 | 42 | 88 | 4 | 541 |
| 730-745 | 9 | 94 | 70 | 25 | 192 | 27 | 17 | 55 | 55 | 32 | 116 | 5 | 697 |
| 745-800 | 4 | 122 | 107 | 51 | 226 | 42 | 37 | 61 | 79 | 52 | 195 | 12 | 988 |
| 800-815 | 3 | 129 | 83 | 46 | 230 | 46 | 19 | 81 | 73 | 29 | 124 | 9 | 872 |
| 815-830 | 4 | 112 | 75 | 36 | 195 | 49 | 26 | 61 | 57 | 29 | 146 | 9 | 799 |
| 830-845 | 6 | 94 | 88 | 52 | 182 | 48 | 29 | 42 | 70 | 47 | 179 | 5 | 842 |
| 845-900 | 2 | 78 | 104 | 68 | 158 | 54 | 42 | 68 | 64 | 35 | 160 | 17 | 850 |
| HOUR TOTALS | | | | | | | | | | | | | |
| 700-800 | 19 | 360 | 245 | 94 | 671 | 116 | 60 | 177 | 234 | 151 | 461 | 22 | 2610 |
| 715-815 | 17 | 435 | 302 | 134 | 788 | 145 | 77 | 233 | 259 | 155 | 523 | 30 | 3098 |
| 730-830 | 20 | 457 | 335 | 158 | 843 | 164 | 99 | 258 | 264 | 142 | 581 | 35 | 3356 |
| 745-845 | 17 | 457 | 353 | 185 | 833 | 185 | 111 | 245 | 279 | 157 | 644 | 35 | 3501 |
| 800-900 | 15 | 413 | 350 | 202 | 765 | 197 | 116 | 252 | 264 | 140 | 609 | 40 | 3363 |

AM PEAK HOUR
745-845


LONE TREE WAY



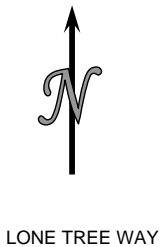
| PEDESTRIAN COUNTS | | | | |
|-------------------|-----------|----------|-----------|----------|
| PERIOD | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG |
| 15 MIN COUNTS | | | | |
| 700-715 | 1 | 0 | 3 | 2 |
| 715-730 | 0 | 0 | 4 | 3 |
| 730-745 | 0 | 5 | 13 | 13 |
| 745-800 | 3 | 8 | 4 | 1 |
| 800-815 | 0 | 1 | 16 | 6 |
| 815-830 | 1 | 5 | 10 | 6 |
| 830-845 | 0 | 6 | 21 | 10 |
| 845-900 | 0 | 4 | 9 | 0 |
| HOUR TOTALS | | | | |
| 700-800 | 4 | 13 | 24 | 19 |
| 715-815 | 3 | 14 | 37 | 23 |
| 730-830 | 4 | 19 | 43 | 26 |
| 745-845 | 4 | 20 | 51 | 23 |
| 800-900 | 1 | 16 | 56 | 22 |

INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S DEER VALLEY ROAD
 E/W LONE TREE WAY

| 15 MIN COUNTS PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTALS |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|
| 400-415 | 3 | 52 | 35 | 44 | 118 | 33 | 40 | 93 | 76 | 50 | 224 | 18 | 786 |
| 415-430 | 3 | 43 | 31 | 36 | 122 | 25 | 34 | 81 | 34 | 38 | 203 | 24 | 674 |
| 430-445 | 7 | 39 | 47 | 50 | 113 | 35 | 45 | 97 | 58 | 33 | 211 | 10 | 745 |
| 445-500 | 5 | 44 | 42 | 38 | 108 | 24 | 26 | 82 | 45 | 36 | 203 | 14 | 667 |
| 500-515 | 6 | 46 | 27 | 36 | 117 | 43 | 44 | 105 | 48 | 31 | 188 | 16 | 707 |
| 515-530 | 2 | 56 | 38 | 43 | 122 | 39 | 42 | 91 | 46 | 45 | 200 | 28 | 752 |
| 530-545 | 3 | 48 | 60 | 37 | 118 | 35 | 42 | 97 | 57 | 28 | 196 | 28 | 749 |
| 545-600 | 3 | 41 | 43 | 38 | 140 | 34 | 40 | 63 | 41 | 43 | 196 | 15 | 697 |
| HOUR TOTALS | | | | | | | | | | | | | |
| 400-500 | 18 | 178 | 155 | 168 | 461 | 117 | 145 | 353 | 213 | 157 | 841 | 66 | 2872 |
| 415-515 | 21 | 172 | 147 | 160 | 460 | 127 | 149 | 365 | 185 | 138 | 805 | 64 | 2793 |
| 430-530 | 20 | 185 | 154 | 167 | 460 | 141 | 157 | 375 | 197 | 145 | 802 | 68 | 2871 |
| 445-545 | 16 | 194 | 167 | 154 | 465 | 141 | 154 | 375 | 196 | 140 | 787 | 86 | 2875 |
| 500-600 | 14 | 191 | 168 | 154 | 497 | 151 | 168 | 356 | 192 | 147 | 780 | 87 | 2905 |

PM PEAK HOUR
500-600

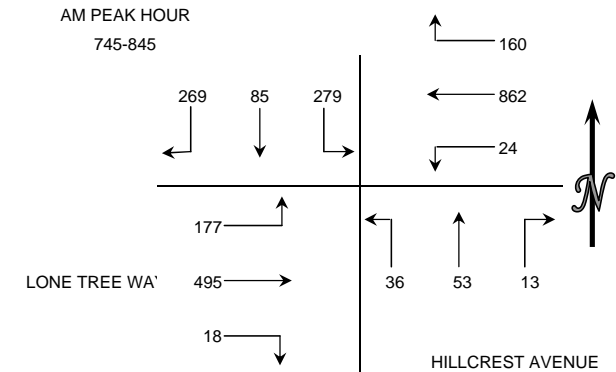


| PEDESTRIAN COUNTS | | | | |
|-------------------|-----------|----------|-----------|----------|
| PERIOD | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG |
| 15 MIN COUNTS | | | | |
| 400-415 | 0 | 9 | 2 | 2 |
| 415-430 | 8 | 2 | 2 | 1 |
| 430-445 | 0 | 0 | 2 | 0 |
| 445-500 | 0 | 0 | 0 | 2 |
| 500-515 | 0 | 0 | 8 | 0 |
| 515-530 | 2 | 3 | 3 | 0 |
| 530-545 | 0 | 0 | 1 | 0 |
| 545-600 | 0 | 0 | 1 | 1 |
| HOUR TOTALS | | | | |
| 400-500 | 8 | 11 | 6 | 5 |
| 415-515 | 8 | 2 | 12 | 3 |
| 430-530 | 2 | 3 | 13 | 2 |
| 445-545 | 2 | 3 | 12 | 2 |
| 500-600 | 2 | 3 | 13 | 1 |

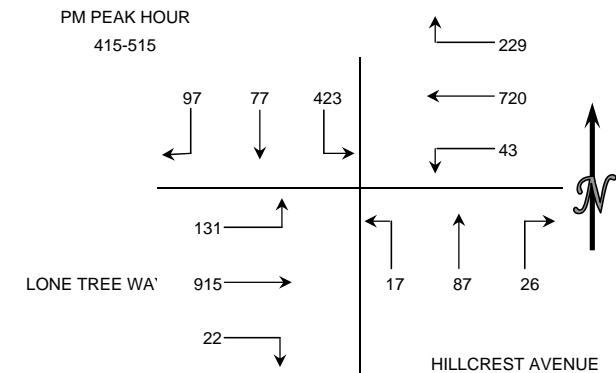
INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIODS: 7:00 AM TO 9:00 AM AND 4:00 PM TO 6:00 PM
 INTERSECTION: N/S HILLCREST AVENUE
 E/W LONE TREE WAY
 CITY: ANTIOCH

| 15 MIN COUNTS 7:00 AM TO 9:00 AM | | | | | | | | | | | | | |
|----------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|-------|
| PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTAL |
| 700-715 | 18 | 8 | 52 | 38 | 116 | 1 | 2 | 20 | 5 | 2 | 75 | 7 | 344 |
| 715-730 | 34 | 7 | 38 | 17 | 151 | 4 | 4 | 8 | 2 | 2 | 66 | 8 | 341 |
| 730-745 | 47 | 12 | 39 | 23 | 212 | 3 | 1 | 18 | 6 | 4 | 92 | 11 | 468 |
| 745-800 | 80 | 29 | 70 | 41 | 240 | 5 | 5 | 16 | 10 | 4 | 136 | 54 | 690 |
| 800-815 | 57 | 20 | 74 | 41 | 217 | 10 | 5 | 17 | 10 | 3 | 128 | 61 | 643 |
| 815-830 | 46 | 11 | 72 | 46 | 218 | 5 | 2 | 12 | 7 | 7 | 114 | 32 | 572 |
| 830-845 | 86 | 25 | 63 | 32 | 187 | 4 | 1 | 8 | 9 | 4 | 117 | 30 | 566 |
| 845-900 | 90 | 30 | 78 | 41 | 172 | 3 | 9 | 6 | 14 | 3 | 138 | 55 | 639 |
| HOUR TOTALS | | | | | | | | | | | | | |
| TIME | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTAL |
| 700-800 | 179 | 56 | 199 | 119 | 719 | 13 | 12 | 62 | 23 | 12 | 369 | 80 | 1843 |
| 715-815 | 218 | 68 | 221 | 122 | 820 | 22 | 15 | 59 | 28 | 13 | 422 | 134 | 2142 |
| 730-830 | 230 | 72 | 255 | 151 | 887 | 23 | 13 | 63 | 33 | 18 | 470 | 158 | 2373 |
| 745-845 | 269 | 85 | 279 | 160 | 862 | 24 | 13 | 53 | 36 | 18 | 495 | 177 | 2471 |
| 800-900 | 279 | 86 | 287 | 160 | 794 | 22 | 17 | 43 | 40 | 17 | 497 | 178 | 2420 |



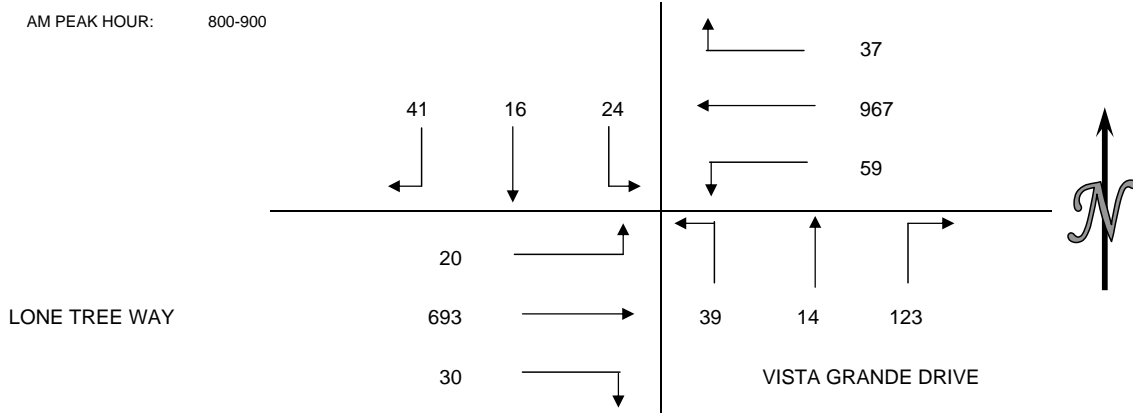
| 15 MIN COUNTS 4:00 PM TO 6:00 PM | | | | | | | | | | | | | |
|----------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|-------|
| PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTAL |
| 400-415 | 15 | 16 | 99 | 51 | 172 | 9 | 6 | 13 | 7 | 11 | 238 | 37 | 674 |
| 415-430 | 9 | 21 | 79 | 57 | 179 | 10 | 8 | 31 | 7 | 8 | 203 | 23 | 635 |
| 430-445 | 37 | 21 | 105 | 47 | 179 | 6 | 10 | 17 | 5 | 5 | 247 | 45 | 724 |
| 445-500 | 19 | 12 | 112 | 54 | 161 | 8 | 3 | 17 | 2 | 6 | 211 | 34 | 639 |
| 500-515 | 32 | 23 | 127 | 71 | 201 | 19 | 5 | 22 | 3 | 3 | 254 | 29 | 789 |
| 515-530 | 14 | 15 | 91 | 38 | 138 | 11 | 1 | 19 | 4 | 3 | 209 | 24 | 567 |
| 530-545 | 16 | 28 | 95 | 51 | 144 | 12 | 9 | 25 | 11 | 7 | 231 | 26 | 655 |
| 545-600 | 22 | 27 | 74 | 52 | 193 | 12 | 6 | 21 | 4 | 13 | 193 | 37 | 654 |
| HOUR TOTALS | | | | | | | | | | | | | |
| TIME | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTAL |
| 400-500 | 80 | 70 | 395 | 209 | 691 | 33 | 27 | 78 | 21 | 30 | 899 | 139 | 2672 |
| 415-515 | 97 | 77 | 423 | 229 | 720 | 43 | 26 | 87 | 17 | 22 | 915 | 131 | 2787 |
| 430-530 | 102 | 71 | 435 | 210 | 679 | 44 | 19 | 75 | 14 | 17 | 921 | 132 | 2719 |
| 445-545 | 81 | 78 | 425 | 214 | 644 | 50 | 18 | 83 | 20 | 19 | 905 | 113 | 2650 |
| 500-600 | 84 | 93 | 387 | 212 | 676 | 54 | 21 | 87 | 22 | 26 | 887 | 116 | 2665 |



INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S VISTA GRANDE DRIVE
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-715 | 5 | 1 | 3 | 1 | 127 | 3 | 15 | 2 | 11 | 1 | 85 | 2 | 256 |
| 715-730 | 11 | 1 | 0 | 1 | 156 | 11 | 25 | 4 | 10 | 3 | 115 | 3 | 340 |
| 730-745 | 13 | 4 | 5 | 5 | 235 | 11 | 31 | 4 | 11 | 2 | 148 | 9 | 478 |
| 745-800 | 23 | 1 | 8 | 3 | 255 | 11 | 34 | 5 | 17 | 4 | 179 | 1 | 541 |
| 800-815 | 20 | 8 | 15 | 5 | 230 | 11 | 30 | 6 | 14 | 8 | 154 | 5 | 506 |
| 815-830 | 7 | 5 | 2 | 9 | 237 | 14 | 28 | 2 | 11 | 4 | 156 | 2 | 477 |
| 830-845 | 5 | 3 | 2 | 11 | 251 | 11 | 30 | 3 | 11 | 10 | 183 | 6 | 526 |
| 845-900 | 9 | 0 | 5 | 12 | 249 | 23 | 35 | 3 | 3 | 8 | 200 | 7 | 554 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 700-800 | 52 | 7 | 16 | 10 | 773 | 36 | 105 | 15 | 49 | 10 | 527 | 15 | 1615 |
| 715-815 | 67 | 14 | 28 | 14 | 876 | 44 | 120 | 19 | 52 | 17 | 596 | 18 | 1865 |
| 730-830 | 63 | 18 | 30 | 22 | 957 | 47 | 123 | 17 | 53 | 18 | 637 | 17 | 2002 |
| 745-845 | 55 | 17 | 27 | 28 | 973 | 47 | 122 | 16 | 53 | 26 | 672 | 14 | 2050 |
| 800-900 | 41 | 16 | 24 | 37 | 967 | 59 | 123 | 14 | 39 | 30 | 693 | 20 | 2063 |



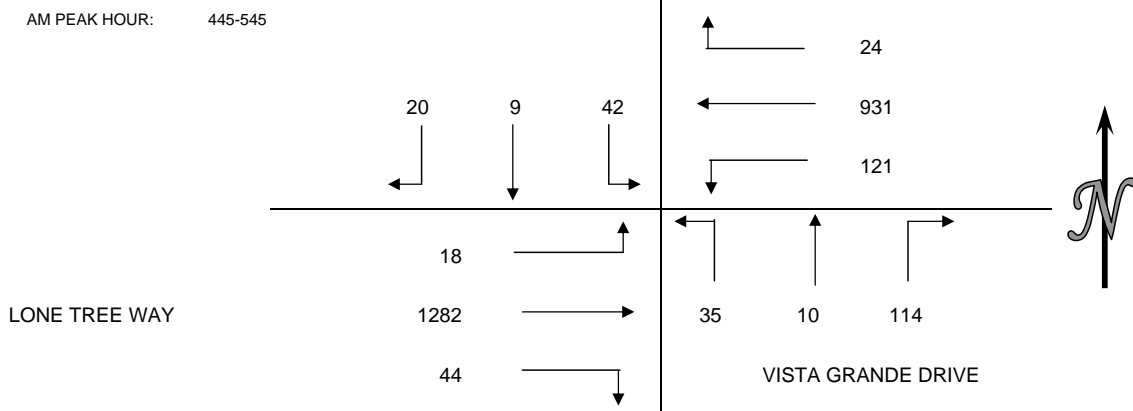
| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 0 | 1 | 1 |
| 715-730 | 2 | 0 | 0 | 0 | 2 |
| 730-745 | 1 | 1 | 2 | 1 | 5 |
| 745-800 | 0 | 0 | 0 | 1 | 1 |
| 800-815 | 0 | 0 | 0 | 0 | 0 |
| 815-830 | 0 | 0 | 0 | 0 | 0 |
| 830-845 | 0 | 0 | 0 | 0 | 0 |
| 845-900 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 3 | 1 | 2 | 3 | 9 |
| 715-815 | 3 | 1 | 2 | 2 | 8 |
| 730-830 | 1 | 1 | 2 | 2 | 6 |
| 745-845 | 0 | 0 | 0 | 1 | 1 |
| 800-900 | 0 | 0 | 0 | 0 | 0 |

| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-715 | 0 | 0 | 1 | 0 | 1 |
| 715-730 | 0 | 0 | 0 | 0 | 0 |
| 730-745 | 0 | 0 | 0 | 0 | 0 |
| 745-800 | 1 | 0 | 0 | 0 | 1 |
| 800-815 | 1 | 0 | 1 | 1 | 3 |
| 815-830 | 0 | 0 | 1 | 0 | 1 |
| 830-845 | 1 | 0 | 1 | 1 | 3 |
| 845-900 | 1 | 0 | 0 | 0 | 1 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 700-800 | 1 | 0 | 1 | 0 | 2 |
| 715-815 | 2 | 0 | 1 | 1 | 4 |
| 730-830 | 2 | 0 | 2 | 1 | 5 |
| 745-845 | 3 | 0 | 3 | 2 | 8 |
| 800-900 | 3 | 0 | 3 | 2 | 8 |

INTERSECTION CAR/PED/BIKE TRAFFIC COUNT RESULTS SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S VISTA GRANDE DRIVE
 E/W LONE TREE WAY
 CITY: ANTIOCH

| VEHICLE COUNTS | | | | | | | | | | | | | |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| 15 MIN COUNTS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-415 | 6 | 2 | 4 | 7 | 218 | 33 | 29 | 4 | 8 | 19 | 309 | 10 | 649 |
| 415-430 | 4 | 1 | 8 | 8 | 183 | 29 | 34 | 4 | 10 | 11 | 296 | 5 | 593 |
| 430-445 | 3 | 1 | 7 | 7 | 198 | 21 | 29 | 3 | 10 | 10 | 329 | 9 | 627 |
| 445-500 | 6 | 0 | 11 | 8 | 229 | 28 | 27 | 2 | 12 | 10 | 312 | 5 | 650 |
| 500-515 | 6 | 3 | 15 | 6 | 250 | 29 | 31 | 2 | 10 | 15 | 315 | 3 | 685 |
| 515-530 | 2 | 2 | 8 | 7 | 247 | 31 | 24 | 2 | 7 | 9 | 327 | 5 | 671 |
| 530-545 | 6 | 4 | 8 | 3 | 205 | 33 | 32 | 4 | 6 | 10 | 328 | 5 | 644 |
| 545-600 | 8 | 2 | 6 | 5 | 232 | 29 | 33 | 6 | 11 | 6 | 267 | 9 | 614 |
| HOUR TOTALS | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| PERIOD | SBRT | SBTH | SBLT | WBRT | WBTH | WBLT | NBRT | NBTH | NBLT | EBRT | EBTH | EBLT | TOTAL |
| 400-500 | 19 | 4 | 30 | 30 | 828 | 111 | 119 | 13 | 40 | 50 | 1246 | 29 | 2519 |
| 415-515 | 19 | 5 | 41 | 29 | 860 | 107 | 121 | 11 | 42 | 46 | 1252 | 22 | 2555 |
| 430-530 | 17 | 6 | 41 | 28 | 924 | 109 | 111 | 9 | 39 | 44 | 1283 | 22 | 2633 |
| 445-545 | 20 | 9 | 42 | 24 | 931 | 121 | 114 | 10 | 35 | 44 | 1282 | 18 | 2650 |
| 500-600 | 22 | 11 | 37 | 21 | 934 | 122 | 120 | 14 | 34 | 40 | 1237 | 22 | 2614 |



| PEDESTRIAN COUNTS | | | | | |
|-------------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 2 | 0 | 0 | 2 |
| 415-430 | 0 | 1 | 0 | 0 | 1 |
| 430-445 | 0 | 1 | 2 | 1 | 4 |
| 445-500 | 0 | 1 | 2 | 0 | 3 |
| 500-515 | 2 | 0 | 0 | 0 | 2 |
| 515-530 | 0 | 0 | 0 | 0 | 0 |
| 530-545 | 1 | 2 | 0 | 0 | 3 |
| 545-600 | 1 | 0 | 0 | 0 | 1 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 0 | 5 | 4 | 1 | 10 |
| 415-515 | 2 | 3 | 4 | 1 | 10 |
| 430-530 | 2 | 2 | 4 | 1 | 9 |
| 445-545 | 3 | 3 | 2 | 0 | 8 |
| 500-600 | 4 | 2 | 0 | 0 | 6 |

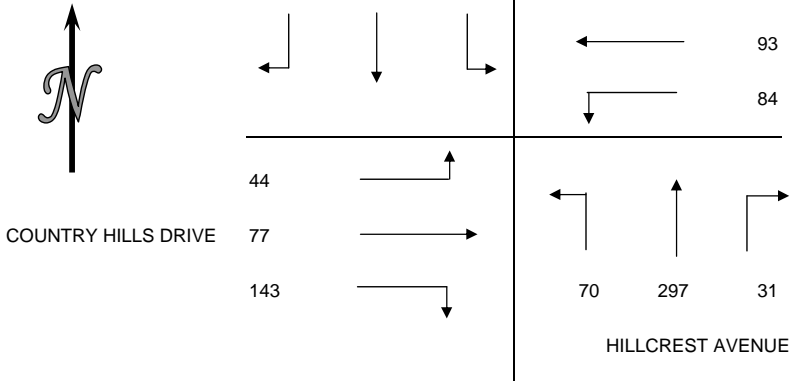
| BICYCLE COUNTS | | | | | |
|----------------|-----------|----------|-----------|----------|-------|
| 15 MIN COUNTS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-415 | 0 | 0 | 0 | 0 | 0 |
| 415-430 | 0 | 0 | 0 | 0 | 0 |
| 430-445 | 1 | 1 | 0 | 0 | 2 |
| 445-500 | 0 | 0 | 3 | 0 | 3 |
| 500-515 | 0 | 0 | 0 | 0 | 0 |
| 515-530 | 1 | 0 | 0 | 2 | 3 |
| 530-545 | 0 | 0 | 0 | 0 | 0 |
| 545-600 | 0 | 0 | 0 | 0 | 0 |
| HOUR TOTALS | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG | TOTAL |
| PERIOD | LEG | LEG | LEG | LEG | |
| 400-500 | 1 | 1 | 3 | 0 | 5 |
| 415-515 | 1 | 1 | 3 | 0 | 5 |
| 430-530 | 2 | 1 | 3 | 2 | 8 |
| 445-545 | 1 | 0 | 3 | 2 | 6 |
| 500-600 | 1 | 0 | 0 | 2 | 3 |

INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S HILLCREST AVENUE
 E/W COUNTRY HILLS DRIVE

| 15 MIN COUNTS PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTALS |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|
| 700-715 | 4 | 46 | 6 | 21 | 2 | 3 | 0 | 41 | 1 | 13 | 6 | 5 | 148 |
| 715-730 | 7 | 60 | 8 | 28 | 9 | 10 | 4 | 50 | 11 | 19 | 7 | 16 | 229 |
| 730-745 | 3 | 70 | 19 | 36 | 18 | 14 | 5 | 69 | 7 | 26 | 7 | 14 | 288 |
| 745-800 | 4 | 105 | 25 | 37 | 32 | 33 | 9 | 62 | 18 | 39 | 33 | 15 | 412 |
| 800-815 | 5 | 118 | 22 | 47 | 41 | 21 | 10 | 95 | 22 | 28 | 28 | 12 | 449 |
| 815-830 | 10 | 113 | 7 | 20 | 14 | 16 | 4 | 69 | 18 | 40 | 12 | 11 | 334 |
| 830-845 | 7 | 103 | 9 | 13 | 6 | 14 | 8 | 71 | 12 | 36 | 4 | 6 | 289 |
| 845-900 | 5 | 125 | 4 | 11 | 2 | 13 | 5 | 62 | 18 | 31 | 7 | 10 | 293 |
| HOUR TOTALS | | | | | | | | | | | | | |
| 700-800 | 18 | 281 | 58 | 122 | 61 | 60 | 18 | 222 | 37 | 97 | 53 | 50 | 1077 |
| 715-815 | 19 | 353 | 74 | 148 | 100 | 78 | 28 | 276 | 58 | 112 | 75 | 57 | 1378 |
| 730-830 | 22 | 406 | 73 | 140 | 105 | 84 | 28 | 295 | 65 | 133 | 80 | 52 | 1483 |
| 745-845 | 26 | 439 | 63 | 117 | 93 | 84 | 31 | 297 | 70 | 143 | 77 | 44 | 1484 |
| 800-900 | 27 | 459 | 42 | 91 | 63 | 64 | 27 | 297 | 70 | 135 | 51 | 39 | 1365 |

AM PEAK HOUR
745-845



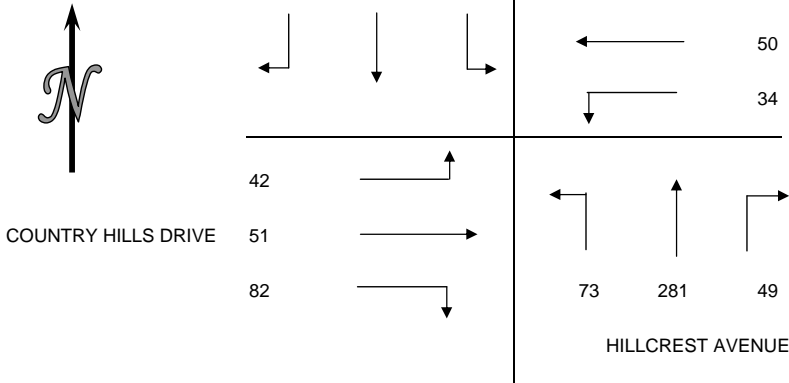
| PEDESTRIAN COUNTS | | | | |
|-------------------|-----------|----------|-----------|----------|
| PERIOD | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG |
| 15 MIN COUNTS | | | | |
| 700-715 | 0 | 1 | 0 | 0 |
| 715-730 | 3 | 0 | 9 | 0 |
| 730-745 | 2 | 0 | 6 | 2 |
| 745-800 | 8 | 0 | 6 | 1 |
| 800-815 | 3 | 0 | 2 | 6 |
| 815-830 | 2 | 2 | 4 | 2 |
| 830-845 | 1 | 0 | 0 | 0 |
| 845-900 | 0 | 0 | 2 | 0 |
| HOUR TOTALS | | | | |
| 700-800 | 13 | 1 | 21 | 3 |
| 715-815 | 16 | 0 | 23 | 9 |
| 730-830 | 15 | 2 | 18 | 11 |
| 745-845 | 14 | 2 | 12 | 9 |
| 800-900 | 6 | 2 | 8 | 8 |

INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S HILLCREST AVENUE
 E/W COUNTRY HILLS DRIVE

| 15 MIN COUNTS PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTALS |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|
| 400-415 | 11 | 97 | 17 | 10 | 20 | 2 | 7 | 76 | 23 | 20 | 12 | 11 | 306 |
| 415-430 | 10 | 71 | 12 | 13 | 16 | 5 | 7 | 75 | 19 | 16 | 12 | 3 | 259 |
| 430-445 | 10 | 91 | 12 | 14 | 13 | 3 | 10 | 70 | 21 | 16 | 8 | 6 | 274 |
| 445-500 | 10 | 89 | 24 | 7 | 13 | 10 | 14 | 76 | 20 | 17 | 8 | 10 | 298 |
| 500-515 | 14 | 92 | 20 | 11 | 13 | 6 | 8 | 66 | 20 | 16 | 10 | 18 | 294 |
| 515-530 | 19 | 99 | 19 | 12 | 12 | 39 | 13 | 75 | 15 | 14 | 8 | 10 | 335 |
| 530-545 | 18 | 83 | 21 | 13 | 13 | -19 | 17 | 71 | 15 | 22 | 20 | 8 | 282 |
| 545-600 | 12 | 102 | 29 | 9 | 12 | 8 | 11 | 69 | 23 | 30 | 13 | 6 | 324 |
| HOUR TOTALS | | | | | | | | | | | | | |
| 400-500 | 41 | 348 | 65 | 44 | 62 | 20 | 38 | 297 | 83 | 69 | 40 | 30 | 1137 |
| 415-515 | 44 | 343 | 68 | 45 | 55 | 24 | 39 | 287 | 80 | 65 | 38 | 37 | 1125 |
| 430-530 | 53 | 371 | 75 | 44 | 51 | 58 | 45 | 287 | 76 | 63 | 34 | 44 | 1201 |
| 445-545 | 61 | 363 | 84 | 43 | 51 | 36 | 52 | 288 | 70 | 69 | 46 | 46 | 1209 |
| 500-600 | 63 | 376 | 89 | 45 | 50 | 34 | 49 | 281 | 73 | 82 | 51 | 42 | 1235 |

PM PEAK HOUR
500-600



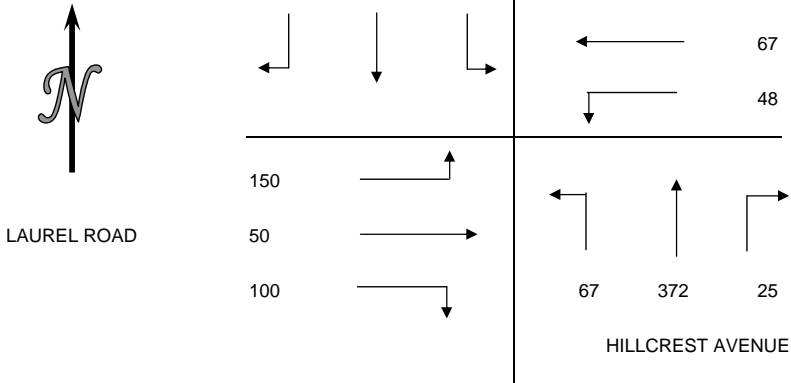
| PEDESTRIAN COUNTS | | | | |
|-------------------|-----------|----------|-----------|----------|
| PERIOD | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG |
| 15 MIN COUNTS | | | | |
| 400-415 | 0 | 0 | 5 | 0 |
| 415-430 | 0 | 0 | 0 | 0 |
| 430-445 | 4 | 0 | 1 | 0 |
| 445-500 | 0 | 1 | 0 | 0 |
| 500-515 | 0 | 0 | 1 | 0 |
| 515-530 | 0 | 0 | 2 | 0 |
| 530-545 | 1 | 0 | 2 | 0 |
| 545-600 | 1 | 0 | 0 | 0 |
| HOUR TOTALS | | | | |
| 400-500 | 4 | 1 | 6 | 0 |
| 415-515 | 4 | 1 | 2 | 0 |
| 430-530 | 4 | 1 | 4 | 0 |
| 445-545 | 1 | 1 | 5 | 0 |
| 500-600 | 2 | 0 | 5 | 0 |

INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 7:00 AM TO 9:00 AM
 INTERSECTION: N/S HILLCREST AVENUE
 E/W LAUREL ROAD

| 15 MIN COUNTS PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTALS |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|
| 700-715 | 3 | 50 | 8 | 38 | 1 | 4 | 1 | 58 | 2 | 3 | 4 | 13 | 185 |
| 715-730 | 4 | 47 | 13 | 37 | 1 | 5 | 2 | 74 | 5 | 5 | 1 | 6 | 200 |
| 730-745 | 8 | 91 | 10 | 47 | 3 | 6 | 3 | 96 | 8 | 14 | 3 | 13 | 302 |
| 745-800 | 15 | 110 | 19 | 50 | 3 | 12 | 4 | 92 | 16 | 24 | 6 | 25 | 376 |
| 800-815 | 28 | 92 | 12 | 40 | 26 | 12 | 11 | 112 | 29 | 22 | 17 | 36 | 437 |
| 815-830 | 32 | 92 | 29 | 34 | 31 | 6 | 6 | 92 | 13 | 25 | 19 | 60 | 439 |
| 830-845 | 5 | 83 | 14 | 31 | 7 | 18 | 4 | 76 | 9 | 29 | 8 | 29 | 313 |
| 845-900 | 3 | 110 | 15 | 19 | 2 | 13 | 14 | 24 | 5 | 6 | 3 | 9 | 223 |
| HOUR TOTALS | | | | | | | | | | | | | |
| 700-800 | 30 | 298 | 50 | 172 | 8 | 27 | 10 | 320 | 31 | 46 | 14 | 57 | 1063 |
| 715-815 | 55 | 340 | 54 | 174 | 33 | 35 | 20 | 374 | 58 | 65 | 27 | 80 | 1315 |
| 730-830 | 83 | 385 | 70 | 171 | 63 | 36 | 24 | 392 | 66 | 85 | 45 | 134 | 1554 |
| 745-845 | 80 | 377 | 74 | 155 | 67 | 48 | 25 | 372 | 67 | 100 | 50 | 150 | 1565 |
| 800-900 | 68 | 377 | 70 | 124 | 66 | 49 | 35 | 304 | 56 | 82 | 47 | 134 | 1412 |

AM PEAK HOUR
745-845



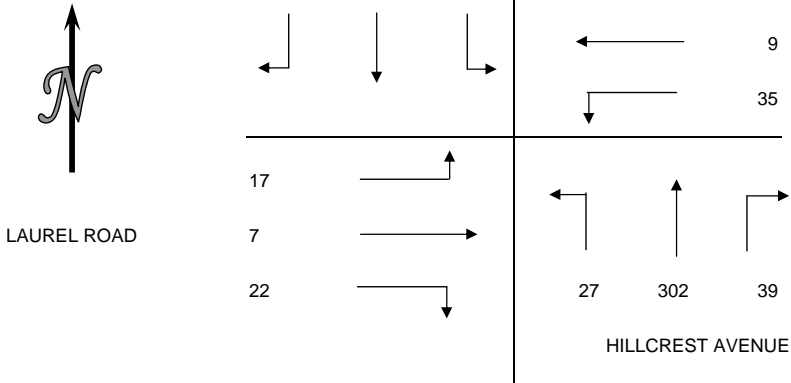
| PEDESTRIAN COUNTS | | | | |
|-------------------|-----------|----------|-----------|----------|
| PERIOD | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG |
| 15 MIN COUNTS | | | | |
| 700-715 | 0 | 0 | 1 | 1 |
| 715-730 | 0 | 0 | 3 | 1 |
| 730-745 | 4 | 0 | 1 | 0 |
| 745-800 | 2 | 5 | 10 | 1 |
| 800-815 | 1 | 1 | 6 | 0 |
| 815-830 | 1 | 5 | 3 | 1 |
| 830-845 | 0 | 1 | 0 | 0 |
| 845-900 | 0 | 5 | 0 | 0 |
| HOUR TOTALS | | | | |
| 700-800 | 6 | 5 | 15 | 3 |
| 715-815 | 7 | 6 | 20 | 2 |
| 730-830 | 8 | 11 | 20 | 2 |
| 745-845 | 4 | 12 | 19 | 2 |
| 800-900 | 2 | 12 | 9 | 1 |

INTERSECTION TURNING MOVEMENT COUNT SUMMARY

CLIENT: KIMLEY -HORN AND ASSOCIATES, INC.
 PROJECT: ANTIOCH TRAFFIC COUNTS
 DATE: THURSDAY MAY 15, 2008
 PERIOD: 4:00 PM TO 6:00 PM
 INTERSECTION: N/S HILLCREST AVENUE
 E/W LAUREL ROAD

| 15 MIN COUNTS PERIOD | 1 SBRT | 2 SBTH | 3 SBLT | 4 WBRT | 5 WBTH | 6 WBLT | 7 NBRT | 8 NBTH | 9 NBLT | 10 EBRT | 11 EBTH | 12 EBLT | TOTALS |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|--------|
| 400-415 | 7 | 104 | 27 | 42 | 0 | 5 | 8 | 87 | 7 | 8 | 4 | 6 | 305 |
| 415-430 | 7 | 90 | 35 | 35 | 4 | 4 | 6 | 90 | 3 | 2 | 0 | 5 | 281 |
| 430-445 | 11 | 105 | 28 | 34 | 2 | 7 | 7 | 75 | 5 | 7 | 2 | 6 | 289 |
| 445-500 | 8 | 119 | 30 | 37 | 1 | 3 | 9 | 77 | 7 | 0 | 3 | 2 | 296 |
| 500-515 | 11 | 106 | 42 | 45 | 1 | 10 | 10 | 81 | 5 | 5 | 2 | 4 | 322 |
| 515-530 | 12 | 123 | 37 | 29 | 3 | 15 | 6 | 80 | 8 | 4 | 2 | 3 | 322 |
| 530-545 | 14 | 114 | 43 | 27 | 3 | 3 | 8 | 72 | 11 | 5 | 2 | 4 | 306 |
| 545-600 | 13 | 116 | 40 | 32 | 2 | 7 | 15 | 69 | 3 | 8 | 1 | 6 | 312 |
| HOURLY TOTALS | | | | | | | | | | | | | |
| 400-500 | 33 | 418 | 120 | 148 | 7 | 19 | 30 | 329 | 22 | 17 | 9 | 19 | 1171 |
| 415-515 | 37 | 420 | 135 | 151 | 8 | 24 | 32 | 323 | 20 | 14 | 7 | 17 | 1188 |
| 430-530 | 42 | 453 | 137 | 145 | 7 | 35 | 32 | 313 | 25 | 16 | 9 | 15 | 1229 |
| 445-545 | 45 | 462 | 152 | 138 | 8 | 31 | 33 | 310 | 31 | 14 | 9 | 13 | 1246 |
| 500-600 | 50 | 459 | 162 | 133 | 9 | 35 | 39 | 302 | 27 | 22 | 7 | 17 | 1262 |

PM PEAK HOUR
500-600



































| PEDESTRIAN COUNTS | | | | |
|-------------------|-----------|----------|-----------|----------|
| PERIOD | NORTH LEG | EAST LEG | SOUTH LEG | WEST LEG |
| 15 MIN COUNTS | | | | |
| 400-415 | 0 | 0 | 1 | 0 |
| 415-430 | 0 | 1 | 0 | 0 |
| 430-445 | 0 | 0 | 0 | 0 |
| 445-500 | 0 | 0 | 0 | 0 |
| 500-515 | 0 | 0 | 0 | 0 |
| 515-530 | 0 | 0 | 0 | 0 |
| 530-545 | 0 | 0 | 0 | 0 |
| 545-600 | 1 | 1 | 2 | 0 |
| HOURLY TOTALS | | | | |
| 400-500 | 0 | 1 | 1 | 0 |
| 415-515 | 0 | 1 | 0 | 0 |
| 430-530 | 0 | 0 | 0 | 0 |
| 445-545 | 0 | 0 | 0 | 0 |
| 500-600 | 1 | 1 | 2 | 0 |

APPENDIX B:
HCM LOS Calculation worksheets

Existing

HCM Signalized Intersection Capacity Analysis
8: Lone Tree Way & Canada Valley

Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |   |    |  |   |   |  |  |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.91 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1613 | 1504 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1613 | 1504 | 1770 | 1863 | 1583 |
| Volume (vph) | 29 | 746 | 52 | 166 | 1005 | 168 | 36 | 14 | 51 | 190 | 31 | 34 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 32 | 829 | 58 | 184 | 1117 | 187 | 40 | 16 | 57 | 211 | 34 | 38 |
| RTOR Reduction (vph) | 0 | 0 | 17 | 0 | 0 | 65 | 0 | 22 | 32 | 0 | 0 | 31 |
| Lane Group Flow (vph) | 32 | 829 | 41 | 184 | 1117 | 122 | 40 | 17 | 2 | 211 | 34 | 7 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 3.6 | 74.5 | 74.5 | 11.2 | 82.1 | 82.1 | 5.0 | 7.3 | 7.3 | 19.0 | 21.3 | 21.3 |
| Effective Green, g (s) | 4.6 | 77.5 | 77.5 | 12.2 | 85.1 | 85.1 | 6.0 | 8.3 | 8.3 | 20.0 | 22.3 | 22.3 |
| Actuated g/C Ratio | 0.04 | 0.60 | 0.60 | 0.09 | 0.65 | 0.65 | 0.05 | 0.06 | 0.06 | 0.15 | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 6.0 | 6.0 | 2.0 | 2.0 | 2.0 | 2.0 | 6.0 | 6.0 |
| Lane Grp Cap (vph) | 63 | 3031 | 944 | 322 | 3329 | 1036 | 158 | 103 | 96 | 272 | 320 | 272 |
| v/s Ratio Prot | c0.02 | 0.16 | | c0.05 | c0.22 | | 0.01 | c0.01 | | c0.12 | 0.02 | |
| v/s Ratio Perm | | | 0.03 | | | 0.08 | | | 0.00 | | | 0.00 |
| v/c Ratio | 0.51 | 0.27 | 0.04 | 0.57 | 0.34 | 0.12 | 0.25 | 0.17 | 0.02 | 0.78 | 0.11 | 0.02 |
| Uniform Delay, d1 | 61.6 | 12.7 | 10.9 | 56.4 | 9.9 | 8.4 | 59.8 | 57.6 | 57.0 | 52.8 | 45.4 | 44.8 |
| Progression Factor | 0.81 | 0.61 | 0.39 | 1.23 | 0.59 | 0.41 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.0 | 0.2 | 0.1 | 1.4 | 0.3 | 0.2 | 0.3 | 0.3 | 0.0 | 11.9 | 0.4 | 0.1 |
| Delay (s) | 51.9 | 7.9 | 4.3 | 70.5 | 6.1 | 3.6 | 60.1 | 57.9 | 57.1 | 64.7 | 45.9 | 44.9 |
| Level of Service | D | A | A | E | A | A | E | E | E | E | D | D |
| Approach Delay (s) | | 9.2 | | | 13.8 | | | 58.4 | | | 59.8 | |
| Approach LOS | | A | | | B | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 18.7 | | | | HCM Level of Service | | | B | | |
| HCM Volume to Capacity ratio | | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 49.9% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
9: Lone Tree Way & SR-4 Bypass SB Off-Ramp













Davidon EIR
Existing AM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|-------|-------|----------------------|------|------|------|------|------|-------|
| Lane Configurations | | ↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Volume (vph) | 0 | 571 | 401 | 72 | 1000 | 0 | 0 | 0 | 0 | 287 | 6 | 353 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 634 | 446 | 80 | 1111 | 0 | 0 | 0 | 0 | 319 | 7 | 392 |
| RTOR Reduction (vph) | 0 | 0 | 171 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 |
| Lane Group Flow (vph) | 0 | 634 | 275 | 80 | 1111 | 0 | 0 | 0 | 0 | 160 | 166 | 342 |
| Confl. Peds. (#/hr) | | | | | | | 2 | | | | | |
| Turn Type | | Perm | | Prot | | | | | | Perm | | Perm |
| Protected Phases | | 2 | | 1 | 6 | | | | | | 4 | |
| Permitted Phases | | | 2 | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 77.6 | 77.6 | 7.1 | 88.7 | | | | | 31.8 | 31.8 | 31.8 |
| Effective Green, g (s) | | 80.1 | 80.1 | 8.1 | 91.2 | | | | | 32.8 | 32.8 | 32.8 |
| Actuated g/C Ratio | | 0.62 | 0.62 | 0.06 | 0.70 | | | | | 0.25 | 0.25 | 0.25 |
| Clearance Time (s) | | 5.5 | 5.5 | 4.0 | 5.5 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 3.0 | 4.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 3133 | 975 | 214 | 3567 | | | | | 424 | 426 | 399 |
| v/s Ratio Prot | | 0.12 | | c0.02 | c0.22 | | | | | | | |
| v/s Ratio Perm | | | 0.17 | | | | | | | 0.10 | 0.10 | c0.22 |
| v/c Ratio | | 0.20 | 0.28 | 0.37 | 0.31 | | | | | 0.38 | 0.39 | 0.86 |
| Uniform Delay, d1 | | 10.9 | 11.6 | 58.5 | 7.4 | | | | | 40.2 | 40.3 | 46.4 |
| Progression Factor | | 0.82 | 1.16 | 1.32 | 0.38 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | 0.7 | 1.1 | 0.2 | | | | | 0.6 | 0.6 | 16.4 |
| Delay (s) | | 9.1 | 14.2 | 78.4 | 3.0 | | | | | 40.7 | 40.9 | 62.7 |
| Level of Service | | A | B | E | A | | | | | D | D | E |
| Approach Delay (s) | | 11.2 | | | 8.1 | | | 0.0 | | | 52.8 | |
| Approach LOS | | B | | | A | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 20.0 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 6.0 | | |
| Intersection Capacity Utilization | | | 47.8% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group
























HCM Signalized Intersection Capacity Analysis
10: Lone Tree Way & On-ramp

Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1697 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1697 | 1583 | | | |
| Volume (vph) | 0 | 662 | 160 | 8 | 671 | 245 | 383 | 29 | 79 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 0 | 744 | 180 | 9 | 754 | 275 | 430 | 33 | 89 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 47 | 0 | 0 | 61 | 0 | 0 | 74 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 744 | 133 | 9 | 754 | 215 | 226 | 237 | 15 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Split | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | 8 | 8 | | | | |
| Permitted Phases | | 2 | | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | | 93.2 | 93.2 | 1.2 | 98.4 | 98.4 | 21.6 | 21.6 | 21.6 | | | |
| Effective Green, g (s) | | 96.2 | 96.2 | 2.2 | 101.4 | 101.4 | 22.6 | 22.6 | 22.6 | | | |
| Actuated g/C Ratio | | 0.74 | 0.74 | 0.02 | 0.78 | 0.78 | 0.17 | 0.17 | 0.17 | | | |
| Clearance Time (s) | | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | | 3763 | 1171 | 30 | 3966 | 1235 | 292 | 295 | 275 | | | |
| v/s Ratio Prot | | c0.15 | | c0.01 | 0.15 | | 0.13 | c0.14 | | | | |
| v/s Ratio Perm | | 0.08 | | | 0.14 | | | 0.01 | | | | |
| v/c Ratio | | 0.20 | 0.11 | 0.30 | 0.19 | 0.17 | 0.77 | 0.80 | 0.06 | | | |
| Uniform Delay, d1 | | 5.1 | 4.8 | 63.1 | 3.7 | 3.6 | 51.3 | 51.6 | 44.8 | | | |
| Progression Factor | | 0.53 | 1.33 | 0.63 | 2.36 | 11.24 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.1 | 0.2 | 2.0 | 0.1 | 0.3 | 11.0 | 13.8 | 0.0 | | | |
| Delay (s) | | 2.9 | 6.6 | 42.0 | 8.8 | 41.2 | 62.3 | 65.4 | 44.8 | | | |
| Level of Service | | A | A | D | A | D | E | E | D | | | |
| Approach Delay (s) | | 3.6 | | 17.7 | | 60.8 | | 0.0 | | | | |
| Approach LOS | | A | | B | | E | | A | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 22.0 | | HCM Level of Service | | C | | | | | | |
| HCM Volume to Capacity ratio | | 0.31 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | Sum of lost time (s) | | 9.0 | | | | | | |
| Intersection Capacity Utilization | | 33.2% | | ICU Level of Service | | A | | | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
11: Lone Tree Way & Shady Willow Rd

























Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1549 | 1770 | 3539 | 1562 | 3433 | 3080 | | 3433 | 1863 | 1563 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1549 | 1770 | 3539 | 1562 | 3433 | 3080 | | 3433 | 1863 | 1563 |
| Volume (vph) | 74 | 484 | 91 | 54 | 837 | 29 | 39 | 47 | 191 | 42 | 35 | 24 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 82 | 538 | 101 | 60 | 930 | 32 | 43 | 52 | 212 | 47 | 39 | 27 |
| RTOR Reduction (vph) | 0 | 0 | 34 | 0 | 0 | 11 | 0 | 185 | 0 | 0 | 0 | 24 |
| Lane Group Flow (vph) | 82 | 538 | 67 | 60 | 930 | 21 | 43 | 79 | 0 | 47 | 39 | 3 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 8.5 | 83.5 | 83.5 | 7.7 | 82.7 | 82.7 | 5.9 | 15.4 | | 5.4 | 14.9 | 14.9 |
| Effective Green, g (s) | 9.5 | 86.5 | 86.5 | 8.7 | 85.7 | 85.7 | 6.9 | 16.4 | | 6.4 | 15.9 | 15.9 |
| Actuated g/C Ratio | 0.07 | 0.67 | 0.67 | 0.07 | 0.66 | 0.66 | 0.05 | 0.13 | | 0.05 | 0.12 | 0.12 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 3.0 | 4.0 | | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 251 | 3383 | 1031 | 118 | 2333 | 1030 | 182 | 389 | | 169 | 228 | 191 |
| v/s Ratio Prot | 0.02 | 0.11 | | c0.03 | c0.26 | | c0.01 | c0.03 | | c0.01 | 0.02 | |
| v/s Ratio Perm | | | 0.04 | | | 0.01 | | | | | | 0.00 |
| v/c Ratio | 0.33 | 0.16 | 0.07 | 0.51 | 0.40 | 0.02 | 0.24 | 0.20 | | 0.28 | 0.17 | 0.02 |
| Uniform Delay, d1 | 57.2 | 8.1 | 7.6 | 58.6 | 10.2 | 7.7 | 59.0 | 50.9 | | 59.6 | 51.1 | 50.2 |
| Progression Factor | 0.88 | 0.88 | 1.72 | 0.93 | 1.61 | 3.11 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.8 | 0.1 | 0.1 | 1.2 | 0.5 | 0.0 | 0.7 | 0.4 | | 0.3 | 0.1 | 0.0 |
| Delay (s) | 51.1 | 7.2 | 13.2 | 55.9 | 17.0 | 23.8 | 59.7 | 51.3 | | 59.9 | 51.3 | 50.2 |
| Level of Service | D | A | B | E | B | C | E | D | | E | D | D |
| Approach Delay (s) | | 13.1 | | | 19.5 | | | 52.5 | | | 54.6 | |
| Approach LOS | | B | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 23.9 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.37 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 58.2% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
12: Lone Tree Way & Empire Avenue

























Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 1770 | 3539 | 1583 | 3433 | 1863 | 1562 | 3433 | 3167 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 1770 | 3539 | 1583 | 3433 | 1863 | 1562 | 3433 | 3167 | |
| Volume (vph) | 168 | 499 | 26 | 81 | 638 | 80 | 89 | 48 | 41 | 105 | 77 | 181 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 187 | 554 | 29 | 90 | 709 | 89 | 99 | 53 | 46 | 117 | 86 | 201 |
| RTOR Reduction (vph) | 0 | 0 | 11 | 0 | 0 | 39 | 0 | 0 | 41 | 0 | 180 | 0 |
| Lane Group Flow (vph) | 187 | 554 | 18 | 90 | 709 | 50 | 99 | 53 | 5 | 117 | 107 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | 1 | 1 | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | Perm | Split | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 17.6 | 78.3 | 78.3 | 10.8 | 71.5 | 71.5 | 12.2 | 12.2 | 12.2 | 12.7 | 12.7 | |
| Effective Green, g (s) | 18.6 | 79.3 | 79.3 | 11.8 | 72.5 | 72.5 | 13.2 | 13.2 | 13.2 | 13.7 | 13.7 | |
| Actuated g/C Ratio | 0.14 | 0.61 | 0.61 | 0.09 | 0.56 | 0.56 | 0.10 | 0.10 | 0.10 | 0.11 | 0.11 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 253 | 3102 | 953 | 161 | 1974 | 883 | 349 | 189 | 159 | 362 | 334 | |
| v/s Ratio Prot | c0.11 | 0.11 | | 0.05 | c0.20 | | c0.03 | 0.03 | | c0.03 | 0.03 | |
| v/s Ratio Perm | | | 0.01 | | | 0.03 | | | 0.00 | | | |
| v/c Ratio | 0.74 | 0.18 | 0.02 | 0.56 | 0.36 | 0.06 | 0.28 | 0.28 | 0.03 | 0.32 | 0.32 | |
| Uniform Delay, d1 | 53.4 | 11.1 | 10.0 | 56.6 | 15.9 | 13.1 | 54.0 | 54.0 | 52.6 | 53.9 | 53.8 | |
| Progression Factor | 1.11 | 0.64 | 0.37 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 9.3 | 0.1 | 0.0 | 2.4 | 0.5 | 0.1 | 0.2 | 0.3 | 0.0 | 0.2 | 0.2 | |
| Delay (s) | 68.7 | 7.2 | 3.7 | 59.0 | 16.4 | 13.2 | 54.2 | 54.3 | 52.7 | 54.0 | 54.0 | |
| Level of Service | E | A | A | E | B | B | D | D | D | D | D | |
| Approach Delay (s) | | 22.0 | | | 20.4 | | | 53.9 | | | 54.0 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 29.9 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 51.6% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

























HCM Signalized Intersection Capacity Analysis
13: Lone Tree Way & Deer Valley Rd.

Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.83 | 1.00 | 1.00 | 0.92 | 1.00 | 0.96 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3539 | 1311 | 1770 | 3539 | 1454 | 3433 | 3245 | | 2000 | 3508 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3539 | 1311 | 1770 | 3539 | 1454 | 3433 | 3245 | | 1770 | 3508 | |
| Volume (vph) | 35 | 644 | 157 | 185 | 833 | 185 | 279 | 245 | 111 | 353 | 457 | 17 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 39 | 724 | 176 | 208 | 936 | 208 | 313 | 275 | 125 | 397 | 513 | 19 |
| RTOR Reduction (vph) | 0 | 0 | 47 | 0 | 0 | 39 | 0 | 42 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 39 | 724 | 129 | 208 | 936 | 169 | 313 | 358 | 0 | 397 | 530 | 0 |
| Confl. Peds. (#/hr) | 44 | | 101 | 101 | | 44 | 58 | | 69 | 69 | | 58 |
| Confl. Bikes (#/hr) | | | 31 | | | 15 | | | 13 | | | 5 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | |
| Actuated Green, G (s) | 7.3 | 38.5 | 38.5 | 18.4 | 49.6 | 49.6 | 16.7 | 24.3 | | 30.3 | 37.9 | |
| Effective Green, g (s) | 8.8 | 40.5 | 40.5 | 19.9 | 51.6 | 51.6 | 18.2 | 25.8 | | 31.8 | 39.4 | |
| Actuated g/C Ratio | 0.07 | 0.31 | 0.31 | 0.15 | 0.40 | 0.40 | 0.14 | 0.20 | | 0.24 | 0.30 | |
| Clearance Time (s) | 4.5 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 3.0 | 3.0 | | 4.0 | 3.0 | |
| Lane Grp Cap (vph) | 120 | 1103 | 408 | 271 | 1405 | 577 | 481 | 644 | | 489 | 1063 | |
| v/s Ratio Prot | 0.02 | 0.20 | | c0.12 | c0.26 | | 0.09 | c0.11 | | c0.20 | 0.15 | |
| v/s Ratio Perm | | | 0.10 | | | 0.12 | | | | | | |
| v/c Ratio | 0.32 | 0.66 | 0.32 | 0.77 | 0.67 | 0.29 | 0.65 | 0.56 | | 0.81 | 0.50 | |
| Uniform Delay, d1 | 57.8 | 38.7 | 34.2 | 52.8 | 32.1 | 26.7 | 52.9 | 46.9 | | 46.3 | 37.2 | |
| Progression Factor | 1.18 | 1.30 | 1.64 | 1.16 | 0.53 | 0.30 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.5 | 2.8 | 1.9 | 7.6 | 1.5 | 0.8 | 3.1 | 1.0 | | 10.4 | 0.4 | |
| Delay (s) | 69.7 | 53.0 | 57.9 | 69.0 | 18.6 | 8.9 | 56.0 | 48.0 | | 56.7 | 37.6 | |
| Level of Service | E | D | E | E | B | A | E | D | | E | D | |
| Approach Delay (s) | | 54.6 | | | 24.9 | | | 51.5 | | | 45.7 | |
| Approach LOS | | D | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 41.7 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.69 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 87.1% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |










HCM Signalized Intersection Capacity Analysis
14: Lone Tree Way & Hillcrest Ave.

Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1515 | 1770 | 3539 | 1520 | 1770 | 3421 | | 1900 | 3288 | 1554 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1515 | 1770 | 3539 | 1520 | 1770 | 3421 | | 1610 | 3288 | 1554 |
| Volume (vph) | 177 | 495 | 18 | 24 | 862 | 160 | 36 | 53 | 13 | 279 | 85 | 269 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 197 | 550 | 20 | 27 | 958 | 178 | 40 | 59 | 14 | 310 | 94 | 299 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 86 | 0 | 12 | 0 | 0 | 0 | 247 |
| Lane Group Flow (vph) | 197 | 550 | 11 | 27 | 958 | 92 | 40 | 61 | 0 | 155 | 249 | 52 |
| Confl. Peds. (#/hr) | 18 | | | 20 | | 18 | 5 | | 10 | 10 | | 5 |
| Confl. Bikes (#/hr) | | | 12 | | | 9 | | | | | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 18.1 | 71.0 | 71.0 | 3.4 | 55.8 | 55.8 | 15.4 | 15.4 | | 20.7 | 20.7 | 20.7 |
| Effective Green, g (s) | 20.1 | 73.0 | 73.0 | 4.9 | 57.8 | 57.8 | 17.4 | 17.4 | | 22.7 | 22.7 | 22.7 |
| Actuated g/C Ratio | 0.15 | 0.56 | 0.56 | 0.04 | 0.44 | 0.44 | 0.13 | 0.13 | | 0.17 | 0.17 | 0.17 |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 274 | 1987 | 851 | 67 | 1573 | 676 | 237 | 458 | | 332 | 574 | 271 |
| v/s Ratio Prot | c0.11 | 0.16 | | 0.02 | c0.27 | | c0.02 | 0.02 | | c0.08 | 0.08 | |
| v/s Ratio Perm | | | 0.01 | | | 0.06 | | | | | | 0.03 |
| v/c Ratio | 0.72 | 0.28 | 0.01 | 0.40 | 0.61 | 0.14 | 0.17 | 0.13 | | 0.47 | 0.43 | 0.19 |
| Uniform Delay, d1 | 52.3 | 14.8 | 12.6 | 61.1 | 27.5 | 21.3 | 49.9 | 49.6 | | 48.2 | 47.9 | 45.8 |
| Progression Factor | 1.31 | 1.10 | 1.95 | 1.18 | 0.73 | 0.62 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 9.8 | 0.3 | 0.0 | 3.5 | 1.6 | 0.4 | 0.7 | 0.3 | | 2.2 | 1.1 | 0.7 |
| Delay (s) | 78.0 | 16.6 | 24.5 | 75.8 | 21.8 | 13.6 | 50.6 | 49.9 | | 50.4 | 49.0 | 46.6 |
| Level of Service | E | B | C | E | C | B | D | D | | D | D | D |
| Approach Delay (s) | | 32.6 | | | 21.8 | | | 50.2 | | | 48.3 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 32.7 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.54 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 61.7% | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
15: Lone Tree Way & Vista Grande





















Davidon EIR
Existing AM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|---|-------|---|---|----------------------|--|---|------|---|---|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.87 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5049 | | 1770 | 5057 | | 1770 | 1612 | | 1770 | 1661 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.66 | 1.00 | | 0.31 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5049 | | 1770 | 5057 | | 1233 | 1612 | | 585 | 1661 | |
| Volume (vph) | 20 | 693 | 30 | 59 | 967 | 37 | 39 | 14 | 123 | 24 | 16 | 41 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 22 | 745 | 32 | 63 | 1040 | 40 | 42 | 15 | 132 | 26 | 17 | 44 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 118 | 0 | 0 | 39 | 0 |
| Lane Group Flow (vph) | 22 | 775 | 0 | 63 | 1078 | 0 | 42 | 29 | 0 | 26 | 22 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | | | | |
| Turn Type | Prot | | | Prot | | | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 5.5 | 93.6 | | 9.5 | 97.6 | | 12.4 | 12.4 | | 12.4 | 12.4 | |
| Effective Green, g (s) | 7.0 | 96.1 | | 11.0 | 100.1 | | 13.9 | 13.9 | | 13.9 | 13.9 | |
| Actuated g/C Ratio | 0.05 | 0.74 | | 0.08 | 0.77 | | 0.11 | 0.11 | | 0.11 | 0.11 | |
| Clearance Time (s) | 4.5 | 5.5 | | 4.5 | 5.5 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 4.0 | 6.0 | | 4.0 | 6.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 95 | 3732 | | 150 | 3894 | | 132 | 172 | | 63 | 178 | |
| v/s Ratio Prot | 0.01 | 0.15 | | c0.04 | c0.21 | | | 0.02 | | | 0.01 | |
| v/s Ratio Perm | | | | | | | 0.03 | | | c0.04 | | |
| v/c Ratio | 0.23 | 0.21 | | 0.42 | 0.28 | | 0.32 | 0.17 | | 0.41 | 0.12 | |
| Uniform Delay, d1 | 58.9 | 5.2 | | 56.5 | 4.4 | | 53.7 | 52.8 | | 54.2 | 52.5 | |
| Progression Factor | 1.02 | 1.10 | | 1.10 | 0.62 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.6 | 0.1 | | 2.2 | 0.1 | | 1.4 | 0.5 | | 4.3 | 0.3 | |
| Delay (s) | 61.9 | 5.8 | | 64.3 | 2.8 | | 55.1 | 53.3 | | 58.6 | 52.8 | |
| Level of Service | E | A | | E | A | | E | D | | E | D | |
| Approach Delay (s) | | 7.4 | | | 6.2 | | | 53.7 | | | 54.6 | |
| Approach LOS | | A | | | A | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 12.6 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.30 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 6.0 | | |
| Intersection Capacity Utilization | | | 47.8% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
16: Country Hills Dr. & Hillcrest Ave
























Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.90 | | 1.00 | 0.92 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1665 | | 1770 | 1691 | | 1770 | 3468 | | 1770 | 3478 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1665 | | 1770 | 1691 | | 1770 | 3468 | | 1770 | 3478 | |
| Volume (vph) | 44 | 77 | 143 | 84 | 93 | 117 | 70 | 297 | 31 | 63 | 439 | 26 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 49 | 86 | 159 | 93 | 103 | 130 | 78 | 330 | 34 | 70 | 488 | 29 |
| RTOR Reduction (vph) | 0 | 39 | 0 | 0 | 26 | 0 | 0 | 3 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 49 | 206 | 0 | 93 | 207 | 0 | 78 | 361 | 0 | 70 | 515 | 0 |
| Confl. Peds. (#/hr) | 3 | | 2 | 2 | | 3 | 45 | | 16 | 16 | | 45 |
| Turn Type | Split | | | Split | | | Prot | | | Prot | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 21.0 | 21.0 | | 20.6 | 20.6 | | 9.5 | 66.4 | | 9.5 | 66.4 | |
| Effective Green, g (s) | 21.5 | 21.5 | | 21.1 | 21.1 | | 10.0 | 67.9 | | 10.0 | 67.9 | |
| Actuated g/C Ratio | 0.16 | 0.16 | | 0.16 | 0.16 | | 0.08 | 0.51 | | 0.08 | 0.51 | |
| Clearance Time (s) | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 4.5 | | 3.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 287 | 270 | | 282 | 269 | | 134 | 1777 | | 134 | 1782 | |
| v/s Ratio Prot | 0.03 | c0.12 | | 0.05 | c0.12 | | c0.04 | 0.10 | | c0.04 | c0.15 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.17 | 0.76 | | 0.33 | 0.77 | | 0.58 | 0.20 | | 0.52 | 0.29 | |
| Uniform Delay, d1 | 47.8 | 53.1 | | 49.4 | 53.4 | | 59.2 | 17.6 | | 59.0 | 18.5 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 12.0 | | 0.7 | 12.4 | | 6.3 | 0.3 | | 3.6 | 0.4 | |
| Delay (s) | 48.1 | 65.0 | | 50.1 | 65.8 | | 65.5 | 17.8 | | 62.6 | 18.9 | |
| Level of Service | D | E | | D | E | | E | B | | E | B | |
| Approach Delay (s) | | 62.2 | | | 61.3 | | | 26.3 | | | 24.1 | |
| Approach LOS | | E | | | E | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 38.8 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.51 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 132.5 | | | Sum of lost time (s) | | | | 15.0 | | |
| Intersection Capacity Utilization | | | 54.2% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
18: Sterling Hill Dr. & Hillcrest Ave

























Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1661 | | 1767 | 1863 | 1583 | 1770 | 3539 | 1545 | 1770 | 3446 | |
| Flt Permitted | 0.69 | 1.00 | | 0.46 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1280 | 1661 | | 855 | 1863 | 1583 | 1770 | 3539 | 1545 | 1770 | 3446 | |
| Volume (vph) | 150 | 50 | 100 | 48 | 67 | 155 | 67 | 372 | 25 | 74 | 377 | 80 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 169 | 56 | 112 | 54 | 75 | 174 | 75 | 418 | 28 | 83 | 424 | 90 |
| RTOR Reduction (vph) | 0 | 91 | 0 | 0 | 0 | 142 | 0 | 0 | 0 | 0 | 10 | 0 |
| Lane Group Flow (vph) | 169 | 77 | 0 | 54 | 75 | 32 | 75 | 418 | 28 | 83 | 504 | 0 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | 9 | 9 | | |
| Turn Type | Perm | | | Perm | | Perm | Prot | | Free | Prot | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | | | Free | | | |
| Actuated Green, G (s) | 16.9 | 16.9 | | 16.9 | 16.9 | 16.9 | 8.3 | 59.8 | 100.0 | 8.8 | 60.3 | |
| Effective Green, g (s) | 18.4 | 18.4 | | 18.4 | 18.4 | 18.4 | 9.3 | 62.8 | 100.0 | 9.8 | 63.3 | |
| Actuated g/C Ratio | 0.18 | 0.18 | | 0.18 | 0.18 | 0.18 | 0.09 | 0.63 | 1.00 | 0.10 | 0.63 | |
| Clearance Time (s) | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.5 | 3.5 | 3.5 | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 236 | 306 | | 157 | 343 | 291 | 165 | 2222 | 1545 | 173 | 2181 | |
| v/s Ratio Prot | | 0.05 | | | 0.04 | | 0.04 | 0.12 | | c0.05 | c0.15 | |
| v/s Ratio Perm | c0.13 | | | 0.06 | | 0.02 | | | c0.02 | | | |
| v/c Ratio | 0.72 | 0.25 | | 0.34 | 0.22 | 0.11 | 0.45 | 0.19 | 0.02 | 0.48 | 0.23 | |
| Uniform Delay, d1 | 38.3 | 34.9 | | 35.5 | 34.7 | 34.0 | 42.9 | 7.8 | 0.0 | 42.7 | 7.9 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.14 | 0.44 | |
| Incremental Delay, d2 | 9.9 | 0.4 | | 1.6 | 0.4 | 0.2 | 2.0 | 0.2 | 0.0 | 2.0 | 0.2 | |
| Delay (s) | 48.2 | 35.3 | | 37.1 | 35.1 | 34.2 | 44.9 | 8.0 | 0.0 | 50.6 | 3.7 | |
| Level of Service | D | D | | D | D | C | D | A | A | D | A | |
| Approach Delay (s) | | 41.8 | | | 34.9 | | | 12.9 | | | 10.2 | |
| Approach LOS | | D | | | C | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.3 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.35 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | | Sum of lost time (s) | | | 6.0 | | |
| Intersection Capacity Utilization | | | 51.4% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
8: Lone Tree Way & Canada Valley




















Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 3433 | 5085 | 1547 | 3433 | 1628 | 1504 | 1770 | 1863 | 1558 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 3433 | 5085 | 1547 | 3433 | 1628 | 1504 | 1770 | 1863 | 1558 |
| Volume (vph) | 54 | 1354 | 55 | 329 | 942 | 253 | 84 | 55 | 173 | 175 | 56 | 22 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 56 | 1410 | 57 | 343 | 981 | 264 | 88 | 57 | 180 | 182 | 58 | 23 |
| RTOR Reduction (vph) | 0 | 0 | 13 | 0 | 0 | 104 | 0 | 40 | 101 | 0 | 0 | 20 |
| Lane Group Flow (vph) | 56 | 1410 | 44 | 343 | 981 | 160 | 88 | 82 | 14 | 182 | 58 | 3 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 4 | | | | | 4 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 8.0 | 66.2 | 66.2 | 17.5 | 75.7 | 75.7 | 11.0 | 14.4 | 14.4 | 13.9 | 17.3 | 17.3 |
| Effective Green, g (s) | 9.0 | 69.2 | 69.2 | 18.5 | 78.7 | 78.7 | 12.0 | 15.4 | 15.4 | 14.9 | 18.3 | 18.3 |
| Actuated g/C Ratio | 0.07 | 0.53 | 0.53 | 0.14 | 0.61 | 0.61 | 0.09 | 0.12 | 0.12 | 0.11 | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 6.0 | 6.0 | 2.0 | 2.0 | 2.0 | 2.0 | 6.0 | 6.0 |
| Lane Grp Cap (vph) | 123 | 2707 | 831 | 489 | 3078 | 937 | 317 | 193 | 178 | 203 | 262 | 219 |
| v/s Ratio Prot | 0.03 | c0.28 | | c0.10 | 0.19 | | 0.03 | c0.05 | | c0.10 | c0.03 | |
| v/s Ratio Perm | | | 0.03 | | | 0.10 | | | 0.01 | | | 0.00 |
| v/c Ratio | 0.46 | 0.52 | 0.05 | 0.70 | 0.32 | 0.17 | 0.28 | 0.43 | 0.08 | 0.90 | 0.22 | 0.01 |
| Uniform Delay, d1 | 58.1 | 19.7 | 14.6 | 53.1 | 12.5 | 11.3 | 55.0 | 53.2 | 51.0 | 56.8 | 49.5 | 48.1 |
| Progression Factor | 0.89 | 0.81 | 1.00 | 1.23 | 0.58 | 0.51 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.7 | 0.5 | 0.1 | 3.5 | 0.3 | 0.4 | 0.2 | 0.6 | 0.1 | 35.1 | 1.2 | 0.1 |
| Delay (s) | 52.6 | 16.5 | 14.8 | 68.7 | 7.6 | 6.1 | 55.1 | 53.8 | 51.0 | 91.9 | 50.7 | 48.2 |
| Level of Service | D | B | B | E | A | A | E | D | D | F | D | D |
| Approach Delay (s) | | 17.7 | | | 20.5 | | | 53.2 | | | 79.0 | |
| Approach LOS | | B | | | C | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.4 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 15.0 | | |
| Intersection Capacity Utilization | | | 63.7% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 9: Lone Tree Way & SB Off-Ramp













Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  |  |  |  | | | | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Volume (vph) | 0 | 1169 | 541 | 98 | 1153 | 0 | 0 | 0 | 0 | 416 | 10 | 361 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1231 | 569 | 103 | 1214 | 0 | 0 | 0 | 0 | 438 | 11 | 380 |
| RTOR Reduction (vph) | 0 | 0 | 228 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 |
| Lane Group Flow (vph) | 0 | 1231 | 341 | 103 | 1214 | 0 | 0 | 0 | 0 | 219 | 230 | 347 |
| Confl. Peds. (#/hr) | | | | | | | 3 | | 3 | | | |
| Turn Type | | Perm | | Prot | | | | | | Perm | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | | 4 | |
| Permitted Phases | | 2 | | | | | | | | 4 | 4 | |
| Actuated Green, G (s) | | 75.3 | 75.3 | 9.0 | 88.3 | | | | | 32.2 | 32.2 | 32.2 |
| Effective Green, g (s) | | 77.8 | 77.8 | 10.0 | 90.8 | | | | | 33.2 | 33.2 | 33.2 |
| Actuated g/C Ratio | | 0.60 | 0.60 | 0.08 | 0.70 | | | | | 0.26 | 0.26 | 0.26 |
| Clearance Time (s) | | 5.5 | 5.5 | 4.0 | 5.5 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 3.0 | 4.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 3043 | 947 | 264 | 3552 | | | | | 429 | 431 | 404 |
| v/s Ratio Prot | | c0.24 | | c0.03 | | 0.24 | | | | | | |
| v/s Ratio Perm | | 0.22 | | | | | | | | 0.13 | 0.14 | c0.22 |
| v/c Ratio | | 0.40 | 0.36 | 0.39 | 0.34 | | | | | 0.51 | 0.53 | 0.86 |
| Uniform Delay, d1 | | 13.8 | 13.4 | 57.1 | 7.8 | | | | | 41.4 | 41.7 | 46.2 |
| Progression Factor | | 0.66 | 1.52 | 1.27 | 0.39 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.3 | 0.9 | 0.9 | 0.3 | | | | | 1.0 | 1.3 | 16.4 |
| Delay (s) | | 9.4 | 21.2 | 73.5 | 3.3 | | | | | 42.5 | 43.0 | 62.6 |
| Level of Service | | A | C | E | A | | | | | D | D | E |
| Approach Delay (s) | | 13.2 | | 8.8 | | | 0.0 | | | 51.9 | | |
| Approach LOS | | B | | A | | | A | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 19.8 | | HCM Level of Service | | B | | | | | | |
| HCM Volume to Capacity ratio | | 0.53 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | Sum of lost time (s) | | 9.0 | | | | | | |
| Intersection Capacity Utilization | | 58.6% | | ICU Level of Service | | B | | | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group
























HCM Signalized Intersection Capacity Analysis
10: Lone Tree Way & NB On-ramp

Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1699 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1699 | 1583 | | | |
| Volume (vph) | 0 | 1404 | 264 | 21 | 831 | 357 | 437 | 43 | 137 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 0 | 1543 | 290 | 23 | 913 | 392 | 480 | 47 | 151 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 87 | 0 | 0 | 93 | 0 | 0 | 122 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1543 | 203 | 23 | 913 | 299 | 257 | 270 | 29 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Split | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | 8 | 8 | | | | |
| Permitted Phases | | 2 | | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | | 88.2 | 88.2 | 4.1 | 96.3 | 96.3 | 23.7 | 23.7 | 23.7 | | | |
| Effective Green, g (s) | | 91.2 | 91.2 | 5.1 | 99.3 | 99.3 | 24.7 | 24.7 | 24.7 | | | |
| Actuated g/C Ratio | | 0.70 | 0.70 | 0.04 | 0.76 | 0.76 | 0.19 | 0.19 | 0.19 | | | |
| Clearance Time (s) | | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | | 3567 | 1111 | 69 | 3884 | 1209 | 319 | 323 | 301 | | | |
| v/s Ratio Prot | | c0.30 | | c0.01 | 0.18 | | 0.15 | c0.16 | | | | |
| v/s Ratio Perm | | 0.13 | | | | 0.19 | | | 0.02 | | | |
| v/c Ratio | | 0.43 | 0.18 | 0.33 | 0.24 | 0.25 | 0.81 | 0.84 | 0.10 | | | |
| Uniform Delay, d1 | | 8.3 | 6.6 | 60.8 | 4.4 | 4.5 | 50.4 | 50.7 | 43.4 | | | |
| Progression Factor | | 0.38 | 0.42 | 0.98 | 0.93 | 1.30 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.4 | 0.3 | 1.0 | 0.1 | 0.5 | 13.0 | 16.2 | 0.1 | | | |
| Delay (s) | | 3.5 | 3.2 | 60.3 | 4.2 | 6.3 | 63.4 | 66.9 | 43.5 | | | |
| Level of Service | | A | A | E | A | A | E | E | D | | | |
| Approach Delay (s) | | 3.5 | | | 5.8 | | | 60.3 | | | 0.0 | |
| Approach LOS | | A | | | A | | | E | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 14.3 | | HCM Level of Service | | | | | B | | | |
| HCM Volume to Capacity ratio | | 0.51 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | Sum of lost time (s) | | | | | 9.0 | | | |
| Intersection Capacity Utilization | | 47.0% | | ICU Level of Service | | | | | A | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
11: Lone Tree Way & Slaten Ranch

































Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1549 | 1770 | 3539 | 1561 | 3433 | 3174 | | 3433 | 1863 | 1561 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1549 | 1770 | 3539 | 1561 | 3433 | 3174 | | 3433 | 1863 | 1561 |
| Volume (vph) | 217 | 892 | 256 | 160 | 803 | 55 | 51 | 76 | 167 | 114 | 67 | 101 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 231 | 949 | 272 | 170 | 854 | 59 | 54 | 81 | 178 | 121 | 71 | 107 |
| RTOR Reduction (vph) | 0 | 0 | 118 | 0 | 0 | 24 | 0 | 155 | 0 | 0 | 0 | 90 |
| Lane Group Flow (vph) | 231 | 949 | 154 | 170 | 854 | 35 | 54 | 104 | 0 | 121 | 71 | 17 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 2 | | | | | 2 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 13.2 | 70.5 | 70.5 | 16.1 | 73.4 | 73.4 | 6.3 | 15.6 | | 9.8 | 19.1 | 19.1 |
| Effective Green, g (s) | 14.2 | 73.5 | 73.5 | 17.1 | 76.4 | 76.4 | 7.3 | 16.6 | | 10.8 | 20.1 | 20.1 |
| Actuated g/C Ratio | 0.11 | 0.57 | 0.57 | 0.13 | 0.59 | 0.59 | 0.06 | 0.13 | | 0.08 | 0.15 | 0.15 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 3.0 | 4.0 | | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 375 | 2875 | 876 | 233 | 2080 | 917 | 193 | 405 | | 285 | 288 | 241 |
| v/s Ratio Prot | 0.07 | 0.19 | | c0.10 | c0.24 | | c0.02 | c0.03 | | c0.04 | 0.04 | |
| v/s Ratio Perm | | | 0.10 | | | 0.02 | | | | | | 0.01 |
| v/c Ratio | 0.62 | 0.33 | 0.18 | 0.73 | 0.41 | 0.04 | 0.28 | 0.26 | | 0.42 | 0.25 | 0.07 |
| Uniform Delay, d1 | 55.3 | 15.1 | 13.6 | 54.2 | 14.6 | 11.3 | 58.8 | 51.1 | | 56.6 | 48.3 | 47.0 |
| Progression Factor | 0.95 | 0.93 | 1.92 | 1.04 | 1.16 | 2.27 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.0 | 0.3 | 0.4 | 9.0 | 0.6 | 0.1 | 0.8 | 0.5 | | 0.4 | 0.2 | 0.0 |
| Delay (s) | 55.6 | 14.4 | 26.6 | 65.2 | 17.5 | 25.8 | 59.6 | 51.6 | | 57.0 | 48.5 | 47.0 |
| Level of Service | E | B | C | E | B | C | E | D | | E | D | D |
| Approach Delay (s) | | 23.2 | | | 25.4 | | | 53.0 | | | 51.4 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 29.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 61.4% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
12: Lone Tree Way & Empire Ave

























Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |   |  |   |  |  |    |    |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.99 | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.91 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 1770 | 3539 | 1540 | 3433 | 1863 | 1562 | 3433 | 3187 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 1770 | 3539 | 1540 | 3433 | 1863 | 1562 | 3433 | 3187 | |
| Volume (vph) | 230 | 759 | 112 | 53 | 702 | 129 | 76 | 46 | 36 | 231 | 115 | 176 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 235 | 774 | 114 | 54 | 716 | 132 | 78 | 47 | 37 | 236 | 117 | 180 |
| RTOR Reduction (vph) | 0 | 0 | 43 | 0 | 0 | 63 | 0 | 0 | 34 | 0 | 157 | 0 |
| Lane Group Flow (vph) | 235 | 774 | 71 | 54 | 716 | 69 | 78 | 47 | 3 | 236 | 140 | 0 |
| Confl. Peds. (#/hr) | 3 | | 1 | 1 | | 3 | 3 | | 1 | 1 | | 3 |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | Perm | Split | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 20.6 | 80.4 | 80.4 | 7.0 | 66.8 | 66.8 | 10.9 | 10.9 | 10.9 | 15.7 | 15.7 | |
| Effective Green, g (s) | 21.6 | 81.4 | 81.4 | 8.0 | 67.8 | 67.8 | 11.9 | 11.9 | 11.9 | 16.7 | 16.7 | |
| Actuated g/C Ratio | 0.17 | 0.63 | 0.63 | 0.06 | 0.52 | 0.52 | 0.09 | 0.09 | 0.09 | 0.13 | 0.13 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 294 | 3184 | 978 | 109 | 1846 | 803 | 314 | 171 | 143 | 441 | 409 | |
| v/s Ratio Prot | c0.13 | 0.15 | | 0.03 | c0.20 | | 0.02 | c0.03 | | c0.07 | 0.04 | |
| v/s Ratio Perm | | | 0.05 | | | 0.04 | | | 0.00 | | | |
| v/c Ratio | 0.80 | 0.24 | 0.07 | 0.50 | 0.39 | 0.09 | 0.25 | 0.27 | 0.02 | 0.54 | 0.34 | |
| Uniform Delay, d1 | 52.1 | 10.7 | 9.5 | 59.0 | 18.7 | 15.6 | 54.9 | 55.0 | 53.8 | 53.0 | 51.6 | |
| Progression Factor | 1.36 | 0.57 | 0.30 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 12.8 | 0.2 | 0.1 | 1.3 | 0.6 | 0.2 | 0.2 | 0.3 | 0.0 | 0.6 | 0.2 | |
| Delay (s) | 83.8 | 6.3 | 3.0 | 60.3 | 19.3 | 15.8 | 55.0 | 55.3 | 53.8 | 53.6 | 51.8 | |
| Level of Service | F | A | A | E | B | B | E | E | D | D | D | |
| Approach Delay (s) | | 22.2 | | | 21.2 | | | 54.8 | | | 52.6 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 29.8 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.47 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 62.6% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

























HCM Signalized Intersection Capacity Analysis
13: Lone Tree Way & Deer Valley Rd.

Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3539 | 1436 | 1770 | 3539 | 1531 | 3433 | 3347 | | 2000 | 3498 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3539 | 1436 | 1770 | 3539 | 1531 | 3433 | 3347 | | 1770 | 3498 | |
| Volume (vph) | 87 | 780 | 147 | 151 | 497 | 154 | 192 | 365 | 168 | 168 | 191 | 14 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 90 | 804 | 152 | 156 | 512 | 159 | 198 | 376 | 173 | 173 | 197 | 14 |
| RTOR Reduction (vph) | 0 | 0 | 32 | 0 | 0 | 54 | 0 | 43 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 90 | 804 | 120 | 156 | 512 | 105 | 198 | 506 | 0 | 173 | 206 | 0 |
| Confl. Peds. (#/hr) | 12 | | | 54 | | 12 | 11 | | 8 | 8 | | 11 |
| Confl. Bikes (#/hr) | | | 11 | | | 9 | | | | | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | |
| Actuated Green, G (s) | 11.8 | 54.1 | 54.1 | 16.3 | 58.6 | 58.6 | 12.5 | 24.0 | | 17.1 | 28.6 | |
| Effective Green, g (s) | 13.3 | 56.1 | 56.1 | 17.8 | 60.6 | 60.6 | 14.0 | 25.5 | | 18.6 | 30.1 | |
| Actuated g/C Ratio | 0.10 | 0.43 | 0.43 | 0.14 | 0.47 | 0.47 | 0.11 | 0.20 | | 0.14 | 0.23 | |
| Clearance Time (s) | 4.5 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 3.0 | 3.0 | | 4.0 | 3.0 | |
| Lane Grp Cap (vph) | 181 | 1527 | 620 | 242 | 1650 | 714 | 370 | 657 | | 286 | 810 | |
| v/s Ratio Prot | 0.05 | c0.23 | | c0.09 | 0.14 | | 0.06 | c0.15 | | c0.09 | 0.06 | |
| v/s Ratio Perm | | | 0.08 | | | 0.07 | | | | | | |
| v/c Ratio | 0.50 | 0.53 | 0.19 | 0.64 | 0.31 | 0.15 | 0.54 | 0.77 | | 0.60 | 0.25 | |
| Uniform Delay, d1 | 55.2 | 27.2 | 22.9 | 53.1 | 21.7 | 19.9 | 54.9 | 49.5 | | 52.3 | 40.8 | |
| Progression Factor | 1.41 | 0.64 | 0.68 | 0.97 | 1.73 | 2.83 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.9 | 1.1 | 0.6 | 4.9 | 0.4 | 0.4 | 1.5 | 5.6 | | 4.1 | 0.2 | |
| Delay (s) | 79.8 | 18.4 | 16.1 | 56.1 | 37.8 | 56.7 | 56.4 | 55.1 | | 56.4 | 41.0 | |
| Level of Service | E | B | B | E | D | E | E | E | | E | D | |
| Approach Delay (s) | | 23.3 | | | 44.9 | | | 55.4 | | | 47.9 | |
| Approach LOS | | C | | | D | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 40.4 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 70.8% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |





















HCM Signalized Intersection Capacity Analysis
14: Lone Tree Way & Hillcrest Ave.

Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.96 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.97 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1521 | 1770 | 5085 | 1520 | 1770 | 3388 | | 2000 | 3271 | 1533 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1521 | 1770 | 5085 | 1520 | 1770 | 3388 | | 1610 | 3271 | 1533 |
| Volume (vph) | 131 | 915 | 22 | 43 | 720 | 229 | 17 | 87 | 26 | 423 | 77 | 97 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 149 | 1040 | 25 | 49 | 818 | 260 | 19 | 99 | 30 | 481 | 88 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 152 | 0 | 25 | 0 | 0 | 0 | 89 |
| Lane Group Flow (vph) | 149 | 1040 | 16 | 49 | 818 | 108 | 19 | 104 | 0 | 241 | 328 | 21 |
| Confl. Peds. (#/hr) | 18 | | 20 | 20 | | 18 | 14 | | 16 | 16 | | 14 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 1 | | | 1 |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 17.3 | 64.7 | 64.7 | 5.2 | 52.1 | 52.1 | 17.4 | 17.4 | | 23.2 | 23.2 | 23.2 |
| Effective Green, g (s) | 19.3 | 66.7 | 66.7 | 6.7 | 54.1 | 54.1 | 19.4 | 19.4 | | 25.2 | 25.2 | 25.2 |
| Actuated g/C Ratio | 0.15 | 0.51 | 0.51 | 0.05 | 0.42 | 0.42 | 0.15 | 0.15 | | 0.19 | 0.19 | 0.19 |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 263 | 1816 | 780 | 91 | 2116 | 633 | 264 | 506 | | 388 | 634 | 297 |
| v/s Ratio Prot | c0.08 | c0.29 | | 0.03 | 0.16 | | 0.01 | c0.03 | | c0.12 | 0.10 | |
| v/s Ratio Perm | | | 0.01 | | | 0.07 | | | | | | 0.01 |
| v/c Ratio | 0.57 | 0.57 | 0.02 | 0.54 | 0.39 | 0.17 | 0.07 | 0.21 | | 0.62 | 0.52 | 0.07 |
| Uniform Delay, d1 | 51.5 | 21.8 | 15.6 | 60.1 | 26.4 | 23.9 | 47.6 | 48.5 | | 48.0 | 47.0 | 42.8 |
| Progression Factor | 0.87 | 0.61 | 0.35 | 1.14 | 0.87 | 0.99 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 4.1 | 1.2 | 0.0 | 5.2 | 0.5 | 0.5 | 0.2 | 0.4 | | 4.3 | 1.4 | 0.2 |
| Delay (s) | 48.6 | 14.5 | 5.5 | 73.6 | 23.4 | 24.1 | 47.8 | 49.0 | | 52.4 | 48.4 | 43.1 |
| Level of Service | D | B | A | E | C | C | D | D | | D | D | D |
| Approach Delay (s) | | 18.5 | | | 25.7 | | | 48.8 | | | 48.9 | |
| Approach LOS | | B | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 29.0 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.52 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 62.0% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
15: Lone Tree Way & Vista Grande





















Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5055 | | 1770 | 5062 | | 1767 | 1605 | | 1770 | 1652 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.74 | 1.00 | | 0.40 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5055 | | 1770 | 5062 | | 1372 | 1605 | | 742 | 1652 | |
| Volume (vph) | 18 | 1282 | 44 | 121 | 931 | 24 | 35 | 10 | 114 | 42 | 9 | 20 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 19 | 1322 | 45 | 125 | 960 | 25 | 36 | 10 | 118 | 43 | 9 | 21 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 105 | 0 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 19 | 1365 | 0 | 125 | 984 | 0 | 36 | 23 | 0 | 43 | 11 | 0 |
| Confl. Peds. (#/hr) | 4 | | 4 | 4 | | 4 | 1 | | | | | 1 |
| Turn Type | Prot | | | Prot | | | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 3.7 | 87.4 | | 15.3 | 99.0 | | 12.8 | 12.8 | | 12.8 | 12.8 | |
| Effective Green, g (s) | 5.2 | 89.9 | | 16.8 | 101.5 | | 14.3 | 14.3 | | 14.3 | 14.3 | |
| Actuated g/C Ratio | 0.04 | 0.69 | | 0.13 | 0.78 | | 0.11 | 0.11 | | 0.11 | 0.11 | |
| Clearance Time (s) | 4.5 | 5.5 | | 4.5 | 5.5 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 4.0 | 6.0 | | 4.0 | 6.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 71 | 3496 | | 229 | 3952 | | 151 | 177 | | 82 | 182 | |
| v/s Ratio Prot | 0.01 | c0.27 | | c0.07 | 0.19 | | | 0.01 | | | 0.01 | |
| v/s Ratio Perm | | | | | | | 0.03 | | | c0.06 | | |
| v/c Ratio | 0.27 | 0.39 | | 0.55 | 0.25 | | 0.24 | 0.13 | | 0.52 | 0.06 | |
| Uniform Delay, d1 | 60.6 | 8.5 | | 53.0 | 3.9 | | 52.9 | 52.2 | | 54.6 | 51.8 | |
| Progression Factor | 0.92 | 0.82 | | 0.96 | 1.43 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.1 | 0.3 | | 2.4 | 0.1 | | 0.8 | 0.3 | | 5.9 | 0.1 | |
| Delay (s) | 57.9 | 7.2 | | 53.2 | 5.7 | | 53.7 | 52.6 | | 60.6 | 52.0 | |
| Level of Service | E | A | | D | A | | D | D | | E | D | |
| Approach Delay (s) | | 7.9 | | | 11.0 | | | 52.8 | | | 57.0 | |
| Approach LOS | | A | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 13.2 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 56.7% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
16: Country Hills Dr. & Hillcrest Ave
























Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.91 | | 1.00 | 0.93 | | 1.00 | 0.98 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1690 | | 1770 | 1710 | | 1770 | 3442 | | 1770 | 3427 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1690 | | 1770 | 1710 | | 1770 | 3442 | | 1770 | 3427 | |
| Volume (vph) | 42 | 51 | 82 | 34 | 50 | 45 | 73 | 281 | 49 | 89 | 376 | 63 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 46 | 55 | 89 | 37 | 54 | 49 | 79 | 305 | 53 | 97 | 409 | 68 |
| RTOR Reduction (vph) | 0 | 36 | 0 | 0 | 20 | 0 | 0 | 5 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 46 | 108 | 0 | 37 | 83 | 0 | 79 | 353 | 0 | 97 | 472 | 0 |
| Confl. Peds. (#/hr) | 10 | | | | | 10 | 20 | | 7 | 7 | | 20 |
| Turn Type | Split | | | Split | | | Prot | | | Prot | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 12.3 | 12.3 | | 9.4 | 9.4 | | 8.9 | 69.2 | | 9.9 | 70.2 | |
| Effective Green, g (s) | 12.8 | 12.8 | | 9.9 | 9.9 | | 9.4 | 70.7 | | 10.4 | 71.7 | |
| Actuated g/C Ratio | 0.11 | 0.11 | | 0.09 | 0.09 | | 0.08 | 0.61 | | 0.09 | 0.62 | |
| Clearance Time (s) | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 4.5 | | 3.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 196 | 187 | | 151 | 146 | | 144 | 2101 | | 159 | 2122 | |
| v/s Ratio Prot | 0.03 | c0.06 | | 0.02 | c0.05 | | c0.04 | 0.10 | | c0.05 | c0.14 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.23 | 0.58 | | 0.25 | 0.57 | | 0.55 | 0.17 | | 0.61 | 0.22 | |
| Uniform Delay, d1 | 47.0 | 48.9 | | 49.5 | 50.9 | | 51.2 | 9.8 | | 50.7 | 9.7 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.6 | 4.2 | | 0.8 | 5.0 | | 4.2 | 0.2 | | 6.8 | 0.2 | |
| Delay (s) | 47.6 | 53.1 | | 50.3 | 55.9 | | 55.4 | 10.0 | | 57.5 | 10.0 | |
| Level of Service | D | D | | D | E | | E | A | | E | A | |
| Approach Delay (s) | | 51.8 | | | 54.4 | | | 18.2 | | | 18.0 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.7 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.37 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 115.8 | | | Sum of lost time (s) | | | 15.0 | | | |
| Intersection Capacity Utilization | | | 51.3% | | | ICU Level of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
18: Laurel Rd. & Hillcrest Ave

Davidon EIR
Existing PM Peak Hour
































| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.89 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1634 | | 1768 | 1863 | 1583 | 1770 | 3539 | 1550 | 1770 | 3479 | |
| Flt Permitted | 0.75 | 1.00 | | 0.74 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1400 | 1634 | | 1374 | 1863 | 1583 | 1770 | 3539 | 1550 | 1770 | 3479 | |
| Volume (vph) | 17 | 7 | 22 | 35 | 9 | 133 | 27 | 302 | 39 | 162 | 459 | 50 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 17 | 7 | 22 | 36 | 9 | 136 | 28 | 308 | 40 | 165 | 468 | 51 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 0 | 0 | 123 | 0 | 0 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 17 | 9 | 0 | 36 | 9 | 13 | 28 | 308 | 40 | 165 | 516 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | 2 | | 2 | 2 | | 2 |
| Turn Type | Perm | | | Perm | | Perm | Prot | | Free | Prot | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | | | Free | | | |
| Actuated Green, G (s) | 8.4 | 8.4 | | 8.4 | 8.4 | 8.4 | 3.4 | 62.6 | 100.0 | 14.5 | 73.7 | |
| Effective Green, g (s) | 9.9 | 9.9 | | 9.9 | 9.9 | 9.9 | 4.4 | 65.6 | 100.0 | 15.5 | 76.7 | |
| Actuated g/C Ratio | 0.10 | 0.10 | | 0.10 | 0.10 | 0.10 | 0.04 | 0.66 | 1.00 | 0.16 | 0.77 | |
| Clearance Time (s) | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.5 | 3.5 | 3.5 | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 139 | 162 | | 136 | 184 | 157 | 78 | 2322 | 1550 | 274 | 2668 | |
| v/s Ratio Prot | | 0.01 | | | 0.00 | | 0.02 | 0.09 | | c0.09 | c0.15 | |
| v/s Ratio Perm | 0.01 | | | c0.03 | | 0.01 | | | 0.03 | | | |
| v/c Ratio | 0.12 | 0.06 | | 0.26 | 0.05 | 0.09 | 0.36 | 0.13 | 0.03 | 0.60 | 0.19 | |
| Uniform Delay, d1 | 41.1 | 40.8 | | 41.7 | 40.8 | 40.9 | 46.4 | 6.5 | 0.0 | 39.4 | 3.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.23 | 0.15 | |
| Incremental Delay, d2 | 0.4 | 0.1 | | 1.2 | 0.1 | 0.3 | 2.8 | 0.1 | 0.0 | 3.4 | 0.1 | |
| Delay (s) | 41.5 | 41.0 | | 42.9 | 40.9 | 41.2 | 49.2 | 6.6 | 0.0 | 51.7 | 0.6 | |
| Level of Service | D | D | | D | D | D | D | A | A | D | A | |
| Approach Delay (s) | | 41.2 | | | 41.5 | | | 9.1 | | | 12.9 | |
| Approach LOS | | D | | | D | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 16.8 | | | | HCM Level of Service | | | B | | |
| HCM Volume to Capacity ratio | | | 0.27 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | | Sum of lost time (s) | | | 6.0 | | |
| Intersection Capacity Utilization | | | 48.4% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

Near-Term No Project

HCM Signalized Intersection Capacity Analysis 8: Lone Tree Way & Canada Valley


Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |   |    |  |   |  |  |  |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.87 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1540 | 1504 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1540 | 1504 | 1770 | 1863 | 1583 |
| Volume (vph) | 29 | 971 | 65 | 211 | 1119 | 168 | 76 | 14 | 184 | 190 | 31 | 34 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 32 | 1079 | 72 | 234 | 1243 | 187 | 84 | 16 | 204 | 211 | 34 | 38 |
| RTOR Reduction (vph) | 0 | 0 | 17 | 0 | 0 | 65 | 0 | 95 | 95 | 0 | 0 | 33 |
| Lane Group Flow (vph) | 32 | 1079 | 55 | 234 | 1243 | 122 | 84 | 23 | 7 | 211 | 34 | 5 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 3.6 | 71.9 | 71.9 | 13.3 | 81.6 | 81.6 | 9.7 | 7.8 | 7.8 | 19.0 | 17.1 | 17.1 |
| Effective Green, g (s) | 4.6 | 74.9 | 74.9 | 14.3 | 84.6 | 84.6 | 10.7 | 8.8 | 8.8 | 20.0 | 18.1 | 18.1 |
| Actuated g/C Ratio | 0.04 | 0.58 | 0.58 | 0.11 | 0.65 | 0.65 | 0.08 | 0.07 | 0.07 | 0.15 | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 6.0 | 6.0 | 2.0 | 2.0 | 2.0 | 2.0 | 6.0 | 6.0 |
| Lane Grp Cap (vph) | 63 | 2930 | 912 | 378 | 3309 | 1030 | 283 | 104 | 102 | 272 | 259 | 220 |
| v/s Ratio Prot | 0.02 | c0.21 | | c0.07 | c0.24 | | 0.02 | c0.01 | | c0.12 | 0.02 | |
| v/s Ratio Perm | | | 0.03 | | | 0.08 | | | 0.00 | | | 0.00 |
| v/c Ratio | 0.51 | 0.37 | 0.06 | 0.62 | 0.38 | 0.12 | 0.30 | 0.22 | 0.07 | 0.78 | 0.13 | 0.02 |
| Uniform Delay, d1 | 61.6 | 14.8 | 12.1 | 55.2 | 10.5 | 8.6 | 56.1 | 57.4 | 56.8 | 52.8 | 49.1 | 48.3 |
| Progression Factor | 0.83 | 0.59 | 0.46 | 1.25 | 0.61 | 0.68 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.0 | 0.3 | 0.1 | 1.9 | 0.3 | 0.2 | 0.2 | 0.4 | 0.1 | 11.9 | 0.7 | 0.1 |
| Delay (s) | 53.2 | 9.0 | 5.7 | 71.2 | 6.7 | 6.0 | 56.3 | 57.7 | 56.9 | 64.7 | 49.7 | 48.4 |
| Level of Service | D | A | A | E | A | A | E | E | E | E | D | D |
| Approach Delay (s) | | 10.0 | | | 15.7 | | | 57.1 | | | 60.7 | |
| Approach LOS | | B | | | B | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.1 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 9.0 | | |
| Intersection Capacity Utilization | | | 52.1% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Lone Tree Way & SR-4 Bypass SB Off-Ramp













Davidon EIR
Near-Term No Project AM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|------|-------|------|-------|----------------------|------|------|------|------|------|-------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Volume (vph) | 0 | 848 | 483 | 72 | 1102 | 0 | 0 | 0 | 0 | 287 | 6 | 410 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 942 | 537 | 80 | 1224 | 0 | 0 | 0 | 0 | 319 | 7 | 456 |
| RTOR Reduction (vph) | 0 | 0 | 234 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 |
| Lane Group Flow (vph) | 0 | 942 | 303 | 80 | 1224 | 0 | 0 | 0 | 0 | 160 | 166 | 422 |
| Confl. Peds. (#/hr) | | | | | | | 2 | | | | | |
| Turn Type | | Perm | | Prot | | | | | | Perm | | Perm |
| Protected Phases | | 2 | | 1 | 6 | | | | | | 4 | |
| Permitted Phases | | | 2 | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 70.8 | 70.8 | 7.0 | 81.8 | | | | | 38.7 | 38.7 | 38.7 |
| Effective Green, g (s) | | 73.3 | 73.3 | 8.0 | 84.3 | | | | | 39.7 | 39.7 | 39.7 |
| Actuated g/C Ratio | | 0.56 | 0.56 | 0.06 | 0.65 | | | | | 0.31 | 0.31 | 0.31 |
| Clearance Time (s) | | 5.5 | 5.5 | 4.0 | 5.5 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 3.0 | 4.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2867 | 893 | 211 | 3297 | | | | | 513 | 516 | 483 |
| v/s Ratio Prot | | 0.19 | | 0.02 | c0.24 | | | | | | | |
| v/s Ratio Perm | | | 0.19 | | | | | | | 0.10 | 0.10 | c0.27 |
| v/c Ratio | | 0.33 | 0.34 | 0.38 | 0.37 | | | | | 0.31 | 0.32 | 0.87 |
| Uniform Delay, d1 | | 15.2 | 15.3 | 58.6 | 10.6 | | | | | 34.7 | 34.8 | 42.8 |
| Progression Factor | | 0.73 | 0.73 | 1.32 | 0.40 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.3 | 1.0 | 1.1 | 0.3 | | | | | 0.3 | 0.4 | 15.9 |
| Delay (s) | | 11.3 | 12.2 | 78.5 | 4.5 | | | | | 35.0 | 35.1 | 58.7 |
| Level of Service | | B | B | E | A | | | | | D | D | E |
| Approach Delay (s) | | 11.6 | | | 9.1 | | | 0.0 | | | 48.9 | |
| Approach LOS | | B | | | A | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 18.8 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.53 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 6.0 | | |
| Intersection Capacity Utilization | | | 53.3% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 10: Lone Tree Way & On-ramp

























Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1696 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1696 | 1583 | | | |
| Volume (vph) | 0 | 792 | 307 | 8 | 738 | 245 | 418 | 29 | 79 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 0 | 890 | 345 | 9 | 829 | 275 | 470 | 33 | 89 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 94 | 0 | 0 | 64 | 0 | 0 | 72 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 890 | 251 | 9 | 829 | 211 | 245 | 258 | 17 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Split | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | 8 | 8 | | | | |
| Permitted Phases | | 2 | | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | | 91.5 | 91.5 | 1.2 | 96.7 | 96.7 | 23.3 | 23.3 | 23.3 | | | |
| Effective Green, g (s) | | 94.5 | 94.5 | 2.2 | 99.7 | 99.7 | 24.3 | 24.3 | 24.3 | | | |
| Actuated g/C Ratio | | 0.73 | 0.73 | 0.02 | 0.77 | 0.77 | 0.19 | 0.19 | 0.19 | | | |
| Clearance Time (s) | | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | | 3696 | 1151 | 30 | 3900 | 1214 | 314 | 317 | 296 | | | |
| v/s Ratio Prot | | c0.18 | | c0.01 | 0.16 | | 0.15 | c0.15 | | | | |
| v/s Ratio Perm | | 0.16 | | | | 0.13 | | | 0.01 | | | |
| v/c Ratio | | 0.24 | 0.22 | 0.30 | 0.21 | 0.17 | 0.78 | 0.81 | 0.06 | | | |
| Uniform Delay, d1 | | 5.9 | 5.8 | 63.1 | 4.2 | 4.1 | 50.3 | 50.7 | 43.4 | | | |
| Progression Factor | | 0.43 | 1.15 | 0.68 | 2.07 | 9.02 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.1 | 0.4 | 2.0 | 0.1 | 0.3 | 11.0 | 14.0 | 0.0 | | | |
| Delay (s) | | 2.7 | 7.0 | 45.2 | 8.9 | 37.1 | 61.3 | 64.7 | 43.5 | | | |
| Level of Service | | A | A | D | A | D | E | E | D | | | |
| Approach Delay (s) | | 3.9 | | | 16.1 | | | 60.1 | | | 0.0 | |
| Approach LOS | | A | | | B | | | E | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 19.8 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.36 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | | Sum of lost time (s) | | | 9.0 | | | | |
| Intersection Capacity Utilization | | 34.3% | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Shady Willow Rd














Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1549 | 1770 | 3539 | 1562 | 3433 | 3080 | | 3433 | 1863 | 1563 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1549 | 1770 | 3539 | 1562 | 3433 | 3080 | | 3433 | 1863 | 1563 |
| Volume (vph) | 74 | 614 | 91 | 54 | 904 | 29 | 39 | 47 | 191 | 42 | 35 | 24 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 82 | 682 | 101 | 60 | 1004 | 32 | 43 | 52 | 212 | 47 | 39 | 27 |
| RTOR Reduction (vph) | 0 | 0 | 34 | 0 | 0 | 10 | 0 | 185 | 0 | 0 | 0 | 24 |
| Lane Group Flow (vph) | 82 | 682 | 67 | 60 | 1004 | 22 | 43 | 79 | 0 | 47 | 39 | 3 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 7.2 | 83.5 | 83.5 | 7.7 | 84.0 | 84.0 | 5.9 | 15.4 | | 5.4 | 14.9 | 14.9 |
| Effective Green, g (s) | 8.2 | 86.5 | 86.5 | 8.7 | 87.0 | 87.0 | 6.9 | 16.4 | | 6.4 | 15.9 | 15.9 |
| Actuated g/C Ratio | 0.06 | 0.67 | 0.67 | 0.07 | 0.67 | 0.67 | 0.05 | 0.13 | | 0.05 | 0.12 | 0.12 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 3.0 | 4.0 | | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 217 | 3383 | 1031 | 118 | 2368 | 1045 | 182 | 389 | | 169 | 228 | 191 |
| v/s Ratio Prot | 0.02 | 0.13 | | c0.03 | c0.28 | | c0.01 | c0.03 | | c0.01 | 0.02 | |
| v/s Ratio Perm | | | 0.04 | | | 0.01 | | | | | | 0.00 |
| v/c Ratio | 0.38 | 0.20 | 0.07 | 0.51 | 0.42 | 0.02 | 0.24 | 0.20 | | 0.28 | 0.17 | 0.02 |
| Uniform Delay, d1 | 58.5 | 8.4 | 7.6 | 58.6 | 9.9 | 7.2 | 59.0 | 50.9 | | 59.6 | 51.1 | 50.2 |
| Progression Factor | 0.93 | 0.91 | 1.74 | 0.92 | 1.23 | 1.98 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.1 | 0.1 | 0.1 | 1.2 | 0.5 | 0.0 | 0.7 | 0.4 | | 0.3 | 0.1 | 0.0 |
| Delay (s) | 55.4 | 7.8 | 13.3 | 55.3 | 12.7 | 14.3 | 59.7 | 51.3 | | 59.9 | 51.3 | 50.2 |
| Level of Service | E | A | B | E | B | B | E | D | | E | D | D |
| Approach Delay (s) | | 13.0 | | | 15.1 | | | 52.5 | | | 54.6 | |
| Approach LOS | | B | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.0 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.38 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 9.0 | | |
| Intersection Capacity Utilization | | | 58.2% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 12: Lone Tree Way & Empire Avenue

























Davidon EIR
Near-Term No Project AM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 1770 | 3539 | 1583 | 3433 | 1863 | 1562 | 3433 | 3145 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 1770 | 3539 | 1583 | 3433 | 1863 | 1562 | 3433 | 3145 | |
| Volume (vph) | 247 | 550 | 26 | 81 | 663 | 80 | 89 | 48 | 41 | 105 | 77 | 223 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 274 | 611 | 29 | 90 | 737 | 89 | 99 | 53 | 46 | 117 | 86 | 248 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 43 | 0 | 0 | 43 | 0 | 222 | 0 |
| Lane Group Flow (vph) | 274 | 611 | 19 | 90 | 737 | 46 | 99 | 53 | 3 | 117 | 112 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | 1 | 1 | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | Perm | Split | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 26.8 | 82.5 | 82.5 | 10.8 | 66.5 | 66.5 | 8.0 | 8.0 | 8.0 | 12.7 | 12.7 | |
| Effective Green, g (s) | 27.8 | 83.5 | 83.5 | 11.8 | 67.5 | 67.5 | 9.0 | 9.0 | 9.0 | 13.7 | 13.7 | |
| Actuated g/C Ratio | 0.21 | 0.64 | 0.64 | 0.09 | 0.52 | 0.52 | 0.07 | 0.07 | 0.07 | 0.11 | 0.11 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 379 | 3266 | 1003 | 161 | 1838 | 822 | 238 | 129 | 108 | 362 | 331 | |
| v/s Ratio Prot | c0.15 | 0.12 | | 0.05 | c0.21 | | c0.03 | 0.03 | | 0.03 | c0.04 | |
| v/s Ratio Perm | | | 0.01 | | | 0.03 | | | 0.00 | | | |
| v/c Ratio | 0.72 | 0.19 | 0.02 | 0.56 | 0.40 | 0.06 | 0.42 | 0.41 | 0.03 | 0.32 | 0.34 | |
| Uniform Delay, d1 | 47.5 | 9.5 | 8.4 | 56.6 | 19.0 | 15.5 | 58.0 | 58.0 | 56.4 | 53.9 | 53.9 | |
| Progression Factor | 1.15 | 0.49 | 0.18 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 5.6 | 0.1 | 0.0 | 2.4 | 0.7 | 0.1 | 0.4 | 0.8 | 0.0 | 0.2 | 0.2 | |
| Delay (s) | 60.3 | 4.8 | 1.6 | 59.0 | 19.6 | 15.6 | 58.4 | 58.7 | 56.5 | 54.0 | 54.2 | |
| Level of Service | E | A | A | E | B | B | E | E | E | D | D | |
| Approach Delay (s) | | 21.3 | | | 23.1 | | | 58.0 | | | 54.1 | |
| Approach LOS | | C | | | C | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 30.9 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.47 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 58.0% | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group
























HCM Signalized Intersection Capacity Analysis
13: Lone Tree Way & Deer Valley Rd.

Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.83 | 1.00 | 1.00 | 0.92 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3539 | 1308 | 1770 | 3539 | 1454 | 3433 | 3150 | | 2000 | 3508 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3539 | 1308 | 1770 | 3539 | 1454 | 3433 | 3150 | | 1770 | 3508 | |
| Volume (vph) | 35 | 689 | 164 | 228 | 921 | 185 | 298 | 245 | 174 | 353 | 457 | 17 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 39 | 774 | 184 | 256 | 1035 | 208 | 335 | 275 | 196 | 397 | 513 | 19 |
| RTOR Reduction (vph) | 0 | 0 | 48 | 0 | 0 | 36 | 0 | 102 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 39 | 774 | 136 | 256 | 1035 | 172 | 335 | 369 | 0 | 397 | 530 | 0 |
| Confl. Peds. (#/hr) | 44 | | 101 | 101 | | 44 | 58 | | 69 | 69 | | 58 |
| Confl. Bikes (#/hr) | | | 31 | | | 15 | | | 13 | | | 5 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | |
| Actuated Green, G (s) | 7.3 | 33.7 | 33.7 | 23.2 | 49.6 | 49.6 | 17.5 | 24.3 | | 30.3 | 37.1 | |
| Effective Green, g (s) | 8.8 | 35.7 | 35.7 | 24.7 | 51.6 | 51.6 | 19.0 | 25.8 | | 31.8 | 38.6 | |
| Actuated g/C Ratio | 0.07 | 0.27 | 0.27 | 0.19 | 0.40 | 0.40 | 0.15 | 0.20 | | 0.24 | 0.30 | |
| Clearance Time (s) | 4.5 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 3.0 | 3.0 | | 4.0 | 3.0 | |
| Lane Grp Cap (vph) | 120 | 972 | 359 | 336 | 1405 | 577 | 502 | 625 | | 489 | 1042 | |
| v/s Ratio Prot | 0.02 | c0.22 | | c0.14 | 0.29 | | 0.10 | c0.12 | | c0.20 | 0.15 | |
| v/s Ratio Perm | | | 0.10 | | | 0.12 | | | | | | |
| v/c Ratio | 0.33 | 0.80 | 0.38 | 0.76 | 0.74 | 0.30 | 0.67 | 0.59 | | 0.81 | 0.51 | |
| Uniform Delay, d1 | 57.8 | 43.8 | 38.2 | 49.9 | 33.4 | 26.8 | 52.5 | 47.3 | | 46.3 | 37.8 | |
| Progression Factor | 1.18 | 1.24 | 1.57 | 1.08 | 0.54 | 0.32 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.5 | 6.3 | 2.8 | 6.0 | 2.1 | 0.8 | 3.3 | 1.5 | | 10.4 | 0.4 | |
| Delay (s) | 69.7 | 60.6 | 62.7 | 59.7 | 20.2 | 9.4 | 55.9 | 48.8 | | 56.7 | 38.2 | |
| Level of Service | E | E | E | E | C | A | E | D | | E | D | |
| Approach Delay (s) | | 61.3 | | | 25.4 | | | 51.7 | | | 46.1 | |
| Approach LOS | | E | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 43.4 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.75 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 89.7% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |





















HCM Signalized Intersection Capacity Analysis
14: Lone Tree Way & Hillcrest Ave.

Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1515 | 1770 | 3539 | 1519 | 1770 | 3421 | | 1900 | 3275 | 1554 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1515 | 1770 | 3539 | 1519 | 1770 | 3421 | | 1610 | 3275 | 1554 |
| Volume (vph) | 218 | 561 | 18 | 24 | 952 | 213 | 36 | 53 | 13 | 405 | 85 | 329 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 242 | 623 | 20 | 27 | 1058 | 237 | 40 | 59 | 14 | 450 | 94 | 366 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 113 | 0 | 13 | 0 | 0 | 0 | 296 |
| Lane Group Flow (vph) | 242 | 623 | 11 | 27 | 1058 | 124 | 40 | 60 | 0 | 225 | 319 | 70 |
| Confl. Peds. (#/hr) | 18 | | | 20 | | 18 | 5 | | 10 | 10 | | 5 |
| Confl. Bikes (#/hr) | | | 12 | | | 9 | | | | | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 26.6 | 71.6 | 71.6 | 4.2 | 48.7 | 48.7 | 11.8 | 11.8 | | 22.9 | 22.9 | 22.9 |
| Effective Green, g (s) | 28.6 | 73.6 | 73.6 | 5.7 | 50.7 | 50.7 | 13.8 | 13.8 | | 24.9 | 24.9 | 24.9 |
| Actuated g/C Ratio | 0.22 | 0.57 | 0.57 | 0.04 | 0.39 | 0.39 | 0.11 | 0.11 | | 0.19 | 0.19 | 0.19 |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 389 | 2004 | 858 | 78 | 1380 | 592 | 188 | 363 | | 364 | 627 | 298 |
| v/s Ratio Prot | c0.14 | 0.18 | | 0.02 | c0.30 | | c0.02 | 0.02 | | c0.12 | 0.10 | |
| v/s Ratio Perm | | | 0.01 | | | 0.08 | | | | | | 0.05 |
| v/c Ratio | 0.62 | 0.31 | 0.01 | 0.35 | 0.77 | 0.21 | 0.21 | 0.17 | | 0.62 | 0.51 | 0.24 |
| Uniform Delay, d1 | 45.8 | 14.8 | 12.3 | 60.3 | 34.5 | 26.3 | 53.1 | 52.9 | | 48.2 | 47.1 | 44.5 |
| Progression Factor | 1.46 | 1.14 | 2.18 | 1.23 | 0.76 | 0.64 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.9 | 0.4 | 0.0 | 2.4 | 3.7 | 0.7 | 1.2 | 0.5 | | 4.5 | 1.4 | 0.9 |
| Delay (s) | 70.9 | 17.3 | 26.9 | 76.6 | 29.9 | 17.5 | 54.3 | 53.3 | | 52.7 | 48.4 | 45.3 |
| Level of Service | E | B | C | E | C | B | D | D | | D | D | D |
| Approach Delay (s) | | 32.2 | | | 28.7 | | | 53.7 | | | 48.2 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 36.0 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.64 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 67.2% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
15: Lone Tree Way & Vista Grande





















Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.87 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5057 | | 1770 | 5061 | | 1770 | 1612 | | 1770 | 1661 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.64 | 1.00 | | 0.37 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5057 | | 1770 | 5061 | | 1188 | 1612 | | 696 | 1661 | |
| Volume (vph) | 20 | 884 | 30 | 59 | 1119 | 37 | 39 | 14 | 123 | 24 | 16 | 41 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 22 | 951 | 32 | 63 | 1203 | 40 | 42 | 15 | 132 | 26 | 17 | 44 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 121 | 0 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 22 | 982 | 0 | 63 | 1242 | 0 | 42 | 26 | 0 | 26 | 21 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | | | | |
| Turn Type | Prot | | | Prot | | | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 5.4 | 96.8 | | 9.5 | 100.9 | | 9.2 | 9.2 | | 9.2 | 9.2 | |
| Effective Green, g (s) | 6.9 | 99.3 | | 11.0 | 103.4 | | 10.7 | 10.7 | | 10.7 | 10.7 | |
| Actuated g/C Ratio | 0.05 | 0.76 | | 0.08 | 0.80 | | 0.08 | 0.08 | | 0.08 | 0.08 | |
| Clearance Time (s) | 4.5 | 5.5 | | 4.5 | 5.5 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 4.0 | 6.0 | | 4.0 | 6.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 94 | 3863 | | 150 | 4025 | | 98 | 133 | | 57 | 137 | |
| v/s Ratio Prot | 0.01 | 0.19 | | c0.04 | c0.25 | | | 0.02 | | | 0.01 | |
| v/s Ratio Perm | | | | | | | 0.04 | | | c0.04 | | |
| v/c Ratio | 0.23 | 0.25 | | 0.42 | 0.31 | | 0.43 | 0.19 | | 0.46 | 0.15 | |
| Uniform Delay, d1 | 59.0 | 4.5 | | 56.5 | 3.6 | | 56.7 | 55.6 | | 56.9 | 55.4 | |
| Progression Factor | 0.93 | 1.03 | | 1.00 | 0.70 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.6 | 0.1 | | 2.2 | 0.2 | | 3.0 | 0.7 | | 5.7 | 0.5 | |
| Delay (s) | 56.6 | 4.8 | | 58.9 | 2.7 | | 59.7 | 56.3 | | 62.6 | 55.9 | |
| Level of Service | E | A | | E | A | | E | E | | E | E | |
| Approach Delay (s) | | 5.9 | | | 5.4 | | | 57.1 | | | 57.9 | |
| Approach LOS | | A | | | A | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 11.2 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.33 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 6.0 | | |
| Intersection Capacity Utilization | | | 50.8% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
16: Country Hills Dr. & Hillcrest Ave
























Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.90 | | 1.00 | 0.92 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1665 | | 1770 | 1691 | | 1770 | 3483 | | 1770 | 3495 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1665 | | 1770 | 1691 | | 1770 | 3483 | | 1770 | 3495 | |
| Volume (vph) | 44 | 77 | 143 | 84 | 93 | 117 | 70 | 384 | 31 | 63 | 623 | 26 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 49 | 86 | 159 | 93 | 103 | 130 | 78 | 427 | 34 | 70 | 692 | 29 |
| RTOR Reduction (vph) | 0 | 39 | 0 | 0 | 26 | 0 | 0 | 2 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 49 | 206 | 0 | 93 | 207 | 0 | 78 | 459 | 0 | 70 | 720 | 0 |
| Confl. Peds. (#/hr) | 3 | | 2 | 2 | | 3 | 45 | | 16 | 16 | | 45 |
| Turn Type | Split | | | Split | | | Prot | | | Prot | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 21.0 | 21.0 | | 20.6 | 20.6 | | 9.5 | 66.4 | | 9.5 | 66.4 | |
| Effective Green, g (s) | 21.5 | 21.5 | | 21.1 | 21.1 | | 10.0 | 67.9 | | 10.0 | 67.9 | |
| Actuated g/C Ratio | 0.16 | 0.16 | | 0.16 | 0.16 | | 0.08 | 0.51 | | 0.08 | 0.51 | |
| Clearance Time (s) | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 4.5 | | 3.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 287 | 270 | | 282 | 269 | | 134 | 1785 | | 134 | 1791 | |
| v/s Ratio Prot | 0.03 | c0.12 | | 0.05 | c0.12 | | c0.04 | 0.13 | | c0.04 | c0.21 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.17 | 0.76 | | 0.33 | 0.77 | | 0.58 | 0.26 | | 0.52 | 0.40 | |
| Uniform Delay, d1 | 47.8 | 53.1 | | 49.4 | 53.4 | | 59.2 | 18.1 | | 59.0 | 19.8 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 12.0 | | 0.7 | 12.4 | | 6.3 | 0.3 | | 3.6 | 0.7 | |
| Delay (s) | 48.1 | 65.0 | | 50.1 | 65.8 | | 65.5 | 18.5 | | 62.6 | 20.5 | |
| Level of Service | D | E | | D | E | | E | B | | E | C | |
| Approach Delay (s) | | 62.2 | | | 61.3 | | | 25.3 | | | 24.2 | |
| Approach LOS | | E | | | E | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 36.4 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 132.5 | | | Sum of lost time (s) | | | 15.0 | | | |
| Intersection Capacity Utilization | | | 54.2% | | | ICU Level of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
18: Sterling Hill Dr. & Hillcrest Ave

Davidon EIR
Near-Term No Project AM Peak Hour

























| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1661 | | 1767 | 1863 | 1583 | 1770 | 3539 | 1545 | 1770 | 3473 | |
| Flt Permitted | 0.69 | 1.00 | | 0.46 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1280 | 1661 | | 855 | 1863 | 1583 | 1770 | 3539 | 1545 | 1770 | 3473 | |
| Volume (vph) | 150 | 50 | 100 | 48 | 67 | 155 | 67 | 459 | 25 | 74 | 561 | 80 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 169 | 56 | 112 | 54 | 75 | 174 | 75 | 516 | 28 | 83 | 630 | 90 |
| RTOR Reduction (vph) | 0 | 91 | 0 | 0 | 0 | 142 | 0 | 0 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 169 | 77 | 0 | 54 | 75 | 32 | 75 | 516 | 28 | 83 | 713 | 0 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | 9 | 9 | | |
| Turn Type | Perm | | | Perm | | Perm | Prot | | Free | Prot | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | | | Free | | | |
| Actuated Green, G (s) | 16.9 | 16.9 | | 16.9 | 16.9 | 16.9 | 8.3 | 59.8 | 100.0 | 8.8 | 60.3 | |
| Effective Green, g (s) | 18.4 | 18.4 | | 18.4 | 18.4 | 18.4 | 9.3 | 62.8 | 100.0 | 9.8 | 63.3 | |
| Actuated g/C Ratio | 0.18 | 0.18 | | 0.18 | 0.18 | 0.18 | 0.09 | 0.63 | 1.00 | 0.10 | 0.63 | |
| Clearance Time (s) | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.5 | 3.5 | 3.5 | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 236 | 306 | | 157 | 343 | 291 | 165 | 2222 | 1545 | 173 | 2198 | |
| v/s Ratio Prot | | 0.05 | | | 0.04 | | 0.04 | 0.15 | | c0.05 | c0.21 | |
| v/s Ratio Perm | c0.13 | | | 0.06 | | 0.02 | | | c0.02 | | | |
| v/c Ratio | 0.72 | 0.25 | | 0.34 | 0.22 | 0.11 | 0.45 | 0.23 | 0.02 | 0.48 | 0.32 | |
| Uniform Delay, d1 | 38.3 | 34.9 | | 35.5 | 34.7 | 34.0 | 42.9 | 8.1 | 0.0 | 42.7 | 8.5 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.14 | 0.44 | |
| Incremental Delay, d2 | 9.9 | 0.4 | | 1.6 | 0.4 | 0.2 | 2.0 | 0.2 | 0.0 | 2.0 | 0.4 | |
| Delay (s) | 48.2 | 35.3 | | 37.1 | 35.1 | 34.2 | 44.9 | 8.3 | 0.0 | 50.6 | 4.1 | |
| Level of Service | D | D | | D | D | C | D | A | A | D | A | |
| Approach Delay (s) | | 41.8 | | | 34.9 | | | 12.4 | | | 8.9 | |
| Approach LOS | | D | | | C | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 19.2 | | | | HCM Level of Service | | | B | | |
| HCM Volume to Capacity ratio | | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | | Sum of lost time (s) | | | 6.0 | | |
| Intersection Capacity Utilization | | | 51.4% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

8: Lone Tree Way & Canada Valley



























Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 3433 | 5085 | 1547 | 3433 | 1595 | 1504 | 1770 | 1863 | 1558 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 3433 | 5085 | 1547 | 3433 | 1595 | 1504 | 1770 | 1863 | 1558 |
| Volume (vph) | 54 | 1586 | 100 | 480 | 1256 | 253 | 110 | 55 | 262 | 175 | 56 | 22 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 56 | 1652 | 104 | 500 | 1308 | 264 | 115 | 57 | 273 | 182 | 58 | 23 |
| RTOR Reduction (vph) | 0 | 0 | 22 | 0 | 0 | 106 | 0 | 66 | 142 | 0 | 0 | 20 |
| Lane Group Flow (vph) | 56 | 1652 | 82 | 500 | 1308 | 158 | 115 | 101 | 21 | 182 | 58 | 3 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 4 | | | | | 4 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 8.0 | 58.8 | 58.8 | 23.9 | 74.7 | 74.7 | 11.8 | 15.4 | 15.4 | 13.9 | 17.5 | 17.5 |
| Effective Green, g (s) | 9.0 | 61.8 | 61.8 | 24.9 | 77.7 | 77.7 | 12.8 | 16.4 | 16.4 | 14.9 | 18.5 | 18.5 |
| Actuated g/C Ratio | 0.07 | 0.48 | 0.48 | 0.19 | 0.60 | 0.60 | 0.10 | 0.13 | 0.13 | 0.11 | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 6.0 | 6.0 | 2.0 | 2.0 | 2.0 | 2.0 | 6.0 | 6.0 |
| Lane Grp Cap (vph) | 123 | 2417 | 743 | 658 | 3039 | 925 | 338 | 201 | 190 | 203 | 265 | 222 |
| v/s Ratio Prot | 0.03 | c0.32 | | c0.15 | 0.26 | | 0.03 | c0.06 | | c0.10 | 0.03 | |
| v/s Ratio Perm | | | 0.05 | | | 0.10 | | | 0.01 | | | 0.00 |
| v/c Ratio | 0.46 | 0.68 | 0.11 | 0.76 | 0.43 | 0.17 | 0.34 | 0.50 | 0.11 | 0.90 | 0.22 | 0.01 |
| Uniform Delay, d1 | 58.1 | 26.5 | 18.9 | 49.7 | 14.2 | 11.7 | 54.7 | 53.0 | 50.3 | 56.8 | 49.4 | 47.9 |
| Progression Factor | 0.88 | 0.76 | 0.91 | 1.28 | 0.64 | 1.09 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.7 | 1.2 | 0.2 | 3.6 | 0.4 | 0.3 | 0.2 | 0.7 | 0.1 | 35.1 | 1.2 | 0.1 |
| Delay (s) | 51.8 | 21.4 | 17.4 | 67.3 | 9.5 | 13.1 | 54.9 | 53.7 | 50.4 | 91.9 | 50.5 | 48.0 |
| Level of Service | D | C | B | E | A | B | D | D | D | F | D | D |
| Approach Delay (s) | | 22.1 | | | 23.9 | | | 52.8 | | | 78.9 | |
| Approach LOS | | C | | | C | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 29.2 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.69 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 75.6% | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
9: Lone Tree Way & SR-4 Bypass SB Off-Ramp













Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |    |  |    |    | | | | |  |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Volume (vph) | 0 | 1419 | 612 | 98 | 1440 | 0 | 0 | 0 | 0 | 416 | 10 | 539 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1494 | 644 | 103 | 1516 | 0 | 0 | 0 | 0 | 438 | 11 | 567 |
| RTOR Reduction (vph) | 0 | 0 | 341 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| Lane Group Flow (vph) | 0 | 1494 | 303 | 103 | 1516 | 0 | 0 | 0 | 0 | 219 | 230 | 555 |
| Confl. Peds. (#/hr) | | | | | | | 3 | | 3 | | | |
| Turn Type | | Perm | | Prot | | | | | | Perm | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | | 4 | |
| Permitted Phases | | 2 | | | | | | | | 4 | 4 | |
| Actuated Green, G (s) | | 58.6 | 58.6 | 8.8 | 71.4 | | | | | 49.1 | 49.1 | 49.1 |
| Effective Green, g (s) | | 61.1 | 61.1 | 9.8 | 73.9 | | | | | 50.1 | 50.1 | 50.1 |
| Actuated g/C Ratio | | 0.47 | 0.47 | 0.08 | 0.57 | | | | | 0.39 | 0.39 | 0.39 |
| Clearance Time (s) | | 5.5 | 5.5 | 4.0 | 5.5 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 3.0 | 4.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2390 | 744 | 259 | 2891 | | | | | 648 | 651 | 610 |
| v/s Ratio Prot | | c0.29 | | 0.03 | c0.30 | | | | | | | |
| v/s Ratio Perm | | 0.19 | | | | | | | | 0.13 | 0.14 | c0.35 |
| v/c Ratio | | 0.63 | 0.41 | 0.40 | 0.52 | | | | | 0.34 | 0.35 | 0.91 |
| Uniform Delay, d1 | | 25.9 | 22.6 | 57.3 | 17.2 | | | | | 28.2 | 28.4 | 37.8 |
| Progression Factor | | 0.58 | 1.48 | 1.11 | 0.53 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.0 | 1.3 | 0.9 | 0.6 | | | | | 0.3 | 0.3 | 17.8 |
| Delay (s) | | 15.9 | 34.7 | 64.5 | 9.8 | | | | | 28.5 | 28.8 | 55.6 |
| Level of Service | | B | C | E | A | | | | | C | C | E |
| Approach Delay (s) | | 21.6 | | | 13.2 | | | 0.0 | | | 43.7 | |
| Approach LOS | | C | | | B | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 23.5 | | HCM Level of Service | | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.74 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | Sum of lost time (s) | | | | 9.0 | | | | |
| Intersection Capacity Utilization | | 67.9% | | ICU Level of Service | | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 10: Lone Tree Way & On-ramp
























Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1697 | 1583 | | | |
| Flt Permitted | | 0.94 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (perm) | | 4763 | 1583 | 1770 | 5085 | 1583 | 1681 | 1697 | 1583 | | | |
| Volume (vph) | 5 | 1540 | 373 | 21 | 1014 | 357 | 541 | 43 | 137 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 5 | 1692 | 410 | 23 | 1114 | 392 | 595 | 47 | 151 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 125 | 0 | 0 | 107 | 0 | 0 | 117 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1697 | 285 | 23 | 1114 | 285 | 313 | 329 | 34 | 0 | 0 | 0 |
| Turn Type | Perm | | Perm | Prot | | Perm | Split | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | 8 | 8 | | | | |
| Permitted Phases | 2 | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | | 83.3 | 83.3 | 4.2 | 91.5 | 91.5 | 28.5 | 28.5 | 28.5 | | | |
| Effective Green, g (s) | | 86.3 | 86.3 | 5.2 | 94.5 | 94.5 | 29.5 | 29.5 | 29.5 | | | |
| Actuated g/C Ratio | | 0.66 | 0.66 | 0.04 | 0.73 | 0.73 | 0.23 | 0.23 | 0.23 | | | |
| Clearance Time (s) | | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | | 3162 | 1051 | 71 | 3696 | 1151 | 381 | 385 | 359 | | | |
| v/s Ratio Prot | | | | 0.01 | c0.22 | | 0.19 | c0.19 | | | | |
| v/s Ratio Perm | | c0.36 | 0.18 | | | 0.18 | | | 0.02 | | | |
| v/c Ratio | | 0.54 | 0.27 | 0.32 | 0.30 | 0.25 | 0.82 | 0.85 | 0.10 | | | |
| Uniform Delay, d1 | | 11.4 | 9.0 | 60.7 | 6.2 | 5.9 | 47.7 | 48.2 | 39.7 | | | |
| Progression Factor | | 0.22 | 0.00 | 0.87 | 1.04 | 1.76 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.6 | 0.6 | 0.9 | 0.2 | 0.5 | 12.7 | 16.1 | 0.0 | | | |
| Delay (s) | | 3.1 | 0.6 | 53.9 | 6.6 | 10.9 | 60.4 | 64.3 | 39.7 | | | |
| Level of Service | | A | A | D | A | B | E | E | D | | | |
| Approach Delay (s) | | 2.6 | | | 8.4 | | | 58.1 | | | 0.0 | |
| Approach LOS | | A | | | A | | | E | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 14.5 | | | | HCM Level of Service | | B | | | |
| HCM Volume to Capacity ratio | | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | 9.0 | | | |
| Intersection Capacity Utilization | | | 78.1% | | | | ICU Level of Service | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Slaten Ranch

Davidon EIR
Near-Term No Project PM Peak Hour































| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1549 | 1770 | 3539 | 1561 | 3433 | 3174 | | 3433 | 1863 | 1561 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1549 | 1770 | 3539 | 1561 | 3433 | 3174 | | 3433 | 1863 | 1561 |
| Volume (vph) | 217 | 1028 | 256 | 160 | 986 | 55 | 51 | 76 | 167 | 114 | 67 | 101 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 231 | 1094 | 272 | 170 | 1049 | 59 | 54 | 81 | 178 | 121 | 71 | 107 |
| RTOR Reduction (vph) | 0 | 0 | 118 | 0 | 0 | 21 | 0 | 155 | 0 | 0 | 0 | 90 |
| Lane Group Flow (vph) | 231 | 1094 | 154 | 170 | 1049 | 38 | 54 | 104 | 0 | 121 | 71 | 17 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 2 | | | | | 2 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 13.2 | 70.5 | 70.5 | 16.1 | 73.4 | 73.4 | 6.3 | 15.6 | | 9.8 | 19.1 | 19.1 |
| Effective Green, g (s) | 14.2 | 73.5 | 73.5 | 17.1 | 76.4 | 76.4 | 7.3 | 16.6 | | 10.8 | 20.1 | 20.1 |
| Actuated g/C Ratio | 0.11 | 0.57 | 0.57 | 0.13 | 0.59 | 0.59 | 0.06 | 0.13 | | 0.08 | 0.15 | 0.15 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 3.0 | 4.0 | | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 375 | 2875 | 876 | 233 | 2080 | 917 | 193 | 405 | | 285 | 288 | 241 |
| v/s Ratio Prot | 0.07 | 0.22 | | c0.10 | c0.30 | | c0.02 | c0.03 | | c0.04 | 0.04 | |
| v/s Ratio Perm | | | 0.10 | | | 0.02 | | | | | | 0.01 |
| v/c Ratio | 0.62 | 0.38 | 0.18 | 0.73 | 0.50 | 0.04 | 0.28 | 0.26 | | 0.42 | 0.25 | 0.07 |
| Uniform Delay, d1 | 55.3 | 15.6 | 13.6 | 54.2 | 15.7 | 11.3 | 58.8 | 51.1 | | 56.6 | 48.3 | 47.0 |
| Progression Factor | 1.06 | 0.85 | 1.50 | 0.98 | 1.13 | 1.99 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.0 | 0.4 | 0.4 | 8.7 | 0.8 | 0.1 | 0.8 | 0.5 | | 0.4 | 0.2 | 0.0 |
| Delay (s) | 61.4 | 13.8 | 20.8 | 61.9 | 18.6 | 22.6 | 59.6 | 51.6 | | 57.0 | 48.5 | 47.0 |
| Level of Service | E | B | C | E | B | C | E | D | | E | D | D |
| Approach Delay (s) | | 21.8 | | | 24.6 | | | 53.0 | | | 51.4 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 28.2 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.49 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 61.4% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue

























Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |   |  |   |  |  |   |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.99 | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 1770 | 3539 | 1540 | 3433 | 1863 | 1562 | 3433 | 3124 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 1770 | 3539 | 1540 | 3433 | 1863 | 1562 | 3433 | 3124 | |
| Volume (vph) | 316 | 809 | 112 | 53 | 772 | 129 | 76 | 46 | 36 | 231 | 115 | 289 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 322 | 826 | 114 | 54 | 788 | 132 | 78 | 47 | 37 | 236 | 117 | 295 |
| RTOR Reduction (vph) | 0 | 0 | 43 | 0 | 0 | 73 | 0 | 0 | 34 | 0 | 257 | 0 |
| Lane Group Flow (vph) | 322 | 826 | 71 | 54 | 788 | 59 | 78 | 47 | 3 | 236 | 155 | 0 |
| Confl. Peds. (#/hr) | 3 | | 1 | 1 | | 3 | 3 | | 1 | 1 | | 3 |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | Perm | Split | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 30.6 | 80.4 | 80.4 | 7.0 | 56.8 | 56.8 | 10.9 | 10.9 | 10.9 | 15.7 | 15.7 | |
| Effective Green, g (s) | 31.6 | 81.4 | 81.4 | 8.0 | 57.8 | 57.8 | 11.9 | 11.9 | 11.9 | 16.7 | 16.7 | |
| Actuated g/C Ratio | 0.24 | 0.63 | 0.63 | 0.06 | 0.44 | 0.44 | 0.09 | 0.09 | 0.09 | 0.13 | 0.13 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 430 | 3184 | 978 | 109 | 1573 | 685 | 314 | 171 | 143 | 441 | 401 | |
| v/s Ratio Prot | c0.18 | 0.16 | | 0.03 | c0.22 | | 0.02 | c0.03 | | c0.07 | 0.05 | |
| v/s Ratio Perm | | | 0.05 | | | 0.04 | | | 0.00 | | | |
| v/c Ratio | 0.75 | 0.26 | 0.07 | 0.50 | 0.50 | 0.09 | 0.25 | 0.27 | 0.02 | 0.54 | 0.39 | |
| Uniform Delay, d1 | 45.5 | 10.8 | 9.5 | 59.0 | 25.8 | 20.8 | 54.9 | 55.0 | 53.8 | 53.0 | 52.0 | |
| Progression Factor | 1.57 | 0.59 | 0.36 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 5.9 | 0.2 | 0.1 | 1.3 | 1.1 | 0.2 | 0.2 | 0.3 | 0.0 | 0.6 | 0.2 | |
| Delay (s) | 77.1 | 6.6 | 3.5 | 60.3 | 26.9 | 21.1 | 55.0 | 55.3 | 53.8 | 53.6 | 52.2 | |
| Level of Service | E | A | A | E | C | C | E | E | D | D | D | |
| Approach Delay (s) | | 24.3 | | | 28.0 | | | 54.8 | | | 52.7 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 33.2 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.55 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 70.7% | | | | ICU Level of Service | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

























HCM Signalized Intersection Capacity Analysis
13: Lone Tree Way & Deer Valley Rd.

Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3539 | 1435 | 1770 | 3539 | 1531 | 3433 | 3297 | | 2000 | 3498 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3539 | 1435 | 1770 | 3539 | 1531 | 3433 | 3297 | | 1770 | 3498 | |
| Volume (vph) | 87 | 903 | 169 | 238 | 588 | 154 | 205 | 365 | 241 | 168 | 191 | 14 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 90 | 931 | 174 | 245 | 606 | 159 | 211 | 376 | 248 | 173 | 197 | 14 |
| RTOR Reduction (vph) | 0 | 0 | 34 | 0 | 0 | 46 | 0 | 87 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 90 | 931 | 140 | 245 | 606 | 113 | 211 | 537 | 0 | 173 | 206 | 0 |
| Confl. Peds. (#/hr) | 12 | | 54 | 54 | | 12 | 11 | | 8 | 8 | | 11 |
| Confl. Bikes (#/hr) | | | 11 | | | 9 | | | | | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | |
| Actuated Green, G (s) | 11.8 | 48.0 | 48.0 | 21.3 | 57.5 | 57.5 | 12.9 | 25.1 | | 17.1 | 29.3 | |
| Effective Green, g (s) | 13.3 | 50.0 | 50.0 | 22.8 | 59.5 | 59.5 | 14.4 | 26.6 | | 18.6 | 30.8 | |
| Actuated g/C Ratio | 0.10 | 0.38 | 0.38 | 0.18 | 0.46 | 0.46 | 0.11 | 0.20 | | 0.14 | 0.24 | |
| Clearance Time (s) | 4.5 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 3.0 | 3.0 | | 4.0 | 3.0 | |
| Lane Grp Cap (vph) | 181 | 1361 | 552 | 310 | 1620 | 701 | 380 | 675 | | 286 | 829 | |
| v/s Ratio Prot | 0.05 | c0.26 | | c0.14 | 0.17 | | 0.06 | c0.16 | | c0.09 | 0.06 | |
| v/s Ratio Perm | | | 0.10 | | | 0.07 | | | | | | |
| v/c Ratio | 0.50 | 0.68 | 0.25 | 0.79 | 0.37 | 0.16 | 0.56 | 0.79 | | 0.60 | 0.25 | |
| Uniform Delay, d1 | 55.2 | 33.4 | 27.3 | 51.3 | 23.1 | 20.6 | 54.8 | 49.1 | | 52.3 | 40.2 | |
| Progression Factor | 1.42 | 0.60 | 0.60 | 1.06 | 1.69 | 2.52 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.9 | 2.4 | 1.0 | 11.0 | 0.6 | 0.4 | 1.8 | 6.4 | | 4.1 | 0.2 | |
| Delay (s) | 80.1 | 22.5 | 17.4 | 65.3 | 39.5 | 52.5 | 56.5 | 55.5 | | 56.4 | 40.4 | |
| Level of Service | F | C | B | E | D | D | E | E | | E | D | |
| Approach Delay (s) | | 26.1 | | | 47.8 | | | 55.8 | | | 47.6 | |
| Approach LOS | | C | | | D | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 42.2 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.72 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 80.0% | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |










HCM Signalized Intersection Capacity Analysis
14: Lone Tree Way & Hillcrest Ave.

Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.96 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.97 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1521 | 1770 | 5085 | 1519 | 1770 | 3388 | | 2000 | 3263 | 1534 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1521 | 1770 | 5085 | 1519 | 1770 | 3388 | | 1610 | 3263 | 1534 |
| Volume (vph) | 232 | 1029 | 22 | 43 | 868 | 369 | 17 | 87 | 26 | 551 | 77 | 153 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 264 | 1169 | 25 | 49 | 986 | 419 | 19 | 99 | 30 | 626 | 88 | 174 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 272 | 0 | 25 | 0 | 0 | 0 | 137 |
| Lane Group Flow (vph) | 264 | 1169 | 16 | 49 | 986 | 147 | 19 | 104 | 0 | 313 | 401 | 37 |
| Confl. Peds. (#/hr) | 18 | | 20 | 20 | | 18 | 14 | | 16 | 16 | | 14 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 1 | | | 1 |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 23.2 | 62.0 | 62.0 | 5.2 | 43.5 | 43.5 | 17.4 | 17.4 | | 25.9 | 25.9 | 25.9 |
| Effective Green, g (s) | 25.2 | 64.0 | 64.0 | 6.7 | 45.5 | 45.5 | 19.4 | 19.4 | | 27.9 | 27.9 | 27.9 |
| Actuated g/C Ratio | 0.19 | 0.49 | 0.49 | 0.05 | 0.35 | 0.35 | 0.15 | 0.15 | | 0.21 | 0.21 | 0.21 |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 343 | 1742 | 749 | 91 | 1780 | 532 | 264 | 506 | | 429 | 700 | 329 |
| v/s Ratio Prot | c0.15 | c0.33 | | 0.03 | 0.19 | | 0.01 | c0.03 | | c0.16 | 0.12 | |
| v/s Ratio Perm | | | 0.01 | | | 0.10 | | | | | | 0.02 |
| v/c Ratio | 0.77 | 0.67 | 0.02 | 0.54 | 0.55 | 0.28 | 0.07 | 0.21 | | 0.73 | 0.87dl | 0.11 |
| Uniform Delay, d1 | 49.7 | 25.0 | 16.9 | 60.1 | 34.1 | 30.4 | 47.6 | 48.5 | | 47.5 | 45.7 | 41.1 |
| Progression Factor | 0.80 | 0.70 | 0.35 | 1.13 | 0.89 | 1.16 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 10.7 | 1.9 | 0.0 | 5.2 | 1.1 | 1.1 | 0.2 | 0.4 | | 7.5 | 1.8 | 0.3 |
| Delay (s) | 50.2 | 19.5 | 5.9 | 73.4 | 31.2 | 36.3 | 47.8 | 49.0 | | 55.0 | 47.5 | 41.4 |
| Level of Service | D | B | A | E | C | D | D | D | | E | D | D |
| Approach Delay (s) | | 24.8 | | | 34.1 | | | 48.8 | | | 49.0 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 34.6 | | | | | | | | | |
| HCM Volume to Capacity ratio | | | 0.63 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 69.8% | | | | | | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| dl Defacto Left Lane. Recode with 1 though lane as a left lane. | | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis 15: Lone Tree Way & Vista Grande





















Davidon EIR
Near-Term No Project PM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|---|-------|---|---|----------------------|--|---|------|---|---|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5060 | | 1770 | 5067 | | 1767 | 1605 | | 1770 | 1652 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.74 | 1.00 | | 0.40 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5060 | | 1770 | 5067 | | 1372 | 1605 | | 742 | 1652 | |
| Volume (vph) | 18 | 1542 | 44 | 121 | 1222 | 24 | 35 | 10 | 114 | 42 | 9 | 20 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 19 | 1590 | 45 | 125 | 1260 | 25 | 36 | 10 | 118 | 43 | 9 | 21 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 105 | 0 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 19 | 1634 | 0 | 125 | 1284 | 0 | 36 | 23 | 0 | 43 | 11 | 0 |
| Confl. Peds. (#/hr) | 4 | | 4 | 4 | | 4 | 1 | | | | | 1 |
| Turn Type | Prot | | | Prot | | | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 3.7 | 87.4 | | 15.3 | 99.0 | | 12.8 | 12.8 | | 12.8 | 12.8 | |
| Effective Green, g (s) | 5.2 | 89.9 | | 16.8 | 101.5 | | 14.3 | 14.3 | | 14.3 | 14.3 | |
| Actuated g/C Ratio | 0.04 | 0.69 | | 0.13 | 0.78 | | 0.11 | 0.11 | | 0.11 | 0.11 | |
| Clearance Time (s) | 4.5 | 5.5 | | 4.5 | 5.5 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 4.0 | 6.0 | | 4.0 | 6.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 71 | 3499 | | 229 | 3956 | | 151 | 177 | | 82 | 182 | |
| v/s Ratio Prot | 0.01 | c0.32 | | c0.07 | 0.25 | | | 0.01 | | | 0.01 | |
| v/s Ratio Perm | | | | | | | 0.03 | | | c0.06 | | |
| v/c Ratio | 0.27 | 0.47 | | 0.55 | 0.32 | | 0.24 | 0.13 | | 0.52 | 0.06 | |
| Uniform Delay, d1 | 60.6 | 9.1 | | 53.0 | 4.2 | | 52.9 | 52.2 | | 54.6 | 51.8 | |
| Progression Factor | 0.91 | 0.80 | | 0.89 | 1.56 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.1 | 0.3 | | 2.4 | 0.2 | | 0.8 | 0.3 | | 5.9 | 0.1 | |
| Delay (s) | 57.5 | 7.7 | | 49.7 | 6.7 | | 53.7 | 52.6 | | 60.6 | 52.0 | |
| Level of Service | E | A | | D | A | | D | D | | E | D | |
| Approach Delay (s) | | 8.3 | | | 10.5 | | | 52.8 | | | 57.0 | |
| Approach LOS | | A | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 12.5 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.49 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 61.7% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
16: Country Hills Dr. & Hillcrest Ave

Davidon EIR
Near-Term No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.91 | | 1.00 | 0.93 | | 1.00 | 0.99 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1690 | | 1770 | 1710 | | 1770 | 3482 | | 1770 | 3458 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1690 | | 1770 | 1710 | | 1770 | 3482 | | 1770 | 3458 | |
| Volume (vph) | 42 | 51 | 82 | 34 | 50 | 45 | 73 | 514 | 49 | 89 | 543 | 63 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 46 | 55 | 89 | 37 | 54 | 49 | 79 | 559 | 53 | 97 | 590 | 68 |
| RTOR Reduction (vph) | 0 | 36 | 0 | 0 | 20 | 0 | 0 | 2 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 46 | 108 | 0 | 37 | 83 | 0 | 79 | 610 | 0 | 97 | 655 | 0 |
| Confl. Peds. (#/hr) | 10 | | | | | 10 | 20 | | 7 | 7 | | 20 |
| Turn Type | Split | | | Split | | | Prot | | | Prot | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 12.3 | 12.3 | | 9.4 | 9.4 | | 8.9 | 69.2 | | 9.9 | 70.2 | |
| Effective Green, g (s) | 12.8 | 12.8 | | 9.9 | 9.9 | | 9.4 | 70.7 | | 10.4 | 71.7 | |
| Actuated g/C Ratio | 0.11 | 0.11 | | 0.09 | 0.09 | | 0.08 | 0.61 | | 0.09 | 0.62 | |
| Clearance Time (s) | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 4.5 | | 3.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 196 | 187 | | 151 | 146 | | 144 | 2126 | | 159 | 2141 | |
| v/s Ratio Prot | 0.03 | c0.06 | | 0.02 | c0.05 | | c0.04 | 0.18 | | c0.05 | c0.19 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.23 | 0.58 | | 0.25 | 0.57 | | 0.55 | 0.29 | | 0.61 | 0.31 | |
| Uniform Delay, d1 | 47.0 | 48.9 | | 49.5 | 50.9 | | 51.2 | 10.6 | | 50.7 | 10.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.6 | 4.2 | | 0.8 | 5.0 | | 4.2 | 0.3 | | 6.8 | 0.4 | |
| Delay (s) | 47.6 | 53.1 | | 50.3 | 55.9 | | 55.4 | 11.0 | | 57.5 | 10.7 | |
| Level of Service | D | D | | D | E | | E | B | | E | B | |
| Approach Delay (s) | | 51.8 | | | 54.4 | | | 16.1 | | | 16.7 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 23.2 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.42 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 115.8 | | | Sum of lost time (s) | | | | 15.0 | | |
| Intersection Capacity Utilization | | | 51.3% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |













c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

18: Laurel Rd. & Hillcrest Ave

Davidon EIR

Near-Term No Project PM Peak Hour


































| |  | | | | | | | | | | | |
|-----------------------------------|--|---|-------|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.89 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1634 | | 1768 | 1863 | 1583 | 1770 | 3539 | 1550 | 1770 | 3494 | |
| Flt Permitted | 0.75 | 1.00 | | 0.74 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1400 | 1634 | | 1374 | 1863 | 1583 | 1770 | 3539 | 1550 | 1770 | 3494 | |
| Volume (vph) | 17 | 7 | 22 | 35 | 9 | 133 | 27 | 535 | 39 | 162 | 626 | 50 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 17 | 7 | 22 | 36 | 9 | 136 | 28 | 546 | 40 | 165 | 639 | 51 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 0 | 0 | 123 | 0 | 0 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 17 | 9 | 0 | 36 | 9 | 13 | 28 | 546 | 40 | 165 | 688 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | 2 | | 2 | 2 | | 2 |
| Turn Type | Perm | | | Perm | | Perm | Prot | | Free | Prot | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | | | Free | | | |
| Actuated Green, G (s) | 8.4 | 8.4 | | 8.4 | 8.4 | 8.4 | 3.4 | 62.6 | 100.0 | 14.5 | 73.7 | |
| Effective Green, g (s) | 9.9 | 9.9 | | 9.9 | 9.9 | 9.9 | 4.4 | 65.6 | 100.0 | 15.5 | 76.7 | |
| Actuated g/C Ratio | 0.10 | 0.10 | | 0.10 | 0.10 | 0.10 | 0.04 | 0.66 | 1.00 | 0.16 | 0.77 | |
| Clearance Time (s) | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.5 | 3.5 | 3.5 | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 139 | 162 | | 136 | 184 | 157 | 78 | 2322 | 1550 | 274 | 2680 | |
| v/s Ratio Prot | | 0.01 | | | 0.00 | | 0.02 | 0.15 | | c0.09 | c0.20 | |
| v/s Ratio Perm | 0.01 | | | c0.03 | | 0.01 | | | 0.03 | | | |
| v/c Ratio | 0.12 | 0.06 | | 0.26 | 0.05 | 0.09 | 0.36 | 0.24 | 0.03 | 0.60 | 0.26 | |
| Uniform Delay, d1 | 41.1 | 40.8 | | 41.7 | 40.8 | 40.9 | 46.4 | 7.0 | 0.0 | 39.4 | 3.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.22 | 0.16 | |
| Incremental Delay, d2 | 0.4 | 0.1 | | 1.2 | 0.1 | 0.3 | 2.8 | 0.2 | 0.0 | 3.4 | 0.2 | |
| Delay (s) | 41.5 | 41.0 | | 42.9 | 40.9 | 41.2 | 49.2 | 7.2 | 0.0 | 51.6 | 0.7 | |
| Level of Service | D | D | | D | D | D | D | A | A | D | A | |
| Approach Delay (s) | | 41.2 | | | 41.5 | | | 8.7 | | | 10.6 | |
| Approach LOS | | D | | | D | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 14.0 | | | | HCM Level of Service | | | B | | |
| HCM Volume to Capacity ratio | | | 0.31 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | | Sum of lost time (s) | | | 6.0 | | |
| Intersection Capacity Utilization | | | 48.4% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

Near-Term With Project













HCM Signalized Intersection Capacity Analysis 8: Lone Tree Way & Canada Valley

Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |   |    |  |   |   |  |   |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.87 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1540 | 1504 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1540 | 1504 | 1770 | 1863 | 1583 |
| Volume (vph) | 49 | 971 | 65 | 211 | 1119 | 233 | 76 | 14 | 184 | 386 | 31 | 94 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 54 | 1079 | 72 | 234 | 1243 | 259 | 84 | 16 | 204 | 429 | 34 | 104 |
| RTOR Reduction (vph) | 0 | 0 | 19 | 0 | 0 | 103 | 0 | 96 | 96 | 0 | 0 | 83 |
| Lane Group Flow (vph) | 54 | 1079 | 53 | 234 | 1243 | 156 | 84 | 22 | 6 | 429 | 34 | 21 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 4.8 | 66.9 | 66.9 | 13.2 | 75.3 | 75.3 | 6.6 | 6.9 | 6.9 | 25.0 | 25.3 | 25.3 |
| Effective Green, g (s) | 5.8 | 69.9 | 69.9 | 14.2 | 78.3 | 78.3 | 7.6 | 7.9 | 7.9 | 26.0 | 26.3 | 26.3 |
| Actuated g/C Ratio | 0.04 | 0.54 | 0.54 | 0.11 | 0.60 | 0.60 | 0.06 | 0.06 | 0.06 | 0.20 | 0.20 | 0.20 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 6.0 | 6.0 | 2.0 | 2.0 | 2.0 | 2.0 | 6.0 | 6.0 |
| Lane Grp Cap (vph) | 79 | 2734 | 851 | 375 | 3063 | 953 | 201 | 94 | 91 | 354 | 377 | 320 |
| v/s Ratio Prot | c0.03 | 0.21 | | c0.07 | c0.24 | | 0.02 | c0.01 | | c0.24 | 0.02 | |
| v/s Ratio Perm | | | 0.03 | | | 0.10 | | | 0.00 | | | 0.01 |
| v/c Ratio | 0.68 | 0.39 | 0.06 | 0.62 | 0.41 | 0.16 | 0.42 | 0.24 | 0.07 | 1.21 | 0.09 | 0.07 |
| Uniform Delay, d1 | 61.2 | 17.6 | 14.4 | 55.3 | 13.6 | 11.4 | 59.1 | 58.2 | 57.6 | 52.0 | 42.1 | 41.9 |
| Progression Factor | 0.83 | 0.58 | 0.43 | 1.23 | 0.61 | 0.79 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 15.5 | 0.4 | 0.1 | 2.1 | 0.4 | 0.3 | 0.5 | 0.5 | 0.1 | 118.7 | 0.3 | 0.2 |
| Delay (s) | 66.5 | 10.7 | 6.3 | 70.3 | 8.7 | 9.3 | 59.6 | 58.6 | 57.7 | 170.7 | 42.4 | 42.2 |
| Level of Service | E | B | A | E | A | A | E | E | E | F | D | D |
| Approach Delay (s) | | 12.9 | | | 17.1 | | | 58.6 | | | 139.4 | |
| Approach LOS | | B | | | B | | | E | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 37.3 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 63.0% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
9: Lone Tree Way & SR-4 Bypass SB Off-Ramp













Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Volume (vph) | 0 | 998 | 528 | 72 | 1142 | 0 | 0 | 0 | 0 | 287 | 6 | 435 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 1109 | 587 | 80 | 1269 | 0 | 0 | 0 | 0 | 319 | 7 | 483 |
| RTOR Reduction (vph) | 0 | 0 | 266 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| Lane Group Flow (vph) | 0 | 1109 | 321 | 80 | 1269 | 0 | 0 | 0 | 0 | 160 | 166 | 453 |
| Confl. Peds. (#/hr) | | | | | | | 2 | | | | | |
| Turn Type | | Perm | | Prot | | | | | | Perm | | Perm |
| Protected Phases | | 2 | | 1 | 6 | | | | | | 4 | |
| Permitted Phases | | | 2 | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 68.5 | 68.5 | 7.0 | 79.5 | | | | | 41.0 | 41.0 | 41.0 |
| Effective Green, g (s) | | 71.0 | 71.0 | 8.0 | 82.0 | | | | | 42.0 | 42.0 | 42.0 |
| Actuated g/C Ratio | | 0.55 | 0.55 | 0.06 | 0.63 | | | | | 0.32 | 0.32 | 0.32 |
| Clearance Time (s) | | 5.5 | 5.5 | 4.0 | 5.5 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 3.0 | 4.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2777 | 865 | 211 | 3207 | | | | | 543 | 546 | 511 |
| v/s Ratio Prot | | 0.22 | | 0.02 | c0.25 | | | | | | | |
| v/s Ratio Perm | | | 0.20 | | | | | | | 0.10 | 0.10 | c0.29 |
| v/c Ratio | | 0.40 | 0.37 | 0.38 | 0.40 | | | | | 0.29 | 0.30 | 0.89 |
| Uniform Delay, d1 | | 17.1 | 16.8 | 58.6 | 11.8 | | | | | 32.9 | 33.0 | 41.7 |
| Progression Factor | | 0.83 | 1.33 | 1.30 | 0.40 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.4 | 1.0 | 1.1 | 0.4 | | | | | 0.3 | 0.3 | 16.8 |
| Delay (s) | | 14.5 | 23.3 | 77.4 | 5.1 | | | | | 33.2 | 33.3 | 58.5 |
| Level of Service | | B | C | E | A | | | | | C | C | E |
| Approach Delay (s) | | 17.5 | | | 9.4 | | | 0.0 | | | 48.4 | |
| Approach LOS | | B | | | A | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.2 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 6.0 | | |
| Intersection Capacity Utilization | | | 55.7% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
10: Lone Tree Way & On-ramp














Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1695 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1695 | 1583 | | | |
| Volume (vph) | 0 | 867 | 382 | 8 | 763 | 245 | 433 | 29 | 79 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 0 | 974 | 429 | 9 | 857 | 275 | 487 | 33 | 89 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 119 | 0 | 0 | 66 | 0 | 0 | 72 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 974 | 310 | 9 | 857 | 209 | 253 | 267 | 17 | 0 | 0 | 0 |
| Turn Type | | | Perm | Prot | | Perm | Split | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | 8 | 8 | | | | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | | 90.8 | 90.8 | 1.2 | 96.0 | 96.0 | 24.0 | 24.0 | 24.0 | | | |
| Effective Green, g (s) | | 93.8 | 93.8 | 2.2 | 99.0 | 99.0 | 25.0 | 25.0 | 25.0 | | | |
| Actuated g/C Ratio | | 0.72 | 0.72 | 0.02 | 0.76 | 0.76 | 0.19 | 0.19 | 0.19 | | | |
| Clearance Time (s) | | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | 3669 | 1142 | 30 | 3872 | 1206 | 323 | 326 | 304 | | | | |
| v/s Ratio Prot | | 0.19 | | c0.01 | 0.17 | | 0.15 | c0.16 | | | | |
| v/s Ratio Perm | | | c0.20 | | | 0.13 | | | 0.01 | | | |
| v/c Ratio | | 0.27 | 0.27 | 0.30 | 0.22 | 0.17 | 0.78 | 0.82 | 0.06 | | | |
| Uniform Delay, d1 | | 6.2 | 6.3 | 63.1 | 4.4 | 4.3 | 49.9 | 50.3 | 42.9 | | | |
| Progression Factor | | 0.45 | 1.92 | 0.66 | 1.91 | 7.79 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.2 | 0.6 | 2.0 | 0.1 | 0.3 | 10.9 | 14.0 | 0.0 | | | |
| Delay (s) | | 3.0 | 12.6 | 43.8 | 8.6 | 33.5 | 60.8 | 64.4 | 42.9 | | | |
| Level of Service | | A | B | D | A | C | E | E | D | | | |
| Approach Delay (s) | | 5.9 | | | 14.9 | | | 59.7 | | | 0.0 | |
| Approach LOS | | A | | | B | | | E | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 19.6 | | HCM Level of Service | | | | | B | | | |
| HCM Volume to Capacity ratio | | 0.38 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | Sum of lost time (s) | | | | | 9.0 | | | |
| Intersection Capacity Utilization | | 36.2% | | ICU Level of Service | | | | | A | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Shady Willow Rd

Davidon EIR
Near-Term Plus Project AM Peak Hour

























| |  | | | | | | | | | | | |
|-----------------------------------|--|---|---|---|---|---|---|---|--|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1549 | 1770 | 3539 | 1562 | 3433 | 3080 | | 3433 | 1863 | 1563 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1549 | 1770 | 3539 | 1562 | 3433 | 3080 | | 3433 | 1863 | 1563 |
| Volume (vph) | 74 | 689 | 91 | 54 | 929 | 29 | 39 | 47 | 191 | 42 | 35 | 24 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 82 | 766 | 101 | 60 | 1032 | 32 | 43 | 52 | 212 | 47 | 39 | 27 |
| RTOR Reduction (vph) | 0 | 0 | 34 | 0 | 0 | 9 | 0 | 185 | 0 | 0 | 0 | 24 |
| Lane Group Flow (vph) | 82 | 766 | 67 | 60 | 1032 | 23 | 43 | 79 | 0 | 47 | 39 | 3 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 7.2 | 83.5 | 83.5 | 7.7 | 84.0 | 84.0 | 5.9 | 15.4 | | 5.4 | 14.9 | 14.9 |
| Effective Green, g (s) | 8.2 | 86.5 | 86.5 | 8.7 | 87.0 | 87.0 | 6.9 | 16.4 | | 6.4 | 15.9 | 15.9 |
| Actuated g/C Ratio | 0.06 | 0.67 | 0.67 | 0.07 | 0.67 | 0.67 | 0.05 | 0.13 | | 0.05 | 0.12 | 0.12 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 3.0 | 4.0 | | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 217 | 3383 | 1031 | 118 | 2368 | 1045 | 182 | 389 | | 169 | 228 | 191 |
| v/s Ratio Prot | 0.02 | 0.15 | | c0.03 | c0.29 | | c0.01 | c0.03 | | c0.01 | 0.02 | |
| v/s Ratio Perm | | | 0.04 | | | 0.01 | | | | | | 0.00 |
| v/c Ratio | 0.38 | 0.23 | 0.07 | 0.51 | 0.44 | 0.02 | 0.24 | 0.20 | | 0.28 | 0.17 | 0.02 |
| Uniform Delay, d1 | 58.5 | 8.6 | 7.6 | 58.6 | 10.0 | 7.2 | 59.0 | 50.9 | | 59.6 | 51.1 | 50.2 |
| Progression Factor | 0.99 | 0.91 | 1.55 | 0.83 | 1.60 | 2.75 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.1 | 0.2 | 0.1 | 1.2 | 0.5 | 0.0 | 0.7 | 0.4 | | 0.3 | 0.1 | 0.0 |
| Delay (s) | 58.7 | 8.0 | 11.9 | 49.9 | 16.6 | 19.8 | 59.7 | 51.3 | | 59.9 | 51.3 | 50.2 |
| Level of Service | E | A | B | D | B | B | E | D | | E | D | D |
| Approach Delay (s) | | 12.8 | | | 18.5 | | | 52.5 | | | 54.6 | |
| Approach LOS | | B | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 22.1 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.39 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 9.0 | | |
| Intersection Capacity Utilization | | | 58.2% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue

























Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 1770 | 3539 | 1583 | 3433 | 1863 | 1562 | 3433 | 3139 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 1770 | 3539 | 1583 | 3433 | 1863 | 1562 | 3433 | 3139 | |
| Volume (vph) | 292 | 580 | 26 | 81 | 673 | 80 | 89 | 48 | 41 | 105 | 77 | 238 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 324 | 644 | 29 | 90 | 748 | 89 | 99 | 53 | 46 | 117 | 86 | 264 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 51 | 0 | 0 | 43 | 0 | 236 | 0 |
| Lane Group Flow (vph) | 324 | 644 | 19 | 90 | 748 | 38 | 99 | 53 | 3 | 117 | 114 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | 1 | 1 | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | Perm | Split | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 38.4 | 82.4 | 82.4 | 10.8 | 54.8 | 54.8 | 8.0 | 8.0 | 8.0 | 12.8 | 12.8 | |
| Effective Green, g (s) | 39.4 | 83.4 | 83.4 | 11.8 | 55.8 | 55.8 | 9.0 | 9.0 | 9.0 | 13.8 | 13.8 | |
| Actuated g/C Ratio | 0.30 | 0.64 | 0.64 | 0.09 | 0.43 | 0.43 | 0.07 | 0.07 | 0.07 | 0.11 | 0.11 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 536 | 3262 | 1002 | 161 | 1519 | 679 | 238 | 129 | 108 | 364 | 333 | |
| v/s Ratio Prot | c0.18 | 0.13 | | 0.05 | c0.21 | | c0.03 | 0.03 | | 0.03 | c0.04 | |
| v/s Ratio Perm | | | 0.01 | | | 0.02 | | | 0.00 | | | |
| v/c Ratio | 0.60 | 0.20 | 0.02 | 0.56 | 0.49 | 0.06 | 0.42 | 0.41 | 0.03 | 0.32 | 0.34 | |
| Uniform Delay, d1 | 38.7 | 9.6 | 8.5 | 56.6 | 26.9 | 21.7 | 58.0 | 58.0 | 56.4 | 53.8 | 53.9 | |
| Progression Factor | 0.77 | 0.46 | 0.14 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.3 | 0.1 | 0.0 | 2.4 | 1.1 | 0.2 | 0.4 | 0.8 | 0.0 | 0.2 | 0.2 | |
| Delay (s) | 31.2 | 4.6 | 1.2 | 59.0 | 28.0 | 21.9 | 58.4 | 58.7 | 56.5 | 54.0 | 54.1 | |
| Level of Service | C | A | A | E | C | C | E | E | E | D | D | |
| Approach Delay (s) | | 13.1 | | | 30.4 | | | 58.0 | | | 54.1 | |
| Approach LOS | | B | | | C | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 30.1 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.51 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 61.3% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

























HCM Signalized Intersection Capacity Analysis
13: Lone Tree Way & Deer Valley Rd.

Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.83 | 1.00 | 1.00 | 0.92 | 1.00 | 0.95 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3539 | 1308 | 1770 | 3539 | 1454 | 3433 | 3150 | | 2000 | 3508 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3539 | 1308 | 1770 | 3539 | 1454 | 3433 | 3150 | | 1770 | 3508 | |
| Volume (vph) | 35 | 709 | 164 | 228 | 981 | 185 | 298 | 245 | 174 | 353 | 457 | 17 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 39 | 797 | 184 | 256 | 1102 | 208 | 335 | 275 | 196 | 397 | 513 | 19 |
| RTOR Reduction (vph) | 0 | 0 | 47 | 0 | 0 | 34 | 0 | 102 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 39 | 797 | 137 | 256 | 1102 | 174 | 335 | 369 | 0 | 397 | 530 | 0 |
| Confl. Peds. (#/hr) | 44 | | 101 | 101 | | 44 | 58 | | 69 | 69 | | 58 |
| Confl. Bikes (#/hr) | | | 31 | | | 15 | | | 13 | | | 5 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | |
| Actuated Green, G (s) | 7.3 | 33.7 | 33.7 | 23.2 | 49.6 | 49.6 | 17.5 | 24.3 | | 30.3 | 37.1 | |
| Effective Green, g (s) | 8.8 | 35.7 | 35.7 | 24.7 | 51.6 | 51.6 | 19.0 | 25.8 | | 31.8 | 38.6 | |
| Actuated g/C Ratio | 0.07 | 0.27 | 0.27 | 0.19 | 0.40 | 0.40 | 0.15 | 0.20 | | 0.24 | 0.30 | |
| Clearance Time (s) | 4.5 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 3.0 | 3.0 | | 4.0 | 3.0 | |
| Lane Grp Cap (vph) | 120 | 972 | 359 | 336 | 1405 | 577 | 502 | 625 | | 489 | 1042 | |
| v/s Ratio Prot | 0.02 | 0.23 | | c0.14 | c0.31 | | 0.10 | c0.12 | | c0.20 | 0.15 | |
| v/s Ratio Perm | | | 0.10 | | | 0.12 | | | | | | |
| v/c Ratio | 0.33 | 0.82 | 0.38 | 0.76 | 0.78 | 0.30 | 0.67 | 0.59 | | 0.81 | 0.51 | |
| Uniform Delay, d1 | 57.8 | 44.1 | 38.2 | 49.9 | 34.3 | 26.9 | 52.5 | 47.3 | | 46.3 | 37.8 | |
| Progression Factor | 1.18 | 1.23 | 1.56 | 1.08 | 0.55 | 0.33 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.5 | 7.2 | 2.8 | 6.0 | 2.7 | 0.8 | 3.3 | 1.5 | | 10.4 | 0.4 | |
| Delay (s) | 69.7 | 61.6 | 62.6 | 59.7 | 21.4 | 9.7 | 55.9 | 48.8 | | 56.7 | 38.2 | |
| Level of Service | E | E | E | E | C | A | E | D | | E | D | |
| Approach Delay (s) | | 62.1 | | | 26.1 | | | 51.7 | | | 46.1 | |
| Approach LOS | | E | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 43.7 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.74 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 89.7% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |










HCM Signalized Intersection Capacity Analysis
14: Lone Tree Way & Hillcrest Ave.

Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1515 | 1770 | 3539 | 1519 | 1770 | 3421 | | 1900 | 3275 | 1554 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1515 | 1770 | 3539 | 1519 | 1770 | 3421 | | 1610 | 3275 | 1554 |
| Volume (vph) | 218 | 581 | 18 | 24 | 1012 | 213 | 36 | 53 | 13 | 405 | 85 | 329 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 242 | 646 | 20 | 27 | 1124 | 237 | 40 | 59 | 14 | 450 | 94 | 366 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 106 | 0 | 13 | 0 | 0 | 0 | 296 |
| Lane Group Flow (vph) | 242 | 646 | 11 | 27 | 1124 | 131 | 40 | 60 | 0 | 225 | 319 | 70 |
| Confl. Peds. (#/hr) | 18 | | | 20 | | 18 | 5 | | 10 | 10 | | 5 |
| Confl. Bikes (#/hr) | | | 12 | | | 9 | | | | | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 26.6 | 71.6 | 71.6 | 4.2 | 48.7 | 48.7 | 11.8 | 11.8 | | 22.9 | 22.9 | 22.9 |
| Effective Green, g (s) | 28.6 | 73.6 | 73.6 | 5.7 | 50.7 | 50.7 | 13.8 | 13.8 | | 24.9 | 24.9 | 24.9 |
| Actuated g/C Ratio | 0.22 | 0.57 | 0.57 | 0.04 | 0.39 | 0.39 | 0.11 | 0.11 | | 0.19 | 0.19 | 0.19 |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 389 | 2004 | 858 | 78 | 1380 | 592 | 188 | 363 | | 364 | 627 | 298 |
| v/s Ratio Prot | c0.14 | 0.18 | | 0.02 | c0.32 | | c0.02 | 0.02 | | c0.12 | 0.10 | |
| v/s Ratio Perm | | | 0.01 | | | 0.09 | | | | | | 0.05 |
| v/c Ratio | 0.62 | 0.32 | 0.01 | 0.35 | 0.81 | 0.22 | 0.21 | 0.17 | | 0.62 | 0.51 | 0.24 |
| Uniform Delay, d1 | 45.8 | 15.0 | 12.3 | 60.3 | 35.4 | 26.5 | 53.1 | 52.9 | | 48.2 | 47.1 | 44.5 |
| Progression Factor | 1.46 | 1.13 | 2.18 | 1.23 | 0.71 | 0.52 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.9 | 0.4 | 0.0 | 2.4 | 4.8 | 0.8 | 1.2 | 0.5 | | 4.5 | 1.4 | 0.9 |
| Delay (s) | 70.9 | 17.4 | 26.9 | 76.4 | 30.0 | 14.6 | 54.3 | 53.3 | | 52.7 | 48.4 | 45.3 |
| Level of Service | E | B | C | E | C | B | D | D | | D | D | D |
| Approach Delay (s) | | 31.8 | | | 28.2 | | | 53.7 | | | 48.2 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 35.6 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.66 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 68.9% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
15: Lone Tree Way & Vista Grande





















Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|---|-------|---|---|----------------------|--|---|------|---|---|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.87 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5057 | | 1770 | 5062 | | 1770 | 1612 | | 1770 | 1661 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.64 | 1.00 | | 0.37 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5057 | | 1770 | 5062 | | 1188 | 1612 | | 696 | 1661 | |
| Volume (vph) | 20 | 904 | 30 | 59 | 1179 | 37 | 39 | 14 | 123 | 24 | 16 | 41 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 22 | 972 | 32 | 63 | 1268 | 40 | 42 | 15 | 132 | 26 | 17 | 44 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 121 | 0 | 0 | 40 | 0 |
| Lane Group Flow (vph) | 22 | 1003 | 0 | 63 | 1307 | 0 | 42 | 26 | 0 | 26 | 21 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | | | | |
| Turn Type | Prot | | | Prot | | | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 5.4 | 96.8 | | 9.5 | 100.9 | | 9.2 | 9.2 | | 9.2 | 9.2 | |
| Effective Green, g (s) | 6.9 | 99.3 | | 11.0 | 103.4 | | 10.7 | 10.7 | | 10.7 | 10.7 | |
| Actuated g/C Ratio | 0.05 | 0.76 | | 0.08 | 0.80 | | 0.08 | 0.08 | | 0.08 | 0.08 | |
| Clearance Time (s) | 4.5 | 5.5 | | 4.5 | 5.5 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 4.0 | 6.0 | | 4.0 | 6.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 94 | 3863 | | 150 | 4026 | | 98 | 133 | | 57 | 137 | |
| v/s Ratio Prot | 0.01 | 0.20 | | c0.04 | c0.26 | | | 0.02 | | | 0.01 | |
| v/s Ratio Perm | | | | | | | 0.04 | | | c0.04 | | |
| v/c Ratio | 0.23 | 0.26 | | 0.42 | 0.32 | | 0.43 | 0.19 | | 0.46 | 0.15 | |
| Uniform Delay, d1 | 59.0 | 4.5 | | 56.5 | 3.7 | | 56.7 | 55.6 | | 56.9 | 55.4 | |
| Progression Factor | 0.93 | 1.05 | | 0.98 | 0.70 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.6 | 0.1 | | 2.2 | 0.2 | | 3.0 | 0.7 | | 5.7 | 0.5 | |
| Delay (s) | 56.7 | 4.9 | | 57.7 | 2.7 | | 59.7 | 56.3 | | 62.6 | 55.9 | |
| Level of Service | E | A | | E | A | | E | E | | E | E | |
| Approach Delay (s) | | 6.0 | | | 5.3 | | | 57.1 | | | 57.9 | |
| Approach LOS | | A | | | A | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 10.9 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.34 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 6.0 | | |
| Intersection Capacity Utilization | | | 51.9% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
16: Country Hills Dr. & Hillcrest Ave
























Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 0.99 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.90 | | 1.00 | 0.90 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1665 | | 1770 | 1667 | | 1770 | 3483 | | 1770 | 3495 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1665 | | 1770 | 1667 | | 1770 | 3483 | | 1770 | 3495 | |
| Volume (vph) | 44 | 77 | 143 | 84 | 93 | 162 | 70 | 384 | 31 | 78 | 623 | 26 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 49 | 86 | 159 | 93 | 103 | 180 | 78 | 427 | 34 | 87 | 692 | 29 |
| RTOR Reduction (vph) | 0 | 39 | 0 | 0 | 35 | 0 | 0 | 3 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 49 | 206 | 0 | 93 | 248 | 0 | 78 | 458 | 0 | 87 | 719 | 0 |
| Confl. Peds. (#/hr) | 3 | | 2 | 2 | | 3 | 45 | | 16 | 16 | | 45 |
| Turn Type | Split | | | Split | | | Prot | | | Prot | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 21.5 | 21.5 | | 24.9 | 24.9 | | 9.7 | 65.9 | | 10.3 | 66.5 | |
| Effective Green, g (s) | 22.0 | 22.0 | | 25.4 | 25.4 | | 10.2 | 67.4 | | 10.8 | 68.0 | |
| Actuated g/C Ratio | 0.16 | 0.16 | | 0.18 | 0.18 | | 0.07 | 0.49 | | 0.08 | 0.49 | |
| Clearance Time (s) | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 4.5 | | 3.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 283 | 266 | | 327 | 308 | | 131 | 1706 | | 139 | 1727 | |
| v/s Ratio Prot | 0.03 | c0.12 | | 0.05 | c0.15 | | c0.04 | 0.13 | | c0.05 | c0.21 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.17 | 0.77 | | 0.28 | 0.80 | | 0.60 | 0.27 | | 0.63 | 0.42 | |
| Uniform Delay, d1 | 49.9 | 55.4 | | 48.3 | 53.7 | | 61.7 | 20.6 | | 61.4 | 22.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 13.0 | | 0.5 | 14.1 | | 7.1 | 0.4 | | 8.5 | 0.7 | |
| Delay (s) | 50.2 | 68.4 | | 48.8 | 67.9 | | 68.8 | 21.0 | | 69.9 | 22.9 | |
| Level of Service | D | E | | D | E | | E | C | | E | C | |
| Approach Delay (s) | | 65.4 | | | 63.1 | | | 27.9 | | | 28.0 | |
| Approach LOS | | E | | | E | | | C | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 40.0 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.60 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 137.6 | | | Sum of lost time (s) | | | 15.0 | | | |
| Intersection Capacity Utilization | | | 55.9% | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
18: Sterling Hill Dr. & Hillcrest Ave


































Davidon EIR
Near-Term Plus Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1661 | | 1767 | 1863 | 1583 | 1770 | 3539 | 1545 | 1770 | 3474 | |
| Flt Permitted | 0.69 | 1.00 | | 0.46 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1280 | 1661 | | 855 | 1863 | 1583 | 1770 | 3539 | 1545 | 1770 | 3474 | |
| Volume (vph) | 150 | 50 | 100 | 48 | 67 | 155 | 67 | 504 | 25 | 74 | 576 | 80 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 169 | 56 | 112 | 54 | 75 | 174 | 75 | 566 | 28 | 83 | 647 | 90 |
| RTOR Reduction (vph) | 0 | 91 | 0 | 0 | 0 | 142 | 0 | 0 | 0 | 0 | 6 | 0 |
| Lane Group Flow (vph) | 169 | 77 | 0 | 54 | 75 | 32 | 75 | 566 | 28 | 83 | 731 | 0 |
| Confl. Peds. (#/hr) | | | 2 | 2 | | | | | 9 | 9 | | |
| Turn Type | Perm | | | Perm | | Perm | Prot | | Free | Prot | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | | | Free | | | |
| Actuated Green, G (s) | 16.9 | 16.9 | | 16.9 | 16.9 | 16.9 | 8.3 | 59.8 | 100.0 | 8.8 | 60.3 | |
| Effective Green, g (s) | 18.4 | 18.4 | | 18.4 | 18.4 | 18.4 | 9.3 | 62.8 | 100.0 | 9.8 | 63.3 | |
| Actuated g/C Ratio | 0.18 | 0.18 | | 0.18 | 0.18 | 0.18 | 0.09 | 0.63 | 1.00 | 0.10 | 0.63 | |
| Clearance Time (s) | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.5 | 3.5 | 3.5 | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 236 | 306 | | 157 | 343 | 291 | 165 | 2222 | 1545 | 173 | 2199 | |
| v/s Ratio Prot | | 0.05 | | | 0.04 | | 0.04 | 0.16 | | c0.05 | c0.21 | |
| v/s Ratio Perm | c0.13 | | | 0.06 | | 0.02 | | | c0.02 | | | |
| v/c Ratio | 0.72 | 0.25 | | 0.34 | 0.22 | 0.11 | 0.45 | 0.25 | 0.02 | 0.48 | 0.33 | |
| Uniform Delay, d1 | 38.3 | 34.9 | | 35.5 | 34.7 | 34.0 | 42.9 | 8.2 | 0.0 | 42.7 | 8.5 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.14 | 0.44 | |
| Incremental Delay, d2 | 9.9 | 0.4 | | 1.6 | 0.4 | 0.2 | 2.0 | 0.3 | 0.0 | 2.0 | 0.4 | |
| Delay (s) | 48.2 | 35.3 | | 37.1 | 35.1 | 34.2 | 44.9 | 8.5 | 0.0 | 50.6 | 4.1 | |
| Level of Service | D | D | | D | D | C | D | A | A | D | A | |
| Approach Delay (s) | | 41.8 | | | 34.9 | | | 12.2 | | | 8.8 | |
| Approach LOS | | D | | | C | | | B | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 18.8 | | | HCM Level of Service | | | B | | | |
| HCM Volume to Capacity ratio | | | 0.41 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | Sum of lost time (s) | | | 6.0 | | | |
| Intersection Capacity Utilization | | | 51.4% | | | ICU Level of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 8: Lone Tree Way & Canada Valley



























Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |   |    |  |   |   |  |   |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 3433 | 5085 | 1547 | 3433 | 1595 | 1504 | 1770 | 1863 | 1558 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 3433 | 5085 | 1547 | 3433 | 1595 | 1504 | 1770 | 1863 | 1558 |
| Volume (vph) | 122 | 1586 | 100 | 480 | 1256 | 474 | 110 | 55 | 262 | 305 | 56 | 62 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 127 | 1652 | 104 | 500 | 1308 | 494 | 115 | 57 | 273 | 318 | 58 | 65 |
| RTOR Reduction (vph) | 0 | 0 | 22 | 0 | 0 | 207 | 0 | 66 | 142 | 0 | 0 | 56 |
| Lane Group Flow (vph) | 127 | 1652 | 82 | 500 | 1308 | 287 | 115 | 101 | 21 | 318 | 58 | 9 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 4 | | | | | 4 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 10.0 | 58.7 | 58.7 | 23.9 | 72.6 | 72.6 | 11.9 | 15.4 | 15.4 | 14.0 | 17.5 | 17.5 |
| Effective Green, g (s) | 11.0 | 61.7 | 61.7 | 24.9 | 75.6 | 75.6 | 12.9 | 16.4 | 16.4 | 15.0 | 18.5 | 18.5 |
| Actuated g/C Ratio | 0.08 | 0.47 | 0.47 | 0.19 | 0.58 | 0.58 | 0.10 | 0.13 | 0.13 | 0.12 | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 6.0 | 6.0 | 2.0 | 2.0 | 2.0 | 2.0 | 6.0 | 6.0 |
| Lane Grp Cap (vph) | 150 | 2413 | 741 | 658 | 2957 | 900 | 341 | 201 | 190 | 204 | 265 | 222 |
| v/s Ratio Prot | c0.07 | c0.32 | | c0.15 | 0.26 | | 0.03 | c0.06 | | c0.18 | 0.03 | |
| v/s Ratio Perm | | | 0.05 | | | 0.19 | | | 0.01 | | | 0.01 |
| v/c Ratio | 0.85 | 0.68 | 0.11 | 0.76 | 0.44 | 0.32 | 0.34 | 0.50 | 0.11 | 1.56 | 0.22 | 0.04 |
| Uniform Delay, d1 | 58.7 | 26.6 | 18.9 | 49.7 | 15.3 | 14.0 | 54.6 | 53.0 | 50.3 | 57.5 | 49.4 | 48.1 |
| Progression Factor | 0.87 | 0.76 | 0.91 | 1.24 | 0.73 | 1.48 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 25.3 | 1.2 | 0.2 | 3.1 | 0.3 | 0.6 | 0.2 | 0.7 | 0.1 | 274.1 | 1.2 | 0.2 |
| Delay (s) | 76.3 | 21.4 | 17.5 | 64.7 | 11.6 | 21.4 | 54.8 | 53.7 | 50.4 | 331.6 | 50.5 | 48.3 |
| Level of Service | E | C | B | E | B | C | D | D | D | F | D | D |
| Approach Delay (s) | | 24.9 | | | 25.2 | | | 52.8 | | | 252.8 | |
| Approach LOS | | C | | | C | | | D | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 47.3 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.79 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 15.0 | | |
| Intersection Capacity Utilization | | | 82.8% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 9: Lone Tree Way & SR-4 Bypass SB Off-Ramp













Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |    |  |    |    | | | | |  |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1689 | 1583 |
| Volume (vph) | 0 | 1519 | 642 | 98 | 1576 | 0 | 0 | 0 | 0 | 416 | 10 | 624 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 1599 | 676 | 103 | 1659 | 0 | 0 | 0 | 0 | 438 | 11 | 657 |
| RTOR Reduction (vph) | 0 | 0 | 389 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Lane Group Flow (vph) | 0 | 1599 | 287 | 103 | 1659 | 0 | 0 | 0 | 0 | 219 | 230 | 650 |
| Confl. Peds. (#/hr) | | | | | | | 3 | | 3 | | | |
| Turn Type | | Perm | | Prot | | | | | | Perm | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | | 4 | |
| Permitted Phases | | 2 | | | | | | | | 4 | 4 | |
| Actuated Green, G (s) | | 52.7 | 52.7 | 8.9 | 65.6 | | | | | 54.9 | 54.9 | 54.9 |
| Effective Green, g (s) | | 55.2 | 55.2 | 9.9 | 68.1 | | | | | 55.9 | 55.9 | 55.9 |
| Actuated g/C Ratio | | 0.42 | 0.42 | 0.08 | 0.52 | | | | | 0.43 | 0.43 | 0.43 |
| Clearance Time (s) | | 5.5 | 5.5 | 4.0 | 5.5 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 4.0 | 4.0 | 3.0 | 4.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2159 | 672 | 261 | 2664 | | | | | 723 | 726 | 681 |
| v/s Ratio Prot | | c0.31 | | 0.03 | c0.33 | | | | | | | |
| v/s Ratio Perm | | 0.18 | | | | | | | | 0.13 | 0.14 | c0.41 |
| v/c Ratio | | 0.74 | 0.43 | 0.39 | 0.62 | | | | | 0.30 | 0.32 | 0.95 |
| Uniform Delay, d1 | | 31.4 | 26.3 | 57.2 | 21.9 | | | | | 24.3 | 24.4 | 35.8 |
| Progression Factor | | 0.72 | 1.85 | 1.05 | 0.59 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 1.5 | 1.3 | 0.9 | 1.0 | | | | | 0.2 | 0.3 | 23.7 |
| Delay (s) | | 24.0 | 49.9 | 61.0 | 14.0 | | | | | 24.5 | 24.7 | 59.5 |
| Level of Service | | C | D | E | B | | | | | C | C | E |
| Approach Delay (s) | | 31.7 | | 16.8 | | | 0.0 | | | 45.4 | | |
| Approach LOS | | C | | B | | | A | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 29.5 | | HCM Level of Service | | | | C | | | | |
| HCM Volume to Capacity ratio | | 0.83 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 130.0 | | Sum of lost time (s) | | | | 9.0 | | | | |
| Intersection Capacity Utilization | | 75.8% | | ICU Level of Service | | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |

c Critical Lane Group














HCM Signalized Intersection Capacity Analysis 10: Lone Tree Way & On-ramp

Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.95 | 0.95 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1696 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.96 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 1770 | 5085 | 1583 | 1681 | 1696 | 1583 | | | |
| Volume (vph) | 0 | 1590 | 428 | 21 | 1099 | 357 | 592 | 43 | 137 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 0 | 1747 | 470 | 23 | 1208 | 392 | 651 | 47 | 151 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 148 | 0 | 0 | 115 | 0 | 0 | 114 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1747 | 322 | 23 | 1208 | 277 | 340 | 358 | 37 | 0 | 0 | 0 |
| Turn Type | | | Perm | Prot | | Perm | Split | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | 8 | 8 | | | | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | | 80.7 | 80.7 | 4.2 | 88.9 | 88.9 | 31.1 | 31.1 | 31.1 | | | |
| Effective Green, g (s) | | 83.7 | 83.7 | 5.2 | 91.9 | 91.9 | 32.1 | 32.1 | 32.1 | | | |
| Actuated g/C Ratio | | 0.64 | 0.64 | 0.04 | 0.71 | 0.71 | 0.25 | 0.25 | 0.25 | | | |
| Clearance Time (s) | | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | | | |
| Lane Grp Cap (vph) | | 3274 | 1019 | 71 | 3595 | 1119 | 415 | 419 | 391 | | | |
| v/s Ratio Prot | | c0.34 | | 0.01 | c0.24 | | 0.20 | c0.21 | | | | |
| v/s Ratio Perm | | | 0.20 | | | 0.18 | | | 0.02 | | | |
| v/c Ratio | | 0.53 | 0.32 | 0.32 | 0.34 | 0.25 | 0.82 | 0.85 | 0.10 | | | |
| Uniform Delay, d1 | | 12.6 | 10.4 | 60.7 | 7.3 | 6.8 | 46.2 | 46.7 | 37.8 | | | |
| Progression Factor | | 0.24 | 0.03 | 0.86 | 1.05 | 1.90 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.5 | 0.7 | 0.9 | 0.2 | 0.5 | 11.4 | 15.0 | 0.0 | | | |
| Delay (s) | | 3.5 | 1.0 | 52.8 | 7.9 | 13.4 | 57.6 | 61.7 | 37.8 | | | |
| Level of Service | | A | A | D | A | B | E | E | D | | | |
| Approach Delay (s) | | 3.0 | | | 9.9 | | | 55.8 | | | 0.0 | |
| Approach LOS | | A | | | A | | | E | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 14.9 | | | | HCM Level of Service | | | | B | |
| HCM Volume to Capacity ratio | | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | | 9.0 | |
| Intersection Capacity Utilization | | | 54.9% | | | | ICU Level of Service | | | | A | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis 11: Lone Tree Way & Slaten Ranch

Davidon EIR
Near-Term Plus Project PM Peak Hour































| |  | | | | | | | | | | | |
|-----------------------------------|--|---|---|---|---|---|---|---|--|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1549 | 1770 | 3539 | 1561 | 3433 | 3174 | | 3433 | 1863 | 1561 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1549 | 1770 | 3539 | 1561 | 3433 | 3174 | | 3433 | 1863 | 1561 |
| Volume (vph) | 217 | 1078 | 256 | 160 | 1071 | 55 | 51 | 76 | 167 | 114 | 67 | 101 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 231 | 1147 | 272 | 170 | 1139 | 59 | 54 | 81 | 178 | 121 | 71 | 107 |
| RTOR Reduction (vph) | 0 | 0 | 118 | 0 | 0 | 20 | 0 | 155 | 0 | 0 | 0 | 90 |
| Lane Group Flow (vph) | 231 | 1147 | 154 | 170 | 1139 | 39 | 54 | 104 | 0 | 121 | 71 | 17 |
| Confl. Peds. (#/hr) | 2 | | 1 | 1 | | 2 | 2 | | | | | 2 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 13.2 | 70.5 | 70.5 | 16.1 | 73.4 | 73.4 | 6.3 | 15.6 | | 9.8 | 19.1 | 19.1 |
| Effective Green, g (s) | 14.2 | 73.5 | 73.5 | 17.1 | 76.4 | 76.4 | 7.3 | 16.6 | | 10.8 | 20.1 | 20.1 |
| Actuated g/C Ratio | 0.11 | 0.57 | 0.57 | 0.13 | 0.59 | 0.59 | 0.06 | 0.13 | | 0.08 | 0.15 | 0.15 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 3.0 | 4.0 | | 2.0 | 2.0 | 2.0 |
| Lane Grp Cap (vph) | 375 | 2875 | 876 | 233 | 2080 | 917 | 193 | 405 | | 285 | 288 | 241 |
| v/s Ratio Prot | 0.07 | 0.23 | | c0.10 | c0.32 | | c0.02 | c0.03 | | c0.04 | 0.04 | |
| v/s Ratio Perm | | | 0.10 | | | 0.03 | | | | | | 0.01 |
| v/c Ratio | 0.62 | 0.40 | 0.18 | 0.73 | 0.55 | 0.04 | 0.28 | 0.26 | | 0.42 | 0.25 | 0.07 |
| Uniform Delay, d1 | 55.3 | 15.9 | 13.6 | 54.2 | 16.3 | 11.3 | 58.8 | 51.1 | | 56.6 | 48.3 | 47.0 |
| Progression Factor | 1.15 | 0.78 | 1.25 | 0.95 | 1.12 | 1.88 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.0 | 0.4 | 0.4 | 8.5 | 0.9 | 0.1 | 0.8 | 0.5 | | 0.4 | 0.2 | 0.0 |
| Delay (s) | 66.6 | 12.7 | 17.5 | 59.9 | 19.3 | 21.4 | 59.6 | 51.6 | | 57.0 | 48.5 | 47.0 |
| Level of Service | E | B | B | E | B | C | E | D | | E | D | D |
| Approach Delay (s) | | 21.1 | | | 24.4 | | | 53.0 | | | 51.4 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 27.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.52 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 61.4% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue

























Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |   |  |   |  |  |   |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.99 | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1562 | 1770 | 3539 | 1540 | 3433 | 1863 | 1562 | 3433 | 3106 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1562 | 1770 | 3539 | 1540 | 3433 | 1863 | 1562 | 3433 | 3106 | |
| Volume (vph) | 346 | 829 | 112 | 53 | 806 | 129 | 76 | 46 | 36 | 231 | 115 | 340 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 353 | 846 | 114 | 54 | 822 | 132 | 78 | 47 | 37 | 236 | 117 | 347 |
| RTOR Reduction (vph) | 0 | 0 | 43 | 0 | 0 | 79 | 0 | 0 | 34 | 0 | 302 | 0 |
| Lane Group Flow (vph) | 353 | 846 | 71 | 54 | 822 | 53 | 78 | 47 | 3 | 236 | 162 | 0 |
| Confl. Peds. (#/hr) | 3 | | 1 | 1 | | 3 | 3 | | 1 | 1 | | 3 |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | Perm | Split | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 35.6 | 80.2 | 80.2 | 7.0 | 51.6 | 51.6 | 10.9 | 10.9 | 10.9 | 15.9 | 15.9 | |
| Effective Green, g (s) | 36.6 | 81.2 | 81.2 | 8.0 | 52.6 | 52.6 | 11.9 | 11.9 | 11.9 | 16.9 | 16.9 | |
| Actuated g/C Ratio | 0.28 | 0.62 | 0.62 | 0.06 | 0.40 | 0.40 | 0.09 | 0.09 | 0.09 | 0.13 | 0.13 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 2.0 | 4.0 | 4.0 | 2.0 | 4.0 | 4.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lane Grp Cap (vph) | 498 | 3176 | 976 | 109 | 1432 | 623 | 314 | 171 | 143 | 446 | 404 | |
| v/s Ratio Prot | c0.20 | 0.17 | | 0.03 | c0.23 | | 0.02 | c0.03 | | c0.07 | 0.05 | |
| v/s Ratio Perm | | | 0.05 | | | 0.03 | | | 0.00 | | | |
| v/c Ratio | 0.71 | 0.27 | 0.07 | 0.50 | 0.57 | 0.09 | 0.25 | 0.27 | 0.02 | 0.53 | 0.40 | |
| Uniform Delay, d1 | 41.9 | 11.0 | 9.6 | 59.0 | 30.0 | 23.9 | 54.9 | 55.0 | 53.8 | 52.8 | 51.9 | |
| Progression Factor | 1.65 | 0.62 | 0.44 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 3.6 | 0.2 | 0.1 | 1.3 | 1.7 | 0.3 | 0.2 | 0.3 | 0.0 | 0.5 | 0.2 | |
| Delay (s) | 72.8 | 7.0 | 4.4 | 60.3 | 31.7 | 24.1 | 55.0 | 55.3 | 53.8 | 53.4 | 52.1 | |
| Level of Service | E | A | A | E | C | C | E | E | D | D | D | |
| Approach Delay (s) | | 24.5 | | | 32.2 | | | 54.8 | | | 52.6 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 34.7 | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 73.9% | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

























HCM Signalized Intersection Capacity Analysis
13: Lone Tree Way & Deer Valley Rd.

Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.94 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3539 | 1435 | 1770 | 3539 | 1531 | 3433 | 3297 | | 2000 | 3498 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3539 | 1435 | 1770 | 3539 | 1531 | 3433 | 3297 | | 1770 | 3498 | |
| Volume (vph) | 87 | 971 | 169 | 238 | 628 | 154 | 205 | 365 | 241 | 168 | 191 | 14 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 90 | 1001 | 174 | 245 | 647 | 159 | 211 | 376 | 248 | 173 | 197 | 14 |
| RTOR Reduction (vph) | 0 | 0 | 32 | 0 | 0 | 43 | 0 | 87 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 90 | 1001 | 142 | 245 | 647 | 116 | 211 | 537 | 0 | 173 | 206 | 0 |
| Confl. Peds. (#/hr) | 12 | | 54 | 54 | | 12 | 11 | | 8 | 8 | | 11 |
| Confl. Bikes (#/hr) | | | 11 | | | 9 | | | | | | |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | |
| Actuated Green, G (s) | 11.8 | 48.0 | 48.0 | 21.3 | 57.5 | 57.5 | 12.9 | 25.1 | | 17.1 | 29.3 | |
| Effective Green, g (s) | 13.3 | 50.0 | 50.0 | 22.8 | 59.5 | 59.5 | 14.4 | 26.6 | | 18.6 | 30.8 | |
| Actuated g/C Ratio | 0.10 | 0.38 | 0.38 | 0.18 | 0.46 | 0.46 | 0.11 | 0.20 | | 0.14 | 0.24 | |
| Clearance Time (s) | 4.5 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | 3.0 | 3.0 | | 4.0 | 3.0 | |
| Lane Grp Cap (vph) | 181 | 1361 | 552 | 310 | 1620 | 701 | 380 | 675 | | 286 | 829 | |
| v/s Ratio Prot | 0.05 | c0.28 | | c0.14 | 0.18 | | 0.06 | c0.16 | | c0.09 | 0.06 | |
| v/s Ratio Perm | | | 0.10 | | | 0.08 | | | | | | |
| v/c Ratio | 0.50 | 0.74 | 0.26 | 0.79 | 0.40 | 0.16 | 0.56 | 0.79 | | 0.60 | 0.25 | |
| Uniform Delay, d1 | 55.2 | 34.3 | 27.3 | 51.3 | 23.4 | 20.7 | 54.8 | 49.1 | | 52.3 | 40.2 | |
| Progression Factor | 1.42 | 0.59 | 0.60 | 1.06 | 1.68 | 2.45 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.9 | 3.1 | 1.0 | 11.0 | 0.6 | 0.4 | 1.8 | 6.4 | | 4.1 | 0.2 | |
| Delay (s) | 80.1 | 23.4 | 17.5 | 65.3 | 40.0 | 51.1 | 56.5 | 55.5 | | 56.4 | 40.4 | |
| Level of Service | F | C | B | E | D | D | E | E | | E | D | |
| Approach Delay (s) | | 26.6 | | | 47.6 | | | 55.8 | | | 47.6 | |
| Approach LOS | | C | | | D | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 42.0 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.74 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 81.8% | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |





















HCM Signalized Intersection Capacity Analysis
14: Lone Tree Way & Hillcrest Ave.

Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.96 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.97 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1521 | 1770 | 5085 | 1519 | 1770 | 3388 | | 2000 | 3263 | 1534 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1521 | 1770 | 5085 | 1519 | 1770 | 3388 | | 1610 | 3263 | 1534 |
| Volume (vph) | 232 | 1097 | 22 | 43 | 908 | 369 | 17 | 87 | 26 | 551 | 77 | 153 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 264 | 1247 | 25 | 49 | 1032 | 419 | 19 | 99 | 30 | 626 | 88 | 174 |
| RTOR Reduction (vph) | 0 | 0 | 8 | 0 | 0 | 272 | 0 | 25 | 0 | 0 | 0 | 137 |
| Lane Group Flow (vph) | 264 | 1247 | 17 | 49 | 1032 | 147 | 19 | 104 | 0 | 313 | 401 | 37 |
| Confl. Peds. (#/hr) | 18 | | 20 | 20 | | 18 | 14 | | 16 | 16 | | 14 |
| Confl. Bikes (#/hr) | | | 3 | | | 8 | | | 1 | | | 1 |
| Turn Type | Prot | | Perm | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 23.2 | 62.0 | 62.0 | 5.2 | 43.5 | 43.5 | 17.4 | 17.4 | | 25.9 | 25.9 | 25.9 |
| Effective Green, g (s) | 25.2 | 64.0 | 64.0 | 6.7 | 45.5 | 45.5 | 19.4 | 19.4 | | 27.9 | 27.9 | 27.9 |
| Actuated g/C Ratio | 0.19 | 0.49 | 0.49 | 0.05 | 0.35 | 0.35 | 0.15 | 0.15 | | 0.21 | 0.21 | 0.21 |
| Clearance Time (s) | 5.0 | 5.0 | 5.0 | 4.5 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 343 | 1742 | 749 | 91 | 1780 | 532 | 264 | 506 | | 429 | 700 | 329 |
| v/s Ratio Prot | c0.15 | c0.35 | | 0.03 | 0.20 | | 0.01 | c0.03 | | c0.16 | 0.12 | |
| v/s Ratio Perm | | | 0.01 | | | 0.10 | | | | | | 0.02 |
| v/c Ratio | 0.77 | 0.72 | 0.02 | 0.54 | 0.58 | 0.28 | 0.07 | 0.21 | | 0.73 | 0.87dl | 0.11 |
| Uniform Delay, d1 | 49.7 | 25.9 | 16.9 | 60.1 | 34.5 | 30.4 | 47.6 | 48.5 | | 47.5 | 45.7 | 41.1 |
| Progression Factor | 0.81 | 0.74 | 0.33 | 1.13 | 0.89 | 1.17 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 10.8 | 2.3 | 0.1 | 5.2 | 1.2 | 1.1 | 0.2 | 0.4 | | 7.5 | 1.8 | 0.3 |
| Delay (s) | 50.9 | 21.4 | 5.6 | 73.3 | 31.9 | 36.6 | 47.8 | 49.0 | | 55.0 | 47.5 | 41.4 |
| Level of Service | D | C | A | E | C | D | D | D | | E | D | D |
| Approach Delay (s) | | 26.2 | | | 34.6 | | | 48.8 | | | 49.0 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 35.1 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.65 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | | Sum of lost time (s) | | | 9.0 | | |
| Intersection Capacity Utilization | | | 69.8% | | | | ICU Level of Service | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| dl Defacto Left Lane. Recode with 1 though lane as a left lane. | | | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
15: Lone Tree Way & Vista Grande










Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.86 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5061 | | 1770 | 5068 | | 1767 | 1605 | | 1770 | 1652 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.74 | 1.00 | | 0.40 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5061 | | 1770 | 5068 | | 1372 | 1605 | | 742 | 1652 | |
| Volume (vph) | 18 | 1610 | 44 | 121 | 1262 | 24 | 35 | 10 | 114 | 42 | 9 | 20 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 19 | 1660 | 45 | 125 | 1301 | 25 | 36 | 10 | 118 | 43 | 9 | 21 |
| RTOR Reduction (vph) | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 105 | 0 | 0 | 19 | 0 |
| Lane Group Flow (vph) | 19 | 1704 | 0 | 125 | 1325 | 0 | 36 | 23 | 0 | 43 | 11 | 0 |
| Confl. Peds. (#/hr) | 4 | | 4 | 4 | | 4 | 1 | | | | | 1 |
| Turn Type | Prot | | | Prot | | | Perm | | | Perm | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | | 8 | | | 4 | |
| Permitted Phases | | | | | | | 8 | | | 4 | | |
| Actuated Green, G (s) | 3.7 | 87.3 | | 15.4 | 99.0 | | 12.8 | 12.8 | | 12.8 | 12.8 | |
| Effective Green, g (s) | 5.2 | 89.8 | | 16.9 | 101.5 | | 14.3 | 14.3 | | 14.3 | 14.3 | |
| Actuated g/C Ratio | 0.04 | 0.69 | | 0.13 | 0.78 | | 0.11 | 0.11 | | 0.11 | 0.11 | |
| Clearance Time (s) | 4.5 | 5.5 | | 4.5 | 5.5 | | 4.5 | 4.5 | | 4.5 | 4.5 | |
| Vehicle Extension (s) | 4.0 | 6.0 | | 4.0 | 6.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 71 | 3496 | | 230 | 3957 | | 151 | 177 | | 82 | 182 | |
| v/s Ratio Prot | 0.01 | c0.34 | | c0.07 | 0.26 | | | 0.01 | | | 0.01 | |
| v/s Ratio Perm | | | | | | | 0.03 | | | c0.06 | | |
| v/c Ratio | 0.27 | 0.49 | | 0.54 | 0.33 | | 0.24 | 0.13 | | 0.52 | 0.06 | |
| Uniform Delay, d1 | 60.6 | 9.4 | | 52.9 | 4.2 | | 52.9 | 52.2 | | 54.6 | 51.8 | |
| Progression Factor | 0.90 | 0.80 | | 0.87 | 1.58 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.1 | 0.4 | | 2.4 | 0.2 | | 0.8 | 0.3 | | 5.9 | 0.1 | |
| Delay (s) | 56.6 | 7.9 | | 48.7 | 6.9 | | 53.7 | 52.6 | | 60.6 | 52.0 | |
| Level of Service | E | A | | D | A | | D | D | | E | D | |
| Approach Delay (s) | | 8.4 | | | 10.5 | | | 52.8 | | | 57.0 | |
| Approach LOS | | A | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 12.5 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.50 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 130.0 | | | Sum of lost time (s) | | | | 9.0 | | |
| Intersection Capacity Utilization | | | 63.0% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
16: Country Hills Dr. & Hillcrest Ave
























Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|---|-------|---|---|----------------------|--|---|------|---|---|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.98 | | 1.00 | 1.00 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.91 | | 1.00 | 0.91 | | 1.00 | 0.99 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1690 | | 1770 | 1668 | | 1770 | 3482 | | 1770 | 3457 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1690 | | 1770 | 1668 | | 1770 | 3482 | | 1770 | 3457 | |
| Volume (vph) | 42 | 51 | 82 | 34 | 50 | 75 | 73 | 514 | 49 | 140 | 543 | 63 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 46 | 55 | 89 | 37 | 54 | 82 | 79 | 559 | 53 | 152 | 590 | 68 |
| RTOR Reduction (vph) | 0 | 37 | 0 | 0 | 33 | 0 | 0 | 3 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 46 | 107 | 0 | 37 | 103 | 0 | 79 | 609 | 0 | 152 | 655 | 0 |
| Confl. Peds. (#/hr) | 10 | | | | | 10 | 20 | | 7 | 7 | | 20 |
| Turn Type | Split | | | Split | | | Prot | | | Prot | | |
| Protected Phases | 4 | 4 | | 8 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 12.7 | 12.7 | | 12.5 | 12.5 | | 9.2 | 65.5 | | 16.4 | 72.7 | |
| Effective Green, g (s) | 13.2 | 13.2 | | 13.0 | 13.0 | | 9.7 | 67.0 | | 16.9 | 74.2 | |
| Actuated g/C Ratio | 0.11 | 0.11 | | 0.11 | 0.11 | | 0.08 | 0.55 | | 0.14 | 0.61 | |
| Clearance Time (s) | 3.5 | 3.5 | | 3.5 | 3.5 | | 3.5 | 4.5 | | 3.5 | 4.5 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 191 | 183 | | 188 | 178 | | 141 | 1911 | | 245 | 2101 | |
| v/s Ratio Prot | 0.03 | c0.06 | | 0.02 | c0.06 | | c0.04 | c0.17 | | c0.09 | 0.19 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.24 | 0.59 | | 0.20 | 0.58 | | 0.56 | 0.32 | | 0.62 | 0.31 | |
| Uniform Delay, d1 | 49.9 | 51.9 | | 49.8 | 51.9 | | 54.1 | 15.1 | | 49.6 | 11.6 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.7 | 4.7 | | 0.5 | 4.5 | | 5.0 | 0.4 | | 4.8 | 0.4 | |
| Delay (s) | 50.5 | 56.6 | | 50.3 | 56.4 | | 59.2 | 15.5 | | 54.4 | 12.0 | |
| Level of Service | D | E | | D | E | | E | B | | D | B | |
| Approach Delay (s) | | 55.1 | | | 55.1 | | | 20.5 | | | 19.9 | |
| Approach LOS | | E | | | E | | | C | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 27.0 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.45 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 122.1 | | | Sum of lost time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | | | 55.6% | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
18: Laurel Rd. & Hillcrest Ave

Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 0.99 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.89 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1634 | | 1768 | 1863 | 1583 | 1770 | 3539 | 1550 | 1770 | 3497 | |
| Flt Permitted | 0.75 | 1.00 | | 0.74 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1400 | 1634 | | 1374 | 1863 | 1583 | 1770 | 3539 | 1550 | 1770 | 3497 | |
| Volume (vph) | 17 | 7 | 22 | 35 | 9 | 133 | 27 | 565 | 39 | 162 | 677 | 50 |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 17 | 7 | 22 | 36 | 9 | 136 | 28 | 577 | 40 | 165 | 691 | 51 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 0 | 0 | 123 | 0 | 0 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 17 | 9 | 0 | 36 | 9 | 13 | 28 | 577 | 40 | 165 | 740 | 0 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | 2 | | 2 | 2 | | 2 |
| Turn Type | Perm | | | Perm | | Perm | Prot | | Free | Prot | | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | | | Free | | | |
| Actuated Green, G (s) | 8.4 | 8.4 | | 8.4 | 8.4 | 8.4 | 3.4 | 62.6 | 100.0 | 14.5 | 73.7 | |
| Effective Green, g (s) | 9.9 | 9.9 | | 9.9 | 9.9 | 9.9 | 4.4 | 65.6 | 100.0 | 15.5 | 76.7 | |
| Actuated g/C Ratio | 0.10 | 0.10 | | 0.10 | 0.10 | 0.10 | 0.04 | 0.66 | 1.00 | 0.16 | 0.77 | |
| Clearance Time (s) | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | 4.0 | 6.0 | | 4.0 | 6.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.5 | 3.5 | 3.5 | 3.0 | 5.0 | | 3.0 | 5.0 | |
| Lane Grp Cap (vph) | 139 | 162 | | 136 | 184 | 157 | 78 | 2322 | 1550 | 274 | 2682 | |
| v/s Ratio Prot | | 0.01 | | | 0.00 | | 0.02 | 0.16 | | c0.09 | c0.21 | |
| v/s Ratio Perm | 0.01 | | | c0.03 | | 0.01 | | | 0.03 | | | |
| v/c Ratio | 0.12 | 0.06 | | 0.26 | 0.05 | 0.09 | 0.36 | 0.25 | 0.03 | 0.60 | 0.28 | |
| Uniform Delay, d1 | 41.1 | 40.8 | | 41.7 | 40.8 | 40.9 | 46.4 | 7.1 | 0.0 | 39.4 | 3.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.22 | 0.16 | |
| Incremental Delay, d2 | 0.4 | 0.1 | | 1.2 | 0.1 | 0.3 | 2.8 | 0.3 | 0.0 | 3.4 | 0.2 | |
| Delay (s) | 41.5 | 41.0 | | 42.9 | 40.9 | 41.2 | 49.2 | 7.3 | 0.0 | 51.6 | 0.8 | |
| Level of Service | D | D | | D | D | D | D | A | A | D | A | |
| Approach Delay (s) | | 41.2 | | | 41.5 | | | 8.7 | | | 10.0 | |
| Approach LOS | | D | | | D | | | A | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 13.6 | | | | HCM Level of Service | | | B | | |
| HCM Volume to Capacity ratio | | | 0.33 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | | Sum of lost time (s) | | | 6.0 | | |
| Intersection Capacity Utilization | | | 48.4% | | | | ICU Level of Service | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

Cumulative No Project

HCM Signalized Intersection Capacity Analysis

1: Laurel Road & Canada Valley





















Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| | → | ↘ | ↙ | ← | ↖ | ↗ |
|-----------------------------------|-------|------|-------|------|----------------------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | | ↘ | ↑↑ | ↘ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | 0.99 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3489 | | 1770 | 3539 | 1770 | 1583 |
| Flt Permitted | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3489 | | 1770 | 3539 | 1770 | 1583 |
| Volume (vph) | 953 | 100 | 238 | 649 | 120 | 229 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 953 | 100 | 238 | 649 | 120 | 229 |
| RTOR Reduction (vph) | 8 | 0 | 0 | 0 | 0 | 178 |
| Lane Group Flow (vph) | 1045 | 0 | 238 | 649 | 120 | 51 |
| Turn Type | | | Prot | | | Perm |
| Protected Phases | 4 | | 3 | 8 | 2 | |
| Permitted Phases | | | | | | 2 |
| Actuated Green, G (s) | 39.8 | | 18.2 | 62.0 | 20.0 | 20.0 |
| Effective Green, g (s) | 39.8 | | 18.2 | 62.0 | 20.0 | 20.0 |
| Actuated g/C Ratio | 0.44 | | 0.20 | 0.69 | 0.22 | 0.22 |
| Clearance Time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 1543 | | 358 | 2438 | 393 | 352 |
| v/s Ratio Prot | c0.30 | | c0.13 | 0.18 | c0.07 | |
| v/s Ratio Perm | | | | | | 0.03 |
| v/c Ratio | 0.68 | | 0.66 | 0.27 | 0.31 | 0.14 |
| Uniform Delay, d1 | 20.0 | | 33.1 | 5.3 | 29.2 | 28.1 |
| Progression Factor | 1.00 | | 0.93 | 0.53 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.4 | | 4.4 | 0.3 | 2.0 | 0.9 |
| Delay (s) | 22.4 | | 35.1 | 3.1 | 31.2 | 29.0 |
| Level of Service | C | | D | A | C | C |
| Approach Delay (s) | 22.4 | | | 11.7 | 29.8 | |
| Approach LOS | C | | | B | C | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 19.4 | | HCM Level of Service | B |
| HCM Volume to Capacity ratio | | | 0.58 | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 59.4% | | ICU Level of Service | B |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Laurel Road & Country Hills Drive


Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.94 | | 1.00 | 0.99 | | 1.00 | 0.86 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3336 | | 1770 | 3515 | | 1770 | 1607 | | 1770 | 1676 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3336 | | 1770 | 3515 | | 1770 | 1607 | | 1770 | 1676 | |
| Volume (vph) | 40 | 679 | 420 | 62 | 633 | 30 | 160 | 20 | 217 | 80 | 30 | 60 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 40 | 679 | 420 | 62 | 633 | 30 | 160 | 20 | 217 | 80 | 30 | 60 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 52 | 0 |
| Lane Group Flow (vph) | 40 | 1099 | 0 | 62 | 660 | 0 | 160 | 237 | 0 | 80 | 38 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 4.4 | 44.3 | | 7.2 | 47.1 | | 11.0 | 17.7 | | 4.8 | 11.5 | |
| Effective Green, g (s) | 4.4 | 44.3 | | 7.2 | 47.1 | | 11.0 | 17.7 | | 4.8 | 11.5 | |
| Actuated g/C Ratio | 0.05 | 0.49 | | 0.08 | 0.52 | | 0.12 | 0.20 | | 0.05 | 0.13 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 87 | 1642 | | 142 | 1840 | | 216 | 316 | | 94 | 214 | |
| v/s Ratio Prot | 0.02 | c0.33 | | 0.04 | c0.19 | | c0.09 | c0.15 | | 0.05 | 0.02 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.46 | 0.67 | | 0.44 | 0.36 | | 0.74 | 0.75 | | 0.85 | 0.18 | |
| Uniform Delay, d1 | 41.6 | 17.3 | | 39.5 | 12.6 | | 38.1 | 34.1 | | 42.2 | 35.0 | |
| Progression Factor | 0.87 | 1.84 | | 0.90 | 0.92 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 3.1 | 1.8 | | 2.1 | 0.5 | | 12.8 | 9.6 | | 48.3 | 0.4 | |
| Delay (s) | 39.3 | 33.5 | | 37.7 | 12.1 | | 50.9 | 43.7 | | 90.6 | 35.4 | |
| Level of Service | D | C | | D | B | | D | D | | F | D | |
| Approach Delay (s) | 33.7 | | | 14.3 | | | 46.6 | | | 61.4 | | |
| Approach LOS | C | | | B | | | D | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 31.9 | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | | 0.63 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | | 67.9% | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Laurel Road & SB SR4 Bypass





















Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|-------|------|------|----------------------|------|------|------|------|-------|--------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑ | | | ↑↑ | | | | | ↘ | ↗ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 0.99 | | | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 3514 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 3514 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 929 | 46 | 0 | 420 | 0 | 0 | 0 | 0 | 840 | 0 | 305 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 929 | 46 | 0 | 420 | 0 | 0 | 0 | 0 | 840 | 0 | 305 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 975 | 0 | 0 | 420 | 0 | 0 | 0 | 0 | 420 | 420 | 305 |
| Turn Type | | | | | | | | | | Perm | custom | |
| Protected Phases | | 2 | | | 6 | | | | | | 4 | 4 |
| Permitted Phases | | | | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 53.4 | | | 53.4 | | | | | 28.6 | 28.6 | 28.6 |
| Effective Green, g (s) | | 53.4 | | | 53.4 | | | | | 28.6 | 28.6 | 28.6 |
| Actuated g/C Ratio | | 0.59 | | | 0.59 | | | | | 0.32 | 0.32 | 0.32 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2085 | | | 2100 | | | | | 534 | 534 | 503 |
| v/s Ratio Prot | | c0.28 | | | 0.12 | | | | | | | 0.19 |
| v/s Ratio Perm | | | | | | | | | | c0.25 | 0.25 | |
| v/c Ratio | | 0.47 | | | 0.20 | | | | | 0.79 | 0.79 | 0.61 |
| Uniform Delay, d1 | | 10.3 | | | 8.4 | | | | | 27.9 | 27.9 | 25.9 |
| Progression Factor | | 0.43 | | | 0.09 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.6 | | | 0.2 | | | | | 7.5 | 7.5 | 2.1 |
| Delay (s) | | 5.0 | | | 1.0 | | | | | 35.4 | 35.4 | 28.0 |
| Level of Service | | A | | | A | | | | | D | D | C |
| Approach Delay (s) | | 5.0 | | | 1.0 | | | 0.0 | | | 33.5 | |
| Approach LOS | | A | | | A | | | A | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 17.2 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.58 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 90.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 77.6% | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Laurel Road & SR4 Bypass NB Ramps






















Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |   | | |   |  | |  |  | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | 1.00 | | 1.00 | 1.00 | | | |
| Frt | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Volume (vph) | 155 | 1615 | 0 | 0 | 565 | 620 | 5 | 0 | 100 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 155 | 1615 | 0 | 0 | 565 | 620 | 5 | 0 | 100 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 155 | 1615 | 0 | 0 | 565 | 620 | 0 | 5 | 100 | 0 | 0 | 0 |
| Turn Type | Prot | | | | Perm | | Perm | custom | | | | |
| Protected Phases | 5 | 2 | | | 6 | | | 8 | 8 | | | |
| Permitted Phases | | | | | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | 18.0 | 71.2 | | | 49.2 | 49.2 | | 10.8 | 10.8 | | | |
| Effective Green, g (s) | 18.0 | 71.2 | | | 49.2 | 49.2 | | 10.8 | 10.8 | | | |
| Actuated g/C Ratio | 0.20 | 0.79 | | | 0.55 | 0.55 | | 0.12 | 0.12 | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | 354 | 2800 | | | 1935 | 865 | | 212 | 190 | | | |
| v/s Ratio Prot | 0.09 | c0.46 | | | 0.16 | | | | c0.06 | | | |
| v/s Ratio Perm | | | | | | c0.39 | | 0.00 | | | | |
| v/c Ratio | 0.44 | 0.58 | | | 0.29 | 0.72 | | 0.02 | 0.53 | | | |
| Uniform Delay, d1 | 31.6 | 3.6 | | | 11.0 | 15.2 | | 34.9 | 37.2 | | | |
| Progression Factor | 1.03 | 0.92 | | | 0.07 | 0.22 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 0.8 | 0.8 | | | 0.3 | 4.1 | | 0.0 | 2.6 | | | |
| Delay (s) | 33.3 | 4.1 | | | 1.1 | 7.4 | | 35.0 | 39.8 | | | |
| Level of Service | C | A | | | A | A | | C | D | | | |
| Approach Delay (s) | | 6.7 | | | 4.4 | | | 39.6 | | | 0.0 | |
| Approach LOS | | A | | | A | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 6.9 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.64 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 90.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 60.3% | | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Laurel Road & Slatten Ranch Road

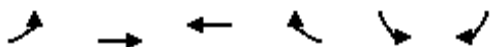
Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.94 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 4897 | | 3433 | 3332 | | 1770 | 3443 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 4897 | | 3433 | 3332 | | 1770 | 3443 | |
| Volume (vph) | 160 | 925 | 630 | 260 | 975 | 320 | 170 | 250 | 160 | 130 | 180 | 40 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 160 | 925 | 630 | 260 | 975 | 320 | 170 | 250 | 160 | 130 | 180 | 40 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 160 | 925 | 630 | 260 | 1295 | 0 | 170 | 410 | 0 | 130 | 220 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | |
| Actuated Green, G (s) | 15.0 | 37.5 | 37.5 | 14.7 | 37.2 | | 11.0 | 14.8 | | 7.0 | 10.8 | |
| Effective Green, g (s) | 15.0 | 37.5 | 37.5 | 14.7 | 37.2 | | 11.0 | 14.8 | | 7.0 | 10.8 | |
| Actuated g/C Ratio | 0.17 | 0.42 | 0.42 | 0.16 | 0.41 | | 0.12 | 0.16 | | 0.08 | 0.12 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 295 | 2119 | 660 | 289 | 2024 | | 420 | 548 | | 138 | 413 | |
| v/s Ratio Prot | 0.09 | 0.18 | | c0.15 | 0.26 | | 0.05 | c0.12 | | c0.07 | 0.06 | |
| v/s Ratio Perm | | | c0.40 | | | | | | | | | |
| v/c Ratio | 0.54 | 0.44 | 0.95 | 0.90 | 0.64 | | 0.40 | 0.75 | | 0.94 | 0.53 | |
| Uniform Delay, d1 | 34.4 | 18.7 | 25.4 | 36.9 | 21.1 | | 36.5 | 35.8 | | 41.3 | 37.2 | |
| Progression Factor | 0.84 | 0.74 | 0.74 | 0.69 | 0.58 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.7 | 0.5 | 22.6 | 25.2 | 1.3 | | 0.6 | 5.5 | | 58.8 | 1.3 | |
| Delay (s) | 30.6 | 14.5 | 41.6 | 50.8 | 13.6 | | 37.1 | 41.4 | | 100.1 | 38.6 | |
| Level of Service | C | B | D | D | B | | D | D | | F | D | |
| Approach Delay (s) | | 25.9 | | | 19.8 | | | 40.1 | | | 61.4 | |
| Approach LOS | | C | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 28.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.90 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 69.7% | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Laurel Road & Live Oak Avenue

Antioch Davidon Homes TIA
2025 No Project AM Peak Hour


























| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|-------|------|-------|------|----------------------|-------|
| Lane Configurations | ←← | ↑↑↑ | ↑↑↑ | | ← | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.91 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.99 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 5034 | | 1770 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 5034 | | 1770 | 1583 |
| Volume (vph) | 290 | 925 | 1245 | 90 | 60 | 310 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 290 | 925 | 1245 | 90 | 60 | 310 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 218 |
| Lane Group Flow (vph) | 290 | 925 | 1326 | 0 | 60 | 92 |
| Turn Type | Prot | | | Perm | | |
| Protected Phases | 7 | 4 | 8 | 6 | | |
| Permitted Phases | | | | | 6 | |
| Actuated Green, G (s) | 12.6 | 55.2 | 38.6 | | 26.8 | 26.8 |
| Effective Green, g (s) | 12.6 | 55.2 | 38.6 | | 26.8 | 26.8 |
| Actuated g/C Ratio | 0.14 | 0.61 | 0.43 | | 0.30 | 0.30 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 481 | 3119 | 2159 | | 527 | 471 |
| v/s Ratio Prot | c0.08 | 0.18 | c0.26 | | 0.03 | |
| v/s Ratio Perm | | | | | | c0.06 |
| v/c Ratio | 0.60 | 0.30 | 0.61 | | 0.11 | 0.20 |
| Uniform Delay, d1 | 36.4 | 8.2 | 19.9 | | 23.0 | 23.6 |
| Progression Factor | 0.90 | 1.41 | 0.62 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.8 | 0.0 | 0.4 | | 0.4 | 0.9 |
| Delay (s) | 34.7 | 11.6 | 12.7 | | 23.4 | 24.5 |
| Level of Service | C | B | B | | C | C |
| Approach Delay (s) | | 17.1 | 12.7 | | 24.3 | |
| Approach LOS | | B | B | | C | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 16.0 | | HCM Level of Service | B |
| HCM Volume to Capacity ratio | | | 0.47 | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 51.9% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Laurel Road & Empire Avenue

























Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3516 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3516 | | 1770 | 3539 | 1583 |
| Volume (vph) | 285 | 650 | 50 | 70 | 850 | 140 | 140 | 220 | 10 | 40 | 310 | 345 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 285 | 650 | 50 | 70 | 850 | 140 | 140 | 220 | 10 | 40 | 310 | 345 |
| RTOR Reduction (vph) | 0 | 0 | 28 | 0 | 0 | 85 | 0 | 4 | 0 | 0 | 0 | 237 |
| Lane Group Flow (vph) | 285 | 650 | 22 | 70 | 850 | 55 | 140 | 226 | 0 | 40 | 310 | 108 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 8 | | | | | | 6 |
| Actuated Green, G (s) | 12.0 | 40.4 | 40.4 | 7.1 | 35.5 | 35.5 | 11.2 | 22.9 | | 3.6 | 15.3 | 15.3 |
| Effective Green, g (s) | 12.0 | 40.4 | 40.4 | 7.1 | 35.5 | 35.5 | 11.2 | 22.9 | | 3.6 | 15.3 | 15.3 |
| Actuated g/C Ratio | 0.13 | 0.45 | 0.45 | 0.08 | 0.39 | 0.39 | 0.12 | 0.25 | | 0.04 | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 458 | 1589 | 711 | 140 | 1396 | 624 | 220 | 895 | | 71 | 602 | 269 |
| v/s Ratio Prot | c0.08 | 0.18 | | 0.04 | c0.24 | | c0.08 | 0.06 | | 0.02 | c0.09 | |
| v/s Ratio Perm | | | 0.01 | | | 0.03 | | | | | | 0.07 |
| v/c Ratio | 0.62 | 0.41 | 0.03 | 0.50 | 0.61 | 0.09 | 0.64 | 0.25 | | 0.56 | 0.51 | 0.40 |
| Uniform Delay, d1 | 36.9 | 16.7 | 13.9 | 39.7 | 21.7 | 17.1 | 37.5 | 26.7 | | 42.4 | 34.0 | 33.3 |
| Progression Factor | 1.19 | 0.71 | 1.62 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.6 | 0.8 | 0.1 | 2.8 | 2.0 | 0.3 | 5.9 | 0.1 | | 9.8 | 0.7 | 1.0 |
| Delay (s) | 46.6 | 12.6 | 22.6 | 42.5 | 23.7 | 17.4 | 43.4 | 26.9 | | 52.3 | 34.7 | 34.3 |
| Level of Service | D | B | C | D | C | B | D | C | | D | C | C |
| Approach Delay (s) | | 22.9 | | | 24.1 | | | 33.1 | | | 35.5 | |
| Approach LOS | | C | | | C | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 27.4 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.60 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | | Sum of lost time (s) | | | 16.0 | | |
| Intersection Capacity Utilization | | | 62.6% | | | | ICU Level of Service | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Lone Tree Way & Canada Valley













Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.87 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1534 | 1504 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1534 | 1504 | 1770 | 1863 | 1583 |
| Volume (vph) | 42 | 950 | 20 | 260 | 1460 | 249 | 50 | 10 | 160 | 328 | 10 | 26 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 42 | 950 | 20 | 260 | 1460 | 249 | 50 | 10 | 160 | 328 | 10 | 26 |
| RTOR Reduction (vph) | 0 | 0 | 11 | 0 | 0 | 117 | 0 | 74 | 74 | 0 | 0 | 21 |
| Lane Group Flow (vph) | 42 | 950 | 9 | 260 | 1460 | 132 | 50 | 16 | 6 | 328 | 10 | 5 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 2.4 | 46.9 | 46.9 | 14.0 | 58.5 | 58.5 | 10.7 | 8.9 | 8.9 | 24.2 | 22.4 | 22.4 |
| Effective Green, g (s) | 2.4 | 46.9 | 46.9 | 14.0 | 58.5 | 58.5 | 10.7 | 8.9 | 8.9 | 24.2 | 22.4 | 22.4 |
| Actuated g/C Ratio | 0.02 | 0.43 | 0.43 | 0.13 | 0.53 | 0.53 | 0.10 | 0.08 | 0.08 | 0.22 | 0.20 | 0.20 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 75 | 2168 | 675 | 437 | 2704 | 842 | 334 | 124 | 122 | 389 | 379 | 322 |
| v/s Ratio Prot | 0.01 | c0.19 | | 0.08 | c0.29 | | 0.01 | c0.01 | | c0.19 | 0.01 | |
| v/s Ratio Perm | | | 0.01 | | | 0.08 | | | 0.00 | | | 0.00 |
| v/c Ratio | 0.56 | 0.44 | 0.01 | 0.59 | 0.54 | 0.16 | 0.15 | 0.13 | 0.05 | 0.84 | 0.03 | 0.02 |
| Uniform Delay, d1 | 53.3 | 22.3 | 18.2 | 45.3 | 16.9 | 13.2 | 45.5 | 47.0 | 46.7 | 41.1 | 35.1 | 35.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.64 | 0.89 | 1.10 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 9.2 | 0.6 | 0.0 | 1.9 | 0.7 | 0.3 | 0.2 | 0.5 | 0.2 | 15.2 | 0.0 | 0.0 |
| Delay (s) | 62.5 | 22.9 | 18.2 | 30.9 | 15.7 | 14.8 | 45.7 | 47.5 | 46.8 | 56.3 | 35.1 | 35.0 |
| Level of Service | E | C | B | C | B | B | D | D | D | E | D | D |
| Approach Delay (s) | | 24.5 | | | 17.6 | | | 46.8 | | | 54.2 | |
| Approach LOS | | C | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 25.1 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 66.4% | | | | ICU Level of Service | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Lone Tree Way & SB SR4 Bypass













Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 1156 | 282 | 160 | 1769 | 0 | 0 | 0 | 0 | 723 | 0 | 200 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1156 | 282 | 160 | 1769 | 0 | 0 | 0 | 0 | 723 | 0 | 200 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1156 | 282 | 160 | 1769 | 0 | 0 | 0 | 0 | 362 | 361 | 200 |
| Turn Type | | Perm | | Prot | | | | | | Split | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | 4 | | 4 |
| Permitted Phases | | 2 | | | | | | | | | | 4 |
| Actuated Green, G (s) | | 53.3 | 53.3 | 16.0 | 73.3 | | | | | 28.7 | 28.7 | 28.7 |
| Effective Green, g (s) | | 53.3 | 53.3 | 16.0 | 73.3 | | | | | 28.7 | 28.7 | 28.7 |
| Actuated g/C Ratio | | 0.48 | 0.48 | 0.15 | 0.67 | | | | | 0.26 | 0.26 | 0.26 |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2464 | 767 | 499 | 3388 | | | | | 439 | 439 | 413 |
| v/s Ratio Prot | | 0.23 | | 0.05 | c0.35 | | | | | c0.22 | 0.21 | |
| v/s Ratio Perm | | | 0.18 | | | | | | | | | 0.13 |
| v/c Ratio | | 0.47 | 0.37 | 0.32 | 0.52 | | | | | 0.82 | 0.82 | 0.48 |
| Uniform Delay, d1 | | 18.9 | 17.8 | 42.1 | 9.4 | | | | | 38.3 | 38.3 | 34.4 |
| Progression Factor | | 1.11 | 1.06 | 1.11 | 0.93 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.6 | 1.2 | 0.3 | 0.5 | | | | | 11.9 | 11.8 | 0.9 |
| Delay (s) | | 21.6 | 20.1 | 47.0 | 9.2 | | | | | 50.2 | 50.0 | 35.3 |
| Level of Service | | C | C | D | A | | | | | D | D | D |
| Approach Delay (s) | | 21.3 | | | 12.4 | | | 0.0 | | | 46.9 | |
| Approach LOS | | C | | | B | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 22.8 | | HCM Level of Service | | C | | | | | | |
| HCM Volume to Capacity ratio | | 0.61 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | Sum of lost time (s) | | 8.0 | | | | | | |
| Intersection Capacity Utilization | | 60.9% | | ICU Level of Service | | B | | | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Lone Tree Way & SR4 Bypass NB Ramps























Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Volume (vph) | 0 | 1580 | 300 | 70 | 1655 | 714 | 274 | 10 | 250 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1580 | 300 | 70 | 1655 | 714 | 274 | 10 | 250 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1580 | 300 | 70 | 1655 | 714 | 274 | 10 | 250 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Perm | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | | |
| Permitted Phases | | | | 2 | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | | 70.4 | 70.4 | 5.6 | 80.0 | 80.0 | 22.0 | 22.0 | 22.0 | | | |
| Effective Green, g (s) | | 70.4 | 70.4 | 5.6 | 80.0 | 80.0 | 22.0 | 22.0 | 22.0 | | | |
| Actuated g/C Ratio | | 0.64 | 0.64 | 0.05 | 0.73 | 0.73 | 0.20 | 0.20 | 0.20 | | | |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 3254 | 1013 | 175 | 3698 | 1151 | 687 | 373 | 317 | | | |
| v/s Ratio Prot | | 0.31 | | 0.02 | 0.33 | | | 0.01 | | | | |
| v/s Ratio Perm | | | 0.19 | | | c0.45 | 0.08 | | c0.16 | | | |
| v/c Ratio | | 0.49 | 0.30 | 0.40 | 0.45 | 0.62 | 0.40 | 0.03 | 0.79 | | | |
| Uniform Delay, d1 | | 10.3 | 8.8 | 50.6 | 6.1 | 7.5 | 38.3 | 35.4 | 41.8 | | | |
| Progression Factor | | 0.15 | 0.17 | 1.05 | 0.68 | 0.98 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.5 | 0.7 | 0.9 | 0.2 | 1.5 | 0.4 | 0.0 | 12.2 | | | |
| Delay (s) | | 2.0 | 2.2 | 54.0 | 4.4 | 8.8 | 38.6 | 35.4 | 54.0 | | | |
| Level of Service | | A | A | D | A | A | D | D | D | | | |
| Approach Delay (s) | | 2.1 | | | 7.1 | | | 45.8 | | | 0.0 | |
| Approach LOS | | A | | | A | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 9.4 | | HCM Level of Service | | | | | A | | | |
| HCM Volume to Capacity ratio | | 0.66 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | Sum of lost time (s) | | | | | 8.0 | | | |
| Intersection Capacity Utilization | | 54.2% | | ICU Level of Service | | | | | A | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Slatten Ranch Road

























Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 0.97 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 1770 | 5063 | | 3433 | 3509 | | 3433 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 1770 | 5063 | | 3433 | 3509 | | 3433 | 3539 | 1583 |
| Volume (vph) | 460 | 1110 | 240 | 70 | 1690 | 50 | 500 | 500 | 30 | 10 | 150 | 280 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 460 | 1110 | 240 | 70 | 1690 | 50 | 500 | 500 | 30 | 10 | 150 | 280 |
| RTOR Reduction (vph) | 0 | 0 | 79 | 0 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 167 |
| Lane Group Flow (vph) | 460 | 1110 | 161 | 70 | 1737 | 0 | 500 | 526 | 0 | 10 | 150 | 113 |
| Turn Type | Prot | pm+ov | | Prot | | | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | 3 | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | 4 |
| Actuated Green, G (s) | 16.8 | 55.0 | 74.0 | 4.8 | 43.0 | | 19.0 | 33.4 | | 0.8 | 15.2 | 15.2 |
| Effective Green, g (s) | 16.8 | 55.0 | 74.0 | 4.8 | 43.0 | | 19.0 | 33.4 | | 0.8 | 15.2 | 15.2 |
| Actuated g/C Ratio | 0.15 | 0.50 | 0.67 | 0.04 | 0.39 | | 0.17 | 0.30 | | 0.01 | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 524 | 2543 | 1065 | 77 | 1979 | | 593 | 1065 | | 25 | 489 | 219 |
| v/s Ratio Prot | c0.13 | 0.22 | 0.03 | 0.04 | c0.34 | | c0.15 | c0.15 | | 0.00 | 0.04 | |
| v/s Ratio Perm | | | 0.08 | | | | | | | | | 0.07 |
| v/c Ratio | 0.88 | 0.44 | 0.15 | 0.91 | 0.88 | | 0.84 | 0.49 | | 0.40 | 0.31 | 0.52 |
| Uniform Delay, d1 | 45.6 | 17.6 | 6.6 | 52.4 | 31.1 | | 44.1 | 31.4 | | 54.4 | 42.7 | 44.0 |
| Progression Factor | 1.26 | 1.42 | 4.04 | 1.21 | 1.46 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 13.8 | 0.5 | 0.1 | 62.2 | 4.8 | | 10.6 | 0.4 | | 10.2 | 0.4 | 2.0 |
| Delay (s) | 71.2 | 25.5 | 26.6 | 125.8 | 50.2 | | 54.6 | 31.7 | | 64.5 | 43.0 | 46.0 |
| Level of Service | E | C | C | F | D | | D | C | | E | D | D |
| Approach Delay (s) | | 37.2 | | | 53.1 | | | 42.8 | | | 45.4 | |
| Approach LOS | | D | | | D | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 44.7 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.79 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 78.6% | | | ICU Level of Service | | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue




















Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3260 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3260 | |
| Volume (vph) | 220 | 680 | 260 | 30 | 1200 | 340 | 510 | 200 | 20 | 90 | 90 | 100 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 680 | 260 | 30 | 1200 | 340 | 510 | 200 | 20 | 90 | 90 | 100 |
| RTOR Reduction (vph) | 0 | 0 | 121 | 0 | 0 | 159 | 0 | 0 | 16 | 0 | 92 | 0 |
| Lane Group Flow (vph) | 220 | 680 | 139 | 30 | 1200 | 181 | 510 | 200 | 4 | 90 | 98 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 22.5 | 59.0 | 59.0 | 4.3 | 40.8 | 40.8 | 22.2 | 19.4 | 19.4 | 11.3 | 8.5 | |
| Effective Green, g (s) | 22.5 | 59.0 | 59.0 | 4.3 | 40.8 | 40.8 | 22.2 | 19.4 | 19.4 | 11.3 | 8.5 | |
| Actuated g/C Ratio | 0.20 | 0.54 | 0.54 | 0.04 | 0.37 | 0.37 | 0.20 | 0.18 | 0.18 | 0.10 | 0.08 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 362 | 2727 | 849 | 69 | 1886 | 587 | 693 | 329 | 279 | 353 | 252 | |
| v/s Ratio Prot | c0.12 | 0.13 | | 0.02 | c0.24 | | c0.15 | c0.11 | | 0.03 | 0.03 | |
| v/s Ratio Perm | | | 0.09 | | | 0.11 | | | 0.00 | | | |
| v/c Ratio | 0.61 | 0.25 | 0.16 | 0.43 | 0.64 | 0.31 | 0.74 | 0.61 | 0.01 | 0.25 | 0.39 | |
| Uniform Delay, d1 | 39.7 | 13.6 | 13.0 | 51.7 | 28.5 | 24.6 | 41.2 | 41.8 | 37.4 | 45.5 | 48.3 | |
| Progression Factor | 1.37 | 1.52 | 7.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.7 | 0.2 | 0.4 | 4.3 | 1.7 | 1.4 | 4.1 | 3.2 | 0.0 | 0.4 | 1.0 | |
| Delay (s) | 57.0 | 21.0 | 91.1 | 56.0 | 30.1 | 25.9 | 45.2 | 45.0 | 37.4 | 45.9 | 49.3 | |
| Level of Service | E | C | F | E | C | C | D | D | D | D | D | |
| Approach Delay (s) | | 43.6 | | | 29.7 | | | 44.9 | | | 48.2 | |
| Approach LOS | | D | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 38.4 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.66 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 69.0% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

13: Lone Tree Way & Deer Valley Rd























Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.97 | | 1.00 | 0.97 | | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 4943 | | 1770 | 4922 | | 3433 | 3381 | | 1770 | 3429 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 4943 | | 1770 | 4922 | | 3433 | 3381 | | 1770 | 3429 | |
| Volume (vph) | 110 | 700 | 160 | 200 | 1320 | 360 | 450 | 520 | 220 | 340 | 380 | 100 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 110 | 700 | 160 | 200 | 1320 | 360 | 450 | 520 | 220 | 340 | 380 | 100 |
| RTOR Reduction (vph) | 0 | 33 | 0 | 0 | 44 | 0 | 0 | 42 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 110 | 827 | 0 | 200 | 1636 | 0 | 450 | 698 | 0 | 340 | 459 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 7.0 | 32.4 | | 15.1 | 40.5 | | 18.5 | 24.0 | | 22.5 | 28.0 | |
| Effective Green, g (s) | 7.0 | 32.4 | | 15.1 | 40.5 | | 18.5 | 24.0 | | 22.5 | 28.0 | |
| Actuated g/C Ratio | 0.06 | 0.29 | | 0.14 | 0.37 | | 0.17 | 0.22 | | 0.20 | 0.25 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 113 | 1456 | | 243 | 1812 | | 577 | 738 | | 362 | 873 | |
| v/s Ratio Prot | 0.06 | 0.17 | | c0.11 | c0.33 | | 0.13 | c0.21 | | c0.19 | c0.13 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.97 | 0.57 | | 0.82 | 0.90 | | 0.78 | 0.95 | | 0.94 | 0.53 | |
| Uniform Delay, d1 | 51.4 | 32.9 | | 46.2 | 32.9 | | 43.8 | 42.4 | | 43.1 | 35.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 75.7 | 1.6 | | 19.7 | 7.8 | | 6.6 | 20.7 | | 31.6 | 0.6 | |
| Delay (s) | 127.2 | 34.5 | | 65.8 | 40.7 | | 50.4 | 63.1 | | 74.7 | 35.9 | |
| Level of Service | F | C | | E | D | | D | E | | E | D | |
| Approach Delay (s) | 45.0 | | | 43.4 | | | 58.3 | | | 52.0 | | |
| Approach LOS | D | | | D | | | E | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 48.8 | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | | 0.92 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | Sum of lost time (s) | | | 16.0 | | | | |
| Intersection Capacity Utilization | | | 93.2% | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

14: Lone Tree Way & Hillcrest Avenue

























Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 5057 | | 1770 | 5085 | 1583 | 1770 | 3256 | | 1610 | 3256 | 1583 |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | 1770 | 5057 | | 1770 | 5085 | 1583 | 1770 | 3256 | | 1610 | 3256 | 1583 |
| Volume (vph) | 288 | 792 | 30 | 40 | 1256 | 400 | 80 | 70 | 80 | 380 | 40 | 464 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 288 | 792 | 30 | 40 | 1256 | 400 | 80 | 70 | 80 | 380 | 40 | 464 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 206 | 0 | 73 | 0 | 0 | 0 | 385 |
| Lane Group Flow (vph) | 288 | 820 | 0 | 40 | 1256 | 194 | 80 | 77 | 0 | 190 | 230 | 79 |
| Turn Type | Prot | | | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 15.0 | 67.6 | | 5.6 | 58.2 | 58.2 | 10.3 | 10.3 | | 20.5 | 20.5 | 20.5 |
| Effective Green, g (s) | 15.0 | 67.6 | | 5.6 | 58.2 | 58.2 | 10.3 | 10.3 | | 20.5 | 20.5 | 20.5 |
| Actuated g/C Ratio | 0.12 | 0.56 | | 0.05 | 0.49 | 0.49 | 0.09 | 0.09 | | 0.17 | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 221 | 2849 | | 83 | 2466 | 768 | 152 | 279 | | 275 | 556 | 270 |
| v/s Ratio Prot | c0.16 | 0.16 | | 0.02 | c0.25 | | c0.05 | 0.02 | | c0.12 | 0.07 | |
| v/s Ratio Perm | | | | | | 0.12 | | | | | | 0.05 |
| v/c Ratio | 1.30 | 0.29 | | 0.48 | 0.51 | 0.25 | 0.53 | 0.28 | | 0.69 | 0.41 | 0.29 |
| Uniform Delay, d1 | 52.5 | 13.7 | | 55.8 | 21.1 | 18.1 | 52.5 | 51.4 | | 46.8 | 44.4 | 43.4 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 165.3 | 0.3 | | 4.4 | 0.8 | 0.8 | 3.3 | 0.5 | | 7.3 | 0.5 | 0.6 |
| Delay (s) | 217.8 | 13.9 | | 60.1 | 21.9 | 18.9 | 55.8 | 51.9 | | 54.1 | 44.9 | 44.0 |
| Level of Service | F | B | | E | C | B | E | D | | D | D | D |
| Approach Delay (s) | | 66.8 | | | 22.1 | | | 53.2 | | | 46.4 | |
| Approach LOS | | E | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 42.1 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.66 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 68.6% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

15: Lone Tree Way & Vista Grande Drive






















Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 1770 | 1863 | 1583 | 1770 | 1653 | 1653 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.70 | 1.00 | 1.00 | 0.74 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 1313 | 1863 | 1583 | 1386 | 1653 | 1653 |
| Volume (vph) | 110 | 892 | 220 | 170 | 1316 | 140 | 300 | 20 | 130 | 70 | 20 | 60 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 110 | 892 | 220 | 170 | 1316 | 140 | 300 | 20 | 130 | 70 | 20 | 60 |
| RTOR Reduction (vph) | 0 | 0 | 104 | 0 | 0 | 64 | 0 | 0 | 99 | 0 | 46 | 0 |
| Lane Group Flow (vph) | 110 | 892 | 116 | 170 | 1316 | 76 | 300 | 20 | 31 | 70 | 34 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 11.9 | 57.8 | 57.8 | 14.2 | 60.1 | 60.1 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |
| Effective Green, g (s) | 11.9 | 57.8 | 57.8 | 14.2 | 60.1 | 60.1 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |
| Actuated g/C Ratio | 0.11 | 0.53 | 0.53 | 0.13 | 0.55 | 0.55 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 191 | 2672 | 832 | 228 | 2778 | 865 | 310 | 440 | 374 | 328 | 391 | 391 |
| v/s Ratio Prot | 0.06 | 0.18 | | c0.10 | c0.26 | | | 0.01 | | | 0.02 | |
| v/s Ratio Perm | | | 0.07 | | | 0.05 | c0.23 | | 0.02 | 0.05 | | |
| v/c Ratio | 0.58 | 0.33 | 0.14 | 0.75 | 0.47 | 0.09 | 0.97 | 0.05 | 0.08 | 0.21 | 0.09 | 0.09 |
| Uniform Delay, d1 | 46.7 | 15.0 | 13.4 | 46.2 | 15.3 | 11.9 | 41.6 | 32.4 | 32.7 | 33.8 | 32.7 | 32.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 4.2 | 0.3 | 0.3 | 12.4 | 0.6 | 0.2 | 41.9 | 0.0 | 0.1 | 0.3 | 0.1 | 0.1 |
| Delay (s) | 50.8 | 15.4 | 13.7 | 58.6 | 15.9 | 12.1 | 83.5 | 32.5 | 32.8 | 34.1 | 32.8 | 32.8 |
| Level of Service | D | B | B | E | B | B | F | C | C | C | C | C |
| Approach Delay (s) | | 18.3 | | | 20.0 | | | 66.6 | | | 33.4 | |
| Approach LOS | | B | | | B | | | E | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.0 | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | | 0.62 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 64.8% | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

16: Country Hills Drive & Hillcrest Avenue























Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 0.97 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1723 | | 1770 | 3446 | | 1770 | 3518 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1723 | | 1770 | 3446 | | 1770 | 3518 | |
| Volume (vph) | 70 | 40 | 50 | 110 | 60 | 60 | 100 | 708 | 150 | 80 | 734 | 30 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 70 | 40 | 50 | 110 | 60 | 60 | 100 | 708 | 150 | 80 | 734 | 30 |
| RTOR Reduction (vph) | 0 | 0 | 46 | 0 | 50 | 0 | 0 | 16 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 70 | 40 | 4 | 110 | 70 | 0 | 100 | 842 | 0 | 80 | 761 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | | | | |
| Actuated Green, G (s) | 5.6 | 5.8 | 5.8 | 8.1 | 8.3 | | 7.9 | 42.9 | | 5.4 | 40.4 | |
| Effective Green, g (s) | 5.6 | 5.8 | 5.8 | 8.1 | 8.3 | | 7.9 | 42.9 | | 5.4 | 40.4 | |
| Actuated g/C Ratio | 0.07 | 0.07 | 0.07 | 0.10 | 0.11 | | 0.10 | 0.55 | | 0.07 | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 127 | 138 | 117 | 183 | 183 | | 179 | 1890 | | 122 | 1817 | |
| v/s Ratio Prot | 0.04 | 0.02 | | c0.06 | c0.04 | | c0.06 | c0.24 | | 0.05 | 0.22 | |
| v/s Ratio Perm | | | 0.00 | | | | | | | | | |
| v/c Ratio | 0.55 | 0.29 | 0.03 | 0.60 | 0.38 | | 0.56 | 0.45 | | 0.66 | 0.42 | |
| Uniform Delay, d1 | 35.1 | 34.3 | 33.6 | 33.5 | 32.6 | | 33.5 | 10.5 | | 35.5 | 11.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 5.1 | 1.2 | 0.1 | 5.5 | 1.3 | | 3.7 | 0.8 | | 12.0 | 0.7 | |
| Delay (s) | 40.2 | 35.4 | 33.7 | 39.0 | 33.9 | | 37.2 | 11.3 | | 47.5 | 12.4 | |
| Level of Service | D | D | C | D | C | | D | B | | D | B | |
| Approach Delay (s) | | 37.0 | | | 36.3 | | | 14.0 | | | 15.7 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 18.7 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 78.2 | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 51.5% | | | ICU Level of Service | | | A | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

18: Laurel Road & Hillcrest Avenue

Antioch Davidon Homes TIA
2025 No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1709 | | 1770 | 1863 | 1583 | 1770 | 3388 | | 1770 | 3474 | |
| Flt Permitted | 0.69 | 1.00 | | 0.63 | 1.00 | 1.00 | 0.24 | 1.00 | | 0.19 | 1.00 | |
| Satd. Flow (perm) | 1290 | 1709 | | 1178 | 1863 | 1583 | 449 | 3388 | | 357 | 3474 | |
| Volume (vph) | 170 | 90 | 110 | 254 | 100 | 195 | 90 | 900 | 358 | 315 | 860 | 120 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 170 | 90 | 110 | 254 | 100 | 195 | 90 | 900 | 358 | 315 | 860 | 120 |
| RTOR Reduction (vph) | 0 | 45 | 0 | 0 | 0 | 38 | 0 | 85 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 170 | 155 | 0 | 254 | 100 | 157 | 90 | 1173 | 0 | 315 | 959 | 0 |
| Turn Type | Perm | | | Perm | | | Perm | Perm | | Perm | | |
| Protected Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Permitted Phases | 4 | | | 8 | | | 2 | | | 6 | | |
| Actuated Green, G (s) | 11.1 | 11.1 | | 11.1 | 11.1 | 11.1 | 20.9 | 20.9 | | 20.9 | 20.9 | |
| Effective Green, g (s) | 11.1 | 11.1 | | 11.1 | 11.1 | 11.1 | 20.9 | 20.9 | | 20.9 | 20.9 | |
| Actuated g/C Ratio | 0.28 | 0.28 | | 0.28 | 0.28 | 0.28 | 0.52 | 0.52 | | 0.52 | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 358 | 474 | | 327 | 517 | 439 | 235 | 1770 | | 187 | 1815 | |
| v/s Ratio Prot | 0.09 | | | 0.05 | | | 0.35 | | | 0.28 | | |
| v/s Ratio Perm | 0.13 | | | c0.22 | | 0.10 | 0.20 | | | c0.88 | | |
| v/c Ratio | 0.47 | 0.33 | | 0.78 | 0.19 | 0.36 | 0.38 | 0.66 | | 1.68 | 0.53 | |
| Uniform Delay, d1 | 12.0 | 11.5 | | 13.3 | 11.0 | 11.6 | 5.7 | 7.0 | | 9.6 | 6.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.0 | 0.4 | | 11.0 | 0.2 | 0.5 | 4.7 | 2.0 | | 330.1 | 1.1 | |
| Delay (s) | 13.0 | 11.9 | | 24.3 | 11.2 | 12.1 | 10.4 | 9.0 | | 339.7 | 7.4 | |
| Level of Service | B | B | | C | B | B | B | A | | F | A | |
| Approach Delay (s) | 12.4 | | | 17.6 | | | 9.0 | | | 88.2 | | |
| Approach LOS | B | | | B | | | A | | | F | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 39.5 | | HCM Level of Service | | | | D | | | |
| HCM Volume to Capacity ratio | | | 1.37 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 40.0 | | Sum of lost time (s) | | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 92.7% | | ICU Level of Service | | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: Laurel Road & Canada Valley





















Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| | → | ↘ | ↙ | ← | ↖ | ↗ |
|-----------------------------------|-------|------|-------|------|----------------------|-------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | | ↘ | ↑↑ | ↘ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | 0.97 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3428 | | 1770 | 3539 | 1770 | 1583 |
| Flt Permitted | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3428 | | 1770 | 3539 | 1770 | 1583 |
| Volume (vph) | 566 | 150 | 421 | 836 | 40 | 278 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 566 | 150 | 421 | 836 | 40 | 278 |
| RTOR Reduction (vph) | 22 | 0 | 0 | 0 | 0 | 225 |
| Lane Group Flow (vph) | 694 | 0 | 421 | 836 | 40 | 53 |
| Turn Type | | | Prot | | | Perm |
| Protected Phases | 4 | | 3 | 8 | 2 | |
| Permitted Phases | | | | | | 2 |
| Actuated Green, G (s) | 36.4 | | 32.6 | 73.0 | 19.0 | 19.0 |
| Effective Green, g (s) | 36.4 | | 32.6 | 73.0 | 19.0 | 19.0 |
| Actuated g/C Ratio | 0.36 | | 0.33 | 0.73 | 0.19 | 0.19 |
| Clearance Time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 1248 | | 577 | 2583 | 336 | 301 |
| v/s Ratio Prot | c0.20 | | c0.24 | 0.24 | 0.02 | |
| v/s Ratio Perm | | | | | | c0.03 |
| v/c Ratio | 0.56 | | 0.73 | 0.32 | 0.12 | 0.18 |
| Uniform Delay, d1 | 25.4 | | 29.8 | 4.8 | 33.6 | 33.9 |
| Progression Factor | 1.00 | | 0.61 | 0.39 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.8 | | 4.1 | 0.3 | 0.7 | 1.3 |
| Delay (s) | 27.2 | | 22.2 | 2.1 | 34.3 | 35.2 |
| Level of Service | C | | C | A | C | D |
| Approach Delay (s) | 27.2 | | | 8.8 | 35.1 | |
| Approach LOS | C | | | A | D | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 18.2 | | HCM Level of Service | B |
| HCM Volume to Capacity ratio | | | 0.54 | | | |
| Actuated Cycle Length (s) | | | 100.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 57.1% | | ICU Level of Service | B |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Laurel Road & Country Hills Drive


Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | 1.00 | 0.85 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3455 | | 1770 | 3494 | | 1770 | 1583 | | 1770 | 1676 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3455 | | 1770 | 3494 | | 1770 | 1583 | | 1770 | 1676 | |
| Volume (vph) | 60 | 636 | 120 | 182 | 1078 | 100 | 90 | 0 | 95 | 50 | 20 | 40 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 60 | 636 | 120 | 182 | 1078 | 100 | 90 | 0 | 95 | 50 | 20 | 40 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 37 | 0 |
| Lane Group Flow (vph) | 60 | 756 | 0 | 182 | 1172 | 0 | 90 | 95 | 0 | 50 | 23 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 7.7 | 41.3 | | 26.8 | 60.4 | | 7.7 | 11.1 | | 4.8 | 8.2 | |
| Effective Green, g (s) | 7.7 | 41.3 | | 26.8 | 60.4 | | 7.7 | 11.1 | | 4.8 | 8.2 | |
| Actuated g/C Ratio | 0.08 | 0.41 | | 0.27 | 0.60 | | 0.08 | 0.11 | | 0.05 | 0.08 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 136 | 1427 | | 474 | 2110 | | 136 | 176 | | 85 | 137 | |
| v/s Ratio Prot | 0.03 | c0.22 | | 0.10 | c0.34 | | c0.05 | c0.06 | | 0.03 | 0.01 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.44 | 0.53 | | 0.38 | 0.56 | | 0.66 | 0.54 | | 0.59 | 0.17 | |
| Uniform Delay, d1 | 44.1 | 22.1 | | 29.9 | 11.8 | | 44.9 | 42.0 | | 46.6 | 42.7 | |
| Progression Factor | 0.88 | 1.53 | | 1.05 | 1.03 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.0 | 1.2 | | 0.5 | 0.9 | | 11.5 | 3.2 | | 10.0 | 0.6 | |
| Delay (s) | 40.6 | 35.0 | | 31.7 | 13.1 | | 56.3 | 45.2 | | 56.6 | 43.3 | |
| Level of Service | D | C | | C | B | | E | D | | E | D | |
| Approach Delay (s) | 35.4 | | | 15.6 | | | 50.6 | | | 49.4 | | |
| Approach LOS | D | | | B | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.3 | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | Sum of lost time (s) | | | 16.0 | | | | |
| Intersection Capacity Utilization | | | 58.0% | | ICU Level of Service | | | B | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Laurel Road & SB SR4 Bypass



















Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|-------|------|------|----------------------|------|------|------|------|------|--------|-------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑ | | | ↑↑ | | | | | ↘ | ↗ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 1.00 | | | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 3532 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 3532 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 770 | 11 | 0 | 890 | 0 | 0 | 0 | 0 | 720 | 0 | 471 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 770 | 11 | 0 | 890 | 0 | 0 | 0 | 0 | 720 | 0 | 471 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 781 | 0 | 0 | 890 | 0 | 0 | 0 | 0 | 360 | 360 | 471 |
| Turn Type | | | | | | | | | | Perm | custom | |
| Protected Phases | | 2 | | | 6 | | | | | | 4 | 4 |
| Permitted Phases | | | | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 56.9 | | | 56.9 | | | | | 35.1 | 35.1 | 35.1 |
| Effective Green, g (s) | | 56.9 | | | 56.9 | | | | | 35.1 | 35.1 | 35.1 |
| Actuated g/C Ratio | | 0.57 | | | 0.57 | | | | | 0.35 | 0.35 | 0.35 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2010 | | | 2014 | | | | | 590 | 590 | 556 |
| v/s Ratio Prot | | 0.22 | | | c0.25 | | | | | | | c0.30 |
| v/s Ratio Perm | | | | | | | | | | 0.21 | 0.21 | |
| v/c Ratio | | 0.39 | | | 0.44 | | | | | 0.61 | 0.61 | 0.85 |
| Uniform Delay, d1 | | 11.9 | | | 12.4 | | | | | 26.8 | 26.8 | 30.0 |
| Progression Factor | | 0.09 | | | 0.24 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.5 | | | 0.7 | | | | | 1.9 | 1.9 | 11.4 |
| Delay (s) | | 1.6 | | | 3.7 | | | | | 28.7 | 28.7 | 41.4 |
| Level of Service | | A | | | A | | | | | C | C | D |
| Approach Delay (s) | | 1.6 | | | 3.7 | | | 0.0 | | | 33.7 | |
| Approach LOS | | A | | | A | | | A | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 15.6 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.60 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 100.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 91.7% | | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Laurel Road & SR4 Bypass NB Ramps




























Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | | |  |  | |  |  | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | 1.00 | | 1.00 | 1.00 | | | |
| Frt | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Volume (vph) | 150 | 1340 | 0 | 0 | 959 | 730 | 41 | 0 | 210 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 150 | 1340 | 0 | 0 | 959 | 730 | 41 | 0 | 210 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 150 | 1340 | 0 | 0 | 959 | 730 | 0 | 41 | 210 | 0 | 0 | 0 |
| Turn Type | Prot | | | | Perm | | Perm | | custom | | | |
| Protected Phases | 5 | 2 | | | 6 | | | 8 | 8 | | | |
| Permitted Phases | | | | | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | 16.0 | 76.1 | | | 56.1 | 56.1 | | 15.9 | 15.9 | | | |
| Effective Green, g (s) | 16.0 | 76.1 | | | 56.1 | 56.1 | | 15.9 | 15.9 | | | |
| Actuated g/C Ratio | 0.16 | 0.76 | | | 0.56 | 0.56 | | 0.16 | 0.16 | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | 283 | 2693 | | | 1985 | 888 | | 281 | 252 | | | |
| v/s Ratio Prot | 0.08 | c0.38 | | | 0.27 | | | | c0.13 | | | |
| v/s Ratio Perm | | | | | | c0.46 | | 0.02 | | | | |
| v/c Ratio | 0.53 | 0.50 | | | 0.48 | 0.82 | | 0.15 | 0.83 | | | |
| Uniform Delay, d1 | 38.5 | 4.6 | | | 13.2 | 17.9 | | 36.2 | 40.8 | | | |
| Progression Factor | 0.89 | 0.60 | | | 0.12 | 0.20 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 1.8 | 0.6 | | | 0.6 | 5.8 | | 0.2 | 20.4 | | | |
| Delay (s) | 36.3 | 3.4 | | | 2.2 | 9.4 | | 36.4 | 61.2 | | | |
| Level of Service | D | A | | | A | A | | D | E | | | |
| Approach Delay (s) | | 6.7 | | | 5.3 | | | 57.2 | | | 0.0 | |
| Approach LOS | | A | | | A | | | E | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 9.7 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.75 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 100.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 66.8% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Laurel Road & Slatten Ranch Road

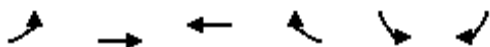
Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |    | |  |   | |  |   | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.92 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 4944 | | 3433 | 3264 | | 1770 | 3427 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 4944 | | 3433 | 3264 | | 1770 | 3427 | |
| Volume (vph) | 100 | 1160 | 290 | 260 | 969 | 220 | 610 | 270 | 290 | 230 | 410 | 110 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 100 | 1160 | 290 | 260 | 969 | 220 | 610 | 270 | 290 | 230 | 410 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 100 | 1160 | 290 | 260 | 1189 | 0 | 610 | 560 | 0 | 230 | 520 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | |
| Actuated Green, G (s) | 9.6 | 29.2 | 29.2 | 17.0 | 36.6 | | 20.3 | 22.5 | | 15.3 | 17.5 | |
| Effective Green, g (s) | 9.6 | 29.2 | 29.2 | 17.0 | 36.6 | | 20.3 | 22.5 | | 15.3 | 17.5 | |
| Actuated g/C Ratio | 0.10 | 0.29 | 0.29 | 0.17 | 0.37 | | 0.20 | 0.22 | | 0.15 | 0.18 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 170 | 1485 | 462 | 301 | 1810 | | 697 | 734 | | 271 | 600 | |
| v/s Ratio Prot | 0.06 | c0.23 | | c0.15 | 0.24 | | c0.18 | 0.17 | | 0.13 | c0.15 | |
| v/s Ratio Perm | | | 0.18 | | | | | | | | | |
| v/c Ratio | 0.59 | 0.78 | 0.63 | 0.86 | 0.66 | | 0.88 | 0.76 | | 0.85 | 0.87 | |
| Uniform Delay, d1 | 43.3 | 32.5 | 30.7 | 40.4 | 26.5 | | 38.6 | 36.3 | | 41.2 | 40.1 | |
| Progression Factor | 0.92 | 0.91 | 0.90 | 0.68 | 0.34 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 4.4 | 3.6 | 5.4 | 19.0 | 1.6 | | 11.8 | 4.7 | | 21.2 | 12.5 | |
| Delay (s) | 44.1 | 33.0 | 33.0 | 46.3 | 10.7 | | 50.5 | 41.0 | | 62.4 | 52.6 | |
| Level of Service | D | C | C | D | B | | D | D | | E | D | |
| Approach Delay (s) | | 33.7 | | | 17.1 | | | 45.9 | | | 55.6 | |
| Approach LOS | | C | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 35.0 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.83 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 82.4% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Laurel Road & Live Oak Avenue

Antioch Davidon Homes TIA
2025 No Project PM Peak Hour


























| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|-------|------|-------|------|----------------------|-------|
| Lane Configurations | ↖↗ | ↑↑↑ | ↑↑↑↗ | | ↖ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.91 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.99 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 5054 | | 1770 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 5054 | | 1770 | 1583 |
| Volume (vph) | 340 | 1340 | 1159 | 50 | 130 | 290 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 340 | 1340 | 1159 | 50 | 130 | 290 |
| RTOR Reduction (vph) | 0 | 0 | 6 | 0 | 0 | 167 |
| Lane Group Flow (vph) | 340 | 1340 | 1203 | 0 | 130 | 123 |
| Turn Type | Prot | | | Perm | | |
| Protected Phases | 7 | 4 | 8 | 6 | | |
| Permitted Phases | | | | | 6 | |
| Actuated Green, G (s) | 15.3 | 49.5 | 30.2 | | 42.5 | 42.5 |
| Effective Green, g (s) | 15.3 | 49.5 | 30.2 | | 42.5 | 42.5 |
| Actuated g/C Ratio | 0.15 | 0.50 | 0.30 | | 0.42 | 0.42 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 525 | 2517 | 1526 | | 752 | 673 |
| v/s Ratio Prot | c0.10 | 0.26 | c0.24 | | 0.07 | |
| v/s Ratio Perm | | | | | | c0.08 |
| v/c Ratio | 0.65 | 0.53 | 0.79 | | 0.17 | 0.18 |
| Uniform Delay, d1 | 39.8 | 17.3 | 32.0 | | 17.8 | 17.9 |
| Progression Factor | 1.21 | 1.28 | 0.84 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.7 | 0.1 | 2.4 | | 0.5 | 0.6 |
| Delay (s) | 50.0 | 22.4 | 29.2 | | 18.3 | 18.5 |
| Level of Service | D | C | C | | B | B |
| Approach Delay (s) | | 28.0 | 29.2 | | 18.5 | |
| Approach LOS | | C | C | | B | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 27.2 | | HCM Level of Service | C |
| HCM Volume to Capacity ratio | | | 0.47 | | | |
| Actuated Cycle Length (s) | | | 100.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 50.4% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Laurel Road & Empire Avenue

























Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3463 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3463 | | 1770 | 3539 | 1583 |
| Volume (vph) | 420 | 890 | 160 | 50 | 686 | 50 | 110 | 360 | 60 | 60 | 300 | 413 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 420 | 890 | 160 | 50 | 686 | 50 | 110 | 360 | 60 | 60 | 300 | 413 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 0 | 29 | 0 | 15 | 0 | 0 | 0 | 309 |
| Lane Group Flow (vph) | 420 | 890 | 82 | 50 | 686 | 21 | 110 | 405 | 0 | 60 | 300 | 104 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 8 | | | | | | 6 |
| Actuated Green, G (s) | 17.1 | 51.4 | 51.4 | 6.8 | 41.1 | 41.1 | 9.9 | 19.0 | | 6.8 | 15.9 | 15.9 |
| Effective Green, g (s) | 17.1 | 51.4 | 51.4 | 6.8 | 41.1 | 41.1 | 9.9 | 19.0 | | 6.8 | 15.9 | 15.9 |
| Actuated g/C Ratio | 0.17 | 0.51 | 0.51 | 0.07 | 0.41 | 0.41 | 0.10 | 0.19 | | 0.07 | 0.16 | 0.16 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 587 | 1819 | 814 | 120 | 1455 | 651 | 175 | 658 | | 120 | 563 | 252 |
| v/s Ratio Prot | c0.12 | c0.25 | | 0.03 | 0.19 | | c0.06 | c0.12 | | 0.03 | 0.08 | |
| v/s Ratio Perm | | | 0.05 | | | 0.01 | | | | | | 0.07 |
| v/c Ratio | 0.72 | 0.49 | 0.10 | 0.42 | 0.47 | 0.03 | 0.63 | 0.62 | | 0.50 | 0.53 | 0.41 |
| Uniform Delay, d1 | 39.2 | 15.8 | 12.5 | 44.7 | 21.5 | 17.6 | 43.3 | 37.2 | | 45.0 | 38.6 | 37.8 |
| Progression Factor | 0.72 | 1.49 | 2.92 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.9 | 0.9 | 0.2 | 2.3 | 1.1 | 0.1 | 6.9 | 1.7 | | 3.3 | 1.0 | 1.1 |
| Delay (s) | 32.2 | 24.3 | 36.6 | 47.0 | 22.6 | 17.7 | 50.2 | 38.9 | | 48.2 | 39.6 | 38.9 |
| Level of Service | C | C | D | D | C | B | D | D | | D | D | D |
| Approach Delay (s) | | 27.9 | | | 23.9 | | | 41.2 | | | 39.9 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 31.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.57 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 60.6% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Lone Tree Way & Canada Valley













Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | 0.91 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.86 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 1770 | 2933 | 1441 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 1770 | 2933 | 1441 | 1770 | 1863 | 1583 |
| Volume (vph) | 69 | 1710 | 60 | 530 | 1090 | 464 | 220 | 20 | 360 | 229 | 20 | 84 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 69 | 1710 | 60 | 530 | 1090 | 464 | 220 | 20 | 360 | 229 | 20 | 84 |
| RTOR Reduction (vph) | 0 | 0 | 32 | 0 | 0 | 202 | 0 | 166 | 166 | 0 | 0 | 78 |
| Lane Group Flow (vph) | 69 | 1710 | 28 | 530 | 1090 | 262 | 220 | 34 | 14 | 229 | 20 | 6 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 6.4 | 46.3 | 46.3 | 22.1 | 62.0 | 62.0 | 18.1 | 8.7 | 8.7 | 16.9 | 7.5 | 7.5 |
| Effective Green, g (s) | 6.4 | 46.3 | 46.3 | 22.1 | 62.0 | 62.0 | 18.1 | 8.7 | 8.7 | 16.9 | 7.5 | 7.5 |
| Actuated g/C Ratio | 0.06 | 0.42 | 0.42 | 0.20 | 0.56 | 0.56 | 0.16 | 0.08 | 0.08 | 0.15 | 0.07 | 0.07 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 200 | 2140 | 666 | 690 | 2866 | 892 | 291 | 232 | 114 | 272 | 127 | 108 |
| v/s Ratio Prot | 0.02 | c0.34 | | c0.15 | 0.21 | | 0.12 | c0.01 | | c0.13 | 0.01 | |
| v/s Ratio Perm | | | 0.02 | | | 0.17 | | | 0.01 | | | 0.00 |
| v/c Ratio | 0.34 | 0.80 | 0.04 | 0.77 | 0.38 | 0.29 | 0.76 | 0.15 | 0.12 | 0.84 | 0.16 | 0.05 |
| Uniform Delay, d1 | 49.8 | 27.8 | 18.8 | 41.5 | 13.3 | 12.5 | 43.8 | 47.2 | 47.1 | 45.3 | 48.3 | 47.9 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.69 | 1.11 | 4.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.0 | 3.2 | 0.1 | 4.4 | 0.3 | 0.7 | 10.7 | 0.3 | 0.5 | 20.4 | 0.6 | 0.2 |
| Delay (s) | 50.8 | 31.0 | 18.9 | 33.2 | 15.1 | 63.3 | 54.5 | 47.5 | 47.6 | 65.6 | 48.9 | 48.1 |
| Level of Service | D | C | B | C | B | E | D | D | D | E | D | D |
| Approach Delay (s) | | 31.4 | | | 30.4 | | | 50.1 | | | 60.2 | |
| Approach LOS | | C | | | C | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 35.3 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.71 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 78.6% | | | | ICU Level of Service | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Lone Tree Way & SB SR4 Bypass













Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 2051 | 368 | 380 | 1844 | 0 | 0 | 0 | 0 | 849 | 0 | 240 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 2051 | 368 | 380 | 1844 | 0 | 0 | 0 | 0 | 849 | 0 | 240 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 2051 | 368 | 380 | 1844 | 0 | 0 | 0 | 0 | 425 | 424 | 240 |
| Turn Type | | Perm | | Prot | | | | | | Split | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | 4 | | 4 |
| Permitted Phases | | 2 | | | | | | | | | | 4 |
| Actuated Green, G (s) | | 52.2 | 52.2 | 15.0 | 71.2 | | | | | 30.8 | 30.8 | 30.8 |
| Effective Green, g (s) | | 52.2 | 52.2 | 15.0 | 71.2 | | | | | 30.8 | 30.8 | 30.8 |
| Actuated g/C Ratio | | 0.47 | 0.47 | 0.14 | 0.65 | | | | | 0.28 | 0.28 | 0.28 |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2413 | 751 | 468 | 3291 | | | | | 471 | 471 | 443 |
| v/s Ratio Prot | | c0.40 | | c0.11 | | 0.36 | | | | c0.25 | | 0.25 |
| v/s Ratio Perm | | 0.23 | | | | | | | | | | 0.15 |
| v/c Ratio | | 0.85 | 0.49 | 0.81 | 0.56 | | | | | 0.90 | 0.90 | 0.54 |
| Uniform Delay, d1 | | 25.5 | 19.8 | 46.1 | 10.7 | | | | | 38.2 | 38.1 | 33.6 |
| Progression Factor | | 0.66 | 0.51 | 0.95 | 0.72 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 2.9 | 1.6 | 9.1 | 0.6 | | | | | 20.3 | 20.0 | 1.4 |
| Delay (s) | | 19.6 | 11.7 | 53.1 | 8.3 | | | | | 58.4 | 58.1 | 35.0 |
| Level of Service | | B | B | D | A | | | | | E | E | C |
| Approach Delay (s) | | 18.4 | | 16.0 | | 0.0 | | 53.2 | | | | |
| Approach LOS | | B | | B | | A | | D | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 24.1 | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | | 0.86 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | | 84.0% | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Lone Tree Way & SR4 Bypass NB Ramps























Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Volume (vph) | 0 | 2620 | 280 | 60 | 1695 | 711 | 530 | 50 | 340 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 2620 | 280 | 60 | 1695 | 711 | 530 | 50 | 340 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 2620 | 280 | 60 | 1695 | 711 | 530 | 50 | 340 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Perm | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | | |
| Permitted Phases | | | | 2 | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | | 67.7 | 67.7 | 3.2 | 74.9 | 74.9 | 27.1 | 27.1 | 27.1 | | | |
| Effective Green, g (s) | | 67.7 | 67.7 | 3.2 | 74.9 | 74.9 | 27.1 | 27.1 | 27.1 | | | |
| Actuated g/C Ratio | | 0.62 | 0.62 | 0.03 | 0.68 | 0.68 | 0.25 | 0.25 | 0.25 | | | |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 3130 | 974 | 100 | 3462 | 1078 | 846 | 459 | 390 | | | |
| v/s Ratio Prot | | c0.52 | | 0.02 | 0.33 | | | 0.03 | | | | |
| v/s Ratio Perm | | | | 0.18 | | c0.45 | 0.15 | | c0.21 | | | |
| v/c Ratio | | 0.84 | 0.29 | 0.60 | 0.49 | 0.66 | 0.63 | 0.11 | 0.87 | | | |
| Uniform Delay, d1 | | 16.8 | 9.9 | 52.8 | 8.4 | 10.2 | 36.9 | 32.1 | 39.8 | | | |
| Progression Factor | | 0.29 | 0.27 | 1.12 | 1.76 | 1.63 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 1.4 | 0.4 | 4.0 | 0.2 | 1.3 | 1.5 | 0.1 | 18.8 | | | |
| Delay (s) | | 6.3 | 3.1 | 63.3 | 15.0 | 17.8 | 38.4 | 32.2 | 58.5 | | | |
| Level of Service | | A | A | E | B | B | D | C | E | | | |
| Approach Delay (s) | | 6.0 | | | 17.0 | | | 45.5 | | | 0.0 | |
| Approach LOS | | A | | | B | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 16.1 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.82 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 78.3% | | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Slatten Ranch Road
































Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 0.97 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 1770 | 5055 | | 3433 | 3445 | | 3433 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 1770 | 5055 | | 3433 | 3445 | | 3433 | 3539 | 1583 |
| Volume (vph) | 470 | 1970 | 530 | 50 | 1476 | 60 | 400 | 370 | 80 | 80 | 550 | 570 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 470 | 1970 | 530 | 50 | 1476 | 60 | 400 | 370 | 80 | 80 | 550 | 570 |
| RTOR Reduction (vph) | 0 | 0 | 57 | 0 | 4 | 0 | 0 | 16 | 0 | 0 | 0 | 264 |
| Lane Group Flow (vph) | 470 | 1970 | 473 | 50 | 1532 | 0 | 400 | 434 | 0 | 80 | 550 | 306 |
| Turn Type | Prot | pm+ov | | Prot | | | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | 3 | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | 4 |
| Actuated Green, G (s) | 22.8 | 53.0 | 67.3 | 6.2 | 36.4 | | 14.3 | 30.6 | | 4.2 | 20.5 | 20.5 |
| Effective Green, g (s) | 22.8 | 53.0 | 67.3 | 6.2 | 36.4 | | 14.3 | 30.6 | | 4.2 | 20.5 | 20.5 |
| Actuated g/C Ratio | 0.21 | 0.48 | 0.61 | 0.06 | 0.33 | | 0.13 | 0.28 | | 0.04 | 0.19 | 0.19 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 712 | 2450 | 969 | 100 | 1673 | | 446 | 958 | | 131 | 660 | 295 |
| v/s Ratio Prot | c0.14 | c0.39 | 0.06 | 0.03 | c0.30 | | c0.12 | 0.13 | | 0.02 | 0.16 | |
| v/s Ratio Perm | | | 0.24 | | | | | | | | | c0.19 |
| v/c Ratio | 0.66 | 0.80 | 0.49 | 0.50 | 0.92 | | 0.90 | 0.45 | | 0.61 | 0.83 | 1.04 |
| Uniform Delay, d1 | 40.0 | 24.1 | 11.8 | 50.4 | 35.3 | | 47.1 | 32.8 | | 52.1 | 43.1 | 44.8 |
| Progression Factor | 0.76 | 0.41 | 0.33 | 0.77 | 1.23 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.3 | 1.6 | 0.2 | 3.4 | 8.3 | | 20.2 | 0.3 | | 8.2 | 8.9 | 62.0 |
| Delay (s) | 31.7 | 11.5 | 4.1 | 42.4 | 51.7 | | 67.3 | 33.1 | | 60.3 | 52.0 | 106.7 |
| Level of Service | C | B | A | D | D | | E | C | | E | D | F |
| Approach Delay (s) | | 13.4 | | | 51.4 | | | 49.2 | | | 78.5 | |
| Approach LOS | | B | | | D | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 39.0 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.87 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 86.6% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue




















Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |    |  |   |  |  |   |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3274 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3274 | |
| Volume (vph) | 160 | 1370 | 600 | 20 | 926 | 160 | 440 | 120 | 40 | 310 | 220 | 220 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 160 | 1370 | 600 | 20 | 926 | 160 | 440 | 120 | 40 | 310 | 220 | 220 |
| RTOR Reduction (vph) | 0 | 0 | 280 | 0 | 0 | 93 | 0 | 0 | 36 | 0 | 187 | 0 |
| Lane Group Flow (vph) | 160 | 1370 | 320 | 20 | 926 | 67 | 440 | 120 | 4 | 310 | 253 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 20.4 | 58.7 | 58.7 | 3.1 | 41.4 | 41.4 | 19.2 | 12.0 | 12.0 | 20.2 | 13.0 | |
| Effective Green, g (s) | 20.4 | 58.7 | 58.7 | 3.1 | 41.4 | 41.4 | 19.2 | 12.0 | 12.0 | 20.2 | 13.0 | |
| Actuated g/C Ratio | 0.19 | 0.53 | 0.53 | 0.03 | 0.38 | 0.38 | 0.17 | 0.11 | 0.11 | 0.18 | 0.12 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 328 | 2714 | 845 | 50 | 1914 | 596 | 599 | 203 | 173 | 630 | 387 | |
| v/s Ratio Prot | 0.09 | c0.27 | | 0.01 | c0.18 | | c0.13 | 0.06 | | 0.09 | c0.08 | |
| v/s Ratio Perm | | | 0.20 | | | 0.04 | | | 0.00 | | | |
| v/c Ratio | 0.49 | 0.50 | 0.38 | 0.40 | 0.48 | 0.11 | 0.73 | 0.59 | 0.03 | 0.49 | 0.65 | |
| Uniform Delay, d1 | 40.1 | 16.4 | 15.0 | 52.5 | 26.2 | 22.3 | 43.0 | 46.7 | 43.8 | 40.3 | 46.4 | |
| Progression Factor | 0.52 | 0.21 | 0.93 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.7 | 0.4 | 0.8 | 5.2 | 0.9 | 0.4 | 4.7 | 4.6 | 0.1 | 0.6 | 3.9 | |
| Delay (s) | 21.8 | 3.9 | 14.7 | 57.7 | 27.0 | 22.7 | 47.6 | 51.2 | 43.8 | 40.9 | 50.3 | |
| Level of Service | C | A | B | E | C | C | D | D | D | D | D | |
| Approach Delay (s) | | 8.3 | | | 27.0 | | | 48.1 | | | 46.4 | |
| Approach LOS | | A | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 24.2 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 68.8% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

13: Lone Tree Way & Deer Valley Rd























Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 4.0 | | 3.5 | 4.0 | | 3.5 | 4.0 | | 3.5 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.95 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5012 | | 1770 | 5007 | | 3433 | 3374 | | 1770 | 3419 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5012 | | 1770 | 5007 | | 3433 | 3374 | | 1770 | 3419 | |
| Volume (vph) | 320 | 1782 | 190 | 190 | 1400 | 160 | 260 | 400 | 180 | 310 | 510 | 150 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 320 | 1782 | 190 | 190 | 1400 | 160 | 260 | 400 | 180 | 310 | 510 | 150 |
| RTOR Reduction (vph) | 0 | 11 | 0 | 0 | 13 | 0 | 0 | 47 | 0 | 0 | 25 | 0 |
| Lane Group Flow (vph) | 320 | 1961 | 0 | 190 | 1547 | 0 | 260 | 533 | 0 | 310 | 635 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 20.0 | 47.0 | | 12.0 | 39.0 | | 10.0 | 18.0 | | 17.0 | 25.0 | |
| Effective Green, g (s) | 20.5 | 47.0 | | 12.5 | 39.0 | | 10.5 | 18.0 | | 17.5 | 25.0 | |
| Actuated g/C Ratio | 0.19 | 0.43 | | 0.11 | 0.35 | | 0.10 | 0.16 | | 0.16 | 0.23 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 330 | 2141 | | 201 | 1775 | | 328 | 552 | | 282 | 777 | |
| v/s Ratio Prot | c0.18 | c0.39 | | 0.11 | 0.31 | | 0.08 | c0.16 | | c0.18 | 0.19 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.97 | 0.92 | | 0.95 | 0.87 | | 0.79 | 0.97 | | 1.10 | 0.82 | |
| Uniform Delay, d1 | 44.4 | 29.6 | | 48.4 | 33.2 | | 48.7 | 45.7 | | 46.2 | 40.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 40.9 | 7.6 | | 47.6 | 6.2 | | 12.3 | 29.5 | | 82.8 | 6.7 | |
| Delay (s) | 85.3 | 37.2 | | 96.1 | 39.4 | | 61.0 | 75.2 | | 129.1 | 47.0 | |
| Level of Service | F | D | | F | D | | E | E | | F | D | |
| Approach Delay (s) | 44.0 | | | 45.5 | | | 70.8 | | | 73.2 | | |
| Approach LOS | D | | | D | | | E | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 53.1 | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | | 0.95 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | Sum of lost time (s) | | | 11.0 | | | | |
| Intersection Capacity Utilization | | | 96.5% | | ICU Level of Service | | | F | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

14: Lone Tree Way & Hillcrest Avenue

























Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 5049 | | 1770 | 5085 | 1583 | 1770 | 3294 | | 1610 | 3274 | 1583 |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (perm) | 1770 | 5049 | | 1770 | 5085 | 1583 | 1770 | 3294 | | 1610 | 3274 | 1583 |
| Volume (vph) | 703 | 1619 | 80 | 100 | 1174 | 480 | 50 | 70 | 60 | 580 | 120 | 446 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 703 | 1619 | 80 | 100 | 1174 | 480 | 50 | 70 | 60 | 580 | 120 | 446 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 368 | 0 | 56 | 0 | 0 | 0 | 349 |
| Lane Group Flow (vph) | 703 | 1695 | 0 | 100 | 1174 | 112 | 50 | 74 | 0 | 290 | 410 | 97 |
| Turn Type | Prot | | | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 43.2 | 57.2 | | 12.0 | 26.0 | 26.0 | 8.7 | 8.7 | | 26.1 | 26.1 | 26.1 |
| Effective Green, g (s) | 43.2 | 57.2 | | 12.0 | 26.0 | 26.0 | 8.7 | 8.7 | | 26.1 | 26.1 | 26.1 |
| Actuated g/C Ratio | 0.36 | 0.48 | | 0.10 | 0.22 | 0.22 | 0.07 | 0.07 | | 0.22 | 0.22 | 0.22 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 637 | 2407 | | 177 | 1102 | 343 | 128 | 239 | | 350 | 712 | 344 |
| v/s Ratio Prot | c0.40 | 0.34 | | 0.06 | c0.23 | | c0.03 | 0.02 | | c0.18 | 0.13 | |
| v/s Ratio Perm | | | | | | 0.07 | | | | | | 0.06 |
| v/c Ratio | 1.10 | 0.70 | | 0.56 | 1.07 | 0.33 | 0.39 | 0.31 | | 0.83 | 0.58 | 0.28 |
| Uniform Delay, d1 | 38.4 | 24.7 | | 51.5 | 47.0 | 39.6 | 53.1 | 52.8 | | 44.8 | 42.0 | 39.1 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 67.4 | 1.8 | | 4.1 | 46.3 | 2.5 | 2.0 | 0.7 | | 14.8 | 1.1 | 0.5 |
| Delay (s) | 105.8 | 26.5 | | 55.6 | 93.3 | 42.1 | 55.1 | 53.6 | | 59.7 | 43.1 | 39.6 |
| Level of Service | F | C | | E | F | D | E | D | | E | D | D |
| Approach Delay (s) | | 49.7 | | | 77.2 | | | 54.0 | | | 45.9 | |
| Approach LOS | | D | | | E | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 57.8 | | | HCM Level of Service | | | E | | | |
| HCM Volume to Capacity ratio | | | 0.97 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 94.9% | | | ICU Level of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

15: Lone Tree Way & Vista Grande Drive






















Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 1770 | 1863 | 1583 | 1770 | 1637 | 1637 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.53 | 1.00 | 1.00 | 0.72 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 985 | 1863 | 1583 | 1349 | 1637 | 1637 |
| Volume (vph) | 190 | 1649 | 390 | 300 | 1204 | 90 | 320 | 50 | 220 | 70 | 40 | 170 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 190 | 1649 | 390 | 300 | 1204 | 90 | 320 | 50 | 220 | 70 | 40 | 170 |
| RTOR Reduction (vph) | 0 | 0 | 186 | 0 | 0 | 53 | 0 | 0 | 147 | 0 | 113 | 0 |
| Lane Group Flow (vph) | 190 | 1649 | 204 | 300 | 1204 | 37 | 320 | 50 | 73 | 70 | 97 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 16.1 | 41.5 | 41.5 | 19.9 | 45.3 | 45.3 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 |
| Effective Green, g (s) | 16.1 | 41.5 | 41.5 | 19.9 | 45.3 | 45.3 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 |
| Actuated g/C Ratio | 0.15 | 0.38 | 0.38 | 0.18 | 0.41 | 0.41 | 0.33 | 0.33 | 0.33 | 0.33 | 0.33 | 0.33 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 259 | 1918 | 597 | 320 | 2094 | 652 | 328 | 620 | 527 | 449 | 545 | 545 |
| v/s Ratio Prot | 0.11 | c0.32 | | c0.17 | c0.24 | | | 0.03 | | | 0.06 | |
| v/s Ratio Perm | | | 0.13 | | | 0.02 | c0.32 | | 0.05 | 0.05 | | |
| v/c Ratio | 0.73 | 0.86 | 0.34 | 0.94 | 0.57 | 0.06 | 0.98 | 0.08 | 0.14 | 0.16 | 0.18 | 0.18 |
| Uniform Delay, d1 | 44.9 | 31.6 | 24.5 | 44.4 | 24.9 | 19.5 | 36.3 | 25.2 | 25.7 | 25.8 | 26.0 | 26.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 10.3 | 5.3 | 1.6 | 33.9 | 1.2 | 0.2 | 42.7 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 |
| Delay (s) | 55.2 | 36.9 | 26.0 | 78.4 | 26.1 | 19.7 | 79.0 | 25.2 | 25.8 | 26.0 | 26.2 | 26.2 |
| Level of Service | E | D | C | E | C | B | E | C | C | C | C | C |
| Approach Delay (s) | | 36.5 | | | 35.6 | | | 54.6 | | | 26.1 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 37.9 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.94 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 92.1% | | | ICU Level of Service | | | | F | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

16: Country Hills Drive & Hillcrest Avenue























Antioch Davidon Homes TIA
2025 No Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1683 | | 1770 | 3506 | | 1770 | 3497 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1683 | | 1770 | 3506 | | 1770 | 3497 | |
| Volume (vph) | 70 | 20 | 100 | 120 | 50 | 90 | 100 | 1053 | 70 | 110 | 916 | 80 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 70 | 20 | 100 | 120 | 50 | 90 | 100 | 1053 | 70 | 110 | 916 | 80 |
| RTOR Reduction (vph) | 0 | 0 | 90 | 0 | 78 | 0 | 0 | 4 | 0 | 0 | 6 | 0 |
| Lane Group Flow (vph) | 70 | 20 | 10 | 120 | 62 | 0 | 100 | 1119 | 0 | 110 | 990 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | | | | |
| Actuated Green, G (s) | 6.1 | 8.4 | 8.4 | 8.7 | 11.0 | | 8.4 | 42.2 | | 7.9 | 41.7 | |
| Effective Green, g (s) | 6.1 | 8.4 | 8.4 | 8.7 | 11.0 | | 8.4 | 42.2 | | 7.9 | 41.7 | |
| Actuated g/C Ratio | 0.07 | 0.10 | 0.10 | 0.10 | 0.13 | | 0.10 | 0.51 | | 0.09 | 0.50 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 130 | 188 | 160 | 185 | 223 | | 179 | 1778 | | 168 | 1753 | |
| v/s Ratio Prot | 0.04 | 0.01 | | c0.07 | c0.04 | | 0.06 | c0.32 | | c0.06 | 0.28 | |
| v/s Ratio Perm | | | 0.01 | | | | | | | | | |
| v/c Ratio | 0.54 | 0.11 | 0.06 | 0.65 | 0.28 | | 0.56 | 0.63 | | 0.65 | 0.56 | |
| Uniform Delay, d1 | 37.2 | 34.0 | 33.8 | 35.8 | 32.5 | | 35.6 | 14.8 | | 36.3 | 14.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 4.2 | 0.3 | 0.2 | 7.6 | 0.7 | | 3.7 | 1.7 | | 8.8 | 1.3 | |
| Delay (s) | 41.4 | 34.2 | 34.0 | 43.4 | 33.2 | | 39.4 | 16.5 | | 45.2 | 15.8 | |
| Level of Service | D | C | C | D | C | | D | B | | D | B | |
| Approach Delay (s) | | 36.8 | | | 37.9 | | | 18.4 | | | 18.7 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 83.2 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 62.8% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

18: Laurel Road & Hillcrest Avenue

Antioch Davidon Homes TIA
2025 No Project PM Peak Hour







| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.91 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1701 | | 1770 | 1863 | 1583 | 1770 | 3419 | | 1770 | 3436 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1701 | | 1770 | 1863 | 1583 | 1770 | 3419 | | 1770 | 3436 | |
| Volume (vph) | 140 | 80 | 110 | 346 | 120 | 240 | 90 | 970 | 283 | 273 | 910 | 220 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 140 | 80 | 110 | 346 | 120 | 240 | 90 | 970 | 283 | 273 | 910 | 220 |
| RTOR Reduction (vph) | 0 | 46 | 0 | 0 | 0 | 194 | 0 | 20 | 0 | 0 | 15 | 0 |
| Lane Group Flow (vph) | 140 | 145 | 0 | 346 | 120 | 46 | 90 | 1233 | 0 | 273 | 1115 | 0 |
| Turn Type | Prot | | | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 8 | | | | | | | | | | | |
| Actuated Green, G (s) | 14.0 | 15.0 | | 22.0 | 23.0 | 23.0 | 8.7 | 50.0 | | 17.0 | 58.3 | |
| Effective Green, g (s) | 14.0 | 15.0 | | 22.0 | 23.0 | 23.0 | 8.7 | 50.0 | | 17.0 | 58.3 | |
| Actuated g/C Ratio | 0.12 | 0.12 | | 0.18 | 0.19 | 0.19 | 0.07 | 0.42 | | 0.14 | 0.49 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 207 | 213 | | 325 | 357 | 303 | 128 | 1425 | | 251 | 1669 | |
| v/s Ratio Prot | 0.08 | c0.08 | | c0.20 | 0.06 | | 0.05 | c0.36 | | c0.15 | 0.32 | |
| v/s Ratio Perm | 0.03 | | | | | | | | | | | |
| v/c Ratio | 0.68 | 0.68 | | 1.06 | 0.34 | 0.15 | 0.70 | 0.87 | | 1.09 | 0.67 | |
| Uniform Delay, d1 | 50.8 | 50.2 | | 49.0 | 41.9 | 40.4 | 54.4 | 31.9 | | 51.5 | 23.5 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 8.4 | 8.3 | | 68.1 | 0.6 | 0.2 | 16.1 | 7.3 | | 82.2 | 2.1 | |
| Delay (s) | 59.3 | 58.5 | | 117.1 | 42.5 | 40.6 | 70.4 | 39.2 | | 133.7 | 25.6 | |
| Level of Service | E | E | | F | D | D | E | D | | F | C | |
| Approach Delay (s) | 58.8 | | | 78.4 | | | 41.3 | | | 46.6 | | |
| Approach LOS | E | | | E | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 51.7 | HCM Level of Service | | | D | | | | | |
| HCM Volume to Capacity ratio | | | 0.92 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sum of lost time (s) | | | 16.0 | | | | | |
| Intersection Capacity Utilization | | | 94.4% | ICU Level of Service | | | F | | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Cumulative With Project

HCM Signalized Intersection Capacity Analysis

1: Laurel Road & Canada Valley





















Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | | ↖ | ↑↑ | ↖ | ↖ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | 0.99 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3489 | | 1770 | 3539 | 1770 | 1583 |
| Flt Permitted | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3489 | | 1770 | 3539 | 1770 | 1583 |
| Volume (vph) | 960 | 100 | 260 | 670 | 120 | 290 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 960 | 100 | 260 | 670 | 120 | 290 |
| RTOR Reduction (vph) | 8 | 0 | 0 | 0 | 0 | 226 |
| Lane Group Flow (vph) | 1052 | 0 | 260 | 670 | 120 | 64 |
| Turn Type | | | Prot | | | Perm |
| Protected Phases | 4 | | 3 | 8 | 2 | |
| Permitted Phases | | | | | | 2 |
| Actuated Green, G (s) | 40.4 | | 17.6 | 62.0 | 20.0 | 20.0 |
| Effective Green, g (s) | 40.4 | | 17.6 | 62.0 | 20.0 | 20.0 |
| Actuated g/C Ratio | 0.45 | | 0.20 | 0.69 | 0.22 | 0.22 |
| Clearance Time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 1566 | | 346 | 2438 | 393 | 352 |
| v/s Ratio Prot | c0.30 | | c0.15 | 0.19 | c0.07 | |
| v/s Ratio Perm | | | | | | 0.04 |
| v/c Ratio | 0.67 | | 0.75 | 0.27 | 0.31 | 0.18 |
| Uniform Delay, d1 | 19.6 | | 34.1 | 5.4 | 29.2 | 28.4 |
| Progression Factor | 1.00 | | 1.01 | 0.42 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.3 | | 8.4 | 0.3 | 2.0 | 1.1 |
| Delay (s) | 21.9 | | 42.9 | 2.5 | 31.2 | 29.5 |
| Level of Service | C | | D | A | C | C |
| Approach Delay (s) | 21.9 | | | 13.8 | 30.0 | |
| Approach LOS | C | | | B | C | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 20.1 | | HCM Level of Service | C |
| HCM Volume to Capacity ratio | | | 0.60 | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 60.8% | | ICU Level of Service | B |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Laurel Road & Country Hills Drive


Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.95 | | 1.00 | 0.99 | | 1.00 | 0.86 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3350 | | 1770 | 3516 | | 1770 | 1599 | | 1770 | 1676 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3350 | | 1770 | 3516 | | 1770 | 1599 | | 1770 | 1676 | |
| Volume (vph) | 40 | 760 | 420 | 100 | 660 | 30 | 160 | 20 | 330 | 80 | 30 | 60 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 40 | 760 | 420 | 100 | 660 | 30 | 160 | 20 | 330 | 80 | 30 | 60 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 50 | 0 |
| Lane Group Flow (vph) | 40 | 1180 | 0 | 100 | 687 | 0 | 160 | 350 | 0 | 80 | 40 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 3.6 | 39.8 | | 7.2 | 43.4 | | 12.2 | 22.2 | | 4.8 | 14.8 | |
| Effective Green, g (s) | 3.6 | 39.8 | | 7.2 | 43.4 | | 12.2 | 22.2 | | 4.8 | 14.8 | |
| Actuated g/C Ratio | 0.04 | 0.44 | | 0.08 | 0.48 | | 0.14 | 0.25 | | 0.05 | 0.16 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 71 | 1481 | | 142 | 1695 | | 240 | 394 | | 94 | 276 | |
| v/s Ratio Prot | 0.02 | c0.35 | | c0.06 | 0.20 | | c0.09 | c0.22 | | 0.05 | 0.02 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.56 | 0.80 | | 0.70 | 0.41 | | 0.67 | 0.89 | | 0.85 | 0.14 | |
| Uniform Delay, d1 | 42.4 | 21.6 | | 40.4 | 15.0 | | 37.0 | 32.7 | | 42.2 | 32.2 | |
| Progression Factor | 0.93 | 1.68 | | 0.91 | 0.92 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 8.0 | 3.7 | | 14.1 | 0.7 | | 6.8 | 20.8 | | 48.3 | 0.2 | |
| Delay (s) | 47.5 | 40.1 | | 51.0 | 14.5 | | 43.8 | 53.5 | | 90.6 | 32.4 | |
| Level of Service | D | D | | D | B | | D | D | | F | C | |
| Approach Delay (s) | 40.3 | | | 19.1 | | | 50.4 | | | 59.8 | | |
| Approach LOS | D | | | B | | | D | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 37.2 | | HCM Level of Service | | | D | | | | |
| HCM Volume to Capacity ratio | | | 0.82 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | | | 16.0 | | | | |
| Intersection Capacity Utilization | | | 79.2% | | ICU Level of Service | | | D | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Laurel Road & SB SR4 Bypass





















Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  | | | | | | | | | | | |
|-----------------------------------|--|-------|------|------|----------------------|------|------|------|------|-------|--------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑ | | | ↑↑ | | | | | ↘ | ↗ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 0.99 | | | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 3498 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 3498 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 1080 | 90 | 0 | 450 | 0 | 0 | 0 | 0 | 840 | 0 | 340 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1080 | 90 | 0 | 450 | 0 | 0 | 0 | 0 | 840 | 0 | 340 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1170 | 0 | 0 | 450 | 0 | 0 | 0 | 0 | 420 | 420 | 340 |
| Turn Type | | | | | | | | | | Perm | custom | |
| Protected Phases | | 2 | | | 6 | | | | | | 4 | 4 |
| Permitted Phases | | | | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 53.4 | | | 53.4 | | | | | 28.6 | 28.6 | 28.6 |
| Effective Green, g (s) | | 53.4 | | | 53.4 | | | | | 28.6 | 28.6 | 28.6 |
| Actuated g/C Ratio | | 0.59 | | | 0.59 | | | | | 0.32 | 0.32 | 0.32 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2075 | | | 2100 | | | | | 534 | 534 | 503 |
| v/s Ratio Prot | | c0.33 | | | 0.13 | | | | | | | 0.21 |
| v/s Ratio Perm | | | | | | | | | | c0.25 | 0.25 | |
| v/c Ratio | | 0.56 | | | 0.21 | | | | | 0.79 | 0.79 | 0.68 |
| Uniform Delay, d1 | | 11.2 | | | 8.5 | | | | | 27.9 | 27.9 | 26.7 |
| Progression Factor | | 0.42 | | | 0.07 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.7 | | | 0.2 | | | | | 7.5 | 7.5 | 3.6 |
| Delay (s) | | 5.4 | | | 0.8 | | | | | 35.4 | 35.4 | 30.3 |
| Level of Service | | A | | | A | | | | | D | D | C |
| Approach Delay (s) | | 5.4 | | | 0.8 | | | 0.0 | | | 33.9 | |
| Approach LOS | | A | | | A | | | A | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 16.7 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.64 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 90.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 83.2% | | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Laurel Road & SR4 Bypass NB Ramps






















Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|--|---|---|--|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |   | | |   |  | |  |  | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | 1.00 | | 1.00 | 1.00 | | | |
| Frt | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Volume (vph) | 260 | 1660 | 0 | 0 | 580 | 620 | 20 | 0 | 100 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 260 | 1660 | 0 | 0 | 580 | 620 | 20 | 0 | 100 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 260 | 1660 | 0 | 0 | 580 | 620 | 0 | 20 | 100 | 0 | 0 | 0 |
| Turn Type | Prot | | | | | Perm | Perm | | custom | | | |
| Protected Phases | 5 | 2 | | | 6 | | | 8 | 8 | | | |
| Permitted Phases | | | | | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | 18.0 | 71.2 | | | 49.2 | 49.2 | | 10.8 | 10.8 | | | |
| Effective Green, g (s) | 18.0 | 71.2 | | | 49.2 | 49.2 | | 10.8 | 10.8 | | | |
| Actuated g/C Ratio | 0.20 | 0.79 | | | 0.55 | 0.55 | | 0.12 | 0.12 | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | 354 | 2800 | | | 1935 | 865 | | 212 | 190 | | | |
| v/s Ratio Prot | c0.15 | 0.47 | | | 0.16 | | | | c0.06 | | | |
| v/s Ratio Perm | | | | | | c0.39 | | 0.01 | | | | |
| v/c Ratio | 0.73 | 0.59 | | | 0.30 | 0.72 | | 0.09 | 0.53 | | | |
| Uniform Delay, d1 | 33.8 | 3.7 | | | 11.1 | 15.2 | | 35.2 | 37.2 | | | |
| Progression Factor | 1.03 | 0.96 | | | 0.07 | 0.22 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 6.4 | 0.8 | | | 0.3 | 4.1 | | 0.2 | 2.6 | | | |
| Delay (s) | 41.2 | 4.3 | | | 1.1 | 7.4 | | 35.4 | 39.8 | | | |
| Level of Service | D | A | | | A | A | | D | D | | | |
| Approach Delay (s) | | 9.3 | | | 4.3 | | | 39.1 | | | 0.0 | |
| Approach LOS | | A | | | A | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 8.6 | | | HCM Level of Service | | | A | | | | |
| HCM Volume to Capacity ratio | | 0.69 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 90.0 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 66.1% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Laurel Road & Slatten Ranch Road

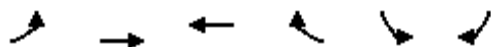
Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.94 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 4899 | | 3433 | 3332 | | 1770 | 3443 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 4899 | | 3433 | 3332 | | 1770 | 3443 | |
| Volume (vph) | 160 | 970 | 630 | 260 | 990 | 320 | 170 | 250 | 160 | 130 | 180 | 40 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 160 | 970 | 630 | 260 | 990 | 320 | 170 | 250 | 160 | 130 | 180 | 40 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 160 | 970 | 630 | 260 | 1310 | 0 | 170 | 410 | 0 | 130 | 220 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | |
| Actuated Green, G (s) | 15.0 | 37.5 | 37.5 | 14.7 | 37.2 | | 11.0 | 14.8 | | 7.0 | 10.8 | |
| Effective Green, g (s) | 15.0 | 37.5 | 37.5 | 14.7 | 37.2 | | 11.0 | 14.8 | | 7.0 | 10.8 | |
| Actuated g/C Ratio | 0.17 | 0.42 | 0.42 | 0.16 | 0.41 | | 0.12 | 0.16 | | 0.08 | 0.12 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 295 | 2119 | 660 | 289 | 2025 | | 420 | 548 | | 138 | 413 | |
| v/s Ratio Prot | 0.09 | 0.19 | | c0.15 | 0.27 | | 0.05 | c0.12 | | c0.07 | 0.06 | |
| v/s Ratio Perm | | | c0.40 | | | | | | | | | |
| v/c Ratio | 0.54 | 0.46 | 0.95 | 0.90 | 0.65 | | 0.40 | 0.75 | | 0.94 | 0.53 | |
| Uniform Delay, d1 | 34.4 | 18.9 | 25.4 | 36.9 | 21.1 | | 36.5 | 35.8 | | 41.3 | 37.2 | |
| Progression Factor | 0.84 | 0.74 | 0.75 | 0.70 | 0.57 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.7 | 0.6 | 22.4 | 25.1 | 1.4 | | 0.6 | 5.5 | | 58.8 | 1.3 | |
| Delay (s) | 30.4 | 14.6 | 41.4 | 51.1 | 13.4 | | 37.1 | 41.4 | | 100.1 | 38.6 | |
| Level of Service | C | B | D | D | B | | D | D | | F | D | |
| Approach Delay (s) | | 25.6 | | | 19.6 | | | 40.1 | | | 61.4 | |
| Approach LOS | | C | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 28.3 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.90 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 69.7% | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Laurel Road & Live Oak Avenue

Antioch Davidon Homes TIA
2025 With Project AM Peak Hour


























| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|-------|------|-------|------|----------------------|-------|
| Lane Configurations | ↖↗ | ↑↑↑ | ↑↑↑↗ | | ↖ | ↗ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.91 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.99 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 5034 | | 1770 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 5034 | | 1770 | 1583 |
| Volume (vph) | 290 | 970 | 1260 | 90 | 60 | 310 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 290 | 970 | 1260 | 90 | 60 | 310 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 0 | 219 |
| Lane Group Flow (vph) | 290 | 970 | 1342 | 0 | 60 | 91 |
| Turn Type | Prot | | | Perm | | |
| Protected Phases | 7 | 4 | 8 | | 6 | |
| Permitted Phases | | | | | | 6 |
| Actuated Green, G (s) | 12.6 | 55.6 | 39.0 | | 26.4 | 26.4 |
| Effective Green, g (s) | 12.6 | 55.6 | 39.0 | | 26.4 | 26.4 |
| Actuated g/C Ratio | 0.14 | 0.62 | 0.43 | | 0.29 | 0.29 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 481 | 3141 | 2181 | | 519 | 464 |
| v/s Ratio Prot | c0.08 | 0.19 | c0.27 | | 0.03 | |
| v/s Ratio Perm | | | | | | c0.06 |
| v/c Ratio | 0.60 | 0.31 | 0.62 | | 0.12 | 0.20 |
| Uniform Delay, d1 | 36.4 | 8.1 | 19.7 | | 23.3 | 23.8 |
| Progression Factor | 0.91 | 1.48 | 0.61 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.8 | 0.0 | 0.4 | | 0.5 | 0.9 |
| Delay (s) | 34.7 | 12.1 | 12.5 | | 23.7 | 24.8 |
| Level of Service | C | B | B | | C | C |
| Approach Delay (s) | | 17.3 | 12.5 | | 24.6 | |
| Approach LOS | | B | B | | C | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 16.0 | | HCM Level of Service | B |
| HCM Volume to Capacity ratio | | | 0.47 | | | |
| Actuated Cycle Length (s) | | | 90.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 52.2% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Laurel Road & Empire Avenue

























Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3516 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3516 | | 1770 | 3539 | 1583 |
| Volume (vph) | 300 | 680 | 50 | 70 | 860 | 140 | 140 | 220 | 10 | 40 | 310 | 350 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 300 | 680 | 50 | 70 | 860 | 140 | 140 | 220 | 10 | 40 | 310 | 350 |
| RTOR Reduction (vph) | 0 | 0 | 28 | 0 | 0 | 85 | 0 | 4 | 0 | 0 | 0 | 236 |
| Lane Group Flow (vph) | 300 | 680 | 22 | 70 | 860 | 55 | 140 | 226 | 0 | 40 | 310 | 114 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 8 | | | | | | 6 |
| Actuated Green, G (s) | 12.3 | 40.4 | 40.4 | 7.1 | 35.2 | 35.2 | 11.2 | 22.9 | | 3.6 | 15.3 | 15.3 |
| Effective Green, g (s) | 12.3 | 40.4 | 40.4 | 7.1 | 35.2 | 35.2 | 11.2 | 22.9 | | 3.6 | 15.3 | 15.3 |
| Actuated g/C Ratio | 0.14 | 0.45 | 0.45 | 0.08 | 0.39 | 0.39 | 0.12 | 0.25 | | 0.04 | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 469 | 1589 | 711 | 140 | 1384 | 619 | 220 | 895 | | 71 | 602 | 269 |
| v/s Ratio Prot | c0.09 | 0.19 | | 0.04 | c0.24 | | c0.08 | 0.06 | | 0.02 | c0.09 | |
| v/s Ratio Perm | | | 0.01 | | | 0.03 | | | | | | 0.07 |
| v/c Ratio | 0.64 | 0.43 | 0.03 | 0.50 | 0.62 | 0.09 | 0.64 | 0.25 | | 0.56 | 0.51 | 0.42 |
| Uniform Delay, d1 | 36.8 | 16.9 | 13.9 | 39.7 | 22.0 | 17.3 | 37.5 | 26.7 | | 42.4 | 34.0 | 33.4 |
| Progression Factor | 1.18 | 0.74 | 1.71 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.8 | 0.8 | 0.1 | 2.8 | 2.1 | 0.3 | 5.9 | 0.1 | | 9.8 | 0.7 | 1.1 |
| Delay (s) | 46.1 | 13.3 | 23.7 | 42.5 | 24.1 | 17.6 | 43.4 | 26.9 | | 52.3 | 34.7 | 34.5 |
| Level of Service | D | B | C | D | C | B | D | C | | D | C | C |
| Approach Delay (s) | | 23.4 | | | 24.5 | | | 33.1 | | | 35.6 | |
| Approach LOS | | C | | | C | | | C | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 27.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.60 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 90.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 63.2% | | | ICU Level of Service | | | B | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Lone Tree Way & Canada Valley













Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | 0.91 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.87 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 1770 | 2938 | 1441 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 1770 | 2938 | 1441 | 1770 | 1863 | 1583 |
| Volume (vph) | 60 | 950 | 20 | 260 | 1460 | 260 | 50 | 10 | 160 | 360 | 10 | 80 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 60 | 950 | 20 | 260 | 1460 | 260 | 50 | 10 | 160 | 360 | 10 | 80 |
| RTOR Reduction (vph) | 0 | 0 | 12 | 0 | 0 | 125 | 0 | 74 | 74 | 0 | 0 | 60 |
| Lane Group Flow (vph) | 60 | 950 | 8 | 260 | 1460 | 135 | 50 | 16 | 6 | 360 | 10 | 20 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 3.2 | 46.5 | 46.5 | 14.0 | 57.3 | 57.3 | 6.2 | 7.8 | 7.8 | 25.7 | 27.3 | 27.3 |
| Effective Green, g (s) | 3.2 | 46.5 | 46.5 | 14.0 | 57.3 | 57.3 | 6.2 | 7.8 | 7.8 | 25.7 | 27.3 | 27.3 |
| Actuated g/C Ratio | 0.03 | 0.42 | 0.42 | 0.13 | 0.52 | 0.52 | 0.06 | 0.07 | 0.07 | 0.23 | 0.25 | 0.25 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 100 | 2150 | 669 | 437 | 2649 | 825 | 100 | 208 | 102 | 414 | 462 | 393 |
| v/s Ratio Prot | 0.02 | c0.19 | | 0.08 | c0.29 | | 0.03 | c0.01 | | c0.20 | 0.01 | |
| v/s Ratio Perm | | | 0.01 | | | 0.09 | | | 0.00 | | | 0.01 |
| v/c Ratio | 0.60 | 0.44 | 0.01 | 0.59 | 0.55 | 0.16 | 0.50 | 0.08 | 0.06 | 0.87 | 0.02 | 0.05 |
| Uniform Delay, d1 | 52.8 | 22.5 | 18.4 | 45.3 | 17.7 | 13.8 | 50.4 | 47.7 | 47.7 | 40.5 | 31.3 | 31.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.64 | 0.87 | 1.14 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 9.7 | 0.7 | 0.0 | 1.9 | 0.7 | 0.4 | 3.9 | 0.2 | 0.2 | 17.4 | 0.0 | 0.1 |
| Delay (s) | 62.5 | 23.2 | 18.5 | 31.0 | 16.1 | 16.2 | 54.3 | 47.9 | 47.9 | 57.9 | 31.3 | 31.5 |
| Level of Service | E | C | B | C | B | B | D | D | D | E | C | C |
| Approach Delay (s) | | 25.4 | | | 18.1 | | | 49.3 | | | 52.6 | |
| Approach LOS | | C | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.2 | | | | HCM Level of Service | | | C | | |
| HCM Volume to Capacity ratio | | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 68.2% | | | | ICU Level of Service | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Lone Tree Way & SB SR4 Bypass













Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 1170 | 300 | 160 | 1780 | 0 | 0 | 0 | 0 | 740 | 0 | 200 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1170 | 300 | 160 | 1780 | 0 | 0 | 0 | 0 | 740 | 0 | 200 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1170 | 300 | 160 | 1780 | 0 | 0 | 0 | 0 | 370 | 370 | 200 |
| Turn Type | | Perm | | Prot | | | | | | Split | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | 4 | | 4 |
| Permitted Phases | | 2 | | | | | | | | | | 4 |
| Actuated Green, G (s) | | 52.5 | 52.5 | 16.0 | 72.5 | | | | | 29.5 | 29.5 | 29.5 |
| Effective Green, g (s) | | 52.5 | 52.5 | 16.0 | 72.5 | | | | | 29.5 | 29.5 | 29.5 |
| Actuated g/C Ratio | | 0.48 | 0.48 | 0.15 | 0.66 | | | | | 0.27 | 0.27 | 0.27 |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2427 | 756 | 499 | 3351 | | | | | 451 | 451 | 425 |
| v/s Ratio Prot | | 0.23 | | 0.05 | c0.35 | | | | | c0.22 | 0.22 | |
| v/s Ratio Perm | | | 0.19 | | | | | | | | | 0.13 |
| v/c Ratio | | 0.48 | 0.40 | 0.32 | 0.53 | | | | | 0.82 | 0.82 | 0.47 |
| Uniform Delay, d1 | | 19.5 | 18.5 | 42.1 | 9.8 | | | | | 37.8 | 37.8 | 33.7 |
| Progression Factor | | 1.05 | 1.01 | 1.11 | 0.95 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.6 | 1.4 | 0.3 | 0.6 | | | | | 11.4 | 11.4 | 0.8 |
| Delay (s) | | 21.1 | 20.1 | 46.9 | 9.9 | | | | | 49.1 | 49.1 | 34.5 |
| Level of Service | | C | C | D | A | | | | | D | D | C |
| Approach Delay (s) | | 20.9 | | | 13.0 | | | 0.0 | | | 46.0 | |
| Approach LOS | | C | | | B | | | A | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 22.8 | | HCM Level of Service | | C | | | | | | |
| HCM Volume to Capacity ratio | | 0.61 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | Sum of lost time (s) | | 8.0 | | | | | | |
| Intersection Capacity Utilization | | 61.6% | | ICU Level of Service | | B | | | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Lone Tree Way & SR4 Bypass NB Ramps























Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Volume (vph) | 0 | 1610 | 300 | 70 | 1660 | 720 | 280 | 10 | 250 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 1610 | 300 | 70 | 1660 | 720 | 280 | 10 | 250 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1610 | 300 | 70 | 1660 | 720 | 280 | 10 | 250 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Perm | | Perm | | | |
| Protected Phases | | 2 | | 1 | | 6 | | | 8 | | | |
| Permitted Phases | | | | 2 | | | 6 | 8 | | 8 | | |
| Actuated Green, G (s) | | 70.4 | 70.4 | 5.6 | 80.0 | 80.0 | 22.0 | 22.0 | 22.0 | | | |
| Effective Green, g (s) | | 70.4 | 70.4 | 5.6 | 80.0 | 80.0 | 22.0 | 22.0 | 22.0 | | | |
| Actuated g/C Ratio | | 0.64 | 0.64 | 0.05 | 0.73 | 0.73 | 0.20 | 0.20 | 0.20 | | | |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 3254 | 1013 | 175 | 3698 | 1151 | 687 | 373 | 317 | | | |
| v/s Ratio Prot | | 0.32 | | 0.02 | 0.33 | | | 0.01 | | | | |
| v/s Ratio Perm | | | 0.19 | | | c0.45 | 0.08 | | c0.16 | | | |
| v/c Ratio | | 0.49 | 0.30 | 0.40 | 0.45 | 0.63 | 0.41 | 0.03 | 0.79 | | | |
| Uniform Delay, d1 | | 10.4 | 8.8 | 50.6 | 6.1 | 7.5 | 38.3 | 35.4 | 41.8 | | | |
| Progression Factor | | 0.22 | 0.25 | 1.04 | 0.68 | 0.98 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.5 | 0.6 | 0.9 | 0.2 | 1.5 | 0.4 | 0.0 | 12.2 | | | |
| Delay (s) | | 2.7 | 2.8 | 53.7 | 4.3 | 8.8 | 38.7 | 35.4 | 54.0 | | | |
| Level of Service | | A | A | D | A | A | D | D | D | | | |
| Approach Delay (s) | | 2.8 | | | 7.1 | | | 45.7 | | | 0.0 | |
| Approach LOS | | A | | | A | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 9.6 | | HCM Level of Service | | | | | A | | | |
| HCM Volume to Capacity ratio | | 0.66 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | Sum of lost time (s) | | | | | 8.0 | | | |
| Intersection Capacity Utilization | | 54.6% | | ICU Level of Service | | | | | A | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Slatten Ranch Road

























Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 0.97 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 1770 | 5063 | | 3433 | 3509 | | 3433 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 1770 | 5063 | | 3433 | 3509 | | 3433 | 3539 | 1583 |
| Volume (vph) | 460 | 1140 | 240 | 70 | 1700 | 50 | 500 | 500 | 30 | 10 | 150 | 280 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 460 | 1140 | 240 | 70 | 1700 | 50 | 500 | 500 | 30 | 10 | 150 | 280 |
| RTOR Reduction (vph) | 0 | 0 | 79 | 0 | 2 | 0 | 0 | 4 | 0 | 0 | 0 | 167 |
| Lane Group Flow (vph) | 460 | 1140 | 161 | 70 | 1748 | 0 | 500 | 526 | 0 | 10 | 150 | 113 |
| Turn Type | Prot | pm+ov | | Prot | | | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | 3 | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | 4 |
| Actuated Green, G (s) | 16.8 | 55.0 | 74.0 | 4.8 | 43.0 | | 19.0 | 33.4 | | 0.8 | 15.2 | 15.2 |
| Effective Green, g (s) | 16.8 | 55.0 | 74.0 | 4.8 | 43.0 | | 19.0 | 33.4 | | 0.8 | 15.2 | 15.2 |
| Actuated g/C Ratio | 0.15 | 0.50 | 0.67 | 0.04 | 0.39 | | 0.17 | 0.30 | | 0.01 | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 524 | 2543 | 1065 | 77 | 1979 | | 593 | 1065 | | 25 | 489 | 219 |
| v/s Ratio Prot | c0.13 | 0.22 | 0.03 | 0.04 | c0.35 | | c0.15 | c0.15 | | 0.00 | 0.04 | |
| v/s Ratio Perm | | | 0.08 | | | | | | | | | 0.07 |
| v/c Ratio | 0.88 | 0.45 | 0.15 | 0.91 | 0.88 | | 0.84 | 0.49 | | 0.40 | 0.31 | 0.52 |
| Uniform Delay, d1 | 45.6 | 17.7 | 6.6 | 52.4 | 31.2 | | 44.1 | 31.4 | | 54.4 | 42.7 | 44.0 |
| Progression Factor | 1.26 | 1.43 | 3.65 | 1.22 | 1.46 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 13.7 | 0.5 | 0.1 | 62.1 | 5.0 | | 10.6 | 0.4 | | 10.2 | 0.4 | 2.0 |
| Delay (s) | 71.3 | 25.9 | 24.0 | 125.9 | 50.5 | | 54.6 | 31.7 | | 64.5 | 43.0 | 46.0 |
| Level of Service | E | C | C | F | D | | D | C | | E | D | D |
| Approach Delay (s) | | 37.0 | | | 53.4 | | | 42.8 | | | 45.4 | |
| Approach LOS | | D | | | D | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 44.7 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.79 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 78.8% | | | ICU Level of Service | | | | D | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue





















Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3260 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3260 | |
| Volume (vph) | 220 | 710 | 260 | 30 | 1210 | 340 | 510 | 200 | 20 | 90 | 90 | 100 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 710 | 260 | 30 | 1210 | 340 | 510 | 200 | 20 | 90 | 90 | 100 |
| RTOR Reduction (vph) | 0 | 0 | 121 | 0 | 0 | 158 | 0 | 0 | 16 | 0 | 92 | 0 |
| Lane Group Flow (vph) | 220 | 710 | 139 | 30 | 1210 | 182 | 510 | 200 | 4 | 90 | 98 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 22.5 | 59.0 | 59.0 | 4.3 | 40.8 | 40.8 | 22.2 | 19.4 | 19.4 | 11.3 | 8.5 | |
| Effective Green, g (s) | 22.5 | 59.0 | 59.0 | 4.3 | 40.8 | 40.8 | 22.2 | 19.4 | 19.4 | 11.3 | 8.5 | |
| Actuated g/C Ratio | 0.20 | 0.54 | 0.54 | 0.04 | 0.37 | 0.37 | 0.20 | 0.18 | 0.18 | 0.10 | 0.08 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 362 | 2727 | 849 | 69 | 1886 | 587 | 693 | 329 | 279 | 353 | 252 | |
| v/s Ratio Prot | c0.12 | 0.14 | | 0.02 | c0.24 | | c0.15 | c0.11 | | 0.03 | 0.03 | |
| v/s Ratio Perm | | | 0.09 | | | 0.12 | | | 0.00 | | | |
| v/c Ratio | 0.61 | 0.26 | 0.16 | 0.43 | 0.64 | 0.31 | 0.74 | 0.61 | 0.01 | 0.25 | 0.39 | |
| Uniform Delay, d1 | 39.7 | 13.7 | 13.0 | 51.7 | 28.6 | 24.6 | 41.2 | 41.8 | 37.4 | 45.5 | 48.3 | |
| Progression Factor | 1.36 | 1.52 | 6.92 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.7 | 0.2 | 0.4 | 4.3 | 1.7 | 1.4 | 4.1 | 3.2 | 0.0 | 0.4 | 1.0 | |
| Delay (s) | 56.9 | 21.1 | 90.1 | 56.0 | 30.3 | 26.0 | 45.2 | 45.0 | 37.4 | 45.9 | 49.3 | |
| Level of Service | E | C | F | E | C | C | D | D | D | D | D | |
| Approach Delay (s) | | 42.8 | | | 29.8 | | | 44.9 | | | 48.2 | |
| Approach LOS | | D | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 38.2 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.66 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 69.2% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

13: Lone Tree Way & Deer Valley Rd























Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.97 | | 1.00 | 0.97 | | 1.00 | 0.96 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 4947 | | 1770 | 4927 | | 3433 | 3381 | | 1770 | 3429 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 4947 | | 1770 | 4927 | | 3433 | 3381 | | 1770 | 3429 | |
| Volume (vph) | 110 | 720 | 160 | 200 | 1380 | 360 | 450 | 520 | 220 | 340 | 380 | 100 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 110 | 720 | 160 | 200 | 1380 | 360 | 450 | 520 | 220 | 340 | 380 | 100 |
| RTOR Reduction (vph) | 0 | 32 | 0 | 0 | 42 | 0 | 0 | 43 | 0 | 0 | 21 | 0 |
| Lane Group Flow (vph) | 110 | 848 | 0 | 200 | 1698 | 0 | 450 | 697 | 0 | 340 | 459 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 7.0 | 33.4 | | 15.1 | 41.5 | | 18.5 | 23.0 | | 22.5 | 27.0 | |
| Effective Green, g (s) | 7.0 | 33.4 | | 15.1 | 41.5 | | 18.5 | 23.0 | | 22.5 | 27.0 | |
| Actuated g/C Ratio | 0.06 | 0.30 | | 0.14 | 0.38 | | 0.17 | 0.21 | | 0.20 | 0.25 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 113 | 1502 | | 243 | 1859 | | 577 | 707 | | 362 | 842 | |
| v/s Ratio Prot | 0.06 | 0.17 | | c0.11 | c0.34 | | 0.13 | c0.21 | | c0.19 | c0.13 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.97 | 0.56 | | 0.82 | 0.91 | | 0.78 | 0.99 | | 0.94 | 0.54 | |
| Uniform Delay, d1 | 51.4 | 32.2 | | 46.2 | 32.5 | | 43.8 | 43.3 | | 43.1 | 36.1 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 75.7 | 1.5 | | 19.7 | 8.4 | | 6.6 | 30.1 | | 31.6 | 0.7 | |
| Delay (s) | 127.2 | 33.7 | | 65.8 | 40.9 | | 50.4 | 73.5 | | 74.7 | 36.9 | |
| Level of Service | F | C | | E | D | | D | E | | E | D | |
| Approach Delay (s) | | 44.1 | | | 43.5 | | | 64.8 | | | 52.6 | |
| Approach LOS | | D | | | D | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 50.2 | | | | | HCM Level of Service | | D | | | |
| HCM Volume to Capacity ratio | | 0.93 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | | | | Sum of lost time (s) | | 16.0 | | | |
| Intersection Capacity Utilization | | 94.4% | | | | | ICU Level of Service | | F | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

14: Lone Tree Way & Hillcrest Avenue






























Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 5058 | | 1770 | 5085 | 1583 | 1770 | 3256 | | 1610 | 3256 | 1583 |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | 1770 | 5058 | | 1770 | 5085 | 1583 | 1770 | 3256 | | 1610 | 3256 | 1583 |
| Volume (vph) | 290 | 810 | 30 | 40 | 1310 | 400 | 80 | 70 | 80 | 380 | 40 | 470 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 290 | 810 | 30 | 40 | 1310 | 400 | 80 | 70 | 80 | 380 | 40 | 470 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 203 | 0 | 73 | 0 | 0 | 0 | 390 |
| Lane Group Flow (vph) | 290 | 838 | 0 | 40 | 1310 | 197 | 80 | 77 | 0 | 190 | 230 | 80 |
| Turn Type | Prot | | | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 14.0 | 67.6 | | 5.6 | 59.2 | 59.2 | 10.3 | 10.3 | | 20.5 | 20.5 | 20.5 |
| Effective Green, g (s) | 14.0 | 67.6 | | 5.6 | 59.2 | 59.2 | 10.3 | 10.3 | | 20.5 | 20.5 | 20.5 |
| Actuated g/C Ratio | 0.12 | 0.56 | | 0.05 | 0.49 | 0.49 | 0.09 | 0.09 | | 0.17 | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 207 | 2849 | | 83 | 2509 | 781 | 152 | 279 | | 275 | 556 | 270 |
| v/s Ratio Prot | c0.16 | 0.17 | | 0.02 | c0.26 | | c0.05 | 0.02 | | c0.12 | 0.07 | |
| v/s Ratio Perm | | | | | | 0.12 | | | | | | 0.05 |
| v/c Ratio | 1.40 | 0.29 | | 0.48 | 0.52 | 0.25 | 0.53 | 0.28 | | 0.69 | 0.41 | 0.30 |
| Uniform Delay, d1 | 53.0 | 13.7 | | 55.8 | 20.7 | 17.6 | 52.5 | 51.4 | | 46.8 | 44.4 | 43.5 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 206.9 | 0.3 | | 4.4 | 0.8 | 0.8 | 3.3 | 0.5 | | 7.3 | 0.5 | 0.6 |
| Delay (s) | 259.9 | 14.0 | | 60.1 | 21.5 | 18.4 | 55.8 | 51.9 | | 54.1 | 44.9 | 44.1 |
| Level of Service | F | B | | E | C | B | E | D | | D | D | D |
| Approach Delay (s) | | 77.1 | | | 21.7 | | | 53.2 | | | 46.4 | |
| Approach LOS | | E | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 44.7 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.67 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 69.7% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

15: Lone Tree Way & Vista Grande Drive






















Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |    |  |  |  |  |  |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 1770 | 1863 | 1583 | 1770 | 1653 | 1653 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.70 | 1.00 | 1.00 | 0.74 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 1313 | 1863 | 1583 | 1386 | 1653 | 1653 |
| Volume (vph) | 110 | 910 | 220 | 170 | 1370 | 140 | 300 | 20 | 130 | 70 | 20 | 60 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 110 | 910 | 220 | 170 | 1370 | 140 | 300 | 20 | 130 | 70 | 20 | 60 |
| RTOR Reduction (vph) | 0 | 0 | 104 | 0 | 0 | 64 | 0 | 0 | 99 | 0 | 46 | 0 |
| Lane Group Flow (vph) | 110 | 910 | 116 | 170 | 1370 | 76 | 300 | 20 | 31 | 70 | 34 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 11.9 | 57.8 | 57.8 | 14.2 | 60.1 | 60.1 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |
| Effective Green, g (s) | 11.9 | 57.8 | 57.8 | 14.2 | 60.1 | 60.1 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |
| Actuated g/C Ratio | 0.11 | 0.53 | 0.53 | 0.13 | 0.55 | 0.55 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 | 0.24 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 191 | 2672 | 832 | 228 | 2778 | 865 | 310 | 440 | 374 | 328 | 391 | 391 |
| v/s Ratio Prot | 0.06 | 0.18 | | c0.10 | c0.27 | | | 0.01 | | | 0.02 | |
| v/s Ratio Perm | | | 0.07 | | | 0.05 | c0.23 | | 0.02 | 0.05 | | |
| v/c Ratio | 0.58 | 0.34 | 0.14 | 0.75 | 0.49 | 0.09 | 0.97 | 0.05 | 0.08 | 0.21 | 0.09 | |
| Uniform Delay, d1 | 46.7 | 15.1 | 13.4 | 46.2 | 15.5 | 11.9 | 41.6 | 32.4 | 32.7 | 33.8 | 32.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 4.2 | 0.3 | 0.3 | 12.4 | 0.6 | 0.2 | 41.9 | 0.0 | 0.1 | 0.3 | 0.1 | |
| Delay (s) | 50.8 | 15.4 | 13.7 | 58.6 | 16.1 | 12.1 | 83.5 | 32.5 | 32.8 | 34.1 | 32.8 | |
| Level of Service | D | B | B | E | B | B | F | C | C | C | C | |
| Approach Delay (s) | | 18.3 | | | 20.1 | | | 66.6 | | | 33.4 | |
| Approach LOS | | B | | | C | | | E | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 26.0 | | | HCM Level of Service | | | C | | | |
| HCM Volume to Capacity ratio | | | 0.63 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 65.9% | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

16: Country Hills Drive & Hillcrest Avenue





















Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 0.97 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1723 | | 1770 | 3447 | | 1770 | 3519 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1723 | | 1770 | 3447 | | 1770 | 3519 | |
| Volume (vph) | 70 | 40 | 50 | 110 | 60 | 60 | 100 | 710 | 150 | 80 | 740 | 30 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 70 | 40 | 50 | 110 | 60 | 60 | 100 | 710 | 150 | 80 | 740 | 30 |
| RTOR Reduction (vph) | 0 | 0 | 46 | 0 | 50 | 0 | 0 | 16 | 0 | 0 | 3 | 0 |
| Lane Group Flow (vph) | 70 | 40 | 4 | 110 | 70 | 0 | 100 | 844 | 0 | 80 | 767 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | | | | |
| Actuated Green, G (s) | 5.6 | 5.8 | 5.8 | 8.1 | 8.3 | | 7.9 | 42.9 | | 5.4 | 40.4 | |
| Effective Green, g (s) | 5.6 | 5.8 | 5.8 | 8.1 | 8.3 | | 7.9 | 42.9 | | 5.4 | 40.4 | |
| Actuated g/C Ratio | 0.07 | 0.07 | 0.07 | 0.10 | 0.11 | | 0.10 | 0.55 | | 0.07 | 0.52 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 127 | 138 | 117 | 183 | 183 | | 179 | 1891 | | 122 | 1818 | |
| v/s Ratio Prot | 0.04 | 0.02 | | c0.06 | c0.04 | | c0.06 | c0.24 | | 0.05 | 0.22 | |
| v/s Ratio Perm | | | 0.00 | | | | | | | | | |
| v/c Ratio | 0.55 | 0.29 | 0.03 | 0.60 | 0.38 | | 0.56 | 0.45 | | 0.66 | 0.42 | |
| Uniform Delay, d1 | 35.1 | 34.3 | 33.6 | 33.5 | 32.6 | | 33.5 | 10.6 | | 35.5 | 11.7 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 5.1 | 1.2 | 0.1 | 5.5 | 1.3 | | 3.7 | 0.8 | | 12.0 | 0.7 | |
| Delay (s) | 40.2 | 35.4 | 33.7 | 39.0 | 33.9 | | 37.2 | 11.3 | | 47.5 | 12.4 | |
| Level of Service | D | D | C | D | C | | D | B | | D | B | |
| Approach Delay (s) | | 37.0 | | | 36.3 | | | 14.0 | | | 15.7 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 18.7 | | | HCM Level of Service | | | | B | | |
| HCM Volume to Capacity ratio | | | 0.43 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 78.2 | | | Sum of lost time (s) | | | | 8.0 | | |
| Intersection Capacity Utilization | | | 51.6% | | | ICU Level of Service | | | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis






















17: Laurel Road & Tree Line Way

Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| | | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|--|
| |  |  |  |  |  |  |  |  |  |  |  |  | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | | |
| Sign Control | Free | | | Free | | | Stop | | | Stop | | | |
| Grade | 0% | | | 0% | | | 0% | | | 0% | | | |
| Volume (veh/h) | 10 | 1234 | 5 | 10 | 916 | 20 | 12 | 0 | 32 | 40 | 0 | 20 | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Hourly flow rate (vph) | 10 | 1234 | 5 | 10 | 916 | 20 | 12 | 0 | 32 | 40 | 0 | 20 | |
| Pedestrians | | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | | |
| Median type | None | | | | | | | | None | | | | |
| Median storage veh | | | | | | | | | | | | | |
| Upstream signal (ft) | 988 | | | 1304 | | | | | | | | | |
| pX, platoon unblocked | 0.96 | | | 0.79 | | | 0.81 | 0.81 | 0.79 | 0.81 | 0.81 | 0.96 | |
| vC, conflicting volume | 936 | | | 1239 | | | 1754 | 2212 | 620 | 1615 | 2205 | 468 | |
| vC1, stage 1 conf vol | | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | | |
| vCu, unblocked vol | 895 | | | 1041 | | | 1560 | 2124 | 261 | 1388 | 2114 | 409 | |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | |
| tC, 2 stage (s) | | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | |
| p0 queue free % | 99 | | | 98 | | | 79 | 100 | 95 | 48 | 100 | 96 | |
| cM capacity (veh/h) | 726 | | | 527 | | | 58 | 39 | 586 | 76 | 39 | 570 | |
| Direction, Lane # | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | NB 2 | SB 1 | SB 2 | | | |
| Volume Total | 10 | 823 | 416 | 10 | 611 | 325 | 12 | 32 | 40 | 20 | | | |
| Volume Left | 10 | 0 | 0 | 10 | 0 | 0 | 12 | 0 | 40 | 0 | | | |
| Volume Right | 0 | 0 | 5 | 0 | 0 | 20 | 0 | 32 | 0 | 20 | | | |
| cSH | 726 | 1700 | 1700 | 527 | 1700 | 1700 | 58 | 586 | 76 | 570 | | | |
| Volume to Capacity | 0.01 | 0.48 | 0.24 | 0.02 | 0.36 | 0.19 | 0.21 | 0.05 | 0.52 | 0.04 | | | |
| Queue Length 95th (ft) | 1 | 0 | 0 | 1 | 0 | 0 | 17 | 4 | 55 | 3 | | | |
| Control Delay (s) | 10.0 | 0.0 | 0.0 | 12.0 | 0.0 | 0.0 | 82.4 | 11.5 | 95.1 | 11.5 | | | |
| Lane LOS | B | | | B | | | F | B | F | B | | | |
| Approach Delay (s) | 0.1 | | | 0.1 | | | 30.8 | | 67.3 | | | | |
| Approach LOS | | | | | | | D | | F | | | | |
| Intersection Summary | | | | | | | | | | | | | |
| Average Delay | 2.4 | | | | | | | | | | | | |
| Intersection Capacity Utilization | 49.8% | | | ICU Level of Service | | | | | | A | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | | |
| | | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
18: Laurel Road & Hillcrest Avenue

Antioch Davidon Homes TIA
2025 With Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1709 | | 1770 | 1863 | 1583 | 1770 | 3388 | | 1770 | 3474 | |
| Flt Permitted | 0.67 | 1.00 | | 0.51 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1250 | 1709 | | 945 | 1863 | 1583 | 1770 | 3388 | | 1770 | 3474 | |
| Volume (vph) | 170 | 90 | 110 | 260 | 100 | 210 | 90 | 900 | 360 | 320 | 860 | 120 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 170 | 90 | 110 | 260 | 100 | 210 | 90 | 900 | 360 | 320 | 860 | 120 |
| RTOR Reduction (vph) | 0 | 38 | 0 | 0 | 0 | 150 | 0 | 34 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 170 | 162 | 0 | 260 | 100 | 60 | 90 | 1226 | 0 | 320 | 972 | 0 |
| Turn Type | Perm | | | Perm | | Perm | Prot | | | Prot | | |
| Protected Phases | 4 | | | 8 | | 8 | 5 | | 2 | 1 | | 6 |
| Permitted Phases | 4 | | | 8 | | 8 | | | | | | |
| Actuated Green, G (s) | 34.1 | 34.1 | | 34.1 | 34.1 | 34.1 | 10.4 | 50.6 | | 23.3 | 63.5 | |
| Effective Green, g (s) | 34.1 | 34.1 | | 34.1 | 34.1 | 34.1 | 10.4 | 50.6 | | 23.3 | 63.5 | |
| Actuated g/C Ratio | 0.28 | 0.28 | | 0.28 | 0.28 | 0.28 | 0.09 | 0.42 | | 0.19 | 0.53 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 355 | 486 | | 269 | 529 | 450 | 153 | 1429 | | 344 | 1838 | |
| v/s Ratio Prot | | 0.09 | | | 0.05 | | 0.05 | c0.36 | | c0.18 | 0.28 | |
| v/s Ratio Perm | 0.14 | | | c0.28 | | 0.04 | | | | | | |
| v/c Ratio | 0.48 | 0.33 | | 0.97 | 0.19 | 0.13 | 0.59 | 0.86 | | 0.93 | 0.53 | |
| Uniform Delay, d1 | 35.6 | 34.0 | | 42.4 | 32.5 | 31.9 | 52.7 | 31.4 | | 47.6 | 18.5 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.0 | 0.4 | | 45.2 | 0.2 | 0.1 | 5.7 | 6.9 | | 31.1 | 1.1 | |
| Delay (s) | 36.6 | 34.4 | | 87.6 | 32.7 | 32.1 | 58.4 | 38.3 | | 78.7 | 19.6 | |
| Level of Service | D | C | | F | C | C | E | D | | E | B | |
| Approach Delay (s) | | 35.4 | | | 57.5 | | | 39.6 | | | 34.1 | |
| Approach LOS | | D | | | E | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 40.0 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.91 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | | Sum of lost time (s) | | | 12.0 | | |
| Intersection Capacity Utilization | | | 93.3% | | | | ICU Level of Service | | | F | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

1: Laurel Road & Canada Valley





















Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|-----------------------------------|-------|------|-------|------|----------------------|-------|
| Lane Configurations | ↑↑ | | ↵ | ↑↑ | ↵ | ↵ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.95 | | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | 0.97 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3432 | | 1770 | 3539 | 1770 | 1583 |
| Flt Permitted | 1.00 | | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3432 | | 1770 | 3539 | 1770 | 1583 |
| Volume (vph) | 590 | 150 | 490 | 850 | 40 | 320 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 590 | 150 | 490 | 850 | 40 | 320 |
| RTOR Reduction (vph) | 21 | 0 | 0 | 0 | 0 | 259 |
| Lane Group Flow (vph) | 719 | 0 | 490 | 850 | 40 | 61 |
| Turn Type | | | Prot | | | Perm |
| Protected Phases | 4 | | 3 | 8 | 2 | |
| Permitted Phases | | | | | | 2 |
| Actuated Green, G (s) | 33.2 | | 35.8 | 73.0 | 19.0 | 19.0 |
| Effective Green, g (s) | 33.2 | | 35.8 | 73.0 | 19.0 | 19.0 |
| Actuated g/C Ratio | 0.33 | | 0.36 | 0.73 | 0.19 | 0.19 |
| Clearance Time (s) | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 1139 | | 634 | 2583 | 336 | 301 |
| v/s Ratio Prot | c0.21 | | c0.28 | 0.24 | 0.02 | |
| v/s Ratio Perm | | | | | | c0.04 |
| v/c Ratio | 0.63 | | 0.77 | 0.33 | 0.12 | 0.20 |
| Uniform Delay, d1 | 28.2 | | 28.5 | 4.8 | 33.6 | 34.1 |
| Progression Factor | 1.00 | | 0.64 | 0.39 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.7 | | 5.0 | 0.3 | 0.7 | 1.5 |
| Delay (s) | 30.9 | | 23.3 | 2.1 | 34.3 | 35.6 |
| Level of Service | C | | C | A | C | D |
| Approach Delay (s) | 30.9 | | | 9.9 | 35.5 | |
| Approach LOS | C | | | A | D | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 20.0 | | HCM Level of Service | C |
| HCM Volume to Capacity ratio | | | 0.60 | | | |
| Actuated Cycle Length (s) | | | 100.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 61.6% | | ICU Level of Service | B |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

2: Laurel Road & Country Hills Drive













Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.95 | | 1.00 | 0.95 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 0.99 | | 1.00 | 0.86 | | 1.00 | 0.90 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 3461 | | 1770 | 3497 | | 1770 | 1599 | | 1770 | 1676 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 3461 | | 1770 | 3497 | | 1770 | 1599 | | 1770 | 1676 | |
| Volume (vph) | 60 | 690 | 120 | 310 | 1170 | 100 | 90 | 10 | 170 | 50 | 20 | 40 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 60 | 690 | 120 | 310 | 1170 | 100 | 90 | 10 | 170 | 50 | 20 | 40 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 35 | 0 |
| Lane Group Flow (vph) | 60 | 810 | 0 | 310 | 1265 | 0 | 90 | 180 | 0 | 50 | 25 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 7.1 | 36.7 | | 26.8 | 56.4 | | 7.7 | 15.7 | | 4.8 | 12.8 | |
| Effective Green, g (s) | 7.1 | 36.7 | | 26.8 | 56.4 | | 7.7 | 15.7 | | 4.8 | 12.8 | |
| Actuated g/C Ratio | 0.07 | 0.37 | | 0.27 | 0.56 | | 0.08 | 0.16 | | 0.05 | 0.13 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 126 | 1270 | | 474 | 1972 | | 136 | 251 | | 85 | 215 | |
| v/s Ratio Prot | 0.03 | c0.23 | | 0.18 | c0.36 | | c0.05 | c0.11 | | 0.03 | 0.01 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.48 | 0.64 | | 0.65 | 0.64 | | 0.66 | 0.72 | | 0.59 | 0.12 | |
| Uniform Delay, d1 | 44.7 | 26.2 | | 32.5 | 14.9 | | 44.9 | 40.0 | | 46.6 | 38.6 | |
| Progression Factor | 0.91 | 1.45 | | 1.01 | 0.96 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.3 | 2.0 | | 2.6 | 1.3 | | 11.5 | 9.4 | | 10.0 | 0.2 | |
| Delay (s) | 43.0 | 39.9 | | 35.5 | 15.5 | | 56.3 | 49.4 | | 56.6 | 38.8 | |
| Level of Service | D | D | | D | B | | E | D | | E | D | |
| Approach Delay (s) | 40.1 | | | 19.4 | | | 51.7 | | | 46.9 | | |
| Approach LOS | D | | | B | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 29.9 | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | | 0.65 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | | 67.8% | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Laurel Road & SB SR4 Bypass





















Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑ | | | ↑↑ | | | | | ↑ | ↑↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.95 | | | 0.95 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 0.99 | | | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 3516 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | | | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 3516 | | | 3539 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 870 | 40 | 0 | 990 | 0 | 0 | 0 | 0 | 720 | 0 | 590 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 870 | 40 | 0 | 990 | 0 | 0 | 0 | 0 | 720 | 0 | 590 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 910 | 0 | 0 | 990 | 0 | 0 | 0 | 0 | 360 | 360 | 590 |
| Turn Type | | | | | | | | | | Perm | custom | |
| Protected Phases | | 2 | | | 6 | | | | | | 4 | 4 |
| Permitted Phases | | | | | | | | | | 4 | | 4 |
| Actuated Green, G (s) | | 49.5 | | | 49.5 | | | | | 42.5 | 42.5 | 42.5 |
| Effective Green, g (s) | | 49.5 | | | 49.5 | | | | | 42.5 | 42.5 | 42.5 |
| Actuated g/C Ratio | | 0.50 | | | 0.50 | | | | | 0.42 | 0.42 | 0.42 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 1740 | | | 1752 | | | | | 714 | 714 | 673 |
| v/s Ratio Prot | | 0.26 | | | c0.28 | | | | | | | c0.37 |
| v/s Ratio Perm | | | | | | | | | | 0.21 | 0.21 | |
| v/c Ratio | | 0.52 | | | 0.57 | | | | | 0.50 | 0.50 | 0.88 |
| Uniform Delay, d1 | | 17.2 | | | 17.7 | | | | | 21.0 | 21.0 | 26.3 |
| Progression Factor | | 0.14 | | | 0.34 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.9 | | | 1.2 | | | | | 0.6 | 0.6 | 12.3 |
| Delay (s) | | 3.2 | | | 7.3 | | | | | 21.6 | 21.6 | 38.7 |
| Level of Service | | A | | | A | | | | | C | C | D |
| Approach Delay (s) | | 3.2 | | | 7.3 | | | 0.0 | | | 29.3 | |
| Approach LOS | | A | | | A | | | A | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 15.1 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.71 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 100.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 102.7% | | | ICU Level of Service | | | G | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

4: Laurel Road & SR4 Bypass NB Ramps




























Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |   | | |   |  | |  |  | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Lane Util. Factor | 1.00 | 0.95 | | | 0.95 | 1.00 | | 1.00 | 1.00 | | | |
| Frt | 1.00 | 1.00 | | | 1.00 | 0.85 | | 1.00 | 0.85 | | | |
| Flt Protected | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Flt Permitted | 0.95 | 1.00 | | | 1.00 | 1.00 | | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | 1770 | 3539 | | | 3539 | 1583 | | 1770 | 1583 | | | |
| Volume (vph) | 220 | 1370 | 0 | 0 | 1010 | 730 | 90 | 0 | 210 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 1370 | 0 | 0 | 1010 | 730 | 90 | 0 | 210 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 220 | 1370 | 0 | 0 | 1010 | 730 | 0 | 90 | 210 | 0 | 0 | 0 |
| Turn Type | Prot | | | Perm | | | Perm | custom | | | | |
| Protected Phases | 5 | 2 | | | 6 | | | 8 | 8 | | | |
| Permitted Phases | | | | | | 6 | 8 | | 8 | | | |
| Actuated Green, G (s) | 16.0 | 76.1 | | | 56.1 | 56.1 | | 15.9 | 15.9 | | | |
| Effective Green, g (s) | 16.0 | 76.1 | | | 56.1 | 56.1 | | 15.9 | 15.9 | | | |
| Actuated g/C Ratio | 0.16 | 0.76 | | | 0.56 | 0.56 | | 0.16 | 0.16 | | | |
| Clearance Time (s) | 4.0 | 4.0 | | | 4.0 | 4.0 | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | 3.0 | 3.0 | | | 3.0 | 3.0 | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | 283 | 2693 | | | 1985 | 888 | | 281 | 252 | | | |
| v/s Ratio Prot | c0.12 | 0.39 | | | 0.29 | | | | c0.13 | | | |
| v/s Ratio Perm | | | | | | c0.46 | | 0.05 | | | | |
| v/c Ratio | 0.78 | 0.51 | | | 0.51 | 0.82 | | 0.32 | 0.83 | | | |
| Uniform Delay, d1 | 40.3 | 4.7 | | | 13.5 | 17.9 | | 37.3 | 40.8 | | | |
| Progression Factor | 0.92 | 0.87 | | | 0.12 | 0.18 | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 11.4 | 0.6 | | | 0.6 | 5.7 | | 0.7 | 20.4 | | | |
| Delay (s) | 48.5 | 4.7 | | | 2.2 | 8.9 | | 37.9 | 61.2 | | | |
| Level of Service | D | A | | | A | A | | D | E | | | |
| Approach Delay (s) | | 10.7 | | | 5.0 | | | 54.2 | | | 0.0 | |
| Approach LOS | | B | | | A | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 11.6 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.82 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 100.0 | | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | 72.4% | | | ICU Level of Service | | | C | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Laurel Road & Slatten Ranch Road

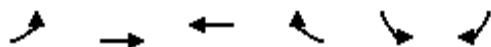
Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |    | |  |   | |  |   | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.92 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 4950 | | 3433 | 3264 | | 1770 | 3427 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 4950 | | 3433 | 3264 | | 1770 | 3427 | |
| Volume (vph) | 100 | 1190 | 290 | 260 | 1020 | 220 | 610 | 270 | 290 | 230 | 410 | 110 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 100 | 1190 | 290 | 260 | 1020 | 220 | 610 | 270 | 290 | 230 | 410 | 110 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 100 | 1190 | 290 | 260 | 1240 | 0 | 610 | 560 | 0 | 230 | 520 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | |
| Actuated Green, G (s) | 9.6 | 29.4 | 29.4 | 16.8 | 36.6 | | 20.3 | 22.5 | | 15.3 | 17.5 | |
| Effective Green, g (s) | 9.6 | 29.4 | 29.4 | 16.8 | 36.6 | | 20.3 | 22.5 | | 15.3 | 17.5 | |
| Actuated g/C Ratio | 0.10 | 0.29 | 0.29 | 0.17 | 0.37 | | 0.20 | 0.22 | | 0.15 | 0.18 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 170 | 1495 | 465 | 297 | 1812 | | 697 | 734 | | 271 | 600 | |
| v/s Ratio Prot | 0.06 | c0.23 | | c0.15 | 0.25 | | c0.18 | 0.17 | | 0.13 | c0.15 | |
| v/s Ratio Perm | | | 0.18 | | | | | | | | | |
| v/c Ratio | 0.59 | 0.80 | 0.62 | 0.88 | 0.68 | | 0.88 | 0.76 | | 0.85 | 0.87 | |
| Uniform Delay, d1 | 43.3 | 32.5 | 30.5 | 40.6 | 26.8 | | 38.6 | 36.3 | | 41.2 | 40.1 | |
| Progression Factor | 0.90 | 0.90 | 0.88 | 0.72 | 0.35 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 4.4 | 3.8 | 5.3 | 20.4 | 1.8 | | 11.8 | 4.7 | | 21.2 | 12.5 | |
| Delay (s) | 43.4 | 33.0 | 32.1 | 49.6 | 11.0 | | 50.5 | 41.0 | | 62.4 | 52.6 | |
| Level of Service | D | C | C | D | B | | D | D | | E | D | |
| Approach Delay (s) | | 33.5 | | | 17.7 | | | 45.9 | | | 55.6 | |
| Approach LOS | | C | | | B | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 35.0 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.84 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | Sum of lost time (s) | | | | 16.0 | | |
| Intersection Capacity Utilization | | | 83.0% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

6: Laurel Road & Live Oak Avenue

Antioch Davidon Homes TIA
2025 With Project PM Peak Hour


























| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
|-----------------------------------|-------|------|-------|------|----------------------|------|
| Lane Configurations | | | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.91 | | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.99 | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 5055 | | 1770 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | 0.95 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 5055 | | 1770 | 1583 |
| Volume (vph) | 340 | 1370 | 1210 | 50 | 130 | 290 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 340 | 1370 | 1210 | 50 | 130 | 290 |
| RTOR Reduction (vph) | 0 | 0 | 5 | 0 | 0 | 175 |
| Lane Group Flow (vph) | 340 | 1370 | 1255 | 0 | 130 | 115 |
| Turn Type | Prot | | | Perm | | |
| Protected Phases | 7 | 4 | 8 | | 6 | |
| Permitted Phases | | | | | | 6 |
| Actuated Green, G (s) | 15.3 | 52.3 | 33.0 | | 39.7 | 39.7 |
| Effective Green, g (s) | 15.3 | 52.3 | 33.0 | | 39.7 | 39.7 |
| Actuated g/C Ratio | 0.15 | 0.52 | 0.33 | | 0.40 | 0.40 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 525 | 2659 | 1668 | | 703 | 628 |
| v/s Ratio Prot | c0.10 | 0.27 | c0.25 | | c0.07 | |
| v/s Ratio Perm | | | | | | 0.07 |
| v/c Ratio | 0.65 | 0.52 | 0.75 | | 0.18 | 0.18 |
| Uniform Delay, d1 | 39.8 | 15.6 | 29.9 | | 19.6 | 19.6 |
| Progression Factor | 1.22 | 1.05 | 0.86 | | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.6 | 0.1 | 1.7 | | 0.6 | 0.6 |
| Delay (s) | 50.0 | 16.4 | 27.2 | | 20.2 | 20.2 |
| Level of Service | D | B | C | | C | C |
| Approach Delay (s) | | 23.1 | 27.2 | | 20.2 | |
| Approach LOS | | C | C | | C | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 24.3 | | HCM Level of Service | C |
| HCM Volume to Capacity ratio | | | 0.48 | | | |
| Actuated Cycle Length (s) | | | 100.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 51.4% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

7: Laurel Road & Empire Avenue

























Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3463 | | 1770 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 3463 | | 1770 | 3539 | 1583 |
| Volume (vph) | 430 | 910 | 160 | 50 | 720 | 50 | 110 | 360 | 60 | 60 | 300 | 430 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 430 | 910 | 160 | 50 | 720 | 50 | 110 | 360 | 60 | 60 | 300 | 430 |
| RTOR Reduction (vph) | 0 | 0 | 78 | 0 | 0 | 30 | 0 | 14 | 0 | 0 | 0 | 303 |
| Lane Group Flow (vph) | 430 | 910 | 82 | 50 | 720 | 20 | 110 | 406 | 0 | 60 | 300 | 127 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | 8 | | | | | | 6 |
| Actuated Green, G (s) | 16.9 | 51.2 | 51.2 | 6.3 | 40.6 | 40.6 | 9.9 | 19.7 | | 6.8 | 16.6 | 16.6 |
| Effective Green, g (s) | 16.9 | 51.2 | 51.2 | 6.3 | 40.6 | 40.6 | 9.9 | 19.7 | | 6.8 | 16.6 | 16.6 |
| Actuated g/C Ratio | 0.17 | 0.51 | 0.51 | 0.06 | 0.41 | 0.41 | 0.10 | 0.20 | | 0.07 | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 580 | 1812 | 810 | 112 | 1437 | 643 | 175 | 682 | | 120 | 587 | 263 |
| v/s Ratio Prot | c0.13 | c0.26 | | 0.03 | 0.20 | | c0.06 | c0.12 | | 0.03 | 0.08 | |
| v/s Ratio Perm | | | 0.05 | | | 0.01 | | | | | | 0.08 |
| v/c Ratio | 0.74 | 0.50 | 0.10 | 0.45 | 0.50 | 0.03 | 0.63 | 0.59 | | 0.50 | 0.51 | 0.48 |
| Uniform Delay, d1 | 39.5 | 16.0 | 12.6 | 45.2 | 22.1 | 17.9 | 43.3 | 36.5 | | 45.0 | 38.0 | 37.8 |
| Progression Factor | 0.69 | 1.33 | 2.57 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 4.8 | 0.9 | 0.2 | 2.8 | 1.3 | 0.1 | 6.9 | 1.4 | | 3.3 | 0.8 | 1.4 |
| Delay (s) | 31.9 | 22.3 | 32.5 | 48.0 | 23.4 | 18.0 | 50.2 | 37.9 | | 48.2 | 38.8 | 39.2 |
| Level of Service | C | | C | D | C | B | D | D | | D | D | D |
| Approach Delay (s) | | 26.1 | | | 24.6 | | | 40.5 | | | 39.7 | |
| Approach LOS | | C | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 30.8 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 100.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 62.6% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

8: Lone Tree Way & Canada Valley













Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | 0.91 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.86 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 1770 | 2933 | 1441 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 3433 | 5085 | 1583 | 1770 | 2933 | 1441 | 1770 | 1863 | 1583 |
| Volume (vph) | 130 | 1710 | 60 | 530 | 1090 | 500 | 220 | 20 | 360 | 250 | 20 | 120 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 130 | 1710 | 60 | 530 | 1090 | 500 | 220 | 20 | 360 | 250 | 20 | 120 |
| RTOR Reduction (vph) | 0 | 0 | 32 | 0 | 0 | 224 | 0 | 167 | 167 | 0 | 0 | 110 |
| Lane Group Flow (vph) | 130 | 1710 | 28 | 530 | 1090 | 276 | 220 | 33 | 13 | 250 | 20 | 10 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | 4 |
| Actuated Green, G (s) | 8.0 | 46.6 | 46.6 | 22.1 | 60.7 | 60.7 | 16.2 | 7.9 | 7.9 | 17.4 | 9.1 | 9.1 |
| Effective Green, g (s) | 8.0 | 46.6 | 46.6 | 22.1 | 60.7 | 60.7 | 16.2 | 7.9 | 7.9 | 17.4 | 9.1 | 9.1 |
| Actuated g/C Ratio | 0.07 | 0.42 | 0.42 | 0.20 | 0.55 | 0.55 | 0.15 | 0.07 | 0.07 | 0.16 | 0.08 | 0.08 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 250 | 2154 | 671 | 690 | 2806 | 874 | 261 | 211 | 103 | 280 | 154 | 131 |
| v/s Ratio Prot | 0.04 | c0.34 | | c0.15 | 0.21 | | 0.12 | c0.01 | | c0.14 | 0.01 | |
| v/s Ratio Perm | | | 0.02 | | | 0.17 | | | 0.01 | | | 0.01 |
| v/c Ratio | 0.52 | 0.79 | 0.04 | 0.77 | 0.39 | 0.32 | 0.84 | 0.16 | 0.13 | 0.89 | 0.13 | 0.08 |
| Uniform Delay, d1 | 49.1 | 27.5 | 18.6 | 41.5 | 14.1 | 13.4 | 45.7 | 47.9 | 47.8 | 45.4 | 46.8 | 46.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.68 | 1.06 | 5.44 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.9 | 3.1 | 0.1 | 4.3 | 0.3 | 0.8 | 21.2 | 0.3 | 0.6 | 27.9 | 0.4 | 0.2 |
| Delay (s) | 51.1 | 30.6 | 18.7 | 32.6 | 15.2 | 73.6 | 66.8 | 48.3 | 48.4 | 73.3 | 47.2 | 46.8 |
| Level of Service | D | C | B | C | B | E | E | D | D | E | D | D |
| Approach Delay (s) | | 31.7 | | | 33.3 | | | 55.1 | | | 63.8 | |
| Approach LOS | | C | | | C | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 37.7 | | | HCM Level of Service | | | D | | | |
| HCM Volume to Capacity ratio | | | 0.75 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 79.8% | | | ICU Level of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

9: Lone Tree Way & SB SR4 Bypass













Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | | | | | ↑ | ↑ | ↑ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | | | | | 0.95 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | | | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | | | | | 0.95 | 0.95 | 1.00 |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | | | | | 1681 | 1681 | 1583 |
| Volume (vph) | 0 | 2060 | 380 | 380 | 1880 | 0 | 0 | 0 | 0 | 860 | 0 | 240 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 2060 | 380 | 380 | 1880 | 0 | 0 | 0 | 0 | 860 | 0 | 240 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 2060 | 380 | 380 | 1880 | 0 | 0 | 0 | 0 | 430 | 430 | 240 |
| Turn Type | | Perm | | Prot | | | | | | Split | | Perm |
| Protected Phases | | 2 | | 1 | | 6 | | | | 4 | | 4 |
| Permitted Phases | | 2 | | | | | | | | | | 4 |
| Actuated Green, G (s) | | 51.9 | 51.9 | 15.0 | 70.9 | | | | | 31.1 | 31.1 | 31.1 |
| Effective Green, g (s) | | 51.9 | 51.9 | 15.0 | 70.9 | | | | | 31.1 | 31.1 | 31.1 |
| Actuated g/C Ratio | | 0.47 | 0.47 | 0.14 | 0.64 | | | | | 0.28 | 0.28 | 0.28 |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | | | | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | | | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 2399 | 747 | 468 | 3278 | | | | | 475 | 475 | 448 |
| v/s Ratio Prot | | c0.41 | | c0.11 | | 0.37 | | | | c0.26 | | 0.26 |
| v/s Ratio Perm | | 0.24 | | | | | | | | | | 0.15 |
| v/c Ratio | | 0.86 | 0.51 | 0.81 | 0.57 | | | | | 0.91 | 0.91 | 0.54 |
| Uniform Delay, d1 | | 25.8 | 20.2 | 46.1 | 11.0 | | | | | 38.0 | 38.0 | 33.3 |
| Progression Factor | | 0.65 | 0.51 | 0.95 | 0.71 | | | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 3.0 | 1.7 | 9.1 | 0.6 | | | | | 20.5 | 20.5 | 1.2 |
| Delay (s) | | 19.7 | 12.1 | 52.9 | 8.5 | | | | | 58.6 | 58.6 | 34.6 |
| Level of Service | | B | B | D | A | | | | | E | E | C |
| Approach Delay (s) | | 18.5 | | 15.9 | | 0.0 | | 53.3 | | | | |
| Approach LOS | | B | | B | | A | | D | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 24.1 | | HCM Level of Service | | | C | | | | |
| HCM Volume to Capacity ratio | | | 0.87 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | Sum of lost time (s) | | | 12.0 | | | | |
| Intersection Capacity Utilization | | | 84.5% | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

10: Lone Tree Way & SR4 Bypass NB Ramps























Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↑↑↑↑ | ↑ | ↑↑ | ↑↑↑ | ↑ | ↑↑ | ↑ | ↑ | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 0.91 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | | | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | | | |
| Flt Protected | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (prot) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Flt Permitted | | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | | | |
| Satd. Flow (perm) | | 5085 | 1583 | 3433 | 5085 | 1583 | 3433 | 1863 | 1583 | | | |
| Volume (vph) | 0 | 2640 | 280 | 60 | 1710 | 730 | 550 | 50 | 340 | 0 | 0 | 0 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 0 | 2640 | 280 | 60 | 1710 | 730 | 550 | 50 | 340 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 2640 | 280 | 60 | 1710 | 730 | 550 | 50 | 340 | 0 | 0 | 0 |
| Turn Type | | Perm | | Prot | | Perm | Perm | | Perm | | | |
| Protected Phases | | 2 | | 1 | 6 | | | 8 | | | | |
| Permitted Phases | | 2 | | | 6 | 8 | | 8 | | | | |
| Actuated Green, G (s) | | 67.7 | 67.7 | 3.2 | 74.9 | 74.9 | 27.1 | 27.1 | 27.1 | | | |
| Effective Green, g (s) | | 67.7 | 67.7 | 3.2 | 74.9 | 74.9 | 27.1 | 27.1 | 27.1 | | | |
| Actuated g/C Ratio | | 0.62 | 0.62 | 0.03 | 0.68 | 0.68 | 0.25 | 0.25 | 0.25 | | | |
| Clearance Time (s) | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 3130 | 974 | 100 | 3462 | 1078 | 846 | 459 | 390 | | | |
| v/s Ratio Prot | | c0.52 | | 0.02 | 0.34 | | | 0.03 | | | | |
| v/s Ratio Perm | | 0.18 | | | | c0.46 | 0.16 | | c0.21 | | | |
| v/c Ratio | | 0.84 | 0.29 | 0.60 | 0.49 | 0.68 | 0.65 | 0.11 | 0.87 | | | |
| Uniform Delay, d1 | | 16.9 | 9.9 | 52.8 | 8.4 | 10.4 | 37.2 | 32.1 | 39.8 | | | |
| Progression Factor | | 0.29 | 0.27 | 1.12 | 1.78 | 1.64 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 1.5 | 0.4 | 3.8 | 0.2 | 1.3 | 1.8 | 0.1 | 18.8 | | | |
| Delay (s) | | 6.4 | 3.0 | 63.1 | 15.2 | 18.4 | 39.0 | 32.2 | 58.5 | | | |
| Level of Service | | A | A | E | B | B | D | C | E | | | |
| Approach Delay (s) | | 6.1 | | | 17.3 | | | 45.7 | | | 0.0 | |
| Approach LOS | | A | | | B | | | D | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 16.3 | | HCM Level of Service | | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.83 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | Sum of lost time (s) | | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 78.7% | | ICU Level of Service | | | | D | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

11: Lone Tree Way & Slatten Ranch Road
































Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 1.00 | 1.00 | 0.91 | | 0.97 | 0.95 | | 0.97 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5085 | 1583 | 1770 | 5056 | | 3433 | 3445 | | 3433 | 3539 | 1583 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5085 | 1583 | 1770 | 5056 | | 3433 | 3445 | | 3433 | 3539 | 1583 |
| Volume (vph) | 470 | 1990 | 530 | 50 | 1510 | 60 | 400 | 370 | 80 | 80 | 550 | 570 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 470 | 1990 | 530 | 50 | 1510 | 60 | 400 | 370 | 80 | 80 | 550 | 570 |
| RTOR Reduction (vph) | 0 | 0 | 57 | 0 | 4 | 0 | 0 | 16 | 0 | 0 | 0 | 264 |
| Lane Group Flow (vph) | 470 | 1990 | 473 | 50 | 1566 | 0 | 400 | 434 | 0 | 80 | 550 | 306 |
| Turn Type | Prot | pm+ov | | Prot | | | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | 3 | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | | | | | | | 4 |
| Actuated Green, G (s) | 22.8 | 53.0 | 67.3 | 6.2 | 36.4 | | 14.3 | 30.6 | | 4.2 | 20.5 | 20.5 |
| Effective Green, g (s) | 22.8 | 53.0 | 67.3 | 6.2 | 36.4 | | 14.3 | 30.6 | | 4.2 | 20.5 | 20.5 |
| Actuated g/C Ratio | 0.21 | 0.48 | 0.61 | 0.06 | 0.33 | | 0.13 | 0.28 | | 0.04 | 0.19 | 0.19 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 712 | 2450 | 969 | 100 | 1673 | | 446 | 958 | | 131 | 660 | 295 |
| v/s Ratio Prot | c0.14 | c0.39 | 0.06 | 0.03 | c0.31 | | c0.12 | 0.13 | | 0.02 | 0.16 | |
| v/s Ratio Perm | | | 0.24 | | | | | | | | | c0.19 |
| v/c Ratio | 0.66 | 0.81 | 0.49 | 0.50 | 0.94 | | 0.90 | 0.45 | | 0.61 | 0.83 | 1.04 |
| Uniform Delay, d1 | 40.0 | 24.3 | 11.8 | 50.4 | 35.7 | | 47.1 | 32.8 | | 52.1 | 43.1 | 44.8 |
| Progression Factor | 0.75 | 0.42 | 0.33 | 0.79 | 1.23 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.2 | 1.7 | 0.2 | 3.4 | 10.1 | | 20.2 | 0.3 | | 8.2 | 8.9 | 62.8 |
| Delay (s) | 31.4 | 11.8 | 4.1 | 43.1 | 54.1 | | 67.3 | 33.1 | | 60.3 | 52.0 | 107.5 |
| Level of Service | C | B | A | D | D | | E | C | | E | D | F |
| Approach Delay (s) | | 13.5 | | | 53.8 | | | 49.2 | | | 78.9 | |
| Approach LOS | | B | | | D | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 39.6 | | | HCM Level of Service | | | | D | | |
| HCM Volume to Capacity ratio | | | 0.88 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 87.2% | | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

12: Lone Tree Way & Empire Avenue





















Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |    |  |   |  |  |   |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3274 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 3433 | 1863 | 1583 | 3433 | 3274 | |
| Volume (vph) | 160 | 1390 | 600 | 20 | 960 | 160 | 440 | 120 | 40 | 310 | 220 | 220 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 160 | 1390 | 600 | 20 | 960 | 160 | 440 | 120 | 40 | 310 | 220 | 220 |
| RTOR Reduction (vph) | 0 | 0 | 280 | 0 | 0 | 89 | 0 | 0 | 36 | 0 | 187 | 0 |
| Lane Group Flow (vph) | 160 | 1390 | 320 | 20 | 960 | 71 | 440 | 120 | 4 | 310 | 253 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Prot | | Perm | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | 2 | | | 6 | | | 8 | | | |
| Actuated Green, G (s) | 20.4 | 58.7 | 58.7 | 3.1 | 41.4 | 41.4 | 19.2 | 12.0 | 12.0 | 20.2 | 13.0 | |
| Effective Green, g (s) | 20.4 | 58.7 | 58.7 | 3.1 | 41.4 | 41.4 | 19.2 | 12.0 | 12.0 | 20.2 | 13.0 | |
| Actuated g/C Ratio | 0.19 | 0.53 | 0.53 | 0.03 | 0.38 | 0.38 | 0.17 | 0.11 | 0.11 | 0.18 | 0.12 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 328 | 2714 | 845 | 50 | 1914 | 596 | 599 | 203 | 173 | 630 | 387 | |
| v/s Ratio Prot | 0.09 | c0.27 | | 0.01 | c0.19 | | c0.13 | 0.06 | | 0.09 | c0.08 | |
| v/s Ratio Perm | | | 0.20 | | | 0.04 | | | 0.00 | | | |
| v/c Ratio | 0.49 | 0.51 | 0.38 | 0.40 | 0.50 | 0.12 | 0.73 | 0.59 | 0.03 | 0.49 | 0.65 | |
| Uniform Delay, d1 | 40.1 | 16.5 | 15.0 | 52.5 | 26.4 | 22.4 | 43.0 | 46.7 | 43.8 | 40.3 | 46.4 | |
| Progression Factor | 0.52 | 0.21 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.7 | 0.4 | 0.8 | 5.2 | 0.9 | 0.4 | 4.7 | 4.6 | 0.1 | 0.6 | 3.9 | |
| Delay (s) | 21.6 | 3.9 | 14.3 | 57.7 | 27.3 | 22.8 | 47.6 | 51.2 | 43.8 | 40.9 | 50.3 | |
| Level of Service | C | A | B | E | C | C | D | D | D | D | D | |
| Approach Delay (s) | | 8.1 | | | 27.2 | | | 48.1 | | | 46.4 | |
| Approach LOS | | A | | | C | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 24.2 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 69.2% | | | ICU Level of Service | | | | C | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

13: Lone Tree Way & Deer Valley Rd























Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.5 | 4.0 | | 3.5 | 4.0 | | 3.5 | 4.0 | | 3.5 | 4.0 | |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | | 0.97 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.99 | | 1.00 | 0.98 | | 1.00 | 0.95 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 5014 | | 1770 | 5009 | | 3433 | 3374 | | 1770 | 3419 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 5014 | | 1770 | 5009 | | 3433 | 3374 | | 1770 | 3419 | |
| Volume (vph) | 320 | 1850 | 190 | 190 | 1440 | 160 | 260 | 400 | 180 | 310 | 510 | 150 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 320 | 1850 | 190 | 190 | 1440 | 160 | 260 | 400 | 180 | 310 | 510 | 150 |
| RTOR Reduction (vph) | 0 | 11 | 0 | 0 | 12 | 0 | 0 | 47 | 0 | 0 | 25 | 0 |
| Lane Group Flow (vph) | 320 | 2029 | 0 | 190 | 1588 | 0 | 260 | 533 | 0 | 310 | 635 | 0 |
| Turn Type | Prot | | | Prot | | | Prot | | | Prot | | |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | 20.0 | 47.0 | | 12.0 | 39.0 | | 10.0 | 18.0 | | 17.0 | 25.0 | |
| Effective Green, g (s) | 20.5 | 47.0 | | 12.5 | 39.0 | | 10.5 | 18.0 | | 17.5 | 25.0 | |
| Actuated g/C Ratio | 0.19 | 0.43 | | 0.11 | 0.35 | | 0.10 | 0.16 | | 0.16 | 0.23 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 330 | 2142 | | 201 | 1776 | | 328 | 552 | | 282 | 777 | |
| v/s Ratio Prot | c0.18 | c0.40 | | 0.11 | 0.32 | | 0.08 | c0.16 | | c0.18 | 0.19 | |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | 0.97 | 0.95 | | 0.95 | 0.89 | | 0.79 | 0.97 | | 1.10 | 0.82 | |
| Uniform Delay, d1 | 44.4 | 30.3 | | 48.4 | 33.5 | | 48.7 | 45.7 | | 46.2 | 40.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 40.9 | 10.5 | | 47.6 | 7.4 | | 12.3 | 29.5 | | 82.8 | 6.7 | |
| Delay (s) | 85.3 | 40.8 | | 96.1 | 40.9 | | 61.0 | 75.2 | | 129.1 | 47.0 | |
| Level of Service | F | D | | F | D | | E | E | | F | D | |
| Approach Delay (s) | 46.8 | | | 46.8 | | | 70.8 | | | 73.2 | | |
| Approach LOS | D | | | D | | | E | | | E | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 54.5 | | HCM Level of Service | | | | D | | | |
| HCM Volume to Capacity ratio | | | 0.97 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | | Sum of lost time (s) | | | | 11.0 | | | |
| Intersection Capacity Utilization | | | 97.8% | | ICU Level of Service | | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

14: Lone Tree Way & Hillcrest Avenue






























Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.91 | 0.91 | 1.00 |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 5051 | | 1770 | 5085 | 1583 | 1770 | 3294 | | 1610 | 3274 | 1583 |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 0.97 | 1.00 |
| Satd. Flow (perm) | 1770 | 5051 | | 1770 | 5085 | 1583 | 1770 | 3294 | | 1610 | 3274 | 1583 |
| Volume (vph) | 710 | 1680 | 80 | 100 | 1210 | 480 | 50 | 70 | 60 | 580 | 120 | 450 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 710 | 1680 | 80 | 100 | 1210 | 480 | 50 | 70 | 60 | 580 | 120 | 450 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 0 | 335 | 0 | 56 | 0 | 0 | 0 | 352 |
| Lane Group Flow (vph) | 710 | 1757 | 0 | 100 | 1210 | 145 | 50 | 74 | 0 | 290 | 410 | 98 |
| Turn Type | Prot | | | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 33.0 | 60.4 | | 8.8 | 36.2 | 36.2 | 8.7 | 8.7 | | 26.1 | 26.1 | 26.1 |
| Effective Green, g (s) | 33.0 | 60.4 | | 8.8 | 36.2 | 36.2 | 8.7 | 8.7 | | 26.1 | 26.1 | 26.1 |
| Actuated g/C Ratio | 0.28 | 0.50 | | 0.07 | 0.30 | 0.30 | 0.07 | 0.07 | | 0.22 | 0.22 | 0.22 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 487 | 2542 | | 130 | 1534 | 478 | 128 | 239 | | 350 | 712 | 344 |
| v/s Ratio Prot | c0.40 | 0.35 | | 0.06 | c0.24 | | c0.03 | 0.02 | | c0.18 | 0.13 | |
| v/s Ratio Perm | | | | | | 0.09 | | | | | | 0.06 |
| v/c Ratio | 1.46 | 0.69 | | 0.77 | 0.79 | 0.30 | 0.39 | 0.31 | | 0.83 | 0.58 | 0.28 |
| Uniform Delay, d1 | 43.5 | 22.7 | | 54.6 | 38.4 | 32.2 | 53.1 | 52.8 | | 44.8 | 42.0 | 39.2 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 217.2 | 1.6 | | 23.5 | 4.2 | 1.6 | 2.0 | 0.7 | | 14.8 | 1.1 | 0.5 |
| Delay (s) | 260.7 | 24.3 | | 78.1 | 42.6 | 33.8 | 55.1 | 53.6 | | 59.7 | 43.1 | 39.6 |
| Level of Service | F | C | | E | D | C | E | D | | E | D | D |
| Approach Delay (s) | | 92.2 | | | 42.2 | | | 54.0 | | | 45.9 | |
| Approach LOS | | F | | | D | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 65.5 | | | HCM Level of Service | | | E | | | |
| HCM Volume to Capacity ratio | | | 0.98 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 96.0% | | | ICU Level of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

15: Lone Tree Way & Vista Grande Drive






















Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |    |  |  |    |  |  |  |  |  |   |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.88 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 1770 | 1863 | 1583 | 1770 | 1637 | 1637 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.53 | 1.00 | 1.00 | 0.72 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 5085 | 1583 | 1770 | 5085 | 1583 | 985 | 1863 | 1583 | 1349 | 1637 | 1637 |
| Volume (vph) | 190 | 1710 | 390 | 300 | 1240 | 90 | 320 | 50 | 220 | 70 | 40 | 170 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 190 | 1710 | 390 | 300 | 1240 | 90 | 320 | 50 | 220 | 70 | 40 | 170 |
| RTOR Reduction (vph) | 0 | 0 | 179 | 0 | 0 | 53 | 0 | 0 | 147 | 0 | 113 | 0 |
| Lane Group Flow (vph) | 190 | 1710 | 211 | 300 | 1240 | 37 | 320 | 50 | 73 | 70 | 97 | 0 |
| Turn Type | Prot | | Perm | Prot | | Perm | Perm | | Perm | Perm | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | | 2 | | | 6 | |
| Permitted Phases | | | 4 | | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 16.1 | 41.5 | 41.5 | 19.9 | 45.3 | 45.3 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 |
| Effective Green, g (s) | 16.1 | 41.5 | 41.5 | 19.9 | 45.3 | 45.3 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 | 36.6 |
| Actuated g/C Ratio | 0.15 | 0.38 | 0.38 | 0.18 | 0.41 | 0.41 | 0.33 | 0.33 | 0.33 | 0.33 | 0.33 | 0.33 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 259 | 1918 | 597 | 320 | 2094 | 652 | 328 | 620 | 527 | 449 | 545 | 545 |
| v/s Ratio Prot | 0.11 | c0.34 | | c0.17 | c0.24 | | | 0.03 | | | 0.06 | |
| v/s Ratio Perm | | | 0.13 | | | 0.02 | c0.32 | | 0.05 | 0.05 | | |
| v/c Ratio | 0.73 | 0.89 | 0.35 | 0.94 | 0.59 | 0.06 | 0.98 | 0.08 | 0.14 | 0.16 | 0.18 | 0.18 |
| Uniform Delay, d1 | 44.9 | 32.1 | 24.6 | 44.4 | 25.2 | 19.5 | 36.3 | 25.2 | 25.7 | 25.8 | 26.0 | 26.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 10.3 | 6.8 | 1.6 | 33.9 | 1.2 | 0.2 | 42.7 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 |
| Delay (s) | 55.2 | 38.9 | 26.2 | 78.4 | 26.4 | 19.7 | 79.0 | 25.2 | 25.8 | 26.0 | 26.2 | 26.2 |
| Level of Service | E | D | C | E | C | B | E | C | C | C | C | C |
| Approach Delay (s) | | 38.1 | | | 35.6 | | | 54.6 | | | 26.1 | |
| Approach LOS | | D | | | D | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 38.6 | | | | HCM Level of Service | | D | | | | |
| HCM Volume to Capacity ratio | | 0.96 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 110.0 | | | | Sum of lost time (s) | | 16.0 | | | | |
| Intersection Capacity Utilization | | 93.3% | | | | ICU Level of Service | | F | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

16: Country Hills Drive & Hillcrest Avenue





















Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  |  | |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1683 | | 1770 | 3506 | | 1770 | 3497 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1863 | 1583 | 1770 | 1683 | | 1770 | 3506 | | 1770 | 3497 | |
| Volume (vph) | 70 | 20 | 100 | 120 | 50 | 90 | 100 | 1060 | 70 | 110 | 920 | 80 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 70 | 20 | 100 | 120 | 50 | 90 | 100 | 1060 | 70 | 110 | 920 | 80 |
| RTOR Reduction (vph) | 0 | 0 | 90 | 0 | 78 | 0 | 0 | 4 | 0 | 0 | 6 | 0 |
| Lane Group Flow (vph) | 70 | 20 | 10 | 120 | 62 | 0 | 100 | 1126 | 0 | 110 | 994 | 0 |
| Turn Type | Prot | | Perm | Prot | | | Prot | | | Prot | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | | | | |
| Actuated Green, G (s) | 6.1 | 8.4 | 8.4 | 8.7 | 11.0 | | 8.4 | 42.2 | | 7.9 | 41.7 | |
| Effective Green, g (s) | 6.1 | 8.4 | 8.4 | 8.7 | 11.0 | | 8.4 | 42.2 | | 7.9 | 41.7 | |
| Actuated g/C Ratio | 0.07 | 0.10 | 0.10 | 0.10 | 0.13 | | 0.10 | 0.51 | | 0.09 | 0.50 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 130 | 188 | 160 | 185 | 223 | | 179 | 1778 | | 168 | 1753 | |
| v/s Ratio Prot | 0.04 | 0.01 | | c0.07 | c0.04 | | 0.06 | c0.32 | | c0.06 | 0.28 | |
| v/s Ratio Perm | | | 0.01 | | | | | | | | | |
| v/c Ratio | 0.54 | 0.11 | 0.06 | 0.65 | 0.28 | | 0.56 | 0.63 | | 0.65 | 0.57 | |
| Uniform Delay, d1 | 37.2 | 34.0 | 33.8 | 35.8 | 32.5 | | 35.6 | 14.9 | | 36.3 | 14.5 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 4.2 | 0.3 | 0.2 | 7.6 | 0.7 | | 3.7 | 1.7 | | 8.8 | 1.3 | |
| Delay (s) | 41.4 | 34.2 | 34.0 | 43.4 | 33.2 | | 39.4 | 16.6 | | 45.2 | 15.8 | |
| Level of Service | D | C | C | D | C | | D | B | | D | B | |
| Approach Delay (s) | | 36.8 | | | 37.9 | | | 18.5 | | | 18.7 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 21.6 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 83.2 | | | Sum of lost time (s) | | | | 12.0 | | |
| Intersection Capacity Utilization | | | 63.0% | | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

17: Laurel Road & Tree Line Way






















Antioch Davidon Homes TIA
2025 With Project PM Peak Hour

| | | | | | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  | |  |  | |  |  | |
| Sign Control | Free | | | Free | | | Stop | | | Stop | | |
| Grade | 0% | | | 0% | | | 0% | | | 0% | | |
| Volume (veh/h) | 20 | 890 | 14 | 35 | 1322 | 50 | 8 | 0 | 21 | 25 | 0 | 20 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Hourly flow rate (vph) | 20 | 890 | 14 | 35 | 1322 | 50 | 8 | 0 | 21 | 25 | 0 | 20 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | None | | | | | | None | | | | | |
| Median storage veh | | | | | | | | | | | | |
| Upstream signal (ft) | 988 | | | 1304 | | | | | | | | |
| pX, platoon unblocked | 0.78 | | | 0.91 | | | 0.83 | 0.83 | 0.91 | 0.83 | 0.83 | 0.78 |
| vC, conflicting volume | 1372 | | | 904 | | | 1688 | 2379 | 452 | 1923 | 2361 | 686 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 1200 | | | 790 | | | 1286 | 2117 | 291 | 1569 | 2095 | 326 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 96 | | | 95 | | | 91 | 100 | 97 | 55 | 100 | 96 |
| cM capacity (veh/h) | 453 | | | 748 | | | 91 | 38 | 639 | 56 | 39 | 526 |
| Direction, Lane # | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | NB 2 | SB 1 | SB 2 | | |
| Volume Total | 20 | 593 | 311 | 35 | 881 | 491 | 8 | 21 | 25 | 20 | | |
| Volume Left | 20 | 0 | 0 | 35 | 0 | 0 | 8 | 0 | 25 | 0 | | |
| Volume Right | 0 | 0 | 14 | 0 | 0 | 50 | 0 | 21 | 0 | 20 | | |
| cSH | 453 | 1700 | 1700 | 748 | 1700 | 1700 | 91 | 639 | 56 | 526 | | |
| Volume to Capacity | 0.04 | 0.35 | 0.18 | 0.05 | 0.52 | 0.29 | 0.09 | 0.03 | 0.45 | 0.04 | | |
| Queue Length 95th (ft) | 3 | 0 | 0 | 4 | 0 | 0 | 7 | 3 | 42 | 3 | | |
| Control Delay (s) | 13.3 | 0.0 | 0.0 | 10.0 | 0.0 | 0.0 | 48.5 | 10.8 | 113.0 | 12.1 | | |
| Lane LOS | B | | | B | | | E | B | F | B | | |
| Approach Delay (s) | 0.3 | | | 0.2 | | | 21.2 | | 68.1 | | | |
| Approach LOS | | | | | | | C | | F | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | 1.8 | | | | | | | | | | | |
| Intersection Capacity Utilization | 52.9% | | | ICU Level of Service | | | A | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |
| | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

18: Laurel Road & Hillcrest Avenue

Antioch Davidon Homes TIA
2025 With Project PM Peak Hour























| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | | 1.00 | 0.95 | |
| Frt | 1.00 | 0.91 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.97 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1701 | | 1770 | 1863 | 1583 | 1770 | 3417 | | 1770 | 3436 | |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1770 | 1701 | | 1770 | 1863 | 1583 | 1770 | 3417 | | 1770 | 3436 | |
| Volume (vph) | 140 | 80 | 110 | 350 | 120 | 250 | 90 | 970 | 290 | 290 | 910 | 220 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 140 | 80 | 110 | 350 | 120 | 250 | 90 | 970 | 290 | 290 | 910 | 220 |
| RTOR Reduction (vph) | 0 | 46 | 0 | 0 | 0 | 200 | 0 | 21 | 0 | 0 | 15 | 0 |
| Lane Group Flow (vph) | 140 | 145 | 0 | 350 | 120 | 50 | 90 | 1239 | 0 | 290 | 1115 | 0 |
| Turn Type | Prot | | | Prot | | Perm | Prot | | | Prot | | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 8 | | | | | | | | | | | |
| Actuated Green, G (s) | 14.0 | 15.0 | | 23.0 | 24.0 | 24.0 | 8.7 | 49.0 | | 17.0 | 57.3 | |
| Effective Green, g (s) | 14.0 | 15.0 | | 23.0 | 24.0 | 24.0 | 8.7 | 49.0 | | 17.0 | 57.3 | |
| Actuated g/C Ratio | 0.12 | 0.12 | | 0.19 | 0.20 | 0.20 | 0.07 | 0.41 | | 0.14 | 0.48 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 207 | 213 | | 339 | 373 | 317 | 128 | 1395 | | 251 | 1641 | |
| v/s Ratio Prot | 0.08 | c0.08 | | c0.20 | 0.06 | | 0.05 | c0.36 | | c0.16 | 0.32 | |
| v/s Ratio Perm | 0.03 | | | | | | | | | | | |
| v/c Ratio | 0.68 | 0.68 | | 1.03 | 0.32 | 0.16 | 0.70 | 0.89 | | 1.16 | 0.68 | |
| Uniform Delay, d1 | 50.8 | 50.2 | | 48.5 | 41.0 | 39.7 | 54.4 | 33.0 | | 51.5 | 24.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 8.4 | 8.3 | | 57.5 | 0.5 | 0.2 | 16.1 | 8.7 | | 105.3 | 2.3 | |
| Delay (s) | 59.3 | 58.5 | | 106.0 | 41.5 | 39.9 | 70.4 | 41.7 | | 156.8 | 26.5 | |
| Level of Service | E | E | | F | D | D | E | D | | F | C | |
| Approach Delay (s) | 58.8 | | | 72.3 | | | 43.6 | | | 53.1 | | |
| Approach LOS | E | | | E | | | D | | | D | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 53.9 | HCM Level of Service | | | D | | | | | |
| HCM Volume to Capacity ratio | | | 0.93 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sum of lost time (s) | | | 16.0 | | | | | |
| Intersection Capacity Utilization | | | 95.8% | ICU Level of Service | | | F | | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Mitigation

HCM Signalized Intersection Capacity Analysis

14: Lone Tree Way & Hillcrest Drive























Antioch Davidon Homes TIA
2025 With Project AM Peak Hour Mitigated

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|---|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5058 | | 1770 | 5085 | 1583 | 1770 | 3256 | | 3433 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5058 | | 1770 | 5085 | 1583 | 1770 | 3256 | | 3433 | 1863 | 1583 |
| Volume (vph) | 290 | 810 | 30 | 40 | 1310 | 400 | 80 | 70 | 80 | 380 | 40 | 470 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 290 | 810 | 30 | 40 | 1310 | 400 | 80 | 70 | 80 | 380 | 40 | 470 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 190 | 0 | 73 | 0 | 0 | 0 | 383 |
| Lane Group Flow (vph) | 290 | 838 | 0 | 40 | 1310 | 210 | 80 | 77 | 0 | 380 | 40 | 87 |
| Turn Type | Prot | | | Prot | | Perm | Split | | | Split | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 8 | 8 | | 4 | 4 | |
| Permitted Phases | | | | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 11.0 | 68.4 | | 5.6 | 63.0 | 63.0 | 10.3 | 10.3 | | 19.7 | 19.7 | 19.7 |
| Effective Green, g (s) | 11.0 | 68.4 | | 5.6 | 63.0 | 63.0 | 10.3 | 10.3 | | 19.7 | 19.7 | 19.7 |
| Actuated g/C Ratio | 0.09 | 0.57 | | 0.05 | 0.52 | 0.52 | 0.09 | 0.09 | | 0.16 | 0.16 | 0.16 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 315 | 2883 | | 83 | 2670 | 831 | 152 | 279 | | 564 | 306 | 260 |
| v/s Ratio Prot | c0.08 | 0.17 | | 0.02 | c0.26 | | c0.05 | 0.02 | | c0.11 | 0.02 | |
| v/s Ratio Perm | | | | | | 0.13 | | | | | | 0.06 |
| v/c Ratio | 0.92 | 0.29 | | 0.48 | 0.49 | 0.25 | 0.53 | 0.28 | | 0.67 | 0.13 | 0.34 |
| Uniform Delay, d1 | 54.1 | 13.3 | | 55.8 | 18.2 | 15.6 | 52.5 | 51.4 | | 47.1 | 42.8 | 44.4 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 31.0 | 0.3 | | 4.4 | 0.6 | 0.7 | 3.3 | 0.5 | | 3.2 | 0.2 | 0.8 |
| Delay (s) | 85.0 | 13.6 | | 60.1 | 18.9 | 16.3 | 55.8 | 51.9 | | 50.3 | 43.0 | 45.1 |
| Level of Service | F | B | | E | B | B | E | D | | D | D | D |
| Approach Delay (s) | | 31.9 | | | 19.2 | | | 53.2 | | | 47.2 | |
| Approach LOS | | C | | | B | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 31.0 | | | HCM Level of Service | | | | C | | |
| HCM Volume to Capacity ratio | | | 0.57 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | Sum of lost time (s) | | | 16.0 | | | |
| Intersection Capacity Utilization | | | 68.8% | | | ICU Level of Service | | | C | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

14: Lone Tree Way & Hillcrest Drive

Antioch Davidon Homes TIA
2025 With Project PM Peak Hour Mitigated

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  | |  |  |  |  |  | |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | | 0.97 | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 3433 | 5051 | | 1770 | 5085 | 1583 | 1770 | 3294 | | 3433 | 1863 | 1583 |
| Flt Permitted | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 3433 | 5051 | | 1770 | 5085 | 1583 | 1770 | 3294 | | 3433 | 1863 | 1583 |
| Volume (vph) | 710 | 1680 | 80 | 100 | 1210 | 480 | 50 | 70 | 60 | 580 | 120 | 450 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 710 | 1680 | 80 | 100 | 1210 | 480 | 50 | 70 | 60 | 580 | 120 | 450 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 0 | 267 | 0 | 56 | 0 | 0 | 0 | 353 |
| Lane Group Flow (vph) | 710 | 1757 | 0 | 100 | 1210 | 213 | 50 | 74 | 0 | 580 | 120 | 97 |
| Turn Type | Prot | | | Prot | | Perm | Prot | | | Prot | | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 3 | 8 | | 7 | 4 | |
| Permitted Phases | | | | | | 6 | | | | | | 4 |
| Actuated Green, G (s) | 23.0 | 69.3 | | 7.0 | 53.3 | 53.3 | 6.3 | 8.7 | | 19.0 | 21.4 | 21.4 |
| Effective Green, g (s) | 23.0 | 69.3 | | 7.0 | 53.3 | 53.3 | 6.3 | 8.7 | | 19.0 | 21.4 | 21.4 |
| Actuated g/C Ratio | 0.19 | 0.58 | | 0.06 | 0.44 | 0.44 | 0.05 | 0.07 | | 0.16 | 0.18 | 0.18 |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 658 | 2917 | | 103 | 2259 | 703 | 93 | 239 | | 544 | 332 | 282 |
| v/s Ratio Prot | c0.21 | c0.35 | | 0.06 | 0.24 | | 0.03 | 0.02 | | c0.17 | c0.06 | |
| v/s Ratio Perm | | | | | | 0.13 | | | | | | 0.06 |
| v/c Ratio | 1.08 | 0.60 | | 0.97 | 0.54 | 0.30 | 0.54 | 0.31 | | 1.07 | 0.36 | 0.34 |
| Uniform Delay, d1 | 48.5 | 16.4 | | 56.4 | 24.3 | 21.4 | 55.4 | 52.8 | | 50.5 | 43.3 | 43.1 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 58.3 | 0.9 | | 79.0 | 0.9 | 1.1 | 5.9 | 0.7 | | 57.4 | 0.7 | 0.7 |
| Delay (s) | 106.8 | 17.4 | | 135.4 | 25.2 | 22.5 | 61.3 | 53.6 | | 107.9 | 44.0 | 43.9 |
| Level of Service | F | B | | F | C | C | E | D | | F | D | D |
| Approach Delay (s) | | 43.1 | | | 30.7 | | | 55.7 | | | 76.2 | |
| Approach LOS | | D | | | C | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 46.3 | | | | | | | | | | |
| HCM Volume to Capacity ratio | | 0.74 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 120.0 | | | | | | | | | | |
| Intersection Capacity Utilization | | 77.4% | | | | | | | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

APPENDIX C:
CCTALOS Calculation worksheets

Existing

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #8 Lone Tree Way/Canada Valley Road
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.382
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        37          Level of Service:          A
*****
Street Name:          Canada Valley Road          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Protected          Protected          Protected          Protected
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    0    1    1          1    0    1    0    1          1    0    3    0    1          2    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:           36    14    51          190    31    34          29    746    52          166    1005    168
Growth Adj:         1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00
Initial Bse:         36    14    51          190    31    34          29    746    52          166    1005    168
User Adj:           1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00
PHF Adj:            0.90    0.90    0.90          0.90    0.90    0.90          0.90    0.90    0.90          0.90    0.90    0.90
PHF Volume:         40    16    57          211    34    38          32    829    58          184    1117    187
Reduct Vol:         0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:        40    16    57          211    34    38          32    829    58          184    1117    187
RTOR Reduct:        0    0    57          0    0    32          0    0    22          0    0    187
RTOR Vol:           40    16    0          211    34    6          32    829    36          184    1117    0
PCE Adj:            1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00
MLF Adj:            1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00          1.00    1.00    1.00
Final Volume:        40    16    0          211    34    6          32    829    36          184    1117    0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:           1650    1650    1650          1650    1650    1650          1650    1650    1650          1650    1650    1650
Adjustment:         0.91    1.00    0.91          1.00    1.00    1.00          1.00    1.00    1.00          0.91    1.00    1.00
Lanes:              2.00    1.00    1.00          1.00    1.00    1.00          1.00    3.00    1.00          2.00    3.00    1.00
Final Sat.:         3000    1650    1500          1650    1650    1650          1650    4950    1650          3000    4950    1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:            0.01    0.01    0.00          0.13    0.02    0.00          0.02    0.17    0.02          0.06    0.23    0.00
Crit Volume:         16          211          32          372
Crit Moves:          ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #9 Lone Tree Way/SB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.513
Loss Time (sec):    0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     47      Level of Service:      A
*****
Street Name:      SB SR 4 Bypass Ramps      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Protected      Protected
Rights:           Include      Include      Include      Include
Min. Green:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:            0 0 0 0 0      1 1 0 0 1      0 0 3 0 1      2 0 3 0 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         0 0 0 0      287 6 353      0 571 401      72 1000 0
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      0 0 0 0      287 6 353      0 571 401      72 1000 0
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:       0 0 0 0      319 7 392      0 634 446      80 1111 0
Reduct Vol:       0 0 0 0      0 0 0      0 0 0      0 0 0
Reduced Vol:      0 0 0 0      319 7 392      0 634 446      80 1111 0
RTOR Reduct:      0 0 0 0      0 0 0      0 0 0      0 0 0
RTOR Vol:         0 0 0 0      319 7 392      0 634 446      80 1111 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      0 0 0 0      319 7 392      0 634 446      80 1111 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:       1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:            0.00 0.00 0.00 1.96 0.04 1.00 0.00 3.00 1.00 2.00 3.00 0.00
Final Sat.:       0 0 0 0      3063 70 1720      0 5160 1720 3127 5160 0
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.00 0.00 0.00 0.10 0.09 0.23 0.00 0.12 0.26 0.03 0.22 0.00
Crit Volume:      0      392      446 40
Crit Moves:      ****      **** ****
*****

```


Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #10 Lone Tree Way/NB SR 4 Bypass Ramps
*****
Cycle (sec):      100          Critical vol./Cap.(X):      0.308
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     33          Level of Service:      A
*****
Street Name:      NB SR 4 Bypass Ramps          Lone Tree Way
Approach:         North Bound          South Bound          East Bound          West Bound
Movement:         L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:          Split Phase          Split Phase          Protected          Protected
Rights:           Include              Include              Include              Include
Min. Green:       0    0    0          0    0    0          0    0    0          0    0    0
Lanes:            1    1    0    0    1    0    0    0    0    0    0    3    0    1    1    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 13 May 2008 << 7:30 - 8:30 AM
Base Vol:        383    29    79          0    0    0          0    662    160          8    671    245
Growth Adj:      1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Initial Bse:     383    29    79          0    0    0          0    662    160          8    671    245
User Adj:        1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
PHF Adj:         0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89
PHF Volume:      430    33    89          0    0    0          0    744    180          9    754    275
Reduct Vol:      0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:     430    33    89          0    0    0          0    744    180          9    754    275
RTOR Reduct:     0    0    9          0    0    0          0    0    180          0    0    0
RTOR Vol:        430    33    80          0    0    0          0    744    0          9    754    275
PCE Adj:         1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
MLF Adj:         1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
FinalVolume:     430    33    80          0    0    0          0    744    0          9    754    275
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720
Adjustment:      0.91  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Lanes:           1.86  0.14  1.00  0.00  0.00  0.00  0.00  3.00  1.00  1.00  3.00  1.00  1.00
Final Sat.:      2907  242  1720          0    0    0          0  5160  1720  1720  5160  1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.15  0.13  0.05  0.00  0.00  0.00  0.00  0.14  0.00  0.01  0.15  0.16
Crit Volume:     231          0          0          0          275
Crit Moves:      ****          ****          ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #11 Lone Tree Way/Slatten Ranch Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.461
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    42      Level of Service:      A
*****
Street Name:      Slatten Ranch Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    1    0      2    0    1    0    1      2    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 7:15 - 8:15 AM
Base Vol:         39    47    191      42    35    24      74    484    91      54    837    29
Growth Adj:       1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:      39    47    191      42    35    24      74    484    91      54    837    29
User Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90      0.90 0.90 0.90      0.90 0.90 0.90      0.90 0.90 0.90
PHF Volume:       43    52    212      47    39    27      82    538    101     60    930    32
Reduct Vol:       0     0     0        0     0     0        0     0     0        0     0     0
Reduced Vol:      43    52    212      47    39    27      82    538    101     60    930    32
RTOR Reduct:      0     0     0        0     0     27       0     0     24       0     0     26
RTOR Vol:         43    52    212      47    39     0      82    538    77      60    930     7
PCE Adj:          1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Final Volume:     43    52    212      47    39     0      82    538    77      60    930     7
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650      1650 1650 1650      1650 1650 1650      1650 1650 1650
Adjustment:       0.91 1.00 1.00      0.91 1.00 1.00      0.91 1.00 1.00      1.00 1.00 1.00
Lanes:           2.00 1.00 1.00      2.00 1.00 1.00      2.00 3.00 1.00      1.00 2.00 1.00
Final Sat.:      3000 1650 1650      3000 1650 1650      3000 4950 1650      1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.01 0.03 0.13      0.02 0.02 0.00      0.03 0.11 0.05      0.04 0.28 0.00
Crit Volume:      212          39          41          465
Crit Moves:      ****          ****          ****          ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #12 Lone Tree Way/Empire Avenue
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.483
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        44          Level of Service:          A
*****
Street Name:          Empire Avenue          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|-----|-----|
Control:               Split Phase          Split Phase          Protected          Protected
Rights:                Include              Include              Include              Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    1    0    1    2    0    1    1    0    1    0    3    0    1    1    0    2    0    1
-----|-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 7:15 - 8:15 AM
Base Vol:             89    48    41    105    77    181    168    499    26    81    638    80
Growth Adj:           1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:           89    48    41    105    77    181    168    499    26    81    638    80
User Adj:             1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:              0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:           99    53    46    117    86    201    187    554    29    90    709    89
Reduct Vol:           0    0    0    0    0    0    0    0    0    0    0    0
Reduced Vol:          99    53    46    117    86    201    187    554    29    90    709    89
RTOR Reduct:          0    0    46    0    0    0    0    0    29    0    0    64
RTOR Vol:             99    53    0    117    86    201    187    554    0    90    709    25
PCE Adj:              1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:              1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Final Volume:         99    53    0    117    86    201    187    554    0    90    709    25
-----|-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:             1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:           0.91 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:                2.00 1.00 1.00 2.00 1.00 1.00 1.00 3.00 1.00 1.00 2.00 1.00
Final Sat.:           3000 1650 1650 3000 1650 1650 1650 4950 1650 1650 3300 1650
-----|-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:              0.03 0.03 0.00 0.04 0.05 0.12 0.11 0.11 0.00 0.05 0.21 0.01
Crit Volume:          49          201    187          354
Crit Moves:          ****          ****    ****          ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #13 Lone Tree Way/Deer Valley Road
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.707
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        78          Level of Service:          C
*****
Street Name:          Deer Valley Road          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Protected          Protected          Protected          Protected
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    1    1    0          1    0    1    1    0          1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 PM
Base Vol:   279  245  111  353  457  17  35  644  157  185  833  185
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 279  245  111  353  457  17  35  644  157  185  833  185
User Adj:   1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:    0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89
PHF Volume: 313  275  125  397  513  19  39  724  176  208  936  208
Reduct Vol:  0    0    0    0    0    0    0    0    0    0    0    0
Reduced Vol: 313  275  125  397  513  19  39  724  176  208  936  208
RTOR Reduct:  0    0    0    0    0    0    0    0    172  0    0    208
RTOR Vol:    313  275  125  397  513  19  39  724  4    208  936  0
PCE Adj:     1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:     1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 313  275  125  397  513  19  39  724  4    208  936  0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:    1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:       2.00 1.38 0.62 1.00 1.93 0.07 1.00 2.00 1.00 1.00 2.00 1.00
Final Sat.: 3000 2271 1029 1650 3182 118 1650 3300 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:     0.10 0.12 0.12 0.24 0.16 0.16 0.02 0.22 0.00 0.13 0.28 0.00
Crit Volume: 200          397          362          208
Crit Moves:  ****          ****          ****          ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #14 Lone Tree Way/Hillcrest Avenue
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.440
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        41          Level of Service:          A
*****
Street Name:          Hillcrest Avenue          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Split Phase          Split Phase          Protected          Protected
Rights:                Include              Include              Include              Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 1  0  1  1  0          1  1  1  0  1          1  0  2  0  1          1  0  3  0  1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:             36   53   13   279   85   269   177   495   18   24   862   160
Growth Adj:           1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:           36   53   13   279   85   269   177   495   18   24   862   160
User Adj:              1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:               0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:            40   59   14   310   94   299   197   550   20   27   958   178
Reduct Vol:            0    0    0    0    0    0    0    0    0    0    0    0
Reduced Vol:           40   59   14   310   94   299   197   550   20   27   958   178
RTOR Reduct:           0    0    0    0    0    197   0    0    20   0    0    171
RTOR Vol:              40   59   14   310   94   102   197   550   0    27   958   7
PCE Adj:               1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:               1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:           40   59   14   310   94   102   197   550   0    27   958   7
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:              1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:            1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:                 1.00 1.61 0.39 2.00 1.00 1.00 1.00 2.00 1.00 1.00 3.00 1.00
Final Sat.:            1650 2650 650 3000 1650 1650 1650 3300 1650 1650 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:               0.02 0.02 0.02 0.10 0.06 0.06 0.12 0.17 0.00 0.02 0.19 0.00
Crit Volume:           40          155          197          319
Crit Moves:           ****          ****          ****          ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #15 Lone Tree Way/Vista Grande Drive
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.322
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    27      Level of Service:      A
*****
Street Name:      Vista Grande Drive      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Permitted      Permitted      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             1 0 0 1 0      1 0 0 1 0      1 0 2 1 0      1 0 2 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 8:00 - 9:00 PM
Base Vol:         39 14 123      24 16 41      20 693 30      59 967 37
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      39 14 123      24 16 41      20 693 30      59 967 37
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93
PHF Volume:       42 15 132      26 17 44      22 745 32      63 1040 40
Reduct Vol:       0 0 0      0 0 0      0 0 0      0 0 0
Reduced Vol:      42 15 132      26 17 44      22 745 32      63 1040 40
RTOR Reduct:      0 0 0      0 0 0      0 0 0      0 0 0
RTOR Vol:         42 15 132      26 17 44      22 745 32      63 1040 40
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      42 15 132      26 17 44      22 745 32      63 1040 40
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:           1.00 0.10 0.90 1.00 0.28 0.72 1.00 2.88 0.12 1.00 2.89 0.11
Final Sat.:       1720 176 1544 1720 483 1237 1720 4946 214 1720 4970 190
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.02 0.09 0.09 0.02 0.04 0.04 0.01 0.15 0.15 0.04 0.21 0.21
Crit Volume:      147      26      22      360
Crit Moves:       ****      ****      ****      ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #16 Country Hills Drive/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.444
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    41      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Country Hills Drive
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Split Phase      Split Phase
Rights:            Include      Include      Include      Include
Min. Green:        0  0  0      0  0  0      0  0  0      0  0  0
Lanes:             1  0  1  1  0      1  0  1  1  0      1  0  0  1  0      1  0  0  1  0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         70  297  31      63  439  26      44  77  143      84  93  117
Growth Adj:        1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
Initial Bse:       70  297  31      63  439  26      44  77  143      84  93  117
User Adj:          0.83 0.83  0.83  0.83 0.83  0.83  0.83 0.83  0.83  0.83 0.83  0.83
PHF Adj:           0.83 0.83  0.83  0.83 0.83  0.83  0.83 0.83  0.83  0.83 0.83  0.83
PHF Volume:        70  297  31      63  439  26      44  77  143      84  93  117
Reduct Vol:        0  0  0      0  0  0      0  0  0      0  0  0
Reduced Vol:       70  297  31      63  439  26      44  77  143      84  93  117
RTOR Reduct:       0  0  0      0  0  0      0  0  0      0  0  0
RTOR Vol:          70  297  31      63  439  26      44  77  143      84  93  117
PCE Adj:           1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
MLF Adj:           1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
Final Volume:      70  297  31      63  439  26      44  77  143      84  93  117
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:          1650 1650  1650  1650 1650  1650 1650  1650  1650 1650  1650
Adjustment:        1.00 1.00  1.00  1.00 1.00  1.00 1.00  1.00  1.00 1.00  1.00
Lanes:             1.00 1.81  0.19  1.00 1.89  0.11  1.00 0.35  0.65  1.00 0.44  0.56
Final Sat.:        1650 2988  312  1650 3115  185  1650  578  1073  1650  731  919
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:           0.04 0.10  0.10  0.04 0.14  0.14  0.03 0.13  0.13  0.05 0.13  0.13
Crit Volume:       70      233      220      210
Crit Moves:        ****      ****      ****      ****
*****

```


Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #18 Laurell/Hillcrest
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.344
Loss Time (sec):    0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     28      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Laurell Road
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Permitted      Permitted
Rights:           Ignore      Include      Include      Include
Min. Green:       0  0  0      0  0  0      0  0  0      0  0  0
Lanes:           1  0  2  0  1      1  0  1  1  0      1  0  0  1  0      1  0  1  0  1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:        67  372  25      74  377  80      150  50  100      48  67  155
Growth Adj:      1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
Initial Bse:     67  372  25      74  377  80      150  50  100      48  67  155
User Adj:        1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
PHF Adj:         0.89 0.89  0.89  0.89 0.89  0.89  0.89 0.89  0.89  0.89 0.89  0.89
PHF Volume:      75  418  28      83  424  90      169  56  112      54  75  174
Reduct Vol:      0  0  0      0  0  0      0  0  0      0  0  0
Reduced Vol:     75  418  28      83  424  90      169  56  112      54  75  174
RTOR Reduct:     0  0  0      0  0  0      0  0  0      0  0  83
RTOR Vol:        75  418  28      83  424  90      169  56  112      54  75  91
PCE Adj:         1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
MLF Adj:         1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00  1.00 1.00  1.00
FinalVolume:     75  418  28      83  424  90      169  56  112      54  75  91
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720 1720  1720  1720 1720  1720 1720 1720  1720 1720 1720
Adjustment:      1.00 1.00  1.00  1.00 1.00  1.00 1.00 1.00  1.00 1.00 1.00
Lanes:           1.00 2.00  1.00  1.00 1.65  0.35 1.00 0.33  0.67  1.00 1.00  1.00
Final Sat.:      1720 3440  1720  1720 2838  602 1720  573  1147  1720 1720  1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.04 0.12  0.02  0.05 0.15  0.15 0.10 0.10  0.10  0.03 0.04  0.05
Crit Volume:      75      257      169      91
Crit Moves:      ****      ****      ****      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #8 Lone Tree Way/Canada Valley Road
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.544
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        50          Level of Service:          A
*****
Street Name:          Canada Valley Road          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|-----|-----|
Control:               Protected          Protected          Protected          Protected
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    0    1    1          1    0    1    0    1          1    0    3    0    1          2    0    3    0    1
-----|-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:            84    55    173          175    56    22          54 1354    55          329 942    253
Growth Adj:          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:          84    55    173          175    56    22          54 1354    55          329 942    253
User Adj:             1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
PHF Adj:              0.96 0.96 0.96          0.96 0.96 0.96          0.96 0.96 0.96          0.96 0.96 0.96
PHF Volume:           88    57    180          182    58    23          56 1410    57          343 981    264
Reduct Vol:           0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:          88    57    180          182    58    23          56 1410    57          343 981    264
RTOR Reduct:          0    0    180          0    0    23          0    0    48          0    0    182
RTOR Vol:             88    57    0          182    58    0          56 1410    9          343 981    81
PCE Adj:              1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:              1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Final Volume:          88    57    0          182    58    0          56 1410    9          343 981    81
-----|-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:             1650 1650 1650          1650 1650 1650          1650 1650 1650          1650 1650 1650
Adjustment:           0.91 1.00 0.91          1.00 1.00 1.00          1.00 1.00 1.00          0.91 1.00 1.00
Lanes:                2.00 1.00 1.00          1.00 1.00 1.00          1.00 3.00 1.00          2.00 3.00 1.00
Final Sat.:           3000 1650 1500          1650 1650 1650          1650 4950 1650          3000 4950 1650
-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:              0.03 0.03 0.00          0.11 0.04 0.00          0.03 0.28 0.01          0.11 0.20 0.05
Crit Volume:           57          182          470          171
Crit Moves:           ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #9 Lone Tree Way/SB SR 4 Bypass Ramps
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.585
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        55          Level of Service:          A
*****
Street Name:          SB SR 4 Bypass Ramps          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|
Control:               Protected          Protected          Protected          Protected
Rights:                Include          Include          Include          Include
Min. Green:            0 0 0 0          0 0 0 0          0 0 0 0          0 0 0 0
Lanes:                 0 0 0 0 0          1 1 0 0 1          0 0 3 0 1          2 0 3 0 0
-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:30 - 5:30 PM
Base Vol:              0 0 0          416 10 361          0 1169 541          98 1153 0
Growth Adj:            1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:           0 0 0          416 10 361          0 1169 541          98 1153 0
User Adj:              1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:               0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95
PHF Volume:            0 0 0          438 11 380          0 1231 569          103 1214 0
Reduct Vol:            0 0 0          0 0 0          0 0 0          0 0 0
Reduced Vol:           0 0 0          438 11 380          0 1231 569          103 1214 0
RTOR Reduct:           0 0 0          0 0 0          0 0 0          0 0 0
RTOR Vol:              0 0 0          438 11 380          0 1231 569          103 1214 0
PCE Adj:               1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:               1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:           0 0 0          438 11 380          0 1231 569          103 1214 0
-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:              1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:            1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:                 0.00 0.00 0.00 1.95 0.05 1.00 0.00 3.00 1.00 2.00 3.00 0.00
Final Sat.:            0 0 0          3054 81 1720          0 5160 1720          3127 5160 0
-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:               0.00 0.00 0.00 0.14 0.13 0.22 0.00 0.24 0.33 0.03 0.24 0.00
Crit Volume:           0          380          569          52
Crit Moves:            *****          *****          *****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #10 Lone Tree Way/NB SR 4 Bypass Ramps
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.481
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        44          Level of Service:          A
*****
Street Name:          NB SR 4 Bypass Ramps          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|-----|-----|
Control:              Split Phase          Split Phase          Protected          Protected
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 1    1    0    0    1          0    0    0    0    0          0    0    3    0    1          1    0    3    0    1
-----|-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 13 May 2008 << 4:45 - 5:45 PM
Base Vol:   437   43   137           0    0    0          0 1404   264          21   831   357
Growth Adj: 1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse: 437   43   137           0    0    0          0 1404   264          21   831   357
User Adj:   1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
PHF Adj:    0.91 0.91 0.91          0.91 0.91 0.91          0.91 0.91 0.91          0.91 0.91 0.91
PHF Volume:  480   47   151           0    0    0          0 1543   290          23   913   392
Reduct Vol:   0    0    0           0    0    0          0    0    0          0    0    0
Reduced Vol:  480   47   151           0    0    0          0 1543   290          23   913   392
RTOR Reduct:  0    0    23           0    0    0          0    0    264          0    0    0
RTOR Vol:    480   47   127           0    0    0          0 1543   26          23   913   392
PCE Adj:     1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:     1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Final Volume: 480   47   127           0    0    0          0 1543   26          23   913   392
-----|-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:    1720 1720 1720          1720 1720 1720          1720 1720 1720          1720 1720 1720
Adjustment:  0.91 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Lanes:       1.82 0.18 1.00          0.00 0.00 0.00          0.00 3.00 1.00          1.00 3.00 1.00
Final Sat.:  2847 308 1720           0    0    0          0 5160 1720          1720 5160 1720
-----|-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:     0.17 0.15 0.07          0.00 0.00 0.00          0.00 0.30 0.02          0.01 0.18 0.23
Crit Volume: 264                      0                      514                      23
Crit Moves:  ****                      ****                      ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #11 Lone Tree Way/Slatten Ranch Road
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.487
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        44          Level of Service:          A
*****
Street Name:          Slatten Ranch Road          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|
Control:               Split Phase          Split Phase          Protected          Protected
Rights:                Include              Include              Include              Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    1    1    0          2    0    1    0    1          2    0    3    0    1          1    0    2    0    1
-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 5:00 - 6:00 PM
Base Vol:             51    76    167          114    67    101          217    892    256          160    803    55
Growth Adj:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:           51    76    167          114    67    101          217    892    256          160    803    55
User Adj:              1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
PHF Adj:               0.94 0.94 0.94          0.94 0.94 0.94          0.94 0.94 0.94          0.94 0.94 0.94
PHF Volume:            54    81    178          121    71    107          231    949    272          170    854    59
Reduct Vol:            0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:           54    81    178          121    71    107          231    949    272          170    854    59
RTOR Reduct:           0    0    0          0    0    107          0    0    30          0    0    59
RTOR Vol:              54    81    178          121    71    0          231    949    242          170    854    0
PCE Adj:               1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:               1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
FinalVolume:           54    81    178          121    71    0          231    949    242          170    854    0
-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:              1650 1650 1650          1650 1650 1650          1650 1650 1650          1650 1650 1650
Adjustment:            0.91 1.00 1.00          0.91 1.00 1.00          0.91 1.00 1.00          1.00 1.00 1.00
Lanes:                 2.00 1.00 1.00          2.00 1.00 1.00          2.00 3.00 1.00          1.00 2.00 1.00
Final Sat.:            3000 1650 1650          3000 1650 1650          3000 4950 1650          1650 3300 1650
-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:               0.02 0.05 0.11          0.04 0.04 0.00          0.08 0.19 0.15          0.10 0.26 0.00
Crit Volume:           178          71          115          427
Crit Moves:            ****          ****          ****          ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #12 Lone Tree Way/Empire Avenue
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.497
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        45          Level of Service:          A
*****
Street Name:          Empire Avenue          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|
Control:               Split Phase          Split Phase          Protected          Protected
Rights:                Include              Include              Include              Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    1    0    1    2    0    1    1    0    1    0    3    0    1    1    0    2    0    1
-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 5:00 - 6:00 PM
Base Vol:           76    46    36    231    115    176    230    759    112    53    702    129
Growth Adj:         1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Initial Bse:        76    46    36    231    115    176    230    759    112    53    702    129
User Adj:           1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
PHF Adj:            0.98  0.98  0.98  0.98  0.98  0.98  0.98  0.98  0.98  0.98  0.98  0.98
PHF Volume:         78    47    37    236    117    180    235    774    114    54    716    132
Reduct Vol:         0     0     0     0     0     0     0     0     0     0     0     0
Reduced Vol:        78    47    37    236    117    180    235    774    114    54    716    132
RTOR Reduct:        0     0     37     0     0     0     0     0     43     0     0    130
RTOR Vol:           78    47     0    236    117    180    235    774     72    54    716     2
PCE Adj:            1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
MLF Adj:            1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
FinalVolume:        78    47     0    236    117    180    235    774     72    54    716     2
-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:           1650  1650  1650  1650  1650  1650  1650  1650  1650  1650  1650  1650
Adjustment:         0.91  1.00  1.00  0.91  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Lanes:              2.00  1.00  1.00  2.00  1.00  1.00  1.00  3.00  1.00  1.00  2.00  1.00
Final Sat.:         3000  1650  1650  3000  1650  1650  1650  4950  1650  1650  3300  1650
-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:            0.03  0.03  0.00  0.08  0.07  0.11  0.14  0.16  0.04  0.03  0.22  0.00
Crit Volume:         47                                180    235                                358
Crit Moves:          ****                                ****    ****                                ****
*****

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Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

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*****
Intersection #13 Lone Tree Way/Deer Valley Road
*****
Cycle (sec):      100          Critical vol./Cap.(X):      0.609
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     58          Level of Service:      B
*****
Street Name:      Deer Valley Road      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Protected      Protected
Rights:           Include      Include      Include      Include
Min. Green:       0    0    0      0    0    0      0    0    0      0    0    0
Lanes:            2    0    1    1    0      1    0    1    1    0      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:        192  365  168      168  191  14      87  780  147      151  497  154
Growth Adj:      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:     192  365  168      168  191  14      87  780  147      151  497  154
User Adj:        1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
PHF Adj:         0.97 0.97 0.97      0.97 0.97 0.97      0.97 0.97 0.97      0.97 0.97 0.97
PHF Volume:      198  376  173      173  197  14      90  804  152      156  512  159
Reduct Vol:      0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:     198  376  173      173  197  14      90  804  152      156  512  159
RTOR Reduct:     0    0    0          0    0    0          0    0    109        0    0    159
RTOR Vol:        198  376  173      173  197  14      90  804  43      156  512  0
PCE Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
FinalVolume:     198  376  173      173  197  14      90  804  43      156  512  0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1650 1650 1650      1650 1650 1650      1650 1650 1650      1650 1650 1650
Adjustment:      0.91 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Lanes:           2.00 1.37 0.63      1.00 1.86 0.14      1.00 2.00 1.00      1.00 2.00 1.00
Final Sat.:      3000 2260 1040      1650 3075 225      1650 3300 1650      1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.07 0.17 0.17      0.10 0.06 0.06      0.05 0.24 0.03      0.09 0.16 0.00
Crit Volume:      275          173          402          156
Crit Moves:      ****          ****          ****          ****
*****

```


Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #14 Lone Tree Way/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.544
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     50      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include           Include           Include           Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             1    0    1    1    0      1    1    1    0    1      1    0    2    0    1      1    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:15 - 5:15 PM
Base Vol:        17    87    26      423    77    97      131    915    22      43    720    229
Growth Adj:      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:     17    87    26      423    77    97      131    915    22      43    720    229
User Adj:        1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
PHF Adj:         0.88 0.88 0.88      0.88 0.88 0.88      0.88 0.88 0.88      0.88 0.88 0.88
PHF Volume:      19    99    30      481    88    110      149 1040    25      49    818    260
Reduct Vol:      0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:     19    99    30      481    88    110      149 1040    25      49    818    260
RTOR Reduct:     0    0    0          0    0    110          0    0    19          0    0    260
RTOR Vol:        19    99    30      481    88    0        149 1040    6        49    818    0
PCE Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Final Volume:    19    99    30      481    88    0        149 1040    6        49    818    0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1650 1650 1650      1650 1650 1650      1650 1650 1650      1650 1650 1650
Adjustment:      1.00 1.00 1.00      0.91 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Lanes:           1.00 1.54 0.46      2.00 1.00 1.00      1.00 2.00 1.00      1.00 3.00 1.00
Final Sat.:     1650 2541 759      3000 1650 1650      1650 3300 1650      1650 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.01 0.04 0.04      0.16 0.05 0.00      0.09 0.32 0.00      0.03 0.17 0.00
Crit Volume:      64    240          520          49
Crit Moves:      ****      ****      ****      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #15 Lone Tree Way/Vista Grande Drive
*****
Cycle (sec):      100          Critical vol./Cap.(X):      0.437
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     33          Level of Service:      A
*****
Street Name:      Vista Grande Drive      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Permitted      Permitted      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             1 0 0 1 0      1 0 0 1 0      1 0 2 1 0      1 0 2 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:45 - 5:45 PM
Base Vol:         35 10 114      42 9 20      18 1282 44      121 931 24
Growth Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:       35 10 114      42 9 20      18 1282 44      121 931 24
User Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:           0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
PHF Volume:        36 10 118      43 9 21      19 1322 45      125 960 25
Reduct Vol:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Reduced Vol:       36 10 118      43 9 21      19 1322 45      125 960 25
RTOR Reduct:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
RTOR Vol:          36 10 118      43 9 21      19 1322 45      125 960 25
PCE Adj:           1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:           1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:       36 10 118      43 9 21      19 1322 45      125 960 25
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:          1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:             1.00 0.08 0.92 1.00 0.31 0.69 1.00 2.90 0.10 1.00 2.92 0.08
Final Sat.:        1720 139 1581 1720 534 1186 1720 4989 171 1720 5030 130
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:           0.02 0.07 0.07 0.03 0.02 0.02 0.01 0.26 0.26 0.07 0.19 0.19
Crit Volume:       128          43          456          125
Crit Moves:        ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #16 Country Hills Drive/Hillcrest Avenue
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.315
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        33          Level of Service:          A
*****
Street Name:          Hillcrest Avenue          Country Hills Drive
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Protected          Protected          Split Phase          Split Phase
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 1  0  1  1  0          1  0  1  1  0          1  0  0  1  0          1  0  0  1  0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:             73  281  49          89  376  63          42  51  82          34  50  45
Growth Adj:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:           73  281  49          89  376  63          42  51  82          34  50  45
User Adj:              0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92
PHF Adj:               0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92
PHF Volume:            73  281  49          89  376  63          42  51  82          34  50  45
Reduct Vol:            0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:           73  281  49          89  376  63          42  51  82          34  50  45
RTOR Reduct:           0    0    0          0    0    0          0    0    0          0    0    0
RTOR Vol:              73  281  49          89  376  63          42  51  82          34  50  45
PCE Adj:               1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:               1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Final Volume:          73  281  49          89  376  63          42  51  82          34  50  45
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:             1650 1650 1650          1650 1650 1650          1650 1650 1650          1650 1650 1650
Adjustment:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Lanes:                1.00 1.70 0.30          1.00 1.71 0.29          1.00 0.38 0.62          1.00 0.53 0.47
Final Sat.:           1650 2810 490          1650 2826 474          1650 633 1017          1650 868 782
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:              0.04 0.10 0.10          0.05 0.13 0.13          0.03 0.08 0.08          0.02 0.06 0.06
Crit Volume:           73          220          133          95
Crit Moves:          ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Base Volume Alternative)

```

*****
Intersection #18 Laurell/Hillcrest
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.219
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        24          Level of Service:          A
*****
Street Name:          Hillcrest Avenue          Laurell Road
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|-----|-----|-----|-----|
Control:               Protected          Protected          Permitted          Permitted
Rights:                Ignore          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 1  0  2  0  1          1  0  1  1  0          1  0  0  1  0          1  0  1  0  1
-----|-----|-----|-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol: 27 302 39 162 459 50 17 7 22 35 9 133
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 27 302 39 162 459 50 17 7 22 35 9 133
User Adj: 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98
PHF Adj: 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98
PHF Volume: 27 302 39 162 459 50 17 7 22 35 9 133
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 27 302 39 162 459 50 17 7 22 35 9 133
RTOR Reduct: 0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol: 27 302 39 162 459 50 17 7 22 35 9 0
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Final Volume: 27 302 39 162 459 50 17 7 22 35 9 0
-----|-----|-----|-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 1.00 2.00 1.00 1.00 1.80 0.20 1.00 0.24 0.76 1.00 1.00 1.00
Final Sat.: 1720 3440 1720 1720 3102 338 1720 415 1305 1720 1720 1720
-----|-----|-----|-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.02 0.09 0.02 0.09 0.15 0.15 0.01 0.02 0.02 0.02 0.01 0.00
Crit Volume: 151 162 29 35
Crit Moves: ****
*****

```

Near-Term No Project

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #8 Lone Tree Way/Canada Valley Road
*****
Cycle (sec):      100      Critical Vol./Cap.(X):      0.454
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    42      Level of Service:      A
*****
Street Name:      Canada Valley Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             2 0 0 1 1      1 0 1 0 1      1 0 3 0 1      2 0 3 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         36 14 51 190 31 34 29 746 52 166 1005 168
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      36 14 51 190 31 34 29 746 52 166 1005 168
Added Vol:        40 0 133 0 0 0 0 225 13 45 114 0
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      76 14 184 190 31 34 29 971 65 211 1119 168
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:       84 16 204 211 34 38 32 1079 72 234 1243 187
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      84 16 204 211 34 38 32 1079 72 234 1243 187
RTOR Reduct:      0 0 129 0 0 32 0 0 46 0 0 187
RTOR Vol:         84 16 76 211 34 6 32 1079 26 234 1243 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      84 16 76 211 34 6 32 1079 26 234 1243 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       0.91 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:            2.00 0.34 1.66 1.00 1.00 1.00 1.00 3.00 1.00 2.00 3.00 1.00
Final Sat.:       3000 564 2487 1650 1650 1650 1650 4950 1650 3000 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.03 0.03 0.03 0.13 0.02 0.00 0.02 0.22 0.02 0.08 0.25 0.00
Crit Volume:      46 211 360 117
Crit Moves:      **** **** **** ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #9 Lone Tree Way/SB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.602
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     57      Level of Service:      B
*****
Street Name:      SB SR 4 Bypass Ramps      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Protected      Protected
Rights:           Include      Include      Include      Include
Min. Green:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:           0 0 0 0 0      1 1 0 0 1      0 0 3 0 1      2 0 3 0 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:        0 0 0 0      287 6 353      0 571 401      72 1000 0
Growth Adj:      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:     0 0 0 0      287 6 353      0 571 401      72 1000 0
Added Vol:       0 0 0 0      0 0 57      0 277 82      0 102 0
PasserByVol:    0 0 0 0      0 0 0      0 0 0      0 0 0
Initial Fut:     0 0 0 0      287 6 410      0 848 483      72 1102 0
User Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:         0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:      0 0 0 0      319 7 456      0 942 537      80 1224 0
Reduct Vol:      0 0 0 0      0 0 0      0 0 0      0 0 0
Reduced Vol:     0 0 0 0      319 7 456      0 942 537      80 1224 0
RTOR Reduct:     0 0 0 0      0 0 0      0 0 0      0 0 0
RTOR Vol:        0 0 0 0      319 7 456      0 942 537      80 1224 0
PCE Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:     0 0 0 0      319 7 456      0 942 537      80 1224 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:      1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:           0.00 0.00 0.00 1.96 0.04 1.00 0.00 3.00 1.00 2.00 3.00 0.00
Final Sat.:      0 0 0 3063 70 1720      0 5160 1720 3127 5160 0
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.00 0.00 0.00 0.10 0.09 0.26 0.00 0.18 0.31 0.03 0.24 0.00
Crit Volume:     0 456 537 40
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #10 Lone Tree Way/NB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.338
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    34      Level of Service:      A
*****
Street Name:      NB SR 4 Bypass Ramps      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             1    1    0    0    1      0    0    0    0    0      0    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 13 May 2008 << 7:30 - 8:30 AM
Base Vol: 383 29 79 0 0 0 0 662 160 8 671 245
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 383 29 79 0 0 0 0 662 160 8 671 245
Added Vol: 35 0 0 0 0 0 0 130 147 0 67 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 418 29 79 0 0 0 0 792 307 8 738 245
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89
PHF Volume: 470 33 89 0 0 0 0 890 345 9 829 275
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 470 33 89 0 0 0 0 890 345 9 829 275
RTOR Reduct: 0 0 9 0 0 0 0 0 0 258 0 0 0
RTOR Vol: 470 33 80 0 0 0 0 890 87 9 829 275
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 470 33 80 0 0 0 0 890 87 9 829 275
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 1.87 0.13 1.00 0.00 0.00 0.00 0.00 3.00 1.00 1.00 3.00 1.00
Final Sat.: 2924 223 1720 0 0 0 0 5160 1720 1720 5160 1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.16 0.15 0.05 0.00 0.00 0.00 0.00 0.17 0.05 0.01 0.16 0.16
Crit Volume: 251 0 297 9
Crit Moves: ****
*****

```


Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #11 Lone Tree Way/Slatten Ranch Road
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.484
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        44          Level of Service:          A
*****
Street Name:          Slatten Ranch Road          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Split Phase          Split Phase          Protected          Protected
Rights:                Include              Include              Include              Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 2    0    1    1    0          2    0    1    0    1          2    0    3    0    1          1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 7:15 - 8:15 AM
Base Vol:             39    47    191          42    35    24          74    484    91          54    837    29
Growth Adj:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:           39    47    191          42    35    24          74    484    91          54    837    29
Added Vol:             0    0    0          0    0    0          0    130    0          0    67    0
PasserByVol:          0    0    0          0    0    0          0    0    0          0    0    0
Initial Fut:           39    47    191          42    35    24          74    614    91          54    904    29
User Adj:              1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
PHF Adj:               0.90 0.90 0.90          0.90 0.90 0.90          0.90 0.90 0.90          0.90 0.90 0.90
PHF Volume:            43    52    212          47    39    27          82    682    101          60    1004    32
Reduct Vol:            0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:           43    52    212          47    39    27          82    682    101          60    1004    32
RTOR Reduct:           0    0    0          0    0    27          0    0    24          0    0    26
RTOR Vol:              43    52    212          47    39    0          82    682    77          60    1004    7
PCE Adj:               1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:               1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Final Volume:          43    52    212          47    39    0          82    682    77          60    1004    7
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:              1650 1650 1650          1650 1650 1650          1650 1650 1650          1650 1650 1650
Adjustment:            0.91 1.00 1.00          0.91 1.00 1.00          0.91 1.00 1.00          1.00 1.00 1.00
Lanes:                 2.00 1.00 1.00          2.00 1.00 1.00          2.00 3.00 1.00          1.00 2.00 1.00
Final Sat.:            3000 1650 1650          3000 1650 1650          3000 4950 1650          1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:               0.01 0.03 0.13          0.02 0.02 0.00          0.03 0.14 0.05          0.04 0.30 0.00
Crit Volume:           212          39          41          502
Crit Moves:            ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #12 Lone Tree Way/Empire Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.573
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    53      Level of Service:      A
*****
Street Name:      Empire Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include           Include           Include           Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    0    1      2    0    1    1    0      1    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 7:15 - 8:15 AM
Base Vol:      89  48  41  105  77  181  168  499  26  81  638  80
Growth Adj:    1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:    89  48  41  105  77  181  168  499  26  81  638  80
Added Vol:      0    0    0    0    0  42  79  51  0  0  25  0
PasserByVol:    0    0    0    0    0  0  0  0  0  0  0  0
Initial Fut:    89  48  41  105  77  223  247  550  26  81  663  80
User Adj:      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:        0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:     99  53  46  117  86  248  274  611  29  90  737  89
Reduct Vol:     0    0    0    0    0  0  0  0  0  0  0  0
Reduced Vol:    99  53  46  117  86  248  274  611  29  90  737  89
RTOR Reduct:    0    0  46  0  0  0  0  0  0  29  0  0  64
RTOR Vol:       99  53  0  117  86  248  274  611  0  90  737  25
PCE Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:    99  53  0  117  86  248  274  611  0  90  737  25
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:       1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:     0.91 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:          2.00 1.00 1.00 2.00 1.00 1.00 1.00 3.00 1.00 1.00 2.00 1.00
Final Sat.:     3000 1650 1650 3000 1650 1650 1650 4950 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:        0.03 0.03 0.00 0.04 0.05 0.15 0.17 0.12 0.00 0.05 0.22 0.01
Crit Volume:     49 248 274 368
Crit Moves:     ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #13 Lone Tree Way/Deer Valley Road
*****
Cycle (sec):      100          Critical vol./Cap.(X):      0.773
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     100          Level of Service:      C
*****
Street Name:      Deer Valley Road      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Protected      Protected
Rights:           Include      Include      Include      Include
Min. Green:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:            2 0 1 1 0      1 0 1 1 0      1 0 2 0 1      1 0 2 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 PM
Base Vol: 279 245 111 353 457 17 35 644 157 185 833 185
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 279 245 111 353 457 17 35 644 157 185 833 185
Added Vol: 19 0 63 0 0 0 0 45 7 43 88 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 298 245 174 353 457 17 35 689 164 228 921 185
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89
PHF Volume: 335 275 196 397 513 19 39 774 184 256 1035 208
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 335 275 196 397 513 19 39 774 184 256 1035 208
RTOR Reduct: 0 0 0 0 0 0 0 0 0 184 0 0 208
RTOR Vol: 335 275 196 397 513 19 39 774 0 256 1035 0
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 335 275 196 397 513 19 39 774 0 256 1035 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 2.00 1.17 0.83 1.00 1.93 0.07 1.00 2.00 1.00 1.00 2.00 1.00
Final sat.: 3000 1930 1370 1650 3182 118 1650 3300 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.11 0.14 0.14 0.24 0.16 0.16 0.02 0.23 0.00 0.16 0.31 0.00
Crit Volume: 235 397 387 256
Crit Moves: ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #14 Lone Tree Way/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.535
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     49      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Lanes:             1 0 1 1 0 1 1 0 2 0 1 1 0 3 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         36 53 13 279 85 269 177 495 18 24 862 160
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      36 53 13 279 85 269 177 495 18 24 862 160
Added Vol:        0 0 0 126 0 60 41 66 0 0 90 53
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      36 53 13 405 85 329 218 561 18 24 952 213
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:       40 59 14 450 94 366 242 623 20 27 1058 237
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      40 59 14 450 94 366 242 623 20 27 1058 237
RTOR Reduct:      0 0 0 0 0 242 0 0 20 0 0 237
RTOR Vol:         40 59 14 450 94 123 242 623 0 27 1058 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      40 59 14 450 94 123 242 623 0 27 1058 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:            1.00 1.61 0.39 2.00 1.00 1.00 1.00 2.00 1.00 1.00 3.00 1.00
Final Sat.:       1650 2650 650 3000 1650 1650 1650 3300 1650 1650 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.02 0.02 0.02 0.15 0.06 0.07 0.15 0.19 0.00 0.02 0.21 0.00
Crit Volume:      40 225 242 353
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #15 Lone Tree Way/Vista Grande Drive
*****
Cycle (sec):          100          Critical Vol./Cap.(X):          0.354
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        29          Level of Service:          A
*****
Street Name:          Vista Grande Drive          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:              Permitted          Permitted          Protected          Protected
Rights:               Include          Include          Include          Include
Min. Green:           0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                1    0    1    0          1    0    1    0          1    0    2    1    0          1    0    2    1    0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 8:00 - 9:00 PM
Base Vol:           39    14    123          24    16    41          20    693    30          59    967    37
Growth Adj:         1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:         39    14    123          24    16    41          20    693    30          59    967    37
Added Vol:           0    0    0          0    0    0          0    191    0          0    152    0
PasserByVol:         0    0    0          0    0    0          0    0    0          0    0    0
Initial Fut:         39    14    123          24    16    41          20    884    30          59    1119    37
User Adj:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
PHF Adj:            0.93 0.93 0.93          0.93 0.93 0.93          0.93 0.93 0.93          0.93 0.93 0.93
PHF Volume:          42    15    132          26    17    44          22    951    32          63    1203    40
Reduct Vol:          0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:         42    15    132          26    17    44          22    951    32          63    1203    40
RTOR Reduct:         0    0    0          0    0    0          0    0    0          0    0    0
RTOR Vol:           42    15    132          26    17    44          22    951    32          63    1203    40
PCE Adj:            1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:            1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
FinalVolume:         42    15    132          26    17    44          22    951    32          63    1203    40
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:           1720 1720 1720          1720 1720 1720          1720 1720 1720          1720 1720 1720
Adjustment:         1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Lanes:              1.00 0.10 0.90          1.00 0.28 0.72          1.00 2.90 0.10          1.00 2.90 0.10
Final Sat.:         1720 176 1544          1720 483 1237          1720 4991 169          1720 4995 165
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:            0.02 0.09 0.09          0.02 0.04 0.04          0.01 0.19 0.19          0.04 0.24 0.24
Crit Volume:         147          26          22          414
Crit Moves:         ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #16 Country Hills Drive/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.500
Loss Time (sec):    0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     46      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Country Hills Drive
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Split Phase      Split Phase
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0      0 0 0      0 0 0      0 0 0
Lanes:             1 0 1 1 0      1 0 1 1 0      1 0 0 1 0      1 0 0 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         70 297 31 63 439 26 44 77 143 84 93 117
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      70 297 31 63 439 26 44 77 143 84 93 117
Added Vol:        0 87 0 0 184 0 0 0 0 0 0 0
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      70 384 31 63 623 26 44 77 143 84 93 117
User Adj:         0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83
PHF Adj:          0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83
PHF Volume:       70 384 31 63 623 26 44 77 143 84 93 117
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      70 384 31 63 623 26 44 77 143 84 93 117
RTOR Reduct:      0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol:         70 384 31 63 623 26 44 77 143 84 93 117
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      70 384 31 63 623 26 44 77 143 84 93 117
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:            1.00 1.85 0.15 1.00 1.92 0.08 1.00 0.35 0.65 1.00 0.44 0.56
Final Sat.:       1650 3053 247 1650 3168 132 1650 578 1073 1650 731 919
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.04 0.13 0.13 0.04 0.20 0.20 0.03 0.13 0.13 0.05 0.13 0.13
Crit Volume:      70 325 220 210
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #18 Laurell/Hillcrest
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.404
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    31      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Laurell Road
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Permitted      Permitted
Rights:            Ignore      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             1 0 2 0 1      1 0 1 1 0      1 0 0 1 0      1 0 1 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         67 372 25 74 377 80 150 50 100 48 67 155
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      67 372 25 74 377 80 150 50 100 48 67 155
Added Vol:        0 87 0 0 184 0 0 0 0 0 0 0
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      67 459 25 74 561 80 150 50 100 48 67 155
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89
PHF Volume:       75 516 28 83 630 90 169 56 112 54 75 174
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      75 516 28 83 630 90 169 56 112 54 75 174
RTOR Reduct:      0 0 0 0 0 0 0 0 0 0 0 83
RTOR Vol:         75 516 28 83 630 90 169 56 112 54 75 91
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      75 516 28 83 630 90 169 56 112 54 75 91
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:            1.00 2.00 1.00 1.00 1.75 0.25 1.00 0.33 0.67 1.00 1.00 1.00
Final Sat.:       1720 3440 1720 1720 3011 429 1720 573 1147 1720 1720 1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.04 0.15 0.02 0.05 0.21 0.21 0.10 0.10 0.10 0.03 0.04 0.05
Crit Volume:      75 360 169 91
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #8 Lone Tree Way/Canada Valley Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.646
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    64      Level of Service:      B
*****
Street Name:      Canada Valley Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             2 0 0 1 1      1 0 1 0 1      1 0 3 0 1      2 0 3 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:         84 55 173 175 56 22 54 1354 55 329 942 253
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      84 55 173 175 56 22 54 1354 55 329 942 253
Added Vol:        26 0 89 0 0 0 0 232 45 151 314 0
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      110 55 262 175 56 22 54 1586 100 480 1256 253
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.96 0.96 0.96 0.96 0.96 0.96 0.96 0.96 0.96 0.96 0.96 0.96
PHF Volume:       115 57 273 182 58 23 56 1652 104 500 1308 264
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      115 57 273 182 58 23 56 1652 104 500 1308 264
RTOR Reduct:      0 0 273 0 0 23 0 0 63 0 0 182
RTOR Vol:         115 57 0 182 58 0 56 1652 41 500 1308 81
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      115 57 0 182 58 0 56 1652 41 500 1308 81
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       0.91 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:            2.00 1.00 1.00 1.00 1.00 1.00 1.00 3.00 1.00 2.00 3.00 1.00
Final Sat.:       3000 1650 1500 1650 1650 1650 1650 4950 1650 3000 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.04 0.03 0.00 0.11 0.04 0.00 0.03 0.33 0.02 0.17 0.26 0.05
Crit Volume:      57 182 551 250
Crit Moves:       ****
*****

```


Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #9 Lone Tree Way/SB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.737
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    87      Level of Service:      C
*****
Street Name:      SB SR 4 Bypass Ramps      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             0 0 0 0 0      1 1 0 0 1      0 0 3 0 1      2 0 3 0 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:30 - 5:30 PM
Base Vol:          0 0 0 0      416 10 361      0 1169 541      98 1153 0
Growth Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:        0 0 0 0      416 10 361      0 1169 541      98 1153 0
Added Vol:          0 0 0 0      0 0 178      0 250 71      0 287 0
PasserByVol:        0 0 0 0      0 0 0      0 0 0      0 0 0
Initial Fut:        0 0 0 0      416 10 539      0 1419 612      98 1440 0
User Adj:           1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:            0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95
PHF Volume:         0 0 0 0      438 11 567      0 1494 644      103 1516 0
Reduct Vol:         0 0 0 0      0 0 0      0 0 0      0 0 0
Reduced Vol:        0 0 0 0      438 11 567      0 1494 644      103 1516 0
RTOR Reduct:        0 0 0 0      0 0 0      0 0 0      0 0 0
RTOR Vol:           0 0 0 0      438 11 567      0 1494 644      103 1516 0
PCE Adj:            1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:            1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:        0 0 0 0      438 11 567      0 1494 644      103 1516 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:          1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:         1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:              0.00 0.00 0.00 1.95 0.05 1.00 0.00 3.00 1.00 2.00 3.00 0.00
Final Sat.:         0 0 0 3054 81 1720      0 5160 1720 3127 5160 0
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:           0.00 0.00 0.00 0.14 0.13 0.33 0.00 0.29 0.37 0.03 0.29 0.00
Crit Volume:        0 567 644 52
Crit Moves:         ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #10 Lone Tree Way/NB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.547
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     50      Level of Service:      A
*****
Street Name:      NB SR 4 Bypass Ramps      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             1    1    0    0    1      0    0    0    0    0      0    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 13 May 2008 << 4:45 - 5:45 PM
Base Vol: 437 43 137 0 0 0 0 1404 264 21 831 357
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 437 43 137 0 0 0 0 1404 264 21 831 357
Added Vol: 104 0 0 0 0 0 0 136 114 0 183 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 541 43 137 0 0 0 0 1540 378 21 1014 357
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.91 0.91 0.91 0.91 0.91 0.91 0.91 0.91 0.91 0.91 0.91 0.91
PHF Volume: 595 47 151 0 0 0 0 1692 415 23 1114 392
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 595 47 151 0 0 0 0 1692 415 23 1114 392
RTOR Reduct: 0 0 23 0 0 0 0 0 327 0 0 0
RTOR Vol: 595 47 127 0 0 0 0 1692 88 23 1114 392
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 595 47 127 0 0 0 0 1692 88 23 1114 392
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 1.85 0.15 1.00 0.00 0.00 0.00 0.00 3.00 1.00 1.00 3.00 1.00
Final Sat.: 2897 253 1720 0 0 0 0 5160 1720 1720 5160 1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.21 0.19 0.07 0.00 0.00 0.00 0.00 0.33 0.05 0.01 0.22 0.23
Crit Volume: 321 0 564 23
Crit Moves: ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #11 Lone Tree Way/Slatten Ranch Road
*****
Cycle (sec):      100      Critical Vol./Cap.(X):      0.546
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    50      Level of Service:      A
*****
Street Name:      Slatten Ranch Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    1    0      2    0    1    0    1      2    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 5:00 - 6:00 PM
Base Vol:         51    76    167    114    67    101    217    892    256    160    803    55
Growth Adj:       1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Initial Bse:      51    76    167    114    67    101    217    892    256    160    803    55
Added Vol:        0     0     0     0     0     0     0    136     0     0    183     0
PasserByVol:      0     0     0     0     0     0     0     0     0     0     0     0
Initial Fut:      51    76    167    114    67    101    217  1028    256    160  986     55
User Adj:         1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
PHF Adj:          0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94
PHF Volume:       54    81    178    121    71    107    231  1094    272    170  1049    59
Reduct Vol:       0     0     0     0     0     0     0     0     0     0     0     0
Reduced Vol:      54    81    178    121    71    107    231  1094    272    170  1049    59
RTOR Reduct:      0     0     0     0     0     0     0     0     30     0     0     59
RTOR Vol:         54    81    178    121    71     0    231  1094    242    170  1049     0
PCE Adj:          1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
MLF Adj:          1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
FinalVolume:      54    81    178    121    71     0    231  1094    242    170  1049     0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650  1650    1650    1650  1650    1650    1650  1650    1650    1650  1650    1650
Adjustment:       0.91  1.00    1.00    0.91  1.00    1.00    0.91  1.00    1.00    1.00  1.00    1.00
Lanes:            2.00  1.00    1.00    2.00  1.00    1.00    2.00  3.00    1.00    1.00  2.00    1.00
Final Sat.:      3000  1650    1650    3000  1650    1650    3000  4950    1650    1650  3300    1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.02  0.05    0.11    0.04  0.04    0.00    0.08  0.22    0.15    0.10  0.32    0.00
Crit Volume:              178              71              115              524
Crit Moves:              ****              ****              ****              ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #12 Lone Tree Way/Empire Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.641
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    64      Level of Service:      B
*****
Street Name:      Empire Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    0    1      2    0    1    1    0      1    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 5:00 - 6:00 PM
Base Vol:        76    46    36      231    115    176      230    759    112      53    702    129
Growth Adj:      1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00
Initial Bse:      76    46    36      231    115    176      230    759    112      53    702    129
Added Vol:        0    0    0        0    0    113      86    50    0        0    70    0
PasserByVol:      0    0    0        0    0    0        0    0    0        0    0    0
Initial Fut:      76    46    36      231    115    289      316    809    112      53    772    129
User Adj:         1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00
PHF Adj:          0.98  0.98  0.98      0.98  0.98  0.98      0.98  0.98  0.98      0.98  0.98  0.98
PHF Volume:       78    47    37      236    117    295      322    826    114      54    788    132
Reduct Vol:       0    0    0        0    0    0        0    0    0        0    0    0
Reduced Vol:      78    47    37      236    117    295      322    826    114      54    788    132
RTOR Reduct:      0    0    37      0    0    0        0    0    43      0    0    130
RTOR Vol:         78    47    0      236    117    295      322    826    72      54    788    2
PCE Adj:          1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00
MLF Adj:          1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00
FinalVolume:      78    47    0      236    117    295      322    826    72      54    788    2
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650  1650  1650      1650  1650  1650      1650  1650  1650      1650  1650  1650
Adjustment:       0.91  1.00  1.00      0.91  1.00  1.00      1.00  1.00  1.00      1.00  1.00  1.00
Lanes:            2.00  1.00  1.00      2.00  1.00  1.00      1.00  3.00  1.00      1.00  2.00  1.00
Final Sat.:       3000  1650  1650      3000  1650  1650      1650  4950  1650      1650  3300  1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.03  0.03  0.00      0.08  0.07  0.18      0.20  0.17  0.04      0.03  0.24  0.00
Crit Volume:       47                                295    322                                394
Crit Moves:       ****                                ****    ****                                ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

Intersection #13 Lone Tree Way/Deer Valley Road

Cycle (sec): 100 Critical vol./Cap.(X): 0.725
Loss Time (sec): 0 (Y+R=4.0 sec) Average Delay (sec/veh): xxxxxx
Optimal Cycle: 83 Level of Service: C

Street Name: Deer Valley Road Lone Tree Way
Approach: North Bound South Bound East Bound West Bound
Movement: L - T - R L - T - R L - T - R L - T - R
Control: Protected Protected Protected Protected
Rights: Include Include Include Include
Min. Green: 0 0 0 0 0 0 0 0 0 0 0 0
Lanes: 2 0 1 1 0 1 0 1 1 0 1 0 2 0 1 1 0 2 0 1
-----|-----|-----|-----|

Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol: 192 365 168 168 191 14 87 780 147 151 497 154
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 192 365 168 168 191 14 87 780 147 151 497 154
Added Vol: 13 0 73 0 0 0 0 123 22 87 91 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 205 365 241 168 191 14 87 903 169 238 588 154
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
PHF Volume: 211 376 248 173 197 14 90 931 174 245 606 159
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 211 376 248 173 197 14 90 931 174 245 606 159
RTOR Reduct: 0 0 0 0 0 0 0 0 116 0 0 159
RTOR Vol: 211 376 248 173 197 14 90 931 58 245 606 0
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 211 376 248 173 197 14 90 931 58 245 606 0
-----|-----|-----|-----|

Saturation Flow Module:
Sat/Lane: 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 2.00 1.20 0.80 1.00 1.86 0.14 1.00 2.00 1.00 1.00 2.00 1.00
Final Sat.: 3000 1988 1312 1650 3075 225 1650 3300 1650 1650 3300 1650
-----|-----|-----|-----|

Capacity Analysis Module:
Vol/Sat: 0.07 0.19 0.19 0.10 0.06 0.06 0.05 0.28 0.04 0.15 0.18 0.00
Crit Volume: 312 173 465 245
Crit Moves: ****

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #14 Lone Tree Way/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.632
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     62      Level of Service:      B
*****
Street Name:      Hillcrest Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Lanes:             1 0 1 1 0 1 1 0 2 0 1 1 0 3 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:15 - 5:15 PM
Base Vol:         17 87 26 423 77 97 131 915 22 43 720 229
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      17 87 26 423 77 97 131 915 22 43 720 229
Added Vol:        0 0 0 128 0 56 101 114 0 0 148 140
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      17 87 26 551 77 153 232 1029 22 43 868 369
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88
PHF Volume:       19 99 30 626 88 174 264 1169 25 49 986 419
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      19 99 30 626 88 174 264 1169 25 49 986 419
RTOR Reduct:      0 0 0 0 0 174 0 0 19 0 0 344
RTOR Vol:         19 99 30 626 88 0 264 1169 6 49 986 75
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      19 99 30 626 88 0 264 1169 6 49 986 75
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:            1.00 1.54 0.46 2.00 1.00 1.00 1.00 2.00 1.00 1.00 3.00 1.00
Final Sat.:       1650 2541 759 3000 1650 1650 1650 3300 1650 1650 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.01 0.04 0.04 0.21 0.05 0.00 0.16 0.35 0.00 0.03 0.20 0.05
Crit Volume:              64 313 585 49
Crit Moves:              **** **** **** ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #15 Lone Tree Way/Vista Grande Drive
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.489
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    36      Level of Service:      A
*****
Street Name:      Vista Grande Drive      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Permitted      Permitted      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             1 0 0 1 0      1 0 0 1 0      1 0 2 1 0      1 0 2 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:45 - 5:45 PM
Base Vol:         35 10 114 42 9 20 18 1282 44 121 931 24
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      35 10 114 42 9 20 18 1282 44 121 931 24
Added Vol:        0 0 0 0 0 0 0 0 260 0 0 291 0
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      35 10 114 42 9 20 18 1542 44 121 1222 24
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
PHF Volume:       36 10 118 43 9 21 19 1590 45 125 1260 25
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      36 10 118 43 9 21 19 1590 45 125 1260 25
RTOR Reduct:      0 0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol:         36 10 118 43 9 21 19 1590 45 125 1260 25
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      36 10 118 43 9 21 19 1590 45 125 1260 25
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:            1.00 0.08 0.92 1.00 0.31 0.69 1.00 2.92 0.08 1.00 2.94 0.06
Final Sat.:       1720 139 1581 1720 534 1186 1720 5017 143 1720 5061 99
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.02 0.07 0.07 0.03 0.02 0.02 0.01 0.32 0.32 0.07 0.25 0.25
Crit Volume:      128 43 545 125
Crit Moves:       ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #16 Country Hills Drive/Hillcrest Avenue
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.363
Loss Time (sec):      0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        36          Level of Service:          A
*****
Street Name:          Hillcrest Avenue          Country Hills Drive
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Protected          Protected          Split Phase          Split Phase
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 1  0  1  1  0          1  0  1  1  0          1  0  0  1  0          1  0  0  1  0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:             73  281  49          89  376  63          42  51  82          34  50  45
Growth Adj:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:          73  281  49          89  376  63          42  51  82          34  50  45
Added Vol:             0  233  0          0  167  0          0  0  0          0  0  0
PasserByVol:          0  0  0          0  0  0          0  0  0          0  0  0
Initial Fut:          73  514  49          89  543  63          42  51  82          34  50  45
User Adj:              0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92
PHF Adj:              0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92          0.92 0.92 0.92
PHF Volume:           73  514  49          89  543  63          42  51  82          34  50  45
Reduct Vol:           0  0  0          0  0  0          0  0  0          0  0  0
Reduced Vol:          73  514  49          89  543  63          42  51  82          34  50  45
RTOR Reduct:          0  0  0          0  0  0          0  0  0          0  0  0
RTOR Vol:             73  514  49          89  543  63          42  51  82          34  50  45
PCE Adj:              1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:              1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
FinalVolume:          73  514  49          89  543  63          42  51  82          34  50  45
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:             1650 1650 1650          1650 1650 1650          1650 1650 1650          1650 1650 1650
Adjustment:           1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Lanes:                1.00 1.83 0.17          1.00 1.79 0.21          1.00 0.38 0.62          1.00 0.53 0.47
Final Sat.:          1650 3013 287          1650 2957 343          1650 633 1017          1650 868 782
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:              0.04 0.17 0.17          0.05 0.18 0.18          0.03 0.08 0.08          0.02 0.06 0.06
Crit Volume:           282          89          133          95
Crit Moves:           ****          ****          ****          ****
*****

```


Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #18 Laurell/Hillcrest
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.287
Loss Time (sec):    0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     26      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Laurell Road
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Permitted      Permitted
Rights:           Ignore      Include      Include      Include
Min. Green:       0  0  0      0  0  0      0  0  0      0  0  0
Lanes:            1  0  2  0  1      1  0  1  1  0      1  0  0  1  0      1  0  1  0  1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:        27  302  39      162  459  50      17  7  22      35  9  133
Growth Adj:      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:     27  302  39      162  459  50      17  7  22      35  9  133
Added Vol:       0  233  0      0  167  0      0  0  0      0  0  0
PasserByVol:    0  0  0      0  0  0      0  0  0      0  0  0
Initial Fut:     27  535  39      162  626  50      17  7  22      35  9  133
User Adj:        0.98 0.98 0.98      0.98 0.98 0.98      0.98 0.98 0.98      0.98 0.98 0.98
PHF Adj:         0.98 0.98 0.98      0.98 0.98 0.98      0.98 0.98 0.98      0.98 0.98 0.98
PHF Volume:      27  535  39      162  626  50      17  7  22      35  9  133
Reduct Vol:      0  0  0      0  0  0      0  0  0      0  0  0
Reduced Vol:     27  535  39      162  626  50      17  7  22      35  9  133
RTOR Reduct:     0  0  0      0  0  0      0  0  0      0  0  133
RTOR Vol:        27  535  39      162  626  50      17  7  22      35  9  0
PCE Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
FinalVolume:     27  535  39      162  626  50      17  7  22      35  9  0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720 1720 1720      1720 1720 1720      1720 1720 1720      1720 1720 1720
Adjustment:      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Lanes:           1.00 2.00 1.00      1.00 1.85 0.15      1.00 0.24 0.76      1.00 1.00 1.00
Final Sat.:      1720 3440 1720      1720 3186 254      1720 415 1305      1720 1720 1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.02 0.16 0.02      0.09 0.20 0.20      0.01 0.02 0.02      0.02 0.01 0.00
Crit Volume:      267      162      29      35
Crit Moves:      ****      ****      ****      ****
*****

```

Near-Term With Project

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #8 Lone Tree Way/Canada Valley Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.586
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    55      Level of Service:      A
*****
Street Name:      Canada Valley Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             2 0 0 1 1      1 0 1 0 1      1 0 3 0 1      2 0 3 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         36 14 51 190 31 34 29 746 52 166 1005 168
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      36 14 51 190 31 34 29 746 52 166 1005 168
Added Vol:        40 0 133 196 0 60 20 225 13 45 114 65
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      76 14 184 386 31 94 49 971 65 211 1119 233
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:       84 16 204 429 34 104 54 1079 72 234 1243 259
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      84 16 204 429 34 104 54 1079 72 234 1243 259
RTOR Reduct:      0 0 129 0 0 54 0 0 46 0 0 259
RTOR Vol:         84 16 76 429 34 50 54 1079 26 234 1243 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      84 16 76 429 34 50 54 1079 26 234 1243 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       0.91 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:            2.00 0.34 1.66 1.00 1.00 1.00 1.00 3.00 1.00 2.00 3.00 1.00
Final sat.:       3000 564 2487 1650 1650 1650 1650 4950 1650 3000 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.03 0.03 0.03 0.26 0.02 0.03 0.03 0.22 0.02 0.08 0.25 0.00
Crit Volume:      46 429 360 117
Crit Moves:      **** **** **** ****
*****

```

Level of Service Computation Report
 CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #9 Lone Tree Way/SB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.648
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     65      Level of Service:      B
*****
Street Name:      SB SR 4 Bypass Ramps      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Protected      Protected
Rights:           Include      Include      Include      Include
Min. Green:       0 0 0 0 0      0 0 0 0 0      0 0 0 0 0      0 0 0 0 0
Lanes:            0 0 0 0 0      1 1 0 0 1      0 0 3 0 1      2 0 3 0 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         0 0 0 0 0      287 6 353      0 571 401      72 1000 0
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      0 0 0 0 0      287 6 353      0 571 401      72 1000 0
Added Vol:        0 0 0 0 0      0 0 82      0 427 127      0 142 0
PasserByVol:      0 0 0 0 0      0 0 0      0 0 0      0 0 0
Initial Fut:      0 0 0 0 0      287 6 435      0 998 528      72 1142 0
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:       0 0 0 0 0      319 7 483      0 1109 587      80 1269 0
Reduct Vol:       0 0 0 0 0      0 0 0      0 0 0      0 0 0
Reduced Vol:      0 0 0 0 0      319 7 483      0 1109 587      80 1269 0
RTOR Reduct:      0 0 0 0 0      0 0 0      0 0 0      0 0 0
RTOR Vol:         0 0 0 0 0      319 7 483      0 1109 587      80 1269 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      0 0 0 0 0      319 7 483      0 1109 587      80 1269 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:       1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:            0.00 0.00 0.00 1.96 0.04 1.00 0.00 3.00 1.00 2.00 3.00 0.00
Final Sat.:       0 0 0 3063 70 1720      0 5160 1720 3127 5160 0
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.00 0.00 0.00 0.10 0.09 0.28 0.00 0.21 0.34 0.03 0.25 0.00
Crit Volume:      0 483 587 40
Crit Moves:       ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #10 Lone Tree Way/NB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.360
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     36      Level of Service:      A
*****
Street Name:      NB SR 4 Bypass Ramps      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Split Phase      Split Phase      Protected      Protected
Rights:           Include          Include          Include          Include
Min. Green:       0    0    0      0    0    0      0    0    0      0    0    0
Lanes:            1    1    0    0    1      0    0    0    0    0      0    0    3    0    1      1    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 13 May 2008 << 7:30 - 8:30 AM
Base Vol:        383    29    79      0    0    0      0    662    160      8    671    245
Growth Adj:      1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Initial Bse:     383    29    79      0    0    0      0    662    160      8    671    245
Added Vol:       50     0     0      0    0    0      0    205    222      0    92     0
PasserByVol:     0     0     0      0    0    0      0     0     0      0     0     0
Initial Fut:     433    29    79      0    0    0      0    867    382      8    763    245
User Adj:        1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
PHF Adj:         0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89  0.89
PHF Volume:      487    33    89      0    0    0      0    974    429      9    857    275
Reduct Vol:      0     0     0      0    0    0      0     0     0      0     0     0
Reduced Vol:     487    33    89      0    0    0      0    974    429      9    857    275
RTOR Reduct:     0     0     9      0    0    0      0     0     268      0     0     0
RTOR Vol:        487    33    80      0    0    0      0    974    162      9    857    275
PCE Adj:         1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
MLF Adj:         1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
FinalVolume:     487    33    80      0    0    0      0    974    162      9    857    275
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720  1720
Adjustment:      0.91  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Lanes:           1.87  0.13  1.00  0.00  0.00  0.00  0.00  3.00  1.00  1.00  3.00  1.00
Final Sat.:      2931  216  1720      0     0     0      0  5160  1720  1720  5160  1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.17  0.15  0.05  0.00  0.00  0.00  0.00  0.19  0.09  0.01  0.17  0.16
Crit Volume:     260      0      325      9
Crit Moves:      ****      ****      ****
*****

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Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #11 Lone Tree Way/Slatten Ranch Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.492
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    45      Level of Service:      A
*****
Street Name:      Slatten Ranch Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    1    0      2    0    1    0    1      2    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 7:15 - 8:15 AM
Base Vol:         39    47    191      42    35    24      74    484    91      54    837    29
Growth Adj:       1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:      39    47    191      42    35    24      74    484    91      54    837    29
Added Vol:        0    0    0      0    0    0      0    205    0      0    92    0
PasserByVol:      0    0    0      0    0    0      0    0    0      0    0    0
Initial Fut:      39    47    191      42    35    24      74    689    91      54    929    29
User Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90      0.90 0.90 0.90      0.90 0.90 0.90      0.90 0.90 0.90
PHF Volume:       43    52    212      47    39    27      82    766    101      60    1032    32
Reduct Vol:       0    0    0      0    0    0      0    0    0      0    0    0
Reduced Vol:      43    52    212      47    39    27      82    766    101      60    1032    32
RTOR Reduct:      0    0    0      0    0    27      0    0    24      0    0    26
RTOR Vol:         43    52    212      47    39    0      82    766    77      60    1032    7
PCE Adj:          1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
FinalVolume:      43    52    212      47    39    0      82    766    77      60    1032    7
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650      1650 1650 1650      1650 1650 1650      1650 1650 1650
Adjustment:       0.91 1.00 1.00      0.91 1.00 1.00      0.91 1.00 1.00      1.00 1.00 1.00
Lanes:            2.00 1.00 1.00      2.00 1.00 1.00      2.00 3.00 1.00      1.00 2.00 1.00
Final Sat.:       3000 1650 1650      3000 1650 1650      3000 4950 1650      1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.01 0.03 0.13      0.02 0.02 0.00      0.03 0.15 0.05      0.04 0.31 0.00
Crit Volume:      212      39      41      516
Crit Moves:      ****      ****      ****      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #12 Lone Tree Way/Empire Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.616
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    59      Level of Service:      B
*****
Street Name:      Empire Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    0    1      2    0    1    1    0      1    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 7:15 - 8:15 AM
Base Vol:      89  48  41  105  77  181  168  499  26  81  638  80
Growth Adj:    1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:    89  48  41  105  77  181  168  499  26  81  638  80
Added Vol:      0    0    0    0    0    57  124  81    0    0    35    0
PasserByVol:    0    0    0    0    0    0    0    0    0    0    0    0
Initial Fut:    89  48  41  105  77  238  292  580  26  81  673  80
User Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:        0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:     99  53  46  117  86  264  324  644  29  90  748  89
Reduct Vol:     0    0    0    0    0    0    0    0    0    0    0    0
Reduced Vol:    99  53  46  117  86  264  324  644  29  90  748  89
RTOR Reduct:    0    0    46    0    0    0    0    0    29  0    0    64
RTOR Vol:       99  53    0  117  86  264  324  644    0  90  748  25
PCE Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:    99  53    0  117  86  264  324  644    0  90  748  25
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:       1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:     0.91 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:          2.00 1.00 1.00 2.00 1.00 1.00 1.00 3.00 1.00 1.00 2.00 1.00
Final Sat.:     3000 1650 1650 3000 1650 1650 1650 4950 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:        0.03 0.03 0.00 0.04 0.05 0.16 0.20 0.13 0.00 0.05 0.23 0.01
Crit Volume:    49      264  324      374
Crit Moves:     ****      ****  ****      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #13 Lone Tree Way/Deer Valley Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.780
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     103      Level of Service:      C
*****
Street Name:      Deer Valley Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             2 0 1 1 0      1 0 1 1 0      1 0 2 0 1      1 0 2 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 PM
Base Vol: 279 245 111 353 457 17 35 644 157 185 833 185
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 279 245 111 353 457 17 35 644 157 185 833 185
Added Vol: 19 0 63 0 0 0 0 65 7 43 148 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 298 245 174 353 457 17 35 709 164 228 981 185
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89
PHF Volume: 335 275 196 397 513 19 39 797 184 256 1102 208
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 335 275 196 397 513 19 39 797 184 256 1102 208
RTOR Reduct: 0 0 0 0 0 0 0 0 0 184 0 0 208
RTOR Vol: 335 275 196 397 513 19 39 797 0 256 1102 0
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 335 275 196 397 513 19 39 797 0 256 1102 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 2.00 1.17 0.83 1.00 1.93 0.07 1.00 2.00 1.00 1.00 2.00 1.00
Final sat.: 3000 1930 1370 1650 3182 118 1650 3300 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.11 0.14 0.14 0.24 0.16 0.16 0.02 0.24 0.00 0.16 0.33 0.00
Crit Volume: 235 397 398 256
Crit Moves: **** **** **** ****
*****

```


Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #14 Lone Tree Way/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.548
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    50      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Lanes:             1 0 1 1 0 1 1 1 0 1 1 0 2 0 1 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         36 53 13 279 85 269 177 495 18 24 862 160
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      36 53 13 279 85 269 177 495 18 24 862 160
Added Vol:        0 0 0 126 0 60 41 86 0 0 150 53
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      36 53 13 405 85 329 218 581 18 24 1012 213
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.90
PHF Volume:       40 59 14 450 94 366 242 646 20 27 1124 237
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      40 59 14 450 94 366 242 646 20 27 1124 237
RTOR Reduct:      0 0 0 0 0 242 0 0 20 0 0 237
RTOR Vol:         40 59 14 450 94 123 242 646 0 27 1124 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      40 59 14 450 94 123 242 646 0 27 1124 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:           1.00 1.61 0.39 2.00 1.00 1.00 1.00 2.00 1.00 1.00 3.00 1.00
Final sat.:       1650 2650 650 3000 1650 1650 1650 3300 1650 1650 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.02 0.02 0.02 0.15 0.06 0.07 0.15 0.20 0.00 0.02 0.23 0.00
Crit Volume:      40 225 242 375
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

Intersection #15 Lone Tree Way/Vista Grande Drive

Cycle (sec): 100 Critical vol./Cap.(X): 0.367
Loss Time (sec): 0 (Y+R=4.0 sec) Average Delay (sec/veh): xxxxxx
Optimal Cycle: 29 Level of Service: A

Street Name: Vista Grande Drive Lone Tree Way
Approach: North Bound South Bound East Bound West Bound
Movement: L - T - R L - T - R L - T - R L - T - R
-----|-----|-----|-----|
Control: Permitted Permitted Protected Protected
Rights: Include Include Include Include
Min. Green: 0 0 0 0 0 0 0 0 0 0 0 0
Lanes: 1 0 0 1 0 1 0 0 1 0 1 0 2 1 0 1 0 2 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 8:00 - 9:00 PM
Base Vol: 39 14 123 24 16 41 20 693 30 59 967 37
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 39 14 123 24 16 41 20 693 30 59 967 37
Added Vol: 0 0 0 0 0 0 0 211 0 0 212 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 39 14 123 24 16 41 20 904 30 59 1179 37
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93
PHF Volume: 42 15 132 26 17 44 22 972 32 63 1268 40
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 42 15 132 26 17 44 22 972 32 63 1268 40
RTOR Reduct: 0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol: 42 15 132 26 17 44 22 972 32 63 1268 40
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Final Volume: 42 15 132 26 17 44 22 972 32 63 1268 40
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 1.00 0.10 0.90 1.00 0.28 0.72 1.00 2.90 0.10 1.00 2.91 0.09
Final Sat.: 1720 176 1544 1720 483 1237 1720 4994 166 1720 5003 157
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.02 0.09 0.09 0.02 0.04 0.04 0.01 0.19 0.19 0.04 0.25 0.25
Crit Volume: 147 26 22 436
Crit Moves: **** **** **** ****

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #16 Country Hills Drive/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.527
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    48      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Country Hills Drive
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Split Phase      Split Phase
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0      0 0 0      0 0 0      0 0 0
Lanes:             1 0 1 1 0      1 0 1 1 0      1 0 0 1 0      1 0 0 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:         70 297 31 63 439 26 44 77 143 84 93 117
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      70 297 31 63 439 26 44 77 143 84 93 117
Added Vol:        0 87 0 15 184 0 0 0 0 0 0 45
PasserByVol:      0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:      70 384 31 78 623 26 44 77 143 84 93 162
User Adj:         0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83
PHF Adj:          0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83
PHF Volume:       70 384 31 78 623 26 44 77 143 84 93 162
Reduct Vol:       0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:      70 384 31 78 623 26 44 77 143 84 93 162
RTOR Reduct:      0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol:         70 384 31 78 623 26 44 77 143 84 93 162
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      70 384 31 78 623 26 44 77 143 84 93 162
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:            1.00 1.85 0.15 1.00 1.92 0.08 1.00 0.35 0.65 1.00 0.36 0.64
Final sat.:       1650 3053 247 1650 3168 132 1650 578 1073 1650 602 1048
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.04 0.13 0.13 0.05 0.20 0.20 0.03 0.13 0.13 0.05 0.15 0.15
Crit Volume:      70 325 220 255
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #18 Laurell/Hillcrest
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.409
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     31      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Laurell Road
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Permitted      Permitted
Rights:           Ignore      Include      Include      Include
Min. Green:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:            1 0 2 0 1      1 0 1 1 0      1 0 0 1 0      1 0 1 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 7:45 - 8:45 AM
Base Vol:        67 372 25 74 377 80 150 50 100 48 67 155
Growth Adj:      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:     67 372 25 74 377 80 150 50 100 48 67 155
Added Vol:       0 132 0 0 199 0 0 0 0 0 0 0
PasserByVol:    0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:     67 504 25 74 576 80 150 50 100 48 67 155
User Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:         0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89
PHF Volume:      75 566 28 83 647 90 169 56 112 54 75 174
Reduct Vol:      0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:     75 566 28 83 647 90 169 56 112 54 75 174
RTOR Reduct:     0 0 0 0 0 0 0 0 0 0 0 83
RTOR Vol:        75 566 28 83 647 90 169 56 112 54 75 91
PCE Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:     75 566 28 83 647 90 169 56 112 54 75 91
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:           1.00 2.00 1.00 1.00 1.76 0.24 1.00 0.33 0.67 1.00 1.00 1.00
Final Sat.:      1720 3440 1720 1720 3020 420 1720 573 1147 1720 1720 1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.04 0.16 0.02 0.05 0.21 0.21 0.10 0.10 0.10 0.03 0.04 0.05
Crit Volume:     75 369 169 91
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #8 Lone Tree Way/Canada Valley Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.728
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    84      Level of Service:      C
*****
Street Name:      Canada Valley Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0  0  0      0  0  0      0  0  0      0  0  0
Lanes:             2  0  0  1  1      1  0  1  0  1      1  0  3  0  1      2  0  3  0  1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:         84  55  173      175  56  22      54 1354  55      329  942  253
Growth Adj:       1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:      84  55  173      175  56  22      54 1354  55      329  942  253
Added Vol:        26  0  89      130  0  40      68  232  45      151  314  221
PasserByVol:      0  0  0      0  0  0      0  0  0      0  0  0
Initial Fut:     110  55  262      305  56  62      122 1586  100      480 1256  474
User Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
PHF Adj:          0.96 0.96 0.96      0.96 0.96 0.96      0.96 0.96 0.96      0.96 0.96 0.96
PHF Volume:       115  57  273      318  58  65      127 1652  104      500 1308  494
Reduct Vol:       0  0  0      0  0  0      0  0  0      0  0  0
Reduced Vol:     115  57  273      318  58  65      127 1652  104      500 1308  494
RTOR Reduct:      0  0  273      0  0  65      0  0  63      0  0  318
RTOR Vol:         115  57  0      318  58  0      127 1652  41      500 1308  176
PCE Adj:          1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
FinalVolume:     115  57  0      318  58  0      127 1652  41      500 1308  176
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1650 1650 1650      1650 1650 1650      1650 1650 1650      1650 1650 1650
Adjustment:       0.91 1.00 0.91      1.00 1.00 1.00      1.00 1.00 1.00      0.91 1.00 1.00
Lanes:            2.00 1.00 1.00      1.00 1.00 1.00      1.00 3.00 1.00      2.00 3.00 1.00
Final Sat.:       3000 1650 1500      1650 1650 1650      1650 4950 1650      3000 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.04 0.03 0.00      0.19 0.04 0.00      0.08 0.33 0.02      0.17 0.26 0.11
Crit Volume:      57      318      551      250
Crit Moves:      ****      ****      ****      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #9 Lone Tree Way/SB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.808
Loss Time (sec):    0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     119      Level of Service:      D
*****
Street Name:      SB SR 4 Bypass Ramps      Lone Tree Way
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Protected      Protected
Rights:           Include      Include      Include      Include
Min. Green:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:            0 0 0 0 0      1 1 0 0 1      0 0 3 0 1      2 0 3 0 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:30 - 5:30 PM
Base Vol:         0 0 0 0      416 10 361      0 1169 541      98 1153 0
Growth Adj:       1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:      0 0 0 0      416 10 361      0 1169 541      98 1153 0
Added Vol:        0 0 0 0      0 0 263      0 350 101      0 423 0
PasserByVol:      0 0 0 0      0 0 0      0 0 0      0 0 0
Initial Fut:      0 0 0 0      416 10 624      0 1519 642      98 1576 0
User Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:          0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95 0.95
PHF Volume:       0 0 0 0      438 11 657      0 1599 676      103 1659 0
Reduct Vol:       0 0 0 0      0 0 0      0 0 0      0 0 0
Reduced Vol:      0 0 0 0      438 11 657      0 1599 676      103 1659 0
RTOR Reduct:      0 0 0 0      0 0 0      0 0 0      0 0 0
RTOR Vol:         0 0 0 0      438 11 657      0 1599 676      103 1659 0
PCE Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:          1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:      0 0 0 0      438 11 657      0 1599 676      103 1659 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:         1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:       1.00 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 0.91 1.00 1.00
Lanes:            0.00 0.00 0.00 1.95 0.05 1.00 0.00 3.00 1.00 2.00 3.00 0.00
Final Sat.:       0 0 0 3054 81 1720      0 5160 1720 3127 5160 0
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:          0.00 0.00 0.00 0.14 0.13 0.38 0.00 0.31 0.39 0.03 0.32 0.00
Crit Volume:      0 657 676 52
Crit Moves:       ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

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*****
Intersection #10 Lone Tree Way/NB SR 4 Bypass Ramps
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.575
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    54      Level of Service:      A
*****
Street Name:      NB SR 4 Bypass Ramps      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             1    1    0    0    1      0    0    0    0    0      0    0    3    0    1      1    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 13 May 2008 << 4:45 - 5:45 PM
Base Vol:         437    43    137      0    0    0      0    1404    264      21    831    357
Growth Adj:        1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00
Initial Bse:       437    43    137      0    0    0      0    1404    264      21    831    357
Added Vol:         155    0    0      0    0    0      0    186    164      0    268    0
PasserByVol:       0    0    0      0    0    0      0    0    0      0    0    0
Initial Fut:       592    43    137      0    0    0      0    1590    428      21    1099    357
User Adj:          1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00
PHF Adj:           0.91    0.91    0.91      0.91    0.91    0.91      0.91    0.91    0.91      0.91    0.91    0.91
PHF Volume:        651    47    151      0    0    0      0    1747    470      23    1208    392
Reduct Vol:        0    0    0      0    0    0      0    0    0      0    0    0
Reduced Vol:       651    47    151      0    0    0      0    1747    470      23    1208    392
RTOR Reduct:       0    0    23      0    0    0      0    0    358      0    0    0
RTOR Vol:          651    47    127      0    0    0      0    1747    113      23    1208    392
PCE Adj:           1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00
MLF Adj:           1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00
FinalVolume:       651    47    127      0    0    0      0    1747    113      23    1208    392
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:          1720    1720    1720      1720    1720    1720      1720    1720    1720      1720    1720    1720
Adjustment:        0.91    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00      1.00    1.00    1.00
Lanes:             1.86    0.14    1.00      0.00    0.00    0.00      0.00    3.00    1.00      1.00    3.00    1.00
Final Sat.:        2915    233    1720      0    0    0      0    5160    1720      1720    5160    1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:           0.22    0.20    0.07      0.00    0.00    0.00      0.00    0.34    0.07      0.01    0.23    0.23
Crit Volume:       349      0      582      23
Crit Moves:       ****      ****      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #11 Lone Tree Way/Slatten Ranch Road
*****
Cycle (sec):      100      Critical Vol./Cap.(X):      0.573
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    53      Level of Service:      A
*****
Street Name:      Slatten Ranch Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    1    0      2    0    1    0    1      2    0    3    0    1      1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 5:00 - 6:00 PM
Base Vol:         51    76    167    114    67    101    217    892    256    160    803    55
Growth Adj:        1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Initial Bse:       51    76    167    114    67    101    217    892    256    160    803    55
Added Vol:         0    0    0      0    0    0      0    186    0      0    268    0
PasserByVol:       0    0    0      0    0    0      0    0    0      0    0    0
Initial Fut:       51    76    167    114    67    101    217  1078    256    160  1071    55
User Adj:          1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
PHF Adj:           0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94  0.94
PHF Volume:        54    81    178    121    71    107    231  1147    272    170  1139    59
Reduct Vol:        0    0    0      0    0    0      0    0    0      0    0    0
Reduced Vol:       54    81    178    121    71    107    231  1147    272    170  1139    59
RTOR Reduct:       0    0    0      0    0    107    0    0    30      0    0    59
RTOR Vol:          54    81    178    121    71    0      231  1147    242    170  1139    0
PCE Adj:           1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
MLF Adj:           1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00  1.00
Final Volume:      54    81    178    121    71    0      231  1147    242    170  1139    0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:          1650  1650  1650  1650  1650  1650  1650  1650  1650  1650  1650  1650
Adjustment:        0.91  1.00  1.00  0.91  1.00  1.00  0.91  1.00  1.00  1.00  1.00  1.00
Lanes:             2.00  1.00  1.00  2.00  1.00  1.00  2.00  3.00  1.00  1.00  2.00  1.00
Final Sat.:        3000  1650  1650  3000  1650  1650  3000  4950  1650  1650  3300  1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:           0.02  0.05  0.11  0.04  0.04  0.00  0.08  0.23  0.15  0.10  0.35  0.00
Crit Volume:                178                71                115                570
Crit Moves:                ****                ****                ****                ****
*****

```


Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #12 Lone Tree Way/Empire Avenue
*****
Cycle (sec):      100          Critical vol./Cap.(X):      0.702
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     76          Level of Service:      C
*****
Street Name:      Empire Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             2    0    1    0    1    2    0    1    1    0    1    0    3    0    1    1    0    2    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 22 May 2008 << 5:00 - 6:00 PM
Base Vol:       76   46   36   231  115  176   230  759  112   53  702  129
Growth Adj:     1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:     76   46   36   231  115  176   230  759  112   53  702  129
Added Vol:       0    0    0    0    0    164   116  70    0    0  104    0
PasserByVol:     0    0    0    0    0    0    0    0    0    0    0    0
Initial Fut:     76   46   36   231  115  340   346  829  112   53  806  129
User Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj:         0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98
PHF Volume:      78   47   37   236  117  347   353  846  114   54  822  132
Reduct Vol:      0    0    0    0    0    0    0    0    0    0    0    0
Reduced Vol:     78   47   37   236  117  347   353  846  114   54  822  132
RTOR Reduct:     0    0    37    0    0    0    0    0    43    0    0  130
RTOR Vol:        78   47    0   236  117  347   353  846   72   54  822    2
PCE Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:     78   47    0   236  117  347   353  846   72   54  822    2
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:      0.91 1.00 1.00 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:           2.00 1.00 1.00 2.00 1.00 1.00 1.00 3.00 1.00 1.00 2.00 1.00
Final Sat.:      3000 1650 1650 3000 1650 1650 1650 4950 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.03 0.03 0.00 0.08 0.07 0.21 0.21 0.17 0.04 0.03 0.25 0.00
Crit Volume:      47          347   353          411
Crit Moves:      ****          ****   ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #13 Lone Tree Way/Deer Valley Road
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.746
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    90      Level of Service:      C
*****
Street Name:      Deer Valley Road      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Protected      Protected      Protected      Protected
Rights:            Include      Include      Include      Include
Min. Green:        0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:             2 0 1 1 0      1 0 1 1 0      1 0 2 0 1      1 0 2 0 1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol: 192 365 168 168 191 14 87 780 147 151 497 154
Growth Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse: 192 365 168 168 191 14 87 780 147 151 497 154
Added Vol: 13 0 73 0 0 0 0 191 22 87 131 0
PasserByVol: 0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut: 205 365 241 168 191 14 87 971 169 238 628 154
User Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
PHF Adj: 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
PHF Volume: 211 376 248 173 197 14 90 1001 174 245 647 159
Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol: 211 376 248 173 197 14 90 1001 174 245 647 159
RTOR Reduct: 0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol: 211 376 248 173 197 14 90 1001 58 245 647 0
PCE Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj: 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume: 211 376 248 173 197 14 90 1001 58 245 647 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane: 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment: 0.91 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes: 2.00 1.20 0.80 1.00 1.86 0.14 1.00 2.00 1.00 1.00 2.00 1.00
Final Sat.: 3000 1988 1312 1650 3075 225 1650 3300 1650 1650 3300 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat: 0.07 0.19 0.19 0.10 0.06 0.06 0.05 0.30 0.04 0.15 0.20 0.00
Crit Volume: 312 173 501 245
Crit Moves: ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #14 Lone Tree Way/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.655
Loss Time (sec):  0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:    66      Level of Service:      B
*****
Street Name:      Hillcrest Avenue      Lone Tree Way
Approach:          North Bound      South Bound      East Bound      West Bound
Movement:          L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:           Split Phase      Split Phase      Protected      Protected
Rights:            Include          Include          Include          Include
Min. Green:        0    0    0      0    0    0      0    0    0      0    0    0
Lanes:             1    0    1    1    0      1    1    1    0    1      1    0    2    0    1      1    0    3    0    1
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:15 - 5:15 PM
Base Vol:        17    87    26      423    77    97      131    915    22      43    720    229
Growth Adj:      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Initial Bse:     17    87    26      423    77    97      131    915    22      43    720    229
Added Vol:       0    0    0        128    0    56      101    182    0        0    188    140
PasserByVol:    0    0    0        0    0    0        0    0    0        0    0    0
Initial Fut:     17    87    26      551    77    153      232    1097    22      43    908    369
User Adj:        1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
PHF Adj:         0.88 0.88 0.88      0.88 0.88 0.88      0.88 0.88 0.88      0.88 0.88 0.88
PHF Volume:      19    99    30      626    88    174      264    1247    25      49    1032    419
Reduct Vol:      0    0    0        0    0    0        0    0    0        0    0    0
Reduced Vol:     19    99    30      626    88    174      264    1247    25      49    1032    419
RTOR Reduct:     0    0    0        0    0    174      0    0    19      0    0    344
RTOR Vol:        19    99    30      626    88    0        264    1247    6        49    1032    75
PCE Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
FinalVolume:     19    99    30      626    88    0        264    1247    6        49    1032    75
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1650 1650 1650      1650 1650 1650      1650 1650 1650      1650 1650 1650
Adjustment:      1.00 1.00 1.00      0.91 1.00 1.00      1.00 1.00 1.00      1.00 1.00 1.00
Lanes:           1.00 1.54 0.46      2.00 1.00 1.00      1.00 2.00 1.00      1.00 3.00 1.00
Final Sat.:      1650 2541 759      3000 1650 1650      1650 3300 1650      1650 4950 1650
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.01 0.04 0.04      0.21 0.05 0.00      0.16 0.38 0.00      0.03 0.21 0.05
Crit Volume:           64    313           623           49
Crit Moves:          ****      ****           ****           ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #15 Lone Tree Way/Vista Grande Drive
*****
Cycle (sec):          100          Critical vol./Cap.(X):          0.502
Loss Time (sec):      0 (Y+R=4.0 sec) Average Delay (sec/veh):      xxxxxx
Optimal Cycle:        37          Level of Service:          A
*****
Street Name:          Vista Grande Drive          Lone Tree Way
Approach:              North Bound          South Bound          East Bound          West Bound
Movement:              L - T - R          L - T - R          L - T - R          L - T - R
-----|-----|-----|-----|
Control:               Permitted          Permitted          Protected          Protected
Rights:                Include          Include          Include          Include
Min. Green:            0    0    0          0    0    0          0    0    0          0    0    0
Lanes:                 1    0    1    0          1    0    1    0          1    0    2    1    0          1    0    2    1    0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 4:45 - 5:45 PM
Base Vol:           35    10    114          42    9    20          18 1282          44    121 931    24
Growth Adj:         1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Initial Bse:         35    10    114          42    9    20          18 1282          44    121 931    24
Added Vol:           0    0    0          0    0    0          0    328    0          0    331    0
PasserByVol:         0    0    0          0    0    0          0    0    0          0    0    0
Initial Fut:         35    10    114          42    9    20          18 1610          44    121 1262    24
User Adj:            1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
PHF Adj:             0.97 0.97 0.97          0.97 0.97 0.97          0.97 0.97 0.97          0.97 0.97 0.97
PHF Volume:          36    10    118          43    9    21          19 1660          45    125 1301    25
Reduct Vol:          0    0    0          0    0    0          0    0    0          0    0    0
Reduced Vol:         36    10    118          43    9    21          19 1660          45    125 1301    25
RTOR Reduct:         0    0    0          0    0    0          0    0    0          0    0    0
RTOR Vol:            36    10    118          43    9    21          19 1660          45    125 1301    25
PCE Adj:             1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
MLF Adj:             1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
FinalVolume:         36    10    118          43    9    21          19 1660          45    125 1301    25
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:            1720 1720 1720          1720 1720 1720          1720 1720 1720          1720 1720 1720
Adjustment:          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00          1.00 1.00 1.00
Lanes:               1.00 0.08 0.92          1.00 0.31 0.69          1.00 2.92 0.08          1.00 2.94 0.06
Final Sat.:          1720 139 1581          1720 534 1186          1720 5023 137          1720 5064 96
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:             0.02 0.07 0.07          0.03 0.02 0.02          0.01 0.33 0.33          0.07 0.26 0.26
Crit Volume:          128          43          568          125
Crit Moves:          ****          ****          ****          ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #16 Country Hills Drive/Hillcrest Avenue
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.412
Loss Time (sec):    0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     39      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Country Hills Drive
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Split Phase      Split Phase
Rights:           Include      Include      Include      Include
Min. Green:       0 0 0      0 0 0      0 0 0      0 0 0
Lanes:           1 0 1 1 0      1 0 1 1 0      1 0 0 1 0      1 0 0 1 0
-----|-----|-----|-----|
Volume Module: >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:       73 281 49 89 376 63 42 51 82 34 50 45
Growth Adj:     1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:    73 281 49 89 376 63 42 51 82 34 50 45
Added Vol:      0 233 0 51 167 0 0 0 0 0 0 30
PasserByVol:    0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:    73 514 49 140 543 63 42 51 82 34 50 75
User Adj:       0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92
PHF Adj:        0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92
PHF Volume:     73 514 49 140 543 63 42 51 82 34 50 75
Reduct Vol:     0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:    73 514 49 140 543 63 42 51 82 34 50 75
RTOR Reduct:    0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol:       73 514 49 140 543 63 42 51 82 34 50 75
PCE Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:        1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:    73 514 49 140 543 63 42 51 82 34 50 75
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:       1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650 1650
Adjustment:     1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:          1.00 1.83 0.17 1.00 1.79 0.21 1.00 0.38 0.62 1.00 0.40 0.60
Final Sat.:     1650 3013 287 1650 2957 343 1650 633 1017 1650 660 990
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:        0.04 0.17 0.17 0.08 0.18 0.18 0.03 0.08 0.08 0.02 0.08 0.08
Crit Volume:     282 140 133 125
Crit Moves:      ****
*****

```

Level of Service Computation Report
CCTALOS Method (Future Volume Alternative)

```

*****
Intersection #18 Laurell/Hillcrest
*****
Cycle (sec):      100      Critical vol./Cap.(X):      0.296
Loss Time (sec):   0 (Y+R=4.0 sec)  Average Delay (sec/veh):      xxxxxx
Optimal Cycle:     26      Level of Service:      A
*****
Street Name:      Hillcrest Avenue      Laurell Road
Approach:         North Bound      South Bound      East Bound      West Bound
Movement:         L - T - R      L - T - R      L - T - R      L - T - R
-----|-----|-----|-----|
Control:          Protected      Protected      Permitted      Permitted
Rights:           Ignore      Include      Include      Include
Min. Green:       0 0 0 0      0 0 0 0      0 0 0 0      0 0 0 0
Lanes:            1 0 2 0 1      1 0 1 1 0      1 0 0 1 0      1 0 1 0 1
-----|-----|-----|-----|
Volume Module:    >> Count Date: 15 May 2008 << 5:00 - 6:00 PM
Base Vol:        27 302 39 162 459 50 17 7 22 35 9 133
Growth Adj:      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Initial Bse:     27 302 39 162 459 50 17 7 22 35 9 133
Added Vol:       0 263 0 0 218 0 0 0 0 0 0 0
PasserByVol:     0 0 0 0 0 0 0 0 0 0 0 0
Initial Fut:     27 565 39 162 677 50 17 7 22 35 9 133
User Adj:        0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98
PHF Adj:         0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98
PHF Volume:      27 565 39 162 677 50 17 7 22 35 9 133
Reduct Vol:      0 0 0 0 0 0 0 0 0 0 0 0
Reduced Vol:     27 565 39 162 677 50 17 7 22 35 9 133
RTOR Reduct:     0 0 0 0 0 0 0 0 0 0 0 0
RTOR Vol:        27 565 39 162 677 50 17 7 22 35 9 0
PCE Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
MLF Adj:         1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
FinalVolume:     27 565 39 162 677 50 17 7 22 35 9 0
-----|-----|-----|-----|
Saturation Flow Module:
Sat/Lane:        1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720 1720
Adjustment:      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
Lanes:           1.00 2.00 1.00 1.00 1.86 0.14 1.00 0.24 0.76 1.00 1.00 1.00
Final Sat.:      1720 3440 1720 1720 3203 237 1720 415 1305 1720 1720 1720
-----|-----|-----|-----|
Capacity Analysis Module:
Vol/Sat:         0.02 0.16 0.02 0.09 0.21 0.21 0.01 0.02 0.02 0.02 0.01 0.00
Crit Volume:      283 162 29 35
Crit Moves:      ****
*****

```

Cumulative No Project

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 1 Canada Valley/Laurel Road

Count Date Time Peak Hour M

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

0 0 0
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 0 --- 0.0 0.0 0.0 0.0 --- 0 RIGHT
STREET NAME:
THRU 953 ---> 2.1 (NO. OF LANES) 2.0<--- 649 THRU Laurel Road
RIGHT 100 --- 1.1 1.0 0.0 1.0 1.0 --- 238 LEFT
<--- ^ --->
| | |
v | v
N
W + E 120 0 229 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Canada Valley

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 229 | 0 * | 1720 | 0.0000 | |
| LEFT (L) | 120 | 120 | 1720 | 0.0698 | 0.0698 |
| EB RIGHT (R) | 100 | 100 | 1720 | 0.0581 | |
| THRU (T) | 953 | 953 | 3440 | 0.2770 | |
| T + R | | 1053 | 3440 | 0.3061 | 0.3061 |
| WB THRU (T) | 649 | 649 | 3440 | 0.1887 | |
| LEFT (L) | 238 | 238 | 1720 | 0.1384 | 0.1384 |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.51
INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 2 Country Hills Dr/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
----- 60 30 80
LEFT 40 --- 1.0 1.1 1.1 1.0 1.1 --- 30 RIGHT
THRU 679 ---> 2.1 (NO. OF LANES) 2.1<--- 633 THRU
RIGHT 420 --- 1.1 1.0 1.1 1.1 1.0 --- 62 LEFT
N
W + E 160 20 217
S LEFT THRU RIGHT Split? N
STREET NAME: Laurel Road
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: Country Hills Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 217 | 217 | 1650 | 0.1315 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 160 | 160 | 1650 | 0.0970 | |
| T + R | | 237 | 1650 | 0.1436 | 0.1436 |
| SB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 30 | 30 | 1650 | 0.0182 | |
| LEFT (L) | 80 | 80 | 1650 | 0.0485 | 0.0485 |
| T + R | | 90 | 1650 | 0.0545 | |
| EB RIGHT (R) | 420 | 420 | 1650 | 0.2545 | |
| THRU (T) | 679 | 679 | 3300 | 0.2058 | |
| LEFT (L) | 40 | 40 | 1650 | 0.0242 | |
| T + R | | 1099 | 3300 | 0.3330 | 0.3330 |
| WB RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| THRU (T) | 633 | 633 | 3300 | 0.1918 | |
| LEFT (L) | 62 | 62 | 1650 | 0.0376 | 0.0376 |
| T + R | | 663 | 3300 | 0.2009 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.56
INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 3 SR 4 Bypass SB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 2-PHASE SIGNAL

300 0 840

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 914 2.1 (NO. OF LANES) 2.0 420 THRU STREET NAME: Laurel Road

RIGHT 46 1.1 0.0 0.0 0.0 0.0 0 LEFT

0 0 0

N
W + E
S

LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 300 | 300 | 1800 | 0.1667 | |
| THRU (T) | 0 | 0 | 1800 | 0.0000 | |
| LEFT (L) | 840 | 840 | 3273 | 0.2566 | 0.2566 |
| T + L | | 840 | 3273 | 0.2566 | |
| EB RIGHT (R) | 46 | 46 | 1800 | 0.0256 | |
| THRU (T) | 914 | 914 | 3600 | 0.2539 | |
| T + R | | 960 | 3600 | 0.2667 | 0.2667 |
| WB THRU (T) | 420 | 420 | 3600 | 0.1167 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.52 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 4 SR 4 Bypass NB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

LEFT 140 1.0 0.0 0.0 0.0 1.0 620 RIGHT
THRU 1615 2.0 (NO. OF LANES) 2.0 565 THRU
RIGHT 0 0.0 1.1 1.1 1.0 0.0 0 LEFT
N
W + E
S
LEFT THRU RIGHT Split? N
STREET NAME: Laurel Road
SIG WARRANTS: Urb=N, Rur=B

STREET NAME: SR 4 Bypass NB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 100 | 100 | 1720 | 0.0581 | 0.0581 |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 5 | 5 | 1720 | 0.0029 | |
| T + L | | 5 | 1720 | 0.0029 | |
| EB THRU (T) | 1615 | 1615 | 3440 | 0.4695 | 0.4695 |
| LEFT (L) | 140 | 140 | 1720 | 0.0814 | |
| WB RIGHT (R) | 620 | 620 | 1720 | 0.3605 | |
| THRU (T) | 565 | 565 | 3440 | 0.1642 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.53 | |
| INTERSECTION LEVEL OF SERVICE: | | | | A | |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 5 Slatten Ranch/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

40 180 130

LEFT 160 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 925 3.0 (NO. OF LANES) 3.1 975 THRU STREET NAME: Laurel Road

RIGHT 630 1.0 2.0 2.1 1.1 1.0 260 LEFT

170 250 160

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S LEFT THRU RIGHT Split? N

STREET NAME: Slatten Ranch

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 160 | 160 | 1650 | 0.0970 | |
| THRU (T) | 250 | 250 | 3300 | 0.0758 | |
| LEFT (L) | 170 | 170 | 3000 | 0.0567 | |
| T + R | | 410 | 3300 | 0.1242 | 0.1242 |
| SB RIGHT (R) | 40 | 40 | 1650 | 0.0242 | |
| THRU (T) | 180 | 180 | 3300 | 0.0545 | |
| LEFT (L) | 130 | 130 | 1650 | 0.0788 | 0.0788 |
| T + R | | 220 | 3300 | 0.0667 | |
| EB RIGHT (R) | 630 | 537 * | 1650 | 0.3255 | 0.3255 |
| THRU (T) | 925 | 925 | 4950 | 0.1869 | |
| LEFT (L) | 160 | 160 | 1650 | 0.0970 | |
| WB RIGHT (R) | 320 | 320 | 1650 | 0.1939 | |
| THRU (T) | 975 | 975 | 4950 | 0.1970 | |
| LEFT (L) | 260 | 260 | 1650 | 0.1576 | 0.1576 |
| T + R | | 1295 | 4950 | 0.2616 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.69

INTERSECTION LEVEL OF SERVICE: B

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 6 Live Oak Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

310 0 60

LEFT 290 2.0 1.0 0.0 1.0 1.1 Split? N

THRU 925 3.0 (NO. OF LANES) 3.1 1245 THRU STREET NAME: Laurel Road

RIGHT 0 0.0 0.0 0.0 0.0 0 LEFT

0 0 0

N
W + E
S

LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Live Oak Ave

MOVEMENT ORIGINAL VOLUME ADJUSTED VOLUME* CAPACITY V/C CRITICAL V/C

SB RIGHT (R) 310 150 * 1720 0.0872 0.0872
LEFT (L) 60 60 1720 0.0349

EB THRU (T) 925 925 5160 0.1793
LEFT (L) 290 290 3127 0.0927 0.0927

WB RIGHT (R) 90 90 1720 0.0523
THRU (T) 1245 1245 5160 0.2413
T + R 1335 5160 0.2587 0.2587

TOTAL VOLUME-TO-CAPACITY RATIO: 0.44

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 7 Empire Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
 ----- 345 310 40
 ^ | | ^
 | | |
 <--- v ---> Split? N
 LEFT 285 --- 2.0 1.0 2.0 1.0 1.0 --- 140 RIGHT
 THRU 650 ---> 2.0 (NO. OF LANES) 2.0<--- 850 THRU STREET NAME:
 RIGHT 50 --- 1.0 1.0 2.1 1.1 1.0 --- 70 LEFT Laurel Road
 <--- ^ --->
 | | |
 v v v
 N 140 220 10 SIG WARRANTS:
 W + E LEFT THRU RIGHT Split? N Urb=Y, Rur=Y
 S

STREET NAME: Empire Ave

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 10 | 10 | 1650 | 0.0061 | |
| THRU (T) | 220 | 220 | 3300 | 0.0667 | |
| LEFT (L) | 140 | 140 | 1650 | 0.0848 | 0.0848 |
| T + R | | 230 | 3300 | 0.0697 | |
| SB RIGHT (R) | 345 | 188 * | 1650 | 0.1139 | 0.1139 |
| THRU (T) | 310 | 310 | 3300 | 0.0939 | |
| LEFT (L) | 40 | 40 | 1650 | 0.0242 | |
| EB RIGHT (R) | 50 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 650 | 650 | 3300 | 0.1970 | |
| LEFT (L) | 285 | 285 | 3000 | 0.0950 | 0.0950 |
| WB RIGHT (R) | 140 | 100 * | 1650 | 0.0606 | |
| THRU (T) | 850 | 850 | 3300 | 0.2576 | 0.2576 |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.55

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 8 Canada Valley/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

26 10 328

LEFT 42 --- 2.0 1.1 1.1 1.0 1.1 --- 249 RIGHT

THRU 950 ---> 3.0 (NO. OF LANES) 3.1<--- 1460 THRU

RIGHT 20 --- 1.0 1.0 1.0 1.0 2.0 --- 260 LEFT

50 10 160

N
W + E
S

LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Canada Valley

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 160 | 17 * | 1650 | 0.0103 | 0.0103 |
| THRU (T) | 10 | 10 | 1650 | 0.0061 | |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |
| SB RIGHT (R) | 26 | 26 | 1650 | 0.0158 | |
| THRU (T) | 10 | 10 | 1650 | 0.0061 | |
| LEFT (L) | 328 | 328 | 1650 | 0.1988 | 0.1988 |
| T + R | | 36 | 1650 | 0.0218 | |
| EB RIGHT (R) | 20 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 950 | 950 | 4950 | 0.1919 | |
| LEFT (L) | 42 | 42 | 3000 | 0.0140 | 0.0140 |
| WB RIGHT (R) | 249 | 249 | 1650 | 0.1509 | |
| THRU (T) | 1460 | 1460 | 4950 | 0.2949 | |
| LEFT (L) | 260 | 260 | 3000 | 0.0867 | |
| T + R | | 1709 | 4950 | 0.3453 | 0.3453 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.57

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 9 SR 4 Bypass SB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

200 0 723

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 1156 3.0 (NO. OF LANES) 3.0 1769 THRU STREET NAME: Lone Tree Way

RIGHT 282 1.0 0.0 0.0 0.0 2.0 160 LEFT

0 0 0

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S LEFT THRU RIGHT Split? N

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 200 | 200 | 1720 | 0.1163 | |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 723 | 723 | 3127 | 0.2312 | 0.2312 |
| T + L | | 723 | 3127 | 0.2312 | |
| EB RIGHT (R) | 282 | 282 | 1720 | 0.1640 | |
| THRU (T) | 1156 | 1156 | 5160 | 0.2240 | |
| WB THRU (T) | 1769 | 1769 | 5160 | 0.3428 | 0.3428 |
| LEFT (L) | 160 | 160 | 3127 | 0.0512 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.57 | |
| INTERSECTION LEVEL OF SERVICE: | | | | A | |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 10 SR 4 Bypass NB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

LEFT 0 0.0 0.0 0.0 1.0 714 RIGHT
THRU 1580 3.0 (NO. OF LANES) 3.0 1655 THRU
RIGHT 300 1.0 2.0 1.0 2.0 70 LEFT
N
W + E 274 10 250
S LEFT THRU RIGHT Split? N
STREET NAME: Lone Tree Way
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass NB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 250 | 211 * | 1720 | 0.1227 | 0.1227 |
| THRU (T) | 10 | 10 | 1720 | 0.0058 | |
| LEFT (L) | 274 | 274 | 3127 | 0.0876 | |
| EB RIGHT (R) | 300 | 149 * | 1720 | 0.0866 | |
| THRU (T) | 1580 | 1580 | 5160 | 0.3062 | |
| WB RIGHT (R) | 714 | 714 | 1720 | 0.4151 | 0.4151 |
| THRU (T) | 1655 | 1655 | 5160 | 0.3207 | |
| LEFT (L) | 70 | 70 | 3127 | 0.0224 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.54 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

=====
Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07
=====

| Count | Date | Time | Peak | Hour |
|-------|------|------|------|------|
|-------|------|------|------|------|

STREET NAME: Slatten Ranch

| MOVEMENT | | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|----------|-----------|--------------------|---------------------|----------|--------------|-----------------|
| NB | RIGHT (R) | 30 | 30 | 1650 | 0.0182 | 0.1667 |
| | THRU (T) | 500 | 500 | 3300 | 0.1515 | |
| | LEFT (L) | 500 | 500 | 3000 | 0.1667 | |
| | T + R | | 530 | 3300 | 0.1606 | |
| SB | RIGHT (R) | 280 | 27 * | 1650 | 0.0164 | 0.0455 |
| | THRU (T) | 150 | 150 | 3300 | 0.0455 | |
| | LEFT (L) | 10 | 10 | 3000 | 0.0033 | |
| EB | RIGHT (R) | 240 | 0 * | 1650 | 0.0000 | 0.1533 |
| | THRU (T) | 1110 | 1110 | 4950 | 0.2242 | |
| | LEFT (L) | 460 | 460 | 3000 | 0.1533 | |
| WB | RIGHT (R) | 50 | 50 | 1650 | 0.0303 | 0.3515 |
| | THRU (T) | 1690 | 1690 | 4950 | 0.3414 | |
| | LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| | T + R | | 1740 | 4950 | 0.3515 | |

INTERSECTION LEVEL OF SERVICE: C

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 12 Empire Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

100 90 90
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 220 --- 1.0 1.1 2.1 1.0 1.0 --- 340 RIGHT
STREET NAME:
THRU 680 ---> 3.0 (NO. OF LANES) 3.0<--- 1200 THRU Lone Tree Way
RIGHT 260 --- 1.0 2.0 1.0 1.0 1.0 --- 30 LEFT
<--- ^ --->
| | |
v | v
N
W + E 510 200 20 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Empire Ave

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 20 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 200 | 200 | 1650 | 0.1212 | |
| LEFT (L) | 510 | 510 | 3000 | 0.1700 | 0.1700 |
| SB RIGHT (R) | 100 | 100 | 1650 | 0.0606 | 0.0606 |
| THRU (T) | 90 | 90 | 3300 | 0.0273 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | |
| T + R | | 190 | 3300 | 0.0576 | |
| EB RIGHT (R) | 260 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 680 | 680 | 4950 | 0.1374 | |
| LEFT (L) | 220 | 220 | 1650 | 0.1333 | 0.1333 |
| WB RIGHT (R) | 340 | 250 * | 1650 | 0.1515 | |
| THRU (T) | 1200 | 1200 | 4950 | 0.2424 | 0.2424 |
| LEFT (L) | 30 | 30 | 1650 | 0.0182 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.61

INTERSECTION LEVEL OF SERVICE: B

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 13 Deer Valley Rd/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

100 380 340

LEFT 110 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 700 3.1 (NO. OF LANES) 3.1 1320 THRU STREET NAME: Lone Tree Way

RIGHT 160 1.1 2.0 2.1 1.1 1.0 200 LEFT

N
W + E
S
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Deer Valley Rd

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 220 | 220 | 1650 | 0.1333 | |
| THRU (T) | 520 | 520 | 3300 | 0.1576 | |
| LEFT (L) | 450 | 450 | 3000 | 0.1500 | |
| T + R | | 740 | 3300 | 0.2242 | 0.2242 |
| SB RIGHT (R) | 100 | 100 | 1650 | 0.0606 | |
| THRU (T) | 380 | 380 | 3300 | 0.1152 | |
| LEFT (L) | 340 | 340 | 1650 | 0.2061 | 0.2061 |
| T + R | | 480 | 3300 | 0.1455 | |
| EB RIGHT (R) | 160 | 160 | 1650 | 0.0970 | |
| THRU (T) | 700 | 700 | 4950 | 0.1414 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| T + R | | 860 | 4950 | 0.1737 | |
| WB RIGHT (R) | 360 | 360 | 1650 | 0.2182 | |
| THRU (T) | 1320 | 1320 | 4950 | 0.2667 | |
| LEFT (L) | 200 | 200 | 1650 | 0.1212 | |
| T + R | | 1680 | 4950 | 0.3394 | 0.3394 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.84

INTERSECTION LEVEL OF SERVICE: D

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 14 Hillcrest Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

464 40 380
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 288 --- 1.0 1.0 2.1 2.1 1.0 --- 400 RIGHT
STREET NAME:
THRU 792 ---> 3.1 (NO. OF LANES) 3.0<--- 1256 THRU Lone Tree Way
RIGHT 30 --- 1.1 1.0 2.1 1.1 1.0 --- 40 LEFT
<--- ^ --->
| | |
v | v
N
W + E 80 70 80 SIG WARRANTS:
S LEFT THRU RIGHT Split? Y Urb=Y, Rur=Y

STREET NAME: Hillcrest Ave

| | | ORIGINAL | ADJUSTED | CAPACITY | V/C | CRITICAL |
|---------------------------------|-----------|----------|----------|----------|--------|----------|
| MOVEMENT | | VOLUME | VOLUME* | | | |
| NB | RIGHT (R) | 80 | 80 | 1650 | 0.0485 | 0.0485 |
| | THRU (T) | 70 | 70 | 3300 | 0.0212 | |
| | LEFT (L) | 80 | 80 | 1650 | 0.0485 | |
| | T + R | | 150 | 3300 | 0.0455 | |
| SB | RIGHT (R) | 464 | 176 * | 1650 | 0.1067 | |
| | THRU (T) | 40 | 40 | 3300 | 0.0121 | |
| | LEFT (L) | 380 | 380 | 3000 | 0.1267 | 0.1267 |
| | T + L | | 420 | 4650 | 0.0903 | |
| EB | RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| | THRU (T) | 792 | 792 | 4950 | 0.1600 | |
| | LEFT (L) | 288 | 288 | 1650 | 0.1745 | 0.1745 |
| | T + R | | 822 | 4950 | 0.1661 | |
| WB | RIGHT (R) | 400 | 191 * | 1650 | 0.1158 | |
| | THRU (T) | 1256 | 1256 | 4950 | 0.2537 | 0.2537 |
| | LEFT (L) | 40 | 40 | 1650 | 0.0242 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | | 0.60 |
| INTERSECTION LEVEL OF SERVICE: | | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 15 Vista Grande Dr/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 5-PHASE SIGNAL
----- 60 20 70
^ | | ^
| | |
LEFT 110 --- 1.0 <--- v ---> 1.0 --- 140 RIGHT Split? N
THRU 892 ---> 3.0 (NO. OF LANES) 3.0<--- 1316 THRU STREET NAME:
RIGHT 220 --- 1.0 1.0 1.0 1.0 --- 170 LEFT Lone Tree Way
v <--- ^ ---> v
N | | |
W + E 300 20 130 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Vista Grande Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 130 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 300 | 300 | 1650 | 0.1818 | 0.1818 |
| SB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| T + R | | 80 | 1650 | 0.0485 | 0.0485 |
| EB RIGHT (R) | 220 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 892 | 892 | 4950 | 0.1802 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| WB RIGHT (R) | 140 | 70 * | 1650 | 0.0424 | |
| THRU (T) | 1316 | 1316 | 4950 | 0.2659 | 0.2659 |
| LEFT (L) | 170 | 170 | 1650 | 0.1030 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.56

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 16 Hillcrest/Country Hills

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
----- 30 734 80
 | | |
 <--- v ---> Split? N
LEFT 70 --- 1.0 1.1 2.1 1.0 1.1 --- 60 RIGHT
THRU 40 ---> 1.0 (NO. OF LANES) 1.1<--- 60 THRU
RIGHT 50 --- 1.0 1.0 2.1 1.1 1.0 --- 110 LEFT
 | | |
 <--- ^ --->
 | | |
N 100 708 150
W + E
S LEFT THRU RIGHT Split? N
SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Hillcrest

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 150 | 150 | 1650 | 0.0909 | |
| THRU (T) | 708 | 708 | 3300 | 0.2145 | |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | |
| T + R | | 858 | 3300 | 0.2600 | 0.2600 |
| SB RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| THRU (T) | 734 | 734 | 3300 | 0.2224 | |
| LEFT (L) | 80 | 80 | 1650 | 0.0485 | 0.0485 |
| T + R | | 764 | 3300 | 0.2315 | |
| EB RIGHT (R) | 50 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 40 | 40 | 1650 | 0.0242 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | 0.0424 |
| WB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 60 | 60 | 1650 | 0.0364 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | |
| T + R | | 120 | 1650 | 0.0727 | 0.0727 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.42 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project AM Peak Hour 10/24/07

INTERSECTION 18 Hillcrest/Laurel

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

120 860 315
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 170 --- 1.0 1.1 2.1 1.0 1.0 --- 195 RIGHT
STREET NAME:
THRU 90 ---> 1.1 (NO. OF LANES) 1.0<--- 100 THRU Laurel
RIGHT 110 --- 1.1 1.0 2.1 1.1 1.0 --- 254 LEFT
<--- ^ --->
| | |
v | v
N
W + E 90 900 358 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Hillcrest

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 358 | 358 | 1650 | 0.2170 | |
| THRU (T) | 900 | 900 | 3300 | 0.2727 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | |
| T + R | | 1258 | 3300 | 0.3812 | 0.3812 |
| SB RIGHT (R) | 120 | 120 | 1650 | 0.0727 | |
| THRU (T) | 860 | 860 | 3300 | 0.2606 | |
| LEFT (L) | 315 | 315 | 1650 | 0.1909 | 0.1909 |
| T + R | | 980 | 3300 | 0.2970 | |
| EB RIGHT (R) | 110 | 110 | 1650 | 0.0667 | |
| THRU (T) | 90 | 90 | 1650 | 0.0545 | |
| LEFT (L) | 170 | 170 | 1650 | 0.1030 | |
| T + R | | 200 | 1650 | 0.1212 | 0.1212 |
| WB RIGHT (R) | 195 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 100 | 100 | 1650 | 0.0606 | |
| LEFT (L) | 254 | 254 | 1650 | 0.1539 | 0.1539 |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.85

INTERSECTION LEVEL OF SERVICE: D

=====

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 1 Canada Valley/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

0 0 0
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 0 --- 0.0 0.0 0.0 0.0 --- 0 RIGHT
STREET NAME:
THRU 566 ---> 2.1 (NO. OF LANES) 2.0<--- 836 THRU Laurel Road
RIGHT 150 --- 1.1 1.0 0.0 1.0 1.0 --- 421 LEFT
<--- ^ --->
| | |
v | v
N
W + E 40 0 278 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Canada Valley

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 278 | 0 * | 1720 | 0.0000 | |
| LEFT (L) | 40 | 40 | 1720 | 0.0233 | 0.0233 |
| EB RIGHT (R) | 150 | 150 | 1720 | 0.0872 | |
| THRU (T) | 566 | 566 | 3440 | 0.1645 | |
| T + R | | 716 | 3440 | 0.2081 | 0.2081 |
| WB THRU (T) | 836 | 836 | 3440 | 0.2430 | |
| LEFT (L) | 421 | 421 | 1720 | 0.2448 | 0.2448 |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.48
INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 2 Country Hills Dr/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

40 20 50

LEFT 60 1.0 1.1 1.1 1.0 1.1 Split? N

THRU 636 2.1 (NO. OF LANES) 2.1 1078 THRU STREET NAME: Laurel Road

RIGHT 120 1.1 1.0 1.1 1.1 1.0 182 LEFT

90 0 95

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S

LEFT THRU RIGHT Split? N

STREET NAME: Country Hills Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 95 | 95 | 1650 | 0.0576 | |
| THRU (T) | 0 | 0 | 1650 | 0.0000 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | 0.0545 |
| T + R | | 95 | 1650 | 0.0576 | |
| SB RIGHT (R) | 40 | 40 | 1650 | 0.0242 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |
| T + R | | 60 | 1650 | 0.0364 | 0.0364 |
| EB RIGHT (R) | 120 | 120 | 1650 | 0.0727 | |
| THRU (T) | 636 | 636 | 3300 | 0.1927 | |
| LEFT (L) | 60 | 60 | 1650 | 0.0364 | 0.0364 |
| T + R | | 756 | 3300 | 0.2291 | |
| WB RIGHT (R) | 100 | 100 | 1650 | 0.0606 | |
| THRU (T) | 1078 | 1078 | 3300 | 0.3267 | |
| LEFT (L) | 182 | 182 | 1650 | 0.1103 | |
| T + R | | 1178 | 3300 | 0.3570 | 0.3570 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.48

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 3 SR 4 Bypass SB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 2-PHASE SIGNAL

471 0 720

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 770 2.1 (NO. OF LANES) 2.0 890 THRU STREET NAME: Laurel Road

RIGHT 11 1.1 0.0 0.0 0.0 0.0 0 LEFT

N
W + E
S
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 471 | 471 | 1800 | 0.2617 | 0.2617 |
| THRU (T) | 0 | 0 | 1800 | 0.0000 | |
| LEFT (L) | 720 | 720 | 3273 | 0.2200 | |
| T + L | | 720 | 3273 | 0.2200 | |
| EB RIGHT (R) | 11 | 11 | 1800 | 0.0061 | |
| THRU (T) | 770 | 770 | 3600 | 0.2139 | |
| T + R | | 781 | 3600 | 0.2169 | |
| WB THRU (T) | 890 | 890 | 3600 | 0.2472 | 0.2472 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.51 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 4 SR 4 Bypass NB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

LEFT 150 --- 1.0 0.0 0.0 0.0 1.0 --- 730 RIGHT
THRU 1340 ---> 2.0 (NO. OF LANES) 2.0<--- 959 THRU
RIGHT 0 --- 0.0 1.1 1.1 1.0 0.0 --- 0 LEFT
N
W + E
S
LEFT THRU RIGHT Split? N
STREET NAME: Laurel Road
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass NB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 210 | 210 | 1720 | 0.1221 | 0.1221 |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 41 | 41 | 1720 | 0.0238 | |
| T + L | | 41 | 1720 | 0.0238 | |
| EB THRU (T) | 1340 | 1340 | 3440 | 0.3895 | |
| LEFT (L) | 150 | 150 | 1720 | 0.0872 | 0.0872 |
| WB RIGHT (R) | 730 | 730 | 1720 | 0.4244 | 0.4244 |
| THRU (T) | 959 | 959 | 3440 | 0.2788 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.63 | |
| INTERSECTION LEVEL OF SERVICE: | | | | B | |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 5 Slatten Ranch/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

110 410 230

LEFT 100 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 1160 3.0 (NO. OF LANES) 3.1 969 THRU STREET NAME: Laurel Road

RIGHT 290 1.0 2.0 2.1 1.1 1.0 260 LEFT

N
W + E
S
610 270 290
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Slatten Ranch

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 290 | 290 | 1650 | 0.1758 | |
| THRU (T) | 270 | 270 | 3300 | 0.0818 | |
| LEFT (L) | 610 | 610 | 3000 | 0.2033 | 0.2033 |
| T + R | | 560 | 3300 | 0.1697 | |
| SB RIGHT (R) | 110 | 110 | 1650 | 0.0667 | |
| THRU (T) | 410 | 410 | 3300 | 0.1242 | |
| LEFT (L) | 230 | 230 | 1650 | 0.1394 | |
| T + R | | 520 | 3300 | 0.1576 | 0.1576 |
| EB RIGHT (R) | 290 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 1160 | 1160 | 4950 | 0.2343 | 0.2343 |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | |
| WB RIGHT (R) | 220 | 220 | 1650 | 0.1333 | |
| THRU (T) | 969 | 969 | 4950 | 0.1958 | |
| LEFT (L) | 260 | 260 | 1650 | 0.1576 | 0.1576 |
| T + R | | 1189 | 4950 | 0.2402 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.75

INTERSECTION LEVEL OF SERVICE: C

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 6 Live Oak Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

290 0 130

LEFT 340 --- 2.0 1.0 0.0 1.0 1.1 --- 50 RIGHT

STREET NAME:

THRU 1340 ---> 3.0 (NO. OF LANES) 3.1<--- 1159 THRU Laurel Road

RIGHT 0 --- 0.0 0.0 0.0 0.0 --- 0 LEFT

<--- ^ --->

0 0 0

SIG WARRANTS:

Urb=Y, Rur=Y

LEFT THRU RIGHT Split? N

STREET NAME: Live Oak Ave

ORIGINAL ADJUSTED V/C CRITICAL
MOVEMENT VOLUME VOLUME* CAPACITY RATIO V/C

SB RIGHT (R) 290 103 * 1720 0.0599
LEFT (L) 130 130 1720 0.0756 0.0756

EB THRU (T) 1340 1340 5160 0.2597
LEFT (L) 340 340 3127 0.1087 0.1087

WB RIGHT (R) 50 50 1720 0.0291
THRU (T) 1159 1159 5160 0.2246
T + R 1209 5160 0.2343 0.2343

TOTAL VOLUME-TO-CAPACITY RATIO: 0.42

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 7 Empire Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
----- 413 300 60
 | | |
 <--- v ---> ^ Split? N
LEFT 420 --- 2.0 1.0 2.0 1.0 1.0 --- 50 RIGHT
THRU 890 ---> 2.0 (NO. OF LANES) 2.0<--- 686 THRU
RIGHT 160 --- 1.0 1.0 2.1 1.1 1.0 --- 50 LEFT
 | | | |
 <--- ^ ---> v
N
W + E 110 360 60
S LEFT THRU RIGHT Split? N
 | | |
 110 360 60
 LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Empire Ave

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 360 | 360 | 3300 | 0.1091 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| T + R | | 420 | 3300 | 0.1273 | |
| SB RIGHT (R) | 413 | 182 * | 1650 | 0.1103 | 0.1103 |
| THRU (T) | 300 | 300 | 3300 | 0.0909 | |
| LEFT (L) | 60 | 60 | 1650 | 0.0364 | |
| EB RIGHT (R) | 160 | 50 * | 1650 | 0.0303 | |
| THRU (T) | 890 | 890 | 3300 | 0.2697 | |
| LEFT (L) | 420 | 420 | 3000 | 0.1400 | 0.1400 |
| WB RIGHT (R) | 50 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 686 | 686 | 3300 | 0.2079 | 0.2079 |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.52

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 8 Canada Valley/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

84 20 229

LEFT 69 --- 2.0 1.1 1.1 1.0 1.1 --- 464 RIGHT Split? N

THRU 1710 ---> 3.0 (NO. OF LANES) 3.1<--- 1090 THRU STREET NAME: Lone Tree Way

RIGHT 60 --- 1.0 1.0 1.0 1.0 2.0 --- 530 LEFT

220 20 360

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S LEFT THRU RIGHT Split? N

STREET NAME: Canada Valley

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 360 | 69 * | 1650 | 0.0418 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 220 | 220 | 1650 | 0.1333 | 0.1333 |
| SB RIGHT (R) | 84 | 84 | 1650 | 0.0509 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 229 | 229 | 1650 | 0.1388 | |
| T + R | | 104 | 1650 | 0.0630 | 0.0630 |
| EB RIGHT (R) | 60 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 1710 | 1710 | 4950 | 0.3455 | 0.3455 |
| LEFT (L) | 69 | 69 | 3000 | 0.0230 | |
| WB RIGHT (R) | 464 | 464 | 1650 | 0.2812 | |
| THRU (T) | 1090 | 1090 | 4950 | 0.2202 | |
| LEFT (L) | 530 | 530 | 3000 | 0.1767 | 0.1767 |
| T + R | | 1554 | 4950 | 0.3139 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.72

INTERSECTION LEVEL OF SERVICE: C

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 9 SR 4 Bypass SB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

240 0 849

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 2051 3.0 (NO. OF LANES) 3.0 1844 THRU STREET NAME: Lone Tree Way

RIGHT 368 1.0 0.0 0.0 0.0 2.0 380 LEFT

N
W + E
S

LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 240 | 240 | 1720 | 0.1395 | |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 849 | 849 | 3127 | 0.2715 | 0.2715 |
| T + L | | 849 | 3127 | 0.2715 | |
| EB RIGHT (R) | 368 | 368 | 1720 | 0.2140 | |
| THRU (T) | 2051 | 2051 | 5160 | 0.3975 | 0.3975 |
| WB THRU (T) | 1844 | 1844 | 5160 | 0.3574 | |
| LEFT (L) | 380 | 380 | 3127 | 0.1215 | 0.1215 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.79 | |
| INTERSECTION LEVEL OF SERVICE: | | | | C | |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 10 SR 4 Bypass NB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

LEFT 0 0.0 0.0 0.0 1.0 711 RIGHT
THRU 2620 3.0 (NO. OF LANES) 3.0 1695 THRU
RIGHT 280 1.0 2.0 1.0 2.0 60 LEFT
N
W + E 530 50 340
S LEFT THRU RIGHT Split? N
STREET NAME: Lone Tree Way
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass NB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 340 | 307 * | 1720 | 0.1785 | 0.1785 |
| THRU (T) | 50 | 50 | 1720 | 0.0291 | |
| LEFT (L) | 530 | 530 | 3127 | 0.1695 | |
| EB RIGHT (R) | 280 | 0 * | 1720 | 0.0000 | |
| THRU (T) | 2620 | 2620 | 5160 | 0.5078 | 0.5078 |
| WB RIGHT (R) | 711 | 711 | 1720 | 0.4134 | |
| THRU (T) | 1695 | 1695 | 5160 | 0.3285 | |
| LEFT (L) | 60 | 60 | 3127 | 0.0192 | 0.0192 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.71 | |
| INTERSECTION LEVEL OF SERVICE: | | | | C | |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 11 Slatten Ranch/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

570 550 80
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 470 --- 2.0 1.0 2.0 2.0 1.1 --- 60 RIGHT
STREET NAME:
THRU 1970 ---> 3.0 (NO. OF LANES) 3.1<--- 1476 THRU Lone Tree Way
RIGHT 530 --- 1.0 2.0 2.1 1.1 1.0 --- 50 LEFT
<--- ^ --->
| | |
v | v
N
W + E 400 370 80 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Slatten Ranch

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 80 | 80 | 1650 | 0.0485 | |
| THRU (T) | 370 | 370 | 3300 | 0.1121 | |
| LEFT (L) | 400 | 400 | 3000 | 0.1333 | 0.1333 |
| T + R | | 450 | 3300 | 0.1364 | |
| SB RIGHT (R) | 570 | 312 * | 1650 | 0.1891 | 0.1891 |
| THRU (T) | 550 | 550 | 3300 | 0.1667 | |
| LEFT (L) | 80 | 80 | 3000 | 0.0267 | |
| EB RIGHT (R) | 530 | 310 * | 1650 | 0.1879 | |
| THRU (T) | 1970 | 1970 | 4950 | 0.3980 | |
| LEFT (L) | 470 | 470 | 3000 | 0.1567 | 0.1567 |
| WB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 1476 | 1476 | 4950 | 0.2982 | |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |
| T + R | | 1536 | 4950 | 0.3103 | 0.3103 |

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TOTAL VOLUME-TO-CAPACITY RATIO: 0.79
INTERSECTION LEVEL OF SERVICE: C

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* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

=====
Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07
=====

| Count | Date | Time | Peak | Hour |
|-------|------|------|------|------|
|-------|------|------|------|------|

| | | | | | | | | | | |
|-------------|------|------|-------|----------------|------|-------|----------|----------|------|----------------|
| CCTA METHOD | | | RIGHT | THRU | LEFT | | | | | 8-PHASE SIGNAL |
| ----- | | | 220 | 220 | 310 | | | | | |
| | | | | | | | | | | |
| | | ^ | | | | | ^ | | | |
| | | | <--- | v | ---> | | | Split? N | | |
| LEFT | 160 | --- | 1.0 | 1.1 | 2.1 | 1.0 | 1.0 | --- | 160 | RIGHT |
| | | | | | | | | | | |
| THRU | 1370 | ---> | 3.0 | (NO. OF LANES) | | | 3.0<--- | 926 | THRU | STREET NAME: |
| | | | | | | | | | | Lone Tree Way |
| RIGHT | 600 | --- | 1.0 | 2.0 | 1.0 | 1.0 | 1.0 | --- | 20 | LEFT |
| | | | | <--- | ^ | ---> | | | | |
| | | v | | | | | | v | | |
| N | | | | 440 | 120 | 40 | | | | SIG WARRANTS: |
| W + E | | | | | | | | | | Urb=Y, Rur=Y |
| S | | | | LEFT | THRU | RIGHT | Split? N | | | |

STREET NAME: Empire Ave

| MOVEMENT | | | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|----------|-----------|--|--------------------|---------------------|----------|--------------|-----------------|
| NB | RIGHT (R) | | 40 | 20 * | 1650 | 0.0121 | |
| | THRU (T) | | 120 | 120 | 1650 | 0.0727 | |
| | LEFT (L) | | 440 | 440 | 3000 | 0.1467 | 0.1467 |
| SB | RIGHT (R) | | 220 | 220 | 1650 | 0.1333 | 0.1333 |
| | THRU (T) | | 220 | 220 | 3300 | 0.0667 | |
| | LEFT (L) | | 310 | 310 | 1650 | 0.1879 | |
| | T + R | | | 440 | 3300 | 0.1333 | |
| EB | RIGHT (R) | | 600 | 358 * | 1650 | 0.2170 | |
| | THRU (T) | | 1370 | 1370 | 4950 | 0.2768 | 0.2768 |
| | LEFT (L) | | 160 | 160 | 1650 | 0.0970 | |
| WB | RIGHT (R) | | 160 | 0 * | 1650 | 0.0000 | |
| | THRU (T) | | 926 | 926 | 4950 | 0.1871 | |
| | LEFT (L) | | 20 | 20 | 1650 | 0.0121 | 0.0121 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.57

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025 . INT , VOL=2025NP . PMV , CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 13 Deer Valley Rd/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

150 510 310
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 320 --- 1.0 1.1 2.1 1.0 1.1 --- 160 RIGHT
STREET NAME:
THRU 1782 ---> 3.1 (NO. OF LANES) 3.1<--- 1400 THRU Lone Tree Way
RIGHT 190 --- 1.1 2.0 2.1 1.1 1.0 --- 190 LEFT
<--- ^ --->
| | |
v | v
N
W + E 260 400 180 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Deer Valley Rd

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 180 | 180 | 1650 | 0.1091 | |
| THRU (T) | 400 | 400 | 3300 | 0.1212 | |
| LEFT (L) | 260 | 260 | 3000 | 0.0867 | |
| T + R | | 580 | 3300 | 0.1758 | 0.1758 |
| SB RIGHT (R) | 150 | 150 | 1650 | 0.0909 | |
| THRU (T) | 510 | 510 | 3300 | 0.1545 | |
| LEFT (L) | 310 | 310 | 1650 | 0.1879 | 0.1879 |
| T + R | | 660 | 3300 | 0.2000 | |
| EB RIGHT (R) | 190 | 190 | 1650 | 0.1152 | |
| THRU (T) | 1782 | 1782 | 4950 | 0.3600 | |
| LEFT (L) | 320 | 320 | 1650 | 0.1939 | |
| T + R | | 1972 | 4950 | 0.3984 | 0.3984 |
| WB RIGHT (R) | 160 | 160 | 1650 | 0.0970 | |
| THRU (T) | 1400 | 1400 | 4950 | 0.2828 | |
| LEFT (L) | 190 | 190 | 1650 | 0.1152 | 0.1152 |
| T + R | | 1560 | 4950 | 0.3152 | |

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TOTAL VOLUME-TO-CAPACITY RATIO: 0.88

INTERSECTION LEVEL OF SERVICE: D

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* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 14 Hillcrest Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

446 120 580

LEFT 703 --- 1.0 1.0 2.1 2.1 1.0 --- 480 RIGHT

THRU 1589 ---> 3.1 (NO. OF LANES) 3.0<--- 1354 THRU

RIGHT 80 --- 1.1 1.0 2.1 1.1 1.0 --- 100 LEFT

<--- ^ --->

N
W + E
S

LEFT THRU RIGHT Split? Y

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Hillcrest Ave

ORIGINAL ADJUSTED V/C CRITICAL
MOVEMENT VOLUME VOLUME* CAPACITY RATIO V/C

NB RIGHT (R) 60 60 1650 0.0364
THRU (T) 70 70 3300 0.0212
LEFT (L) 50 50 1650 0.0303
T + R 130 3300 0.0394 0.0394

SB RIGHT (R) 446 0 * 1650 0.0000
THRU (T) 120 120 3300 0.0364
LEFT (L) 580 580 3000 0.1933 0.1933
T + L 700 4650 0.1505

EB RIGHT (R) 80 80 1650 0.0485
THRU (T) 1589 1589 4950 0.3210
LEFT (L) 703 703 1650 0.4261 0.4261
T + R 1669 4950 0.3372

WB RIGHT (R) 480 161 * 1650 0.0976
THRU (T) 1354 1354 4950 0.2735 0.2735
LEFT (L) 100 100 1650 0.0606

TOTAL VOLUME-TO-CAPACITY RATIO: 0.93

INTERSECTION LEVEL OF SERVICE: E

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 15 Vista Grande Dr/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 5-PHASE SIGNAL
----- 170 40 70
 | | |
 <--- v ---> Split? N
LEFT 190 --- 1.0 1.1 1.1 1.0 1.0 --- 90 RIGHT
THRU 1649 ---> 3.0 (NO. OF LANES) 3.0<--- 1204 THRU
RIGHT 390 --- 1.0 1.0 1.0 1.0 1.0 --- 300 LEFT
 | | |
 <--- ^ --->
 | | |
N 320 50 220
W + E
S LEFT THRU RIGHT Split? N
SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Vista Grande Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 220 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 50 | 50 | 1650 | 0.0303 | |
| LEFT (L) | 320 | 320 | 1650 | 0.1939 | 0.1939 |
| SB RIGHT (R) | 170 | 170 | 1650 | 0.1030 | |
| THRU (T) | 40 | 40 | 1650 | 0.0242 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| T + R | | 210 | 1650 | 0.1273 | 0.1273 |
| EB RIGHT (R) | 390 | 70 * | 1650 | 0.0424 | |
| THRU (T) | 1649 | 1649 | 4950 | 0.3331 | 0.3331 |
| LEFT (L) | 190 | 190 | 1650 | 0.1152 | |
| WB RIGHT (R) | 90 | 20 * | 1650 | 0.0121 | |
| THRU (T) | 1204 | 1204 | 4950 | 0.2432 | |
| LEFT (L) | 300 | 300 | 1650 | 0.1818 | 0.1818 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.84 | |
| INTERSECTION LEVEL OF SERVICE: | | | | D | |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 16 Hillcrest/Country Hills

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
----- 80 916 110
 | | |
 <--- v ---> ^ Split? N
LEFT 70 --- 1.0 1.1 2.1 1.0 1.1 --- 90 RIGHT
THRU 20 ---> 1.0 (NO. OF LANES) 1.1<--- 50 THRU
RIGHT 100 --- 1.0 1.0 2.1 1.1 1.0 --- 120 LEFT
 | ^ | | v
 v | | | v
N 100 1053 70
W + E
S LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Hillcrest

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 70 | 70 | 1650 | 0.0424 | |
| THRU (T) | 1053 | 1053 | 3300 | 0.3191 | |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | |
| T + R | | 1123 | 3300 | 0.3403 | 0.3403 |
| SB RIGHT (R) | 80 | 80 | 1650 | 0.0485 | |
| THRU (T) | 916 | 916 | 3300 | 0.2776 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| T + R | | 996 | 3300 | 0.3018 | |
| EB RIGHT (R) | 100 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | 0.0424 |
| WB RIGHT (R) | 90 | 90 | 1650 | 0.0545 | |
| THRU (T) | 50 | 50 | 1650 | 0.0303 | |
| LEFT (L) | 120 | 120 | 1650 | 0.0727 | |
| T + R | | 140 | 1650 | 0.0848 | 0.0848 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.53

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 No Project PM Peak Hour 10/24/07

INTERSECTION 18 Hillcrest/Laurel

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

220 910 273
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 140 --- 1.0 1.1 2.1 1.0 1.0 --- 240 RIGHT
STREET NAME:
THRU 80 ---> 1.1 (NO. OF LANES) 1.0<--- 120 THRU Laurel
RIGHT 110 --- 1.1 1.0 2.1 1.1 1.0 --- 346 LEFT
<--- ^ --->
| | |
v | v
N |
W + E 90 970 283 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Hillcrest

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 283 | 283 | 1650 | 0.1715 | |
| THRU (T) | 970 | 970 | 3300 | 0.2939 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | |
| T + R | | 1253 | 3300 | 0.3797 | 0.3797 |
| SB RIGHT (R) | 220 | 220 | 1650 | 0.1333 | |
| THRU (T) | 910 | 910 | 3300 | 0.2758 | |
| LEFT (L) | 273 | 273 | 1650 | 0.1655 | 0.1655 |
| T + R | | 1130 | 3300 | 0.3424 | |
| EB RIGHT (R) | 110 | 110 | 1650 | 0.0667 | |
| THRU (T) | 80 | 80 | 1650 | 0.0485 | |
| LEFT (L) | 140 | 140 | 1650 | 0.0848 | |
| T + R | | 190 | 1650 | 0.1152 | 0.1152 |
| WB RIGHT (R) | 240 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 120 | 120 | 1650 | 0.0727 | |
| LEFT (L) | 346 | 346 | 1650 | 0.2097 | 0.2097 |

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TOTAL VOLUME-TO-CAPACITY RATIO: 0.87

INTERSECTION LEVEL OF SERVICE: D

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* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025NP.PMV,CAP=

Cumulative With Project

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 1 Canada Valley/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

0 0 0
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 0 --- 0.0 0.0 0.0 0.0 --- 0 RIGHT
STREET NAME:
THRU 960 ---> 2.1 (NO. OF LANES) 2.0<--- 670 THRU Laurel Road
RIGHT 100 --- 1.1 1.0 0.0 1.0 1.0 --- 260 LEFT
<--- ^ --->
| | |
v | v
N
W + E 120 0 290 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Canada Valley

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 290 | 30 * | 1720 | 0.0174 | |
| LEFT (L) | 120 | 120 | 1720 | 0.0698 | 0.0698 |
| EB RIGHT (R) | 100 | 100 | 1720 | 0.0581 | |
| THRU (T) | 960 | 960 | 3440 | 0.2791 | |
| T + R | | 1060 | 3440 | 0.3081 | 0.3081 |
| WB THRU (T) | 670 | 670 | 3440 | 0.1948 | |
| LEFT (L) | 260 | 260 | 1720 | 0.1512 | 0.1512 |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.53
INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 2 Country Hills Dr/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

60 30 80
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 40 --- 1.0 1.1 1.1 1.0 1.1 --- 30 RIGHT
STREET NAME:
THRU 760 ---> 2.1 (NO. OF LANES) 2.1<--- 660 THRU Laurel Road
RIGHT 420 --- 1.1 1.0 1.1 1.1 1.0 --- 100 LEFT
| | |
<--- ^ --->
v | v
N |
W + E 160 20 330 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Country Hills Dr

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 330 | 330 | 1650 | 0.2000 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 160 | 160 | 1650 | 0.0970 | |
| T + R | | 350 | 1650 | 0.2121 | 0.2121 |
| SB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 30 | 30 | 1650 | 0.0182 | |
| LEFT (L) | 80 | 80 | 1650 | 0.0485 | 0.0485 |
| T + R | | 90 | 1650 | 0.0545 | |
| EB RIGHT (R) | 420 | 420 | 1650 | 0.2545 | |
| THRU (T) | 760 | 760 | 3300 | 0.2303 | |
| LEFT (L) | 40 | 40 | 1650 | 0.0242 | |
| T + R | | 1180 | 3300 | 0.3576 | 0.3576 |
| WB RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| THRU (T) | 660 | 660 | 3300 | 0.2000 | |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | 0.0606 |
| T + R | | 690 | 3300 | 0.2091 | |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.68

INTERSECTION LEVEL OF SERVICE: B

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* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 3 SR 4 Bypass SB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 2-PHASE SIGNAL

340 0 840

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 1080 2.1 (NO. OF LANES) 2.0 450 THRU STREET NAME: Laurel Road

RIGHT 90 1.1 0.0 0.0 0.0 0.0 0 LEFT

N
W + E
S
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 340 | 340 | 1800 | 0.1889 | |
| THRU (T) | 0 | 0 | 1800 | 0.0000 | |
| LEFT (L) | 840 | 840 | 3273 | 0.2566 | 0.2566 |
| T + L | | 840 | 3273 | 0.2566 | |
| EB RIGHT (R) | 90 | 90 | 1800 | 0.0500 | |
| THRU (T) | 1080 | 1080 | 3600 | 0.3000 | |
| T + R | | 1170 | 3600 | 0.3250 | 0.3250 |
| WB THRU (T) | 450 | 450 | 3600 | 0.1250 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.58 | |
| INTERSECTION LEVEL OF SERVICE: | | | | A | |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 4 SR 4 Bypass NB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

LEFT 260 --- 1.0 0.0 0.0 0.0 1.0 --- 620 RIGHT
THRU 1660 ---> 2.0 (NO. OF LANES) 2.0<--- 580 THRU
RIGHT 0 --- 0.0 1.1 1.1 1.0 0.0 --- 0 LEFT
N
W + E
S
LEFT THRU RIGHT Split? N

STREET NAME: SR 4 Bypass NB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 100 | 100 | 1720 | 0.0581 | 0.0581 |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 20 | 20 | 1720 | 0.0116 | |
| T + L | | 20 | 1720 | 0.0116 | |
| EB THRU (T) | 1660 | 1660 | 3440 | 0.4826 | |
| LEFT (L) | 260 | 260 | 1720 | 0.1512 | 0.1512 |
| WB RIGHT (R) | 620 | 620 | 1720 | 0.3605 | 0.3605 |
| THRU (T) | 580 | 580 | 3440 | 0.1686 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.57 | |
| INTERSECTION LEVEL OF SERVICE: | | | | A | |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 5 Slatten Ranch/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

40 180 130

LEFT 160 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 970 3.0 (NO. OF LANES) 3.1 990 THRU STREET NAME: Laurel Road

RIGHT 630 1.0 2.0 2.1 1.1 1.0 260 LEFT

170 250 160

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S LEFT THRU RIGHT Split? N

STREET NAME: Slatten Ranch

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 160 | 160 | 1650 | 0.0970 | |
| THRU (T) | 250 | 250 | 3300 | 0.0758 | |
| LEFT (L) | 170 | 170 | 3000 | 0.0567 | |
| T + R | | 410 | 3300 | 0.1242 | 0.1242 |
| SB RIGHT (R) | 40 | 40 | 1650 | 0.0242 | |
| THRU (T) | 180 | 180 | 3300 | 0.0545 | |
| LEFT (L) | 130 | 130 | 1650 | 0.0788 | 0.0788 |
| T + R | | 220 | 3300 | 0.0667 | |
| EB RIGHT (R) | 630 | 537 * | 1650 | 0.3255 | 0.3255 |
| THRU (T) | 970 | 970 | 4950 | 0.1960 | |
| LEFT (L) | 160 | 160 | 1650 | 0.0970 | |
| WB RIGHT (R) | 320 | 320 | 1650 | 0.1939 | |
| THRU (T) | 990 | 990 | 4950 | 0.2000 | |
| LEFT (L) | 260 | 260 | 1650 | 0.1576 | 0.1576 |
| T + R | | 1310 | 4950 | 0.2646 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.69

INTERSECTION LEVEL OF SERVICE: B

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 6 Live Oak Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

310 0 60

LEFT 290 --- 2.0 1.0 0.0 1.0 1.1 --- 90 RIGHT

THRU 970 ---> 3.0 (NO. OF LANES) 3.1<--- 1260 THRU STREET NAME: Laurel Road

RIGHT 0 --- 0.0 0.0 0.0 0.0 --- 0 LEFT

N
W + E
S
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Live Oak Ave

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 310 | 150 * | 1720 | 0.0872 | 0.0872 |
| LEFT (L) | 60 | 60 | 1720 | 0.0349 | |
| EB THRU (T) | 970 | 970 | 5160 | 0.1880 | |
| LEFT (L) | 290 | 290 | 3127 | 0.0927 | 0.0927 |
| WB RIGHT (R) | 90 | 90 | 1720 | 0.0523 | |
| THRU (T) | 1260 | 1260 | 5160 | 0.2442 | |
| T + R | | 1350 | 5160 | 0.2616 | 0.2616 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.44 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 7 Empire Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
 ----- 350 310 40
 ^ | | ^
 | | |
 <--- v ---> Split? N
 LEFT 300 --- 2.0 1.0 2.0 1.0 1.0 --- 140 RIGHT
 THRU 680 ---> 2.0 (NO. OF LANES) 2.0<--- 860 THRU STREET NAME:
 RIGHT 50 --- 1.0 1.0 2.1 1.1 1.0 --- 70 LEFT Laurel Road
 ^ | | ^
 | | |
 <--- v --->
 N | | |
 W + E 140 220 10 SIG WARRANTS:
 S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Empire Ave

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 10 | 10 | 1650 | 0.0061 | |
| THRU (T) | 220 | 220 | 3300 | 0.0667 | |
| LEFT (L) | 140 | 140 | 1650 | 0.0848 | 0.0848 |
| T + R | | 230 | 3300 | 0.0697 | |
| SB RIGHT (R) | 350 | 185 * | 1650 | 0.1121 | 0.1121 |
| THRU (T) | 310 | 310 | 3300 | 0.0939 | |
| LEFT (L) | 40 | 40 | 1650 | 0.0242 | |
| EB RIGHT (R) | 50 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 680 | 680 | 3300 | 0.2061 | |
| LEFT (L) | 300 | 300 | 3000 | 0.1000 | 0.1000 |
| WB RIGHT (R) | 140 | 100 * | 1650 | 0.0606 | |
| THRU (T) | 860 | 860 | 3300 | 0.2606 | 0.2606 |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.56

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 8 Canada Valley/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

80 10 360

LEFT 60 --- 2.0 1.1 1.1 1.0 1.1 --- 260 RIGHT Split? N

THRU 950 ---> 3.0 (NO. OF LANES) 3.1<--- 1460 THRU STREET NAME: Lone Tree Way

RIGHT 20 --- 1.0 1.0 1.0 1.0 2.0 --- 260 LEFT

50 10 160

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S LEFT THRU RIGHT Split? N

STREET NAME: Canada Valley

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 160 | 17 * | 1650 | 0.0103 | 0.0103 |
| THRU (T) | 10 | 10 | 1650 | 0.0061 | |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |
| SB RIGHT (R) | 80 | 80 | 1650 | 0.0485 | |
| THRU (T) | 10 | 10 | 1650 | 0.0061 | |
| LEFT (L) | 360 | 360 | 1650 | 0.2182 | 0.2182 |
| T + R | | 90 | 1650 | 0.0545 | |
| EB RIGHT (R) | 20 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 950 | 950 | 4950 | 0.1919 | |
| LEFT (L) | 60 | 60 | 3000 | 0.0200 | 0.0200 |
| WB RIGHT (R) | 260 | 260 | 1650 | 0.1576 | |
| THRU (T) | 1460 | 1460 | 4950 | 0.2949 | |
| LEFT (L) | 260 | 260 | 3000 | 0.0867 | |
| T + R | | 1720 | 4950 | 0.3475 | 0.3475 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.60

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 9 SR 4 Bypass SB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

200 0 740

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 1170 3.0 (NO. OF LANES) 3.0 1780 THRU STREET NAME: Lone Tree Way

RIGHT 300 1.0 0.0 0.0 0.0 2.0 160 LEFT

0 0 0

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S LEFT THRU RIGHT Split? N

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 200 | 200 | 1720 | 0.1163 | |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 740 | 740 | 3127 | 0.2366 | 0.2366 |
| T + L | | 740 | 3127 | 0.2366 | |
| EB RIGHT (R) | 300 | 300 | 1720 | 0.1744 | |
| THRU (T) | 1170 | 1170 | 5160 | 0.2267 | |
| WB THRU (T) | 1780 | 1780 | 5160 | 0.3450 | 0.3450 |
| LEFT (L) | 160 | 160 | 3127 | 0.0512 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.58 | |
| INTERSECTION LEVEL OF SERVICE: | | | | A | |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 10 SR 4 Bypass NB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

0 0 0
| | |
^ | ^
| | |
LEFT 0 --- 0.0 <--- v ---> 1.0 --- 720 RIGHT Split? N
STREET NAME:
THRU 1610 ---> 3.0 (NO. OF LANES) 3.0<--- 1660 THRU Lone Tree Way
RIGHT 300 --- 1.0 2.0 1.0 1.0 2.0 --- 70 LEFT
| | |
<--- ^ --->
| | |
v v
N
W + E 280 10 250 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass NB

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 250 | 211 * | 1720 | 0.1227 | 0.1227 |
| THRU (T) | 10 | 10 | 1720 | 0.0058 | |
| LEFT (L) | 280 | 280 | 3127 | 0.0895 | |
| EB RIGHT (R) | 300 | 146 * | 1720 | 0.0849 | |
| THRU (T) | 1610 | 1610 | 5160 | 0.3120 | |
| WB RIGHT (R) | 720 | 720 | 1720 | 0.4186 | 0.4186 |
| THRU (T) | 1660 | 1660 | 5160 | 0.3217 | |
| LEFT (L) | 70 | 70 | 3127 | 0.0224 | |

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TOTAL VOLUME-TO-CAPACITY RATIO: 0.54
INTERSECTION LEVEL OF SERVICE: A

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* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 11 Slatten Ranch/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
 ----- 280 150 10
 ^ | | ^
 | | |
 <--- v ---> Split? N
 LEFT 460 --- 2.0 1.0 2.0 2.0 1.1 --- 50 RIGHT
 THRU 1140 ---> 3.0 (NO. OF LANES) 3.1<--- 1700 THRU
 RIGHT 240 --- 1.0 2.0 2.1 1.1 1.0 --- 70 LEFT
 ^ | | ^
 | | |
 <--- v --->
 N | |
 W + E 500 500 30
 S LEFT THRU RIGHT Split? N
 STREET NAME: Lone Tree Way
 SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: Slatten Ranch

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| THRU (T) | 500 | 500 | 3300 | 0.1515 | |
| LEFT (L) | 500 | 500 | 3000 | 0.1667 | 0.1667 |
| T + R | | 530 | 3300 | 0.1606 | |
| SB RIGHT (R) | 280 | 27 * | 1650 | 0.0164 | |
| THRU (T) | 150 | 150 | 3300 | 0.0455 | 0.0455 |
| LEFT (L) | 10 | 10 | 3000 | 0.0033 | |
| EB RIGHT (R) | 240 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 1140 | 1140 | 4950 | 0.2303 | |
| LEFT (L) | 460 | 460 | 3000 | 0.1533 | 0.1533 |
| WB RIGHT (R) | 50 | 50 | 1650 | 0.0303 | |
| THRU (T) | 1700 | 1700 | 4950 | 0.3434 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| T + R | | 1750 | 4950 | 0.3535 | 0.3535 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.72

INTERSECTION LEVEL OF SERVICE: C

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 12 Empire Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

100 90 90
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 220 --- 1.0 1.1 2.1 1.0 1.0 --- 340 RIGHT
STREET NAME:
THRU 710 ---> 3.0 (NO. OF LANES) 3.0<--- 1210 THRU Lone Tree Way
RIGHT 260 --- 1.0 2.0 1.0 1.0 1.0 --- 30 LEFT
<--- ^ --->
| | |
v | v
N
W + E 510 200 20 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Empire Ave

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 20 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 200 | 200 | 1650 | 0.1212 | |
| LEFT (L) | 510 | 510 | 3000 | 0.1700 | 0.1700 |
| SB RIGHT (R) | 100 | 100 | 1650 | 0.0606 | 0.0606 |
| THRU (T) | 90 | 90 | 3300 | 0.0273 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | |
| T + R | | 190 | 3300 | 0.0576 | |
| EB RIGHT (R) | 260 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 710 | 710 | 4950 | 0.1434 | |
| LEFT (L) | 220 | 220 | 1650 | 0.1333 | 0.1333 |
| WB RIGHT (R) | 340 | 250 * | 1650 | 0.1515 | |
| THRU (T) | 1210 | 1210 | 4950 | 0.2444 | 0.2444 |
| LEFT (L) | 30 | 30 | 1650 | 0.0182 | |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.61
INTERSECTION LEVEL OF SERVICE: B

=====

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 13 Deer Valley Rd/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

100 380 340

LEFT 110 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 720 3.1 (NO. OF LANES) 3.1 1380 THRU STREET NAME: Lone Tree Way

RIGHT 160 1.1 2.0 2.1 1.1 1.0 200 LEFT

N
W + E
S
450 520 220
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Deer Valley Rd

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 220 | 220 | 1650 | 0.1333 | |
| THRU (T) | 520 | 520 | 3300 | 0.1576 | |
| LEFT (L) | 450 | 450 | 3000 | 0.1500 | |
| T + R | | 740 | 3300 | 0.2242 | 0.2242 |
| SB RIGHT (R) | 100 | 100 | 1650 | 0.0606 | |
| THRU (T) | 380 | 380 | 3300 | 0.1152 | |
| LEFT (L) | 340 | 340 | 1650 | 0.2061 | 0.2061 |
| T + R | | 480 | 3300 | 0.1455 | |
| EB RIGHT (R) | 160 | 160 | 1650 | 0.0970 | |
| THRU (T) | 720 | 720 | 4950 | 0.1455 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| T + R | | 880 | 4950 | 0.1778 | |
| WB RIGHT (R) | 360 | 360 | 1650 | 0.2182 | |
| THRU (T) | 1380 | 1380 | 4950 | 0.2788 | |
| LEFT (L) | 200 | 200 | 1650 | 0.1212 | |
| T + R | | 1740 | 4950 | 0.3515 | 0.3515 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.85

INTERSECTION LEVEL OF SERVICE: D

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 14 Hillcrest Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

470 40 380

LEFT 290 1.0 1.0 2.1 2.1 1.0 Split? N

THRU 810 3.1 (NO. OF LANES) 3.0 1310 THRU STREET NAME: Lone Tree Way

RIGHT 30 1.1 1.0 2.1 1.1 1.0 40 LEFT

80 70 80

N
W + E
S

LEFT THRU RIGHT Split? Y

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Hillcrest Ave

MOVEMENT ORIGINAL VOLUME ADJUSTED VOLUME* CAPACITY V/C CRITICAL V/C

NB RIGHT (R) 80 80 1650 0.0485 0.0485
THRU (T) 70 70 3300 0.0212
LEFT (L) 80 80 1650 0.0485
T + R 150 3300 0.0455

SB RIGHT (R) 470 180 * 1650 0.1091
THRU (T) 40 40 3300 0.0121
LEFT (L) 380 380 3000 0.1267 0.1267
T + L 420 4650 0.0903

EB RIGHT (R) 30 30 1650 0.0182
THRU (T) 810 810 4950 0.1636
LEFT (L) 290 290 1650 0.1758 0.1758
T + R 840 4950 0.1697

WB RIGHT (R) 400 191 * 1650 0.1158
THRU (T) 1310 1310 4950 0.2646 0.2646
LEFT (L) 40 40 1650 0.0242

TOTAL VOLUME-TO-CAPACITY RATIO: 0.62

INTERSECTION LEVEL OF SERVICE: B

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 15 Vista Grande Dr/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 5-PHASE SIGNAL

60 20 70

LEFT 110 1.0 1.1 1.1 1.0 1.0 Split? N

THRU 910 3.0 (NO. OF LANES) 3.0 1370 THRU STREET NAME:
Lone Tree Way

RIGHT 220 1.0 1.0 1.0 1.0 170 LEFT

300 20 130
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Vista Grande Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 130 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 300 | 300 | 1650 | 0.1818 | 0.1818 |
| SB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| T + R | | 80 | 1650 | 0.0485 | 0.0485 |
| EB RIGHT (R) | 220 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 910 | 910 | 4950 | 0.1838 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| WB RIGHT (R) | 140 | 70 * | 1650 | 0.0424 | |
| THRU (T) | 1370 | 1370 | 4950 | 0.2768 | 0.2768 |
| LEFT (L) | 170 | 170 | 1650 | 0.1030 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.57

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 16 Hillcrest/Country Hills

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL
----- 30 740 80
 | | |
 <--- v ---> Split? N
LEFT 70 --- 1.0 1.1 2.1 1.0 1.1 --- 60 RIGHT
THRU 40 ---> 1.0 (NO. OF LANES) 1.1<--- 60 THRU
RIGHT 50 --- 1.0 1.0 2.1 1.1 1.0 --- 110 LEFT
 | | |
 <--- ^ ---> v
N
W + E 100 710 150 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Hillcrest

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 150 | 150 | 1650 | 0.0909 | |
| THRU (T) | 710 | 710 | 3300 | 0.2152 | |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | |
| T + R | | 860 | 3300 | 0.2606 | 0.2606 |
| SB RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| THRU (T) | 740 | 740 | 3300 | 0.2242 | |
| LEFT (L) | 80 | 80 | 1650 | 0.0485 | 0.0485 |
| T + R | | 770 | 3300 | 0.2333 | |
| EB RIGHT (R) | 50 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 40 | 40 | 1650 | 0.0242 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | 0.0424 |
| WB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 60 | 60 | 1650 | 0.0364 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | |
| T + R | | 120 | 1650 | 0.0727 | 0.0727 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.42 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project AM Peak Hour 10/24/07

INTERSECTION 18 Hillcrest/Laurel

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

120 860 320

LEFT 170 --- 1.0 1.1 2.1 1.0 1.0 --- 210 RIGHT

THRU 80 ---> 1.1 (NO. OF LANES) 1.0<--- 100 THRU STREET NAME: Laurel

RIGHT 110 --- 1.1 1.0 2.1 1.1 1.0 --- 260 LEFT

90 900 360

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S

LEFT THRU RIGHT Split? N

STREET NAME: Hillcrest

ORIGINAL ADJUSTED V/C CRITICAL
MOVEMENT VOLUME VOLUME* CAPACITY RATIO V/C

NB RIGHT (R) 360 360 1650 0.2182
THRU (T) 900 900 3300 0.2727
LEFT (L) 90 90 1650 0.0545
T + R 1260 3300 0.3818 0.3818

SB RIGHT (R) 120 120 1650 0.0727
THRU (T) 860 860 3300 0.2606
LEFT (L) 320 320 1650 0.1939 0.1939
T + R 980 3300 0.2970

EB RIGHT (R) 110 110 1650 0.0667
THRU (T) 80 80 1650 0.0485
LEFT (L) 170 170 1650 0.1030
T + R 190 1650 0.1152 0.1152

WB RIGHT (R) 210 0 * 1650 0.0000
THRU (T) 100 100 1650 0.0606
LEFT (L) 260 260 1650 0.1576 0.1576

TOTAL VOLUME-TO-CAPACITY RATIO: 0.85

INTERSECTION LEVEL OF SERVICE: D

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 1 Canada Valley/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

0 0 0
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 0 --- 0.0 0.0 0.0 0.0 --- 0 RIGHT
STREET NAME:
THRU 590 ---> 2.1 (NO. OF LANES) 2.0<--- 850 THRU Laurel Road
RIGHT 150 --- 1.1 1.0 0.0 1.0 1.0 --- 490 LEFT
<--- ^ --->
| | |
v | v
N |
W + E 40 0 320
S LEFT THRU RIGHT Split? N
SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Canada Valley

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 320 | 0 * | 1720 | 0.0000 | |
| LEFT (L) | 40 | 40 | 1720 | 0.0233 | 0.0233 |
| EB RIGHT (R) | 150 | 150 | 1720 | 0.0872 | |
| THRU (T) | 590 | 590 | 3440 | 0.1715 | |
| T + R | | 740 | 3440 | 0.2151 | 0.2151 |
| WB THRU (T) | 850 | 850 | 3440 | 0.2471 | |
| LEFT (L) | 490 | 490 | 1720 | 0.2849 | 0.2849 |

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TOTAL VOLUME-TO-CAPACITY RATIO: 0.52
INTERSECTION LEVEL OF SERVICE: A

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* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 2 Country Hills Dr/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

40 20 50

LEFT 60 1.0 1.1 1.1 1.0 1.1 Split? N

THRU 690 2.1 (NO. OF LANES) 2.1 1170 THRU STREET NAME: Laurel Road

RIGHT 120 1.1 1.0 1.1 1.1 1.0 310 LEFT

90 0 170

N SIG WARRANTS: Urb=Y, Rur=Y
W + E
S

LEFT THRU RIGHT Split? N

STREET NAME: Country Hills Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 170 | 170 | 1650 | 0.1030 | 0.1030 |
| THRU (T) | 0 | 0 | 1650 | 0.0000 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | |
| T + R | | 170 | 1650 | 0.1030 | |
| SB RIGHT (R) | 40 | 40 | 1650 | 0.0242 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | 0.0303 |
| T + R | | 60 | 1650 | 0.0364 | |
| EB RIGHT (R) | 120 | 120 | 1650 | 0.0727 | |
| THRU (T) | 690 | 690 | 3300 | 0.2091 | |
| LEFT (L) | 60 | 60 | 1650 | 0.0364 | |
| T + R | | 810 | 3300 | 0.2455 | 0.2455 |
| WB RIGHT (R) | 100 | 100 | 1650 | 0.0606 | |
| THRU (T) | 1170 | 1170 | 3300 | 0.3545 | |
| LEFT (L) | 310 | 310 | 1650 | 0.1879 | 0.1879 |
| T + R | | 1270 | 3300 | 0.3848 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.57

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 3 SR 4 Bypass SB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 2-PHASE SIGNAL
----- 590 0 720
LEFT 0 --- 0.0 1.0 1.1 2.1 0.0 --- 0 RIGHT
THRU 870 ---> 2.1 (NO. OF LANES) 2.0<--- 990 THRU
RIGHT 40 --- 1.1 0.0 0.0 0.0 0.0 --- 0 LEFT
N
W + E
S
LEFT THRU RIGHT Split? N
STREET NAME: Laurel Road
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 590 | 590 | 1800 | 0.3278 | 0.3278 |
| THRU (T) | 0 | 0 | 1800 | 0.0000 | |
| LEFT (L) | 720 | 720 | 3273 | 0.2200 | |
| T + L | | 720 | 3273 | 0.2200 | |
| EB RIGHT (R) | 40 | 40 | 1800 | 0.0222 | |
| THRU (T) | 870 | 870 | 3600 | 0.2417 | |
| T + R | | 910 | 3600 | 0.2528 | |
| WB THRU (T) | 990 | 990 | 3600 | 0.2750 | 0.2750 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.60 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 4 SR 4 Bypass NB/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

0 0 0
| | |
^ | ^
| | |
LEFT 220 --- 1.0 0.0 0.0 0.0 1.0 --- 730 RIGHT
THRU 1370 ---> 2.0 (NO. OF LANES) 2.0<--- 1010 THRU
RIGHT 0 --- 0.0 1.1 1.1 1.0 0.0 --- 0 LEFT
| | |
<--- ^ --->
| | |
N | |
W + E 90 0 210
S LEFT THRU RIGHT Split? N
STREET NAME: Laurel Road
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass NB

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 210 | 210 | 1720 | 0.1221 | 0.1221 |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 90 | 90 | 1720 | 0.0523 | |
| T + L | | 90 | 1720 | 0.0523 | |
| EB THRU (T) | 1370 | 1370 | 3440 | 0.3983 | |
| LEFT (L) | 220 | 220 | 1720 | 0.1279 | 0.1279 |
| WB RIGHT (R) | 730 | 730 | 1720 | 0.4244 | 0.4244 |
| THRU (T) | 1010 | 1010 | 3440 | 0.2936 | |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.67
INTERSECTION LEVEL OF SERVICE: B

=====

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 5 Slatten Ranch/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

110 410 230

LEFT 100 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 1190 3.0 (NO. OF LANES) 3.1 1020 THRU STREET NAME:
Laurel Road

RIGHT 290 1.0 2.0 2.1 1.1 1.0 260 LEFT

N
W + E
S
610 270 290
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Slatten Ranch

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 290 | 290 | 1650 | 0.1758 | |
| THRU (T) | 270 | 270 | 3300 | 0.0818 | |
| LEFT (L) | 610 | 610 | 3000 | 0.2033 | 0.2033 |
| T + R | | 560 | 3300 | 0.1697 | |
| SB RIGHT (R) | 110 | 110 | 1650 | 0.0667 | |
| THRU (T) | 410 | 410 | 3300 | 0.1242 | |
| LEFT (L) | 230 | 230 | 1650 | 0.1394 | |
| T + R | | 520 | 3300 | 0.1576 | 0.1576 |
| EB RIGHT (R) | 290 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 1190 | 1190 | 4950 | 0.2404 | 0.2404 |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | |
| WB RIGHT (R) | 220 | 220 | 1650 | 0.1333 | |
| THRU (T) | 1020 | 1020 | 4950 | 0.2061 | |
| LEFT (L) | 260 | 260 | 1650 | 0.1576 | 0.1576 |
| T + R | | 1240 | 4950 | 0.2505 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.76

INTERSECTION LEVEL OF SERVICE: C

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 6 Live Oak Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL
----- 290 0 130
LEFT 340 --- 2.0 1.0 0.0 1.0 1.1 --- 50 RIGHT
THRU 1370 ---> 3.0 (NO. OF LANES) 3.1<--- 1210 THRU
RIGHT 0 --- 0.0 0.0 0.0 0.0 --- 0 LEFT
N
W + E
S
LEFT THRU RIGHT Split? N
STREET NAME: Laurel Road
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: Live Oak Ave

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|--------------------|---------------------|----------|--------------|-----------------|
| SB RIGHT (R) | 290 | 103 * | 1720 | 0.0599 | |
| LEFT (L) | 130 | 130 | 1720 | 0.0756 | 0.0756 |
| EB THRU (T) | 1370 | 1370 | 5160 | 0.2655 | |
| LEFT (L) | 340 | 340 | 3127 | 0.1087 | 0.1087 |
| WB RIGHT (R) | 50 | 50 | 1720 | 0.0291 | |
| THRU (T) | 1210 | 1210 | 5160 | 0.2345 | |
| T + R | | 1260 | 5160 | 0.2442 | 0.2442 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.43 |
| INTERSECTION LEVEL OF SERVICE: | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 7 Empire Ave/Laurel Road

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

430 300 60
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 430 --- 2.0 1.0 2.0 1.0 1.0 --- 50 RIGHT
STREET NAME:
THRU 910 ---> 2.0 (NO. OF LANES) 2.0<--- 720 THRU Laurel Road
RIGHT 160 --- 1.0 1.0 2.1 1.1 1.0 --- 50 LEFT
<--- ^ --->
| | |
v | v
N
W + E 110 360 60 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Empire Ave

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 360 | 360 | 3300 | 0.1091 | |
| LEFT (L) | 110 | 110 | 1650 | 0.0667 | 0.0667 |
| T + R | | 420 | 3300 | 0.1273 | |
| SB RIGHT (R) | 430 | 194 * | 1650 | 0.1176 | 0.1176 |
| THRU (T) | 300 | 300 | 3300 | 0.0909 | |
| LEFT (L) | 60 | 60 | 1650 | 0.0364 | |
| EB RIGHT (R) | 160 | 50 * | 1650 | 0.0303 | |
| THRU (T) | 910 | 910 | 3300 | 0.2758 | |
| LEFT (L) | 430 | 430 | 3000 | 0.1433 | 0.1433 |
| WB RIGHT (R) | 50 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 720 | 720 | 3300 | 0.2182 | 0.2182 |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.55

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 8 Canada Valley/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

120 20 350

LEFT 130 --- 2.0 1.1 1.1 1.0 1.1 --- 500 RIGHT

THRU 1710 ---> 3.0 (NO. OF LANES) 3.1<--- 1090 THRU

RIGHT 60 --- 1.0 1.0 1.0 1.0 2.0 --- 530 LEFT

W + E S LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Canada Valley

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 360 | 69 * | 1650 | 0.0418 | 0.0418 |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 220 | 220 | 1650 | 0.1333 | |
| SB RIGHT (R) | 120 | 120 | 1650 | 0.0727 | |
| THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| LEFT (L) | 350 | 350 | 1650 | 0.2121 | 0.2121 |
| T + R | | 140 | 1650 | 0.0848 | |
| EB RIGHT (R) | 60 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 1710 | 1710 | 4950 | 0.3455 | 0.3455 |
| LEFT (L) | 130 | 130 | 3000 | 0.0433 | |
| WB RIGHT (R) | 500 | 500 | 1650 | 0.3030 | |
| THRU (T) | 1090 | 1090 | 4950 | 0.2202 | |
| LEFT (L) | 530 | 530 | 3000 | 0.1767 | 0.1767 |
| T + R | | 1590 | 4950 | 0.3212 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.78

INTERSECTION LEVEL OF SERVICE: C

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 9 SR 4 Bypass SB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

240 0 860

LEFT 0 0.0 1.0 1.1 2.1 0.0 Split? N

THRU 2060 3.0 (NO. OF LANES) 3.0 1880 THRU STREET NAME: Lone Tree Way

RIGHT 380 1.0 0.0 0.0 0.0 2.0 380 LEFT

0 0 0

N
W + E
S

LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass SB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| SB RIGHT (R) | 240 | 240 | 1720 | 0.1395 | |
| THRU (T) | 0 | 0 | 1720 | 0.0000 | |
| LEFT (L) | 860 | 860 | 3127 | 0.2750 | 0.2750 |
| T + L | | 860 | 3127 | 0.2750 | |
| EB RIGHT (R) | 380 | 380 | 1720 | 0.2209 | |
| THRU (T) | 2060 | 2060 | 5160 | 0.3992 | 0.3992 |
| WB THRU (T) | 1880 | 1880 | 5160 | 0.3643 | |
| LEFT (L) | 380 | 380 | 3127 | 0.1215 | 0.1215 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | 0.80 |
| INTERSECTION LEVEL OF SERVICE: | | | | | C |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 10 SR 4 Bypass NB/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 3-PHASE SIGNAL

LEFT 0 0.0 0.0 0.0 1.0 730 RIGHT
THRU 2640 3.0 (NO. OF LANES) 3.0 1710 THRU
RIGHT 280 1.0 2.0 1.0 2.0 60 LEFT
N
W + E 550 50 340
S LEFT THRU RIGHT Split? N
STREET NAME: Lone Tree Way
SIG WARRANTS: Urb=Y, Rur=Y

STREET NAME: SR 4 Bypass NB

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|---------------------------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 340 | 307 * | 1720 | 0.1785 | 0.1785 |
| THRU (T) | 50 | 50 | 1720 | 0.0291 | |
| LEFT (L) | 550 | 550 | 3127 | 0.1759 | |
| EB RIGHT (R) | 280 | 0 * | 1720 | 0.0000 | |
| THRU (T) | 2640 | 2640 | 5160 | 0.5116 | 0.5116 |
| WB RIGHT (R) | 730 | 730 | 1720 | 0.4244 | |
| THRU (T) | 1710 | 1710 | 5160 | 0.3314 | |
| LEFT (L) | 60 | 60 | 3127 | 0.0192 | 0.0192 |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | 0.71 | |
| INTERSECTION LEVEL OF SERVICE: | | | | C | |

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

```
=====
Condition: Antioch Davidon 2025 With Project PM Peak Hour          10/24/07
=====
```

| Count | Date | Time | Peak | Hour |
|-------|------|------|------|------|
|-------|------|------|------|------|

| STREET NAME: Slatten Ranch | | | | | | |
|---------------------------------|-----------|--------------------|---------------------|----------|--------------|-----------------|
| MOVEMENT | | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
| NB | RIGHT (R) | 80 | 80 | 1650 | 0.0485 | 0.1333 |
| | THRU (T) | 370 | 370 | 3300 | 0.1121 | |
| | LEFT (L) | 400 | 400 | 3000 | 0.1333 | |
| | T + R | | 450 | 3300 | 0.1364 | |
| SB | RIGHT (R) | 570 | 312 * | 1650 | 0.1891 | 0.1891 |
| | THRU (T) | 550 | 550 | 3300 | 0.1667 | |
| | LEFT (L) | 80 | 80 | 3000 | 0.0267 | |
| EB | RIGHT (R) | 530 | 310 * | 1650 | 0.1879 | 0.1567 |
| | THRU (T) | 1990 | 1990 | 4950 | 0.4020 | |
| | LEFT (L) | 470 | 470 | 3000 | 0.1567 | |
| WB | RIGHT (R) | 60 | 60 | 1650 | 0.0364 | 0.3172 |
| | THRU (T) | 1510 | 1510 | 4950 | 0.3051 | |
| | LEFT (L) | 50 | 50 | 1650 | 0.0303 | |
| | T + R | | 1570 | 4950 | 0.3172 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | | 0.80 |
| INTERSECTION LEVEL OF SERVICE: | | | | | | C |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 12 Empire Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

220 220 310

LEFT 160 1.0 1.1 2.1 1.0 1.0 Split? N

THRU 1390 3.0 (NO. OF LANES) 3.0 960 THRU STREET NAME: Lone Tree Way

RIGHT 600 1.0 2.0 1.0 1.0 1.0 20 LEFT

440 120 40

W + E SIG WARRANTS: Urb=Y, Rur=Y

S LEFT THRU RIGHT Split? N

STREET NAME: Empire Ave

MOVEMENT ORIGINAL VOLUME ADJUSTED VOLUME* CAPACITY V/C CRITICAL V/C

NB RIGHT (R) 40 20 * 1650 0.0121
THRU (T) 120 120 1650 0.0727
LEFT (L) 440 440 3000 0.1467 0.1467

SB RIGHT (R) 220 220 1650 0.1333 0.1333
THRU (T) 220 220 3300 0.0667
LEFT (L) 310 310 1650 0.1879
T + R 440 3300 0.1333

EB RIGHT (R) 600 358 * 1650 0.2170
THRU (T) 1390 1390 4950 0.2808 0.2808
LEFT (L) 160 160 1650 0.0970

WB RIGHT (R) 160 0 * 1650 0.0000
THRU (T) 960 960 4950 0.1939
LEFT (L) 20 20 1650 0.0121 0.0121

TOTAL VOLUME-TO-CAPACITY RATIO: 0.57

INTERSECTION LEVEL OF SERVICE: A

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 13 Deer Valley Rd/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

150 510 310

LEFT 320 1.0 1.1 2.1 1.0 1.1 Split? N

THRU 1850 3.1 (NO. OF LANES) 3.1 1440 THRU STREET NAME: Lone Tree Way

RIGHT 190 1.1 2.0 2.1 1.1 1.0 190 LEFT

N
W + E
S
260 400 180
LEFT THRU RIGHT Split? N

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Deer Valley Rd

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|-----------------|------------------|----------|-----------|--------------|
| NB RIGHT (R) | 180 | 180 | 1650 | 0.1091 | |
| THRU (T) | 400 | 400 | 3300 | 0.1212 | |
| LEFT (L) | 260 | 260 | 3000 | 0.0867 | |
| T + R | | 580 | 3300 | 0.1758 | 0.1758 |
| SB RIGHT (R) | 150 | 150 | 1650 | 0.0909 | |
| THRU (T) | 510 | 510 | 3300 | 0.1545 | |
| LEFT (L) | 310 | 310 | 1650 | 0.1879 | 0.1879 |
| T + R | | 660 | 3300 | 0.2000 | |
| EB RIGHT (R) | 190 | 190 | 1650 | 0.1152 | |
| THRU (T) | 1850 | 1850 | 4950 | 0.3737 | |
| LEFT (L) | 320 | 320 | 1650 | 0.1939 | |
| T + R | | 2040 | 4950 | 0.4121 | 0.4121 |
| WB RIGHT (R) | 160 | 160 | 1650 | 0.0970 | |
| THRU (T) | 1440 | 1440 | 4950 | 0.2909 | |
| LEFT (L) | 190 | 190 | 1650 | 0.1152 | 0.1152 |
| T + R | | 1600 | 4950 | 0.3232 | |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.89

INTERSECTION LEVEL OF SERVICE: D

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 14 Hillcrest Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

450 120 580

LEFT 710 1.0 1.0 2.1 2.1 1.0 Split? N

THRU 1650 3.1 (NO. OF LANES) 3.0 1390 THRU STREET NAME: Lone Tree Way

RIGHT 80 1.1 1.0 2.1 1.1 1.0 100 LEFT

50 70 60

SIG WARRANTS: Urb=Y, Rur=Y

LEFT THRU RIGHT Split? Y

STREET NAME: Hillcrest Ave

ORIGINAL ADJUSTED V/C CRITICAL
MOVEMENT VOLUME VOLUME* CAPACITY RATIO V/C

NB RIGHT (R) 60 60 1650 0.0364
THRU (T) 70 70 3300 0.0212
LEFT (L) 50 50 1650 0.0303
T + R 130 3300 0.0394 0.0394

SB RIGHT (R) 450 0 * 1650 0.0000
THRU (T) 120 120 3300 0.0364
LEFT (L) 580 580 3000 0.1933 0.1933
T + L 700 4650 0.1505

EB RIGHT (R) 80 80 1650 0.0485
THRU (T) 1650 1650 4950 0.3333
LEFT (L) 710 710 1650 0.4303 0.4303
T + R 1730 4950 0.3495

WB RIGHT (R) 480 161 * 1650 0.0976
THRU (T) 1390 1390 4950 0.2808 0.2808
LEFT (L) 100 100 1650 0.0606

TOTAL VOLUME-TO-CAPACITY RATIO: 0.94

INTERSECTION LEVEL OF SERVICE: E

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 15 Vista Grande Dr/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 5-PHASE SIGNAL
----- 170 40 70
 | | |
 <--- v ---> Split? N
LEFT 190 --- 1.0 1.1 1.1 1.0 1.0 --- 90 RIGHT
THRU 1710 ---> 3.0 (NO. OF LANES) 3.0<--- 1240 THRU
RIGHT 390 --- 1.0 1.0 1.0 1.0 1.0 --- 300 LEFT
 | | |
 <--- ^ --->
 | | |
N 320 50 220
W + E
S LEFT THRU RIGHT Split? N

STREET NAME:
Lone Tree Way

SIG WARRANTS:
Urb=Y, Rur=Y

STREET NAME: Vista Grande Dr

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 220 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 50 | 50 | 1650 | 0.0303 | |
| LEFT (L) | 320 | 320 | 1650 | 0.1939 | 0.1939 |
| SB RIGHT (R) | 170 | 170 | 1650 | 0.1030 | |
| THRU (T) | 40 | 40 | 1650 | 0.0242 | |
| LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| T + R | | 210 | 1650 | 0.1273 | 0.1273 |
| EB RIGHT (R) | 390 | 70 * | 1650 | 0.0424 | |
| THRU (T) | 1710 | 1710 | 4950 | 0.3455 | 0.3455 |
| LEFT (L) | 190 | 190 | 1650 | 0.1152 | |
| WB RIGHT (R) | 90 | 20 * | 1650 | 0.0121 | |
| THRU (T) | 1240 | 1240 | 4950 | 0.2505 | |
| LEFT (L) | 300 | 300 | 1650 | 0.1818 | 0.1818 |

TOTAL VOLUME-TO-CAPACITY RATIO: 0.85

INTERSECTION LEVEL OF SERVICE: D

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025.INT,VOL=2025WP.PMV,CAP=

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=====
Condition: Antioch Davidon 2025 With Project PM Peak Hour          10/24/07
=====
```

| Count | Date | Time | Peak | Hour |
|-------|------|------|------|------|
|-------|------|------|------|------|

| STREET NAME: Hillcrest | | | | | | |
|---------------------------------|-----------|--------------------|---------------------|----------|--------------|-----------------|
| MOVEMENT | | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
| NB | RIGHT (R) | 70 | 70 | 1650 | 0.0424 | 0.3424 |
| | THRU (T) | 1060 | 1060 | 3300 | 0.3212 | |
| | LEFT (L) | 100 | 100 | 1650 | 0.0606 | |
| | T + R | | 1130 | 3300 | 0.3424 | |
| SB | RIGHT (R) | 80 | 80 | 1650 | 0.0485 | 0.0667 |
| | THRU (T) | 920 | 920 | 3300 | 0.2788 | |
| | LEFT (L) | 110 | 110 | 1650 | 0.0667 | |
| | T + R | | 1000 | 3300 | 0.3030 | |
| EB | RIGHT (R) | 100 | 0 * | 1650 | 0.0000 | 0.0424 |
| | THRU (T) | 20 | 20 | 1650 | 0.0121 | |
| | LEFT (L) | 70 | 70 | 1650 | 0.0424 | |
| WB | RIGHT (R) | 90 | 90 | 1650 | 0.0545 | 0.0848 |
| | THRU (T) | 50 | 50 | 1650 | 0.0303 | |
| | LEFT (L) | 120 | 120 | 1650 | 0.0727 | |
| | T + R | | 140 | 1650 | 0.0848 | |
| TOTAL VOLUME-TO-CAPACITY RATIO: | | | | | | 0.54 |
| INTERSECTION LEVEL OF SERVICE: | | | | | | A |

* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 With Project PM Peak Hour 10/24/07

INTERSECTION 18 Hillcrest/Laurel

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

220 910 290
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 140 --- 1.0 1.1 2.1 1.0 1.0 --- 250 RIGHT
STREET NAME:
THRU 80 ---> 1.1 (NO. OF LANES) 1.0<--- 210 THRU Laurel
RIGHT 110 --- 1.1 1.0 2.1 1.1 1.0 --- 350 LEFT
<--- ^ --->
| | |
v | v
N |
W + E 90 970 290 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Hillcrest

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 290 | 290 | 1650 | 0.1758 | |
| THRU (T) | 970 | 970 | 3300 | 0.2939 | |
| LEFT (L) | 90 | 90 | 1650 | 0.0545 | |
| T + R | | 1260 | 3300 | 0.3818 | 0.3818 |
| SB RIGHT (R) | 220 | 220 | 1650 | 0.1333 | |
| THRU (T) | 910 | 910 | 3300 | 0.2758 | |
| LEFT (L) | 290 | 290 | 1650 | 0.1758 | 0.1758 |
| T + R | | 1130 | 3300 | 0.3424 | |
| EB RIGHT (R) | 110 | 110 | 1650 | 0.0667 | |
| THRU (T) | 80 | 80 | 1650 | 0.0485 | |
| LEFT (L) | 140 | 140 | 1650 | 0.0848 | |
| T + R | | 190 | 1650 | 0.1152 | 0.1152 |
| WB RIGHT (R) | 250 | 0 * | 1650 | 0.0000 | |
| THRU (T) | 210 | 210 | 1650 | 0.1273 | |
| LEFT (L) | 350 | 350 | 1650 | 0.2121 | 0.2121 |

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TOTAL VOLUME-TO-CAPACITY RATIO: 0.88

INTERSECTION LEVEL OF SERVICE: D

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* ADJUSTED FOR RIGHT TURN ON RED
INT=2025.INT,VOL=2025WP.PMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 AM Peak Hour Mitigated 10/24/07

INTERSECTION 14 Hillcrest Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

470 40 380
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 290 --- 2.0 1.0 1.0 2.0 1.0 --- 400 RIGHT
STREET NAME:
THRU 810 ---> 3.1 (NO. OF LANES) 3.0<--- 1310 THRU Lone Tree Way
RIGHT 30 --- 1.1 1.0 2.1 1.1 1.0 --- 40 LEFT
| | |
<--- ^ --->
v | v
N |
W + E 80 70 80 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Hillcrest Ave

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 80 | 80 | 1650 | 0.0485 | |
| THRU (T) | 70 | 70 | 3300 | 0.0212 | |
| LEFT (L) | 80 | 80 | 1650 | 0.0485 | 0.0485 |
| T + R | | 150 | 3300 | 0.0455 | |
| SB RIGHT (R) | 470 | 311 * | 1650 | 0.1885 | 0.1885 |
| THRU (T) | 40 | 40 | 1650 | 0.0242 | |
| LEFT (L) | 380 | 380 | 3000 | 0.1267 | |
| EB RIGHT (R) | 30 | 30 | 1650 | 0.0182 | |
| THRU (T) | 810 | 810 | 4950 | 0.1636 | |
| LEFT (L) | 290 | 290 | 3000 | 0.0967 | 0.0967 |
| T + R | | 840 | 4950 | 0.1697 | |
| WB RIGHT (R) | 400 | 191 * | 1650 | 0.1158 | |
| THRU (T) | 1310 | 1310 | 4950 | 0.2646 | 0.2646 |
| LEFT (L) | 40 | 40 | 1650 | 0.0242 | |

=====

TOTAL VOLUME-TO-CAPACITY RATIO: 0.60
INTERSECTION LEVEL OF SERVICE: A

=====

* ADJUSTED FOR RIGHT TURN ON RED

INT=2025MIT.INT,VOL=2025WP.AMV,CAP=

CCTALOS Software ver. 2.35 by TJKM Transportation Consultants

Condition: Antioch Davidon 2025 PM Peak Hour Mitigated 10/23/07

INTERSECTION 14 Hillcrest Ave/Lone Tree Way

Count Date Time Peak Hour

CCTA METHOD RIGHT THRU LEFT 8-PHASE SIGNAL

450 120 580
| | |
^ | ^
| | |
<--- v ---> Split? N
LEFT 710 --- 2.0 1.0 1.0 2.0 1.0 --- 480 RIGHT
STREET NAME:
THRU 1650 ---> 3.1 (NO. OF LANES) 3.0<--- 1390 THRU Lone Tree Way
RIGHT 80 --- 1.1 1.0 2.1 1.1 1.0 --- 100 LEFT
<--- ^ --->
| | |
v | v
N
W + E 50 70 60 SIG WARRANTS:
S LEFT THRU RIGHT Split? N Urb=Y, Rur=Y

STREET NAME: Hillcrest Ave

=====

| MOVEMENT | ORIGINAL VOLUME | ADJUSTED VOLUME* | CAPACITY | V/C RATIO | CRITICAL V/C |
|--------------|--------------------|---------------------|----------|--------------|-----------------|
| NB RIGHT (R) | 60 | 60 | 1650 | 0.0364 | |
| THRU (T) | 70 | 70 | 3300 | 0.0212 | |
| LEFT (L) | 50 | 50 | 1650 | 0.0303 | |
| T + R | | 130 | 3300 | 0.0394 | 0.0394 |
| SB RIGHT (R) | 450 | 60 * | 1650 | 0.0364 | |
| THRU (T) | 120 | 120 | 1650 | 0.0727 | |
| LEFT (L) | 580 | 580 | 3000 | 0.1933 | 0.1933 |
| EB RIGHT (R) | 80 | 80 | 1650 | 0.0485 | |
| THRU (T) | 1650 | 1650 | 4950 | 0.3333 | |
| LEFT (L) | 710 | 710 | 3000 | 0.2367 | 0.2367 |
| T + R | | 1730 | 4950 | 0.3495 | |
| WB RIGHT (R) | 480 | 161 * | 1650 | 0.0976 | |
| THRU (T) | 1390 | 1390 | 4950 | 0.2808 | 0.2808 |
| LEFT (L) | 100 | 100 | 1650 | 0.0606 | |

=====













TOTAL VOLUME-TO-CAPACITY RATIO: 0.75
INTERSECTION LEVEL OF SERVICE: C

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APPENDIX D:
Lone Tree Way/Canada Valley Road
Queuing Reports













Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 32 | 829 | 58 | 184 | 1117 | 187 | 40 | 39 | 34 | 211 | 34 | 38 |
| v/c Ratio | 0.30 | 0.26 | 0.06 | 0.57 | 0.32 | 0.16 | 0.23 | 0.36 | 0.30 | 0.76 | 0.11 | 0.13 |
| Control Delay | 53.3 | 8.3 | 2.9 | 68.6 | 6.6 | 1.1 | 62.0 | 31.8 | 18.3 | 57.4 | 43.6 | 12.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 53.3 | 8.3 | 2.9 | 68.6 | 6.6 | 1.1 | 62.0 | 31.8 | 18.3 | 57.4 | 43.6 | 12.4 |
| Queue Length 50th (ft) | 27 | 61 | 3 | 77 | 93 | 1 | 17 | 13 | 0 | 173 | 25 | 0 |
| Queue Length 95th (ft) | m48 | 68 | m11 | 119 | 150 | 10 | 37 | 52 | 35 | 244 | 52 | 30 |
| Internal Link Dist (ft) | 900 | | 775 | | | | 542 | | | | 1064 | |
| Turn Bay Length (ft) | 300 | 120 | | 300 | 150 | | | 170 | | | | |
| Base Capacity (vph) | 123 | 3137 | 992 | 401 | 3447 | 1134 | 185 | 525 | 498 | 381 | 889 | 775 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.26 | 0.26 | 0.06 | 0.46 | 0.32 | 0.16 | 0.22 | 0.07 | 0.07 | 0.55 | 0.04 | 0.05 |
| Intersection Summary | | | | | | | | | | | | |
| m Volume for 95th percentile queue is metered by upstream signal. | | | | | | | | | | | | |













Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 56 | 1410 | 57 | 343 | 981 | 264 | 88 | 122 | 115 | 182 | 58 | 23 |
| v/c Ratio | 0.41 | 0.53 | 0.07 | 0.68 | 0.32 | 0.25 | 0.29 | 0.58 | 0.44 | 0.79 | 0.19 | 0.08 |
| Control Delay | 58.9 | 22.9 | 15.3 | 69.7 | 8.6 | 1.4 | 58.6 | 33.5 | 8.8 | 69.4 | 42.9 | 13.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 58.9 | 22.9 | 15.3 | 69.7 | 8.6 | 1.4 | 58.6 | 33.5 | 8.8 | 69.4 | 42.9 | 13.4 |
| Queue Length 50th (ft) | 42 | 226 | 10 | 148 | 78 | 0 | 37 | 66 | 0 | 148 | 43 | 0 |
| Queue Length 95th (ft) | m61 | 324 | m23 | 159 | 162 | 21 | 64 | 115 | 51 | #245 | 71 | 22 |
| Internal Link Dist (ft) | | 905 | | | 760 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 150 | 2671 | 834 | 532 | 3093 | 1044 | 363 | 508 | 521 | 259 | 645 | 554 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.37 | 0.53 | 0.07 | 0.64 | 0.32 | 0.25 | 0.24 | 0.24 | 0.22 | 0.70 | 0.09 | 0.04 |
| Intersection Summary | | | | | | | | | | | | |
| # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. | | | | | | | | | | | | |
| m Volume for 95th percentile queue is metered by upstream signal. | | | | | | | | | | | | |













Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Existing AM Peak Hour with Split Phasing

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 32 | 829 | 58 | 184 | 1117 | 187 | 40 | 39 | 34 | 119 | 126 | 38 |
| v/c Ratio | 0.40 | 0.26 | 0.06 | 0.57 | 0.31 | 0.16 | 0.21 | 0.35 | 0.30 | 0.51 | 0.53 | 0.15 |
| Control Delay | 63.1 | 6.3 | 1.5 | 64.6 | 5.2 | 0.6 | 58.2 | 31.8 | 18.4 | 52.4 | 52.6 | 14.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 63.1 | 6.3 | 1.5 | 64.6 | 5.2 | 0.6 | 58.2 | 31.8 | 18.4 | 52.4 | 52.6 | 14.1 |
| Queue Length 50th (ft) | 28 | 49 | 3 | 67 | 87 | 1 | 17 | 13 | 0 | 98 | 105 | 0 |
| Queue Length 95th (ft) | m50 | 43 | m6 | 120 | 98 | 6 | 36 | 52 | 35 | 160 | 167 | 32 |
| Internal Link Dist (ft) | 900 | | | 775 | | | 542 | | | 1064 | | |
| Turn Bay Length (ft) | 300 | | | 120 | 300 | | | 150 | | | 170 | |
| Base Capacity (vph) | 82 | 3217 | 1016 | 349 | 3605 | 1176 | 1003 | 488 | 464 | 491 | 499 | 490 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.39 | 0.26 | 0.06 | 0.53 | 0.31 | 0.16 | 0.04 | 0.08 | 0.07 | 0.24 | 0.25 | 0.08 |
| Intersection Summary | | | | | | | | | | | | |
| m Volume for 95th percentile queue is metered by upstream signal. | | | | | | | | | | | | |













Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Existing PM Peak Hour with Split Phasing

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 56 | 1410 | 57 | 343 | 981 | 264 | 88 | 122 | 115 | 117 | 123 | 23 |
| v/c Ratio | 0.49 | 0.61 | 0.08 | 0.49 | 0.32 | 0.25 | 0.30 | 0.67 | 0.49 | 0.44 | 0.45 | 0.09 |
| Control Delay | 63.7 | 28.4 | 17.1 | 52.7 | 8.6 | 1.0 | 54.5 | 36.4 | 10.3 | 48.4 | 48.5 | 13.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 63.7 | 28.4 | 17.1 | 52.7 | 8.6 | 1.0 | 54.5 | 36.4 | 10.3 | 48.4 | 48.5 | 13.7 |
| Queue Length 50th (ft) | 43 | 226 | 10 | 128 | 72 | 0 | 36 | 66 | 0 | 97 | 103 | 0 |
| Queue Length 95th (ft) | m63 | #558 | m23 | 150 | 179 | 13 | 60 | 132 | 58 | 134 | 140 | 22 |
| Internal Link Dist (ft) | | 905 | | | 760 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 123 | 2324 | 727 | 703 | 3107 | 1048 | 1003 | 508 | 521 | 491 | 504 | 472 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.46 | 0.61 | 0.08 | 0.49 | 0.32 | 0.25 | 0.09 | 0.24 | 0.22 | 0.24 | 0.24 | 0.05 |
| Intersection Summary | | | | | | | | | | | | |
| # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. | | | | | | | | | | | | |
| m Volume for 95th percentile queue is metered by upstream signal. | | | | | | | | | | | | |













Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Near-Term No Project AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 32 | 1079 | 72 | 234 | 1243 | 187 | 84 | 118 | 102 | 211 | 34 | 38 |
| v/c Ratio | 0.36 | 0.36 | 0.08 | 0.62 | 0.36 | 0.17 | 0.30 | 0.62 | 0.55 | 0.77 | 0.12 | 0.14 |
| Control Delay | 57.9 | 9.6 | 3.8 | 73.6 | 6.9 | 1.5 | 61.1 | 15.6 | 11.4 | 59.4 | 43.8 | 12.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 57.9 | 9.6 | 3.8 | 73.6 | 6.9 | 1.5 | 61.1 | 15.6 | 11.4 | 59.4 | 43.8 | 12.4 |
| Queue Length 50th (ft) | 28 | 72 | 2 | 103 | 89 | 1 | 35 | 13 | 0 | 172 | 25 | 0 |
| Queue Length 95th (ft) | m49 | 130 | 20 | 148 | 188 | 14 | 63 | 77 | 57 | 249 | 51 | 29 |
| Internal Link Dist (ft) | | 900 | | | 775 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 95 | 2965 | 940 | 418 | 3406 | 1122 | 283 | 533 | 523 | 354 | 817 | 715 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.34 | 0.36 | 0.08 | 0.56 | 0.36 | 0.17 | 0.30 | 0.22 | 0.20 | 0.60 | 0.04 | 0.05 |
| Intersection Summary | | | | | | | | | | | | |
| m Volume for 95th percentile queue is metered by upstream signal. | | | | | | | | | | | | |

Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Near-Term No Project PM Peak Hour













| |  |  |  |  |  |  |  |  |  |  |  |  |
|---|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 56 | 1652 | 104 | 500 | 1308 | 264 | 115 | 167 | 163 | 182 | 58 | 23 |
| v/c Ratio | 0.41 | 0.67 | 0.13 | 0.76 | 0.42 | 0.25 | 0.34 | 0.65 | 0.50 | 0.90 | 0.20 | 0.09 |
| Control Delay | 55.2 | 22.7 | 13.3 | 70.2 | 10.4 | 2.9 | 58.3 | 28.7 | 7.5 | 96.9 | 44.5 | 13.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 55.2 | 22.7 | 13.3 | 70.2 | 10.4 | 2.9 | 58.3 | 28.7 | 7.5 | 96.9 | 44.5 | 13.7 |
| Queue Length 50th (ft) | 41 | 250 | 8 | 212 | 77 | 0 | 48 | 78 | 0 | 154 | 44 | 0 |
| Queue Length 95th (ft) | m61 | #488 | m49 | #295 | 272 | m53 | 79 | 131 | 57 | #292 | 71 | 22 |
| Internal Link Dist (ft) | | 905 | | | 760 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 150 | 2451 | 775 | 657 | 3104 | 1047 | 375 | 520 | 555 | 204 | 588 | 507 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.37 | 0.67 | 0.13 | 0.76 | 0.42 | 0.25 | 0.31 | 0.32 | 0.29 | 0.89 | 0.10 | 0.05 |
| Intersection Summary | | | | | | | | | | | | |
| # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. | | | | | | | | | | | | |
| m Volume for 95th percentile queue is metered by upstream signal. | | | | | | | | | | | | |

Queues

Davidon EIR

8: Lone Tree Way & Canada Valley

Near-Term No Project AM Peak Hour with Split Phasing













| |  |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 32 | 1079 | 72 | 234 | 1243 | 187 | 84 | 118 | 102 | 119 | 126 | 38 |
| v/c Ratio | 0.59 | 0.36 | 0.08 | 0.59 | 0.36 | 0.16 | 0.37 | 0.60 | 0.52 | 0.51 | 0.53 | 0.15 |
| Control Delay | 88.4 | 7.2 | 1.6 | 63.2 | 6.5 | 0.5 | 57.5 | 15.6 | 11.4 | 52.4 | 52.6 | 14.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 88.4 | 7.2 | 1.6 | 63.2 | 6.5 | 0.5 | 57.5 | 15.6 | 11.4 | 52.4 | 52.6 | 14.1 |
| Queue Length 50th (ft) | 28 | 67 | 2 | 86 | 103 | 0 | 35 | 13 | 0 | 98 | 105 | 0 |
| Queue Length 95th (ft) | m#58 | 139 | 7 | 134 | 115 | 5 | 61 | 77 | 57 | 160 | 167 | 32 |
| Internal Link Dist (ft) | | 900 | | | 775 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 54 | 2988 | 946 | 395 | 3471 | 1137 | 1003 | 522 | 512 | 491 | 499 | 490 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.59 | 0.36 | 0.08 | 0.59 | 0.36 | 0.16 | 0.08 | 0.23 | 0.20 | 0.24 | 0.25 | 0.08 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

m Volume for 95th percentile queue is metered by upstream signal.

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 56 | 1652 | 104 | 500 | 1308 | 264 | 115 | 167 | 163 | 117 | 123 | 23 |
| v/c Ratio | 0.82 | 0.98 | 0.19 | 0.46 | 0.42 | 0.25 | 0.34 | 0.74 | 0.55 | 0.44 | 0.45 | 0.09 |
| Control Delay | 106.7 | 48.2 | 14.4 | 44.8 | 8.1 | 1.2 | 53.6 | 31.6 | 8.9 | 48.4 | 48.5 | 13.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 106.7 | 48.2 | 14.4 | 44.8 | 8.1 | 1.2 | 53.6 | 31.6 | 8.9 | 48.4 | 48.5 | 13.7 |
| Queue Length 50th (ft) | 47 | 293 | 14 | 194 | 86 | 0 | 47 | 78 | 0 | 97 | 103 | 0 |
| Queue Length 95th (ft) | m#84 | #742 | m34 | 213 | 221 | m8 | 74 | 154 | 68 | 134 | 140 | 22 |
| Internal Link Dist (ft) | | 905 | | | 760 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 68 | 1687 | 543 | 1094 | 3112 | 1038 | 1003 | 520 | 555 | 491 | 504 | 472 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.82 | 0.98 | 0.19 | 0.46 | 0.42 | 0.25 | 0.11 | 0.32 | 0.29 | 0.24 | 0.24 | 0.05 |

Intersection Summary













95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

m Volume for 95th percentile queue is metered by upstream signal.

Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Near-Term Plus Project AM Peak Hour













| |  |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 54 | 1079 | 72 | 234 | 1243 | 259 | 84 | 118 | 102 | 429 | 34 | 104 |
| v/c Ratio | 0.59 | 0.39 | 0.08 | 0.62 | 0.40 | 0.24 | 0.42 | 0.62 | 0.55 | 1.21 | 0.09 | 0.26 |
| Control Delay | 70.4 | 11.1 | 3.8 | 72.4 | 8.8 | 1.7 | 64.7 | 15.6 | 11.4 | 162.7 | 41.5 | 7.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 70.4 | 11.1 | 3.8 | 72.4 | 8.8 | 1.7 | 64.7 | 15.6 | 11.4 | 162.7 | 41.5 | 7.9 |
| Queue Length 50th (ft) | 47 | 72 | 2 | 105 | 105 | 1 | 35 | 13 | 0 | ~441 | 24 | 0 |
| Queue Length 95th (ft) | m#90 | 128 | 20 | 146 | 197 | 26 | 63 | 77 | 57 | #648 | 51 | 47 |
| Internal Link Dist (ft) | 900 | | | 775 | | | 542 | | | 1064 | | |
| Turn Bay Length (ft) | 300 | | | 120 | 300 | | | 150 | | | 170 | |
| Base Capacity (vph) | 95 | 2736 | 871 | 418 | 3095 | 1065 | 211 | 533 | 523 | 354 | 817 | 752 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.57 | 0.39 | 0.08 | 0.56 | 0.40 | 0.24 | 0.40 | 0.22 | 0.20 | 1.21 | 0.04 | 0.14 |

Intersection Summary

- ~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
- m Volume for 95th percentile queue is metered by upstream signal.

Queues
8: Lone Tree Way & Canada Valley

Davidon EIR
Near-Term Plus Project PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 127 | 1652 | 104 | 500 | 1308 | 494 | 115 | 167 | 163 | 318 | 58 | 65 |
| v/c Ratio | 0.85 | 0.68 | 0.13 | 0.76 | 0.44 | 0.44 | 0.34 | 0.65 | 0.50 | 1.56 | 0.20 | 0.22 |
| Control Delay | 84.8 | 22.7 | 13.3 | 67.2 | 12.4 | 3.5 | 58.2 | 28.7 | 7.5 | 311.5 | 44.5 | 9.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 84.8 | 22.7 | 13.3 | 67.2 | 12.4 | 3.5 | 58.2 | 28.7 | 7.5 | 311.5 | 44.5 | 9.3 |
| Queue Length 50th (ft) | 101 | 235 | 8 | 213 | 95 | 0 | 48 | 78 | 0 | ~378 | 44 | 0 |
| Queue Length 95th (ft) | m#194 | #487 | m49 | m272 | m298 | m95 | 79 | 131 | 57 | #565 | 71 | 35 |
| Internal Link Dist (ft) | | 905 | | | 760 | | | 542 | | | 1064 | |
| Turn Bay Length (ft) | 300 | | 120 | 300 | | | 150 | | | 170 | | |
| Base Capacity (vph) | 150 | 2446 | 773 | 656 | 2989 | 1113 | 379 | 520 | 555 | 204 | 588 | 536 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.85 | 0.68 | 0.13 | 0.76 | 0.44 | 0.44 | 0.30 | 0.32 | 0.29 | 1.56 | 0.10 | 0.12 |

Intersection Summary

- ~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
- m Volume for 95th percentile queue is metered by upstream signal.

APPENDIX D:
Vista Grande/Canada Valley/Pinnacle View Way
Signal Warrant Worksheet

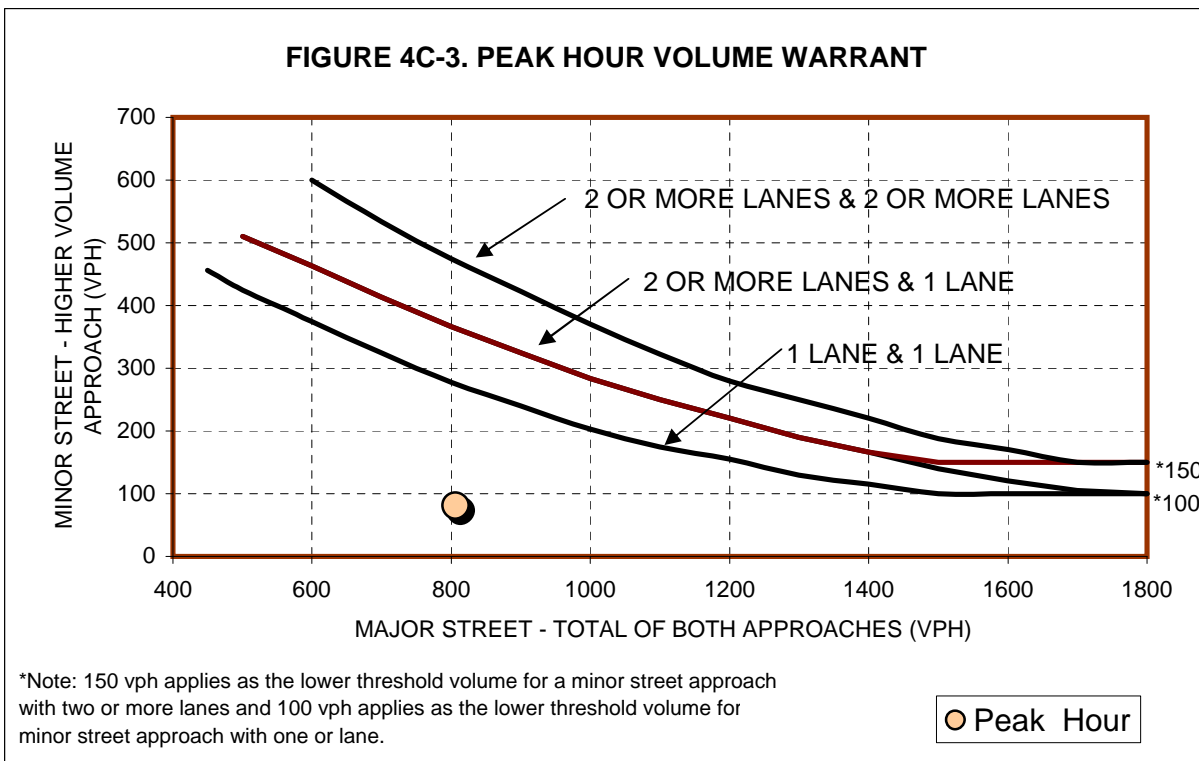
Warrant 3B: Peak Hour Volume

The peak hour volume warrant is satisfied when the plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour of the higher volume minor street approach (one direction only) for one hour (any four consecutive 15-minute periods) of an average day falls above the curve in Figure 4-5 for the existing combination of approach lanes.

Analysis

| | |
|--------------|-------------|
| | No of lanes |
| Major Street | 1 |
| Minor Street | 1 |

| | | |
|-----------|--|--|
| Peak Hour | | |
| Time | Vehicles Per Hour | |
| | Major Street (Sum of both approaches) | Minor street (High volume approach) |
| 8:00 AM | 807 | 81 |



Warrant

NOT MET

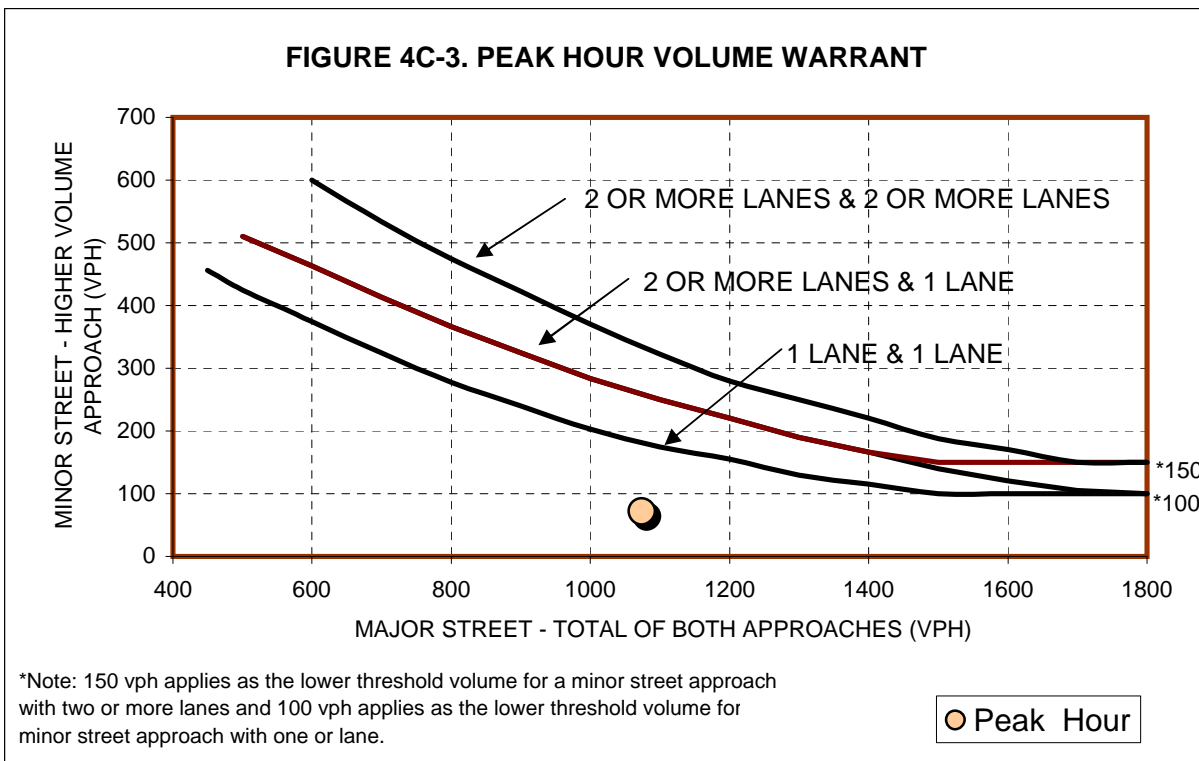
Warrant 3B: Peak Hour Volume

The peak hour volume warrant is satisfied when the plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour of the higher volume minor street approach (one direction only) for one hour (any four consecutive 15-minute periods) of an average day falls above the curve in Figure 4-5 for the existing combination of approach lanes.

Analysis

| | |
|--------------|-------------|
| | No of lanes |
| Major Street | 1 |
| Minor Street | 1 |

| Time | Vehicles Per Hour | |
|---------|---|---|
| | Major Street (Sum of both approaches) | Minor street (High volume approach) |
| 5:00 PM | 1,074 | 71 |



Warrant

NOT MET

Appendix B

Biological Assessment

BIOLOGICAL ASSESSMENT

DAVIDON SUBDIVISION 8846

ANTIOCH, CONTRA COSTA COUNTY

CALIFORNIA

Prepared for:

Richard T. Loewke, AICP
547 Wycombe Court
San Ramon, CA 94583
Ph. 925-831-8016
Fax 925-931-8019

Prepared by:

Trish Tatarian
Wildlife Research Associates
1119 Burbank Avenue
Santa Rosa, CA 95407
Ph. 707-544-6273
Fax 707-544-6317

October 19, 2007

BIOLOGICAL ASSESSMENT TABLE OF CONTENTS

| | |
|---|-----------|
| SUMMARY | IV |
| 1.0 INTRODUCTION | 1 |
| 1.1 PROJECT DESCRIPTION | 1 |
| 2.0 METHODS AND LIMITATIONS | 1 |
| 3.0 EXISTING CONDITIONS..... | 2 |
| 3.1 SETTING | 2 |
| 3.2 VEGETATION COMMUNITIES | 2 |
| 3.3 WILDLIFE HABITATS | 3 |
| 3.4 WILDLIFE MOVEMENT CORRIDORS..... | 4 |
| 4.0 SPECIAL-STATUS SPECIES AND NATURAL COMMUNITIES..... | 4 |
| 4.1 SPECIAL-STATUS VEGETATION COMMUNITIES..... | 5 |
| 4.2 SPECIAL-STATUS PLANT SPECIES..... | 5 |
| 4.3 SPECIAL-STATUS WILDLIFE SPECIES | 6 |
| 4.2.1 <i>Federal and State Threatened and Endangered Wildlife Species</i> | 7 |
| 4.2.2 <i>Other Special-Status Wildlife Species</i> | 9 |
| 5.0 IMPACTS AND MITIGATION MEASURES | 12 |
| 6.0 LITERATURE CITED..... | 16 |

LIST OF FIGURES

| <u>FIGURE</u> | <u>TITLE</u> | <u>PAGE</u> |
|---------------|-----------------------|-------------|
| 1 | Project Location..... | 14 |

LIST OF APPENDICES

| <u>APPENDIX</u> | <u>TITLE</u> |
|-----------------|---|
| A | Potentially-Occurring Special-Status Plant Species A-1 |
| B | Potentially-Occurring Special-Status Wildlife Species B-1 |

SUMMARY

The Davidon Subdivision 8846 property, consisting of portions of the former R. Jacuzzi and V. Jacuzzi Ranch properties, contains approximately 171 acres of undeveloped land located north of Lone Tree Way, west of Neroly Road, and south of the Contra Costa Canal, south of Highway 4, within eastern Contra Costa County, California. The northern boundary is formed by lands of the approved Laurel Ranch subdivision (Bixby Company LLC), the eastern boundary is formed by lands owned by the State Route 4 Bypass Authority, the western boundary by an established residential subdivision, and the southern boundary is formed by the residential development of the Sand Creek Ranch (Shea Homes). Northeast of the project site is the old V. Jacuzzi homestead (owned by Deliza Ranch LLC).

Wildlife Research Associates conducted this revised biological assessment of the proposed project to assess the potential for the presence of special-status biological resources and to evaluate the potential biological constraints to the proposed project.

Habitats within the Davidon Subdivision 8846 property (the “subject property”) have been altered as the result of cattle grazing, orchard removal, and annual disking of non-native grasslands and ruderal habitat.

A review of the California Natural Diversity Data Base (CNDDB 2007), revealed that a total of 6 special status vegetation communities, 31 special-status plant species and 45 special status animal species have been reported within the region of the study area. One special-status vegetation community, coastal and valley freshwater marsh, occurs within the project site on the southwestern portion of the site. Please refer to *Wetland Delineation, Southwest Corner of Rolling Hills Ranch* (Michael Wood Biological Consulting 2002) for further details.

None of the special-status plant species are considered to have any potential for occurrence within the study area, due to a lack of suitable habitat, or the fact that they would have been recognizable during previous surveys (Michael Brandman Associates 2003).

Several special status animal species either have potential to occur or occur on the property or adjacent lands. One California special concern species, the western burrowing owl (*Athene cunicularia hypugea*), is known to nest on the subject property (CNDDB 2007). One state-listed fully-protected bird species, the white-tailed kite (*Elanus caeruleus*) is known to nest on the Deliza Ranch parcel (CNDDB 2007). Two other bird species; loggerhead shrike (*Lanius ludovicianus*) and American kestrel (*Falco sparverius*) are also known to nest on the Deliza Ranch (CNDDB 2007) and are protected under Fish and Game Code Section 3503.5. Burrowing owls were also documented on the Deliza Ranch on lands that were acquired and mitigated for by the State Route 4 Bypass Authority for Segment 1 of the State Route 4 Bypass (Loewke 2003). Other raptor (birds of prey) species, including northern harrier (*Circus cyaneus*), and red-tailed hawk (*Buteo jamaicensis*) are considered to have a moderate potential to occur within the study area, based on the presence of suitable nesting habitat (grasslands and trees). Several passerine (perching bird) species, including western meadowlark (*Sturnella neglecta*), may be nesting on the site in the non-native grasslands.

Surveys were conducted in 2005 to identify the location and population of burrowing owls utilizing the site for nesting and foraging purposes. The surveys were followed by a CDFG-authorized banding of owls, which lead to the identification of 2 adult and 7 juvenile owls within the southwesterly corner of the site. Based on this documentation, the project sponsor, Davidon Homes, implemented mitigation for the loss of corresponding nesting and foraging habitat

through purchase of 19.5 burrowing owl conservation credits in the CDFG-approved Haera Wildlife Conservation Bank, operated by Wildlands, Inc. Owls were subsequently excluded from the southwesterly portion of the site in accordance with CDFG authorized procedures.

To avoid impacts to special-status nesting passerine and raptor species prior to project ground breaking, we recommend the following actions:

- Remove remaining suitable nesting habitat prior to the nesting season (February 1 through August 31).
- Conduct pre-construction surveys for nesting raptors and passerines. If any of the aforementioned species are present, construction shall be delayed until after the nesting season (February-August).

Please refer to the mitigation measures at the end of this document for more details.

1.0 INTRODUCTION

Wildlife Research Associates was contracted by Mr. Richard T. Loewke to prepare a biological assessment of the approximate 171-acre Davidon Subdivision 8846 property located in the eastern portion of the City of Antioch, Contra Costa County, California (Figure 1). The Davidon Subdivision property consists of undeveloped land, and is located north of Lone Tree Way, west of Neroly Road, south of the Contra Costa Canal and Highway 4, and west of the State Route 4 Bypass Segment 1. The northern boundary is formed by lands Laurel Ranch subdivision (Bixby Company LLC), the eastern boundary is formed by lands owned by the State Route 4 Bypass Authority. The southern boundary abuts the Sand Creek Ranch development, built in 2005 by Shea Homes. Additional residential development occurs on the western boundary along Canada Valley Road, and Segment 1 of the State Route 4 Bypass has recently been constructed adjoining the easterly boundary of the project.

This report presents the updated results of a reconnaissance-level survey of the study area, a discussion of the existing plant communities and wildlife habitats on-site, the potential for occurrence of special-status natural communities, and special-status plant and animal species on-site, and identifies potential impacts and mitigation measures.

1.1 Project Description

The Davidon Subdivision project study area (APN 053-060-023 and 053-072-013) includes the following proposed uses: (a) approximately 91 acres of residential lots, 27 acres of open space, 8 acres of community park, and 37 acres of major roads. An additional 7 acres are identified as remainder parcels.

2.0 METHODS AND LIMITATIONS

Information on special-status plant species was compiled through a review of the California Natural Diversity Data Base (CNDDDB) (CNDDDB 2007) for the Antioch North, Antioch South, Brentwood, and Jersey Island 7.5-minute U.S. Geological Survey (USGS) topographic quadrangles, the California Native Plant Society's (CNPS) Inventory of Rare and Endangered Vascular Plants of California (Skinner and Pavlik 1999), the California Department of Fish and Game's (CDFG) Special Plants List (CDFG 2007a) and the USFWS list of special-status plants (USFWS 2007).

A list of special-status wildlife species known or expected to occur on the site was compiled through a review of the CNDDDB (CNDDDB 2007), the CDFG's Special Animals List (CDFG 2007b), State and Federally Listed Endangered and Threatened Animals of California (CDFG 2007c) and the USFWS list of special-status animals (USFWS 2007).

A site visit was conducted on September 20, 2007 by Wildlife Research Associates ecologist Trish Tatarian. The reconnaissance-level site visit was intended only as an initial evaluation of on-site and adjacent habitat types. For the purposes of this report, the property consists of all lands within the property boundaries (approximately 171- acres) and will be referred to as the study area.

Focused surveys for western burrowing owl were conducted in 2005, 2006 and 2007 in the southwest corner of the project site (see below). Focused surveys for other special-status wildlife species were not conducted as part of this effort.

Reports reviewed for this project include the *Biological Resources Assessment, Laurel Ranch Subdivision, Contra Costa County, California* (Michael Brandman Associates 2003), *State Route 4 Bypass Project, Biological Assessment* (Wildlife Research Associates 2003), *Highway 4 Bypass Rare Plants* (Wood Biological Consulting 2003b), *Wetland Delineation, Southwest Corner of Rolling Hills Ranch* (Michael Wood Biological Consulting 2002), *Lindsey Basin: Biological Constraints Analysis* (Environmental Science Associates (ESA) 1994a), *State Route 4 Bypass Project, Final Environmental Impact Report* (ESA 1994b), *Habitat Assessment for California Red-legged Frog* (ESA) 1998a), the Draft EIR for *Future Urbanization Area #2 Specific Plan* (Mundie & Associates 1995), SR 4 Bypass Segment 1 Biological Assessment, as issued by the USFWS (USFWS 2005) and Section 1603 Agreement issued for Segment 1 of the SR 4 Bypass by the CDFG on May 10, 2005 (CDFG 2005).

3.0 EXISTING CONDITIONS

3.1 Setting

The study area is located within the San Francisco Bay/Delta Bioregion (Welsh 1994). This bioregion is located within central California and is located west of the interface of two significant freshwater systems, the Sacramento and San Joaquin Rivers. Habitats within this bioregion include both mesic (moist) habitats, such as freshwater marsh, and xeric (dry) habitats, such as open grasslands, and are typical of a Mediterranean climate. Annual winter precipitation averages 12 inches (Mundie and Associates 1995). The weather in the Antioch area is influenced by Mt. Diablo in the west, and the xeric regime is created by the adiabatic conditions influenced by the mountain.

Located approximately 11.5 miles northeast of Mt. Diablo, and approximately 2.7 miles south of the San Joaquin River, the study area is situated within the southeast corner of the City of Antioch in eastern Contra Costa County. The study area is located within Section 23, Township 2N and Range 2E on the Brentwood U.S. Geological Survey (USGS) 7.5-minute topographic quadrangle map.

Approximately 171-acres in size, the study area is, located south of the existing State Route 4 Highway, west of the new State Route 4 Bypass and north of Lone Tree Way. Ranging in elevations between 100 to 225 feet above sea level, the lands are comprised of south- and east-facing slopes. The central portion of the study area has been altered by off-road vehicle use. Historically, the Davidon Subdivision study area partially supported cattle grazing, orchards and row crops.

A small artificially created freshwater wetland occurs on the southwest corner of the study area. A temporary 48" reinforced concrete pipe outfall once lead onto the study area, conveying water from beneath Canada Valley Road (Michael Wood Biological Consulting 2002). This pipe has since been converted to carry storm water to the East Antioch Creek flood control channel.

3.2 Vegetation Communities

Although once supporting orchards in the eastern portion of the site, the dominant vegetation community on the site is non-native grassland and comprises approximately 171 acres. This community is typically composed of a dense to sparse cover of annual grasses, often associated with numerous species of annual and perennial forbs. These grasslands grow actively during winter and spring, remain dormant during summer and early fall, and persist only as seed until conditions are favorable for germination (Holland 1986). The presence of this assemblage of non-native, annual grasses originating in the Mediterranean region is a consequence of permanent

alterations to the once widely distributed, pristine perennial grasslands of California. The conversion of native perennial grassland into non-native annual species has resulted from a combination of (1) invasion by alien plant species, (2) changes in the kinds of animals and their grazing patterns, (3) cultivation, and (4) fire regime (Heady 1988). Non-native grassland is generally found on fine-textured, clay-rich soils, which are moist to saturated during winter rains and dry during the summer and fall (Holland 1986). Scattered native wildflower species, representing remnants of the original vegetation, may also be common. Non-native annual grassland, such as found within the Rolling Hills Ranch study area, conforms to the California annual grassland series described in Sawyer and Keeler-Wolf (1995).

Non-native annual grasses of European origin make up the dominant species. On site, these include wild oats (*Avena fatua*), brome grasses (*Bromus* spp.), hare barley (*Hordeum murinum* ssp. *leporinum*), and annual ryegrass (*Lolium multiflorum*), among others. Common non-native forbs also detected include bristly ox-tongue (*Picris echinoides*), doveweed (*Eremocarpus setigerus*), yellow star thistle (*Centaurea solstitialis*), hoary mustard (*Hirschfeldia incana*), prickly lettuce (*Lactuca serriola*), tarplant (*Hemizonia fitchii*), and curly dock (*Rumex crispus*), among others. Native forbs present within this community include common fiddleneck (*Amsinckia menziesii*), bellardia (*Bellardia trixago*) and bull thistle (*Cirsium vulgare*), species common in disturbed habitats.

Seasonal wetlands occurring on the site comprise of approximately 0.17 –acres and consist of annual and perennial native and non-native wetland associated plant species (Michael Wood Biological Consulting 2002). This vegetation community typically resembles a wetland community only following the wet season or when water is present. Please refer to the *Wetland Delineation, Southern Corner of Rolling Hills Ranch* (Wood Biological 2005) for further details. This wetland falls under the classification of coastal and valley freshwater marsh.

Species observed within the freshwater marsh on site included cattails (*Typha latifolia* and *T. angustifolia*), as well as three-square (*Scirpus americanus*), toad rush (*Juncus bufonius*), umbrella sedge (*Cyperus eragrostis*) and loosestrife (*Lythrum hyssopifolia*) (Michael Wood Biological Consulting 2002).

3.3 Wildlife Habitats

Grassland habitat, including native and non-native grasslands, provides both primary habitat, such as nesting and foraging, and secondary habitat, such as a movement corridor. Reptiles, such as western fence lizard (*Sceloporus occidentalis*), can be found in this habitat, feeding on invertebrates found within and beneath debris. This habitat also attracts seed-eating and insect-eating species of birds and mammals. California quail (*Lophortyx californicus*), mourning dove (*Zenaidura macroura*), and meadowlark (*Sturnella neglecta*) are a few seed-eaters that nest and forage in grasslands. Insect-eaters such as scrub jay (*Aphelocoma coerulescens*) use the habitat for foraging only. Grasslands are important foraging grounds for aerial and ground foraging insect-eating bat species such as myotis (*Myotis* spp.) and pallid bat (*Antrozous pallidus*). A large number of other mammal species such as California vole (*Microtus californicus*), deer mouse (*Peromyscus maniculatus*), Botta's pocket gopher (*Thomomys bottae*), California ground squirrel (*Spermophilus beecheyi*) and California jackrabbit (*Lepus californicus*) also forage and nest within grasslands. Small rodents attract raptors (birds of prey) such as owls that hunt at night, as well as day-hunting raptors such as white-tailed kite (*Elanus leucureus*), and red-tailed hawk (*Buteo jamaicensis*), among others. On the project site, three different coyote (*Canis latrans*) have been observed.

Small, individual almond trees, remnants and volunteers from the previous orchards on site, once occurred throughout the grasslands areas. In 2006, many of these trees were removed with a subsequent removal follow-up in 2007.

The freshwater marsh on the site does not remain wet long enough to provide more than a few weeks of wildlife habitat. Nesting birds, such as red-winged blackbirds (*Agelaius phoeniceus*) may use the cattails for nesting and foraging. Mourning doves may use the adjacent areas for nesting.

3.4 Wildlife Movement Corridors

Wildlife movement includes migration (i.e., usually one way per season), inter-population movement (i.e., long-term genetic flow) and small travel pathways (i.e., daily movement corridors within an animal's territory). While small travel pathways usually facilitate movement for daily home range activities such as foraging or escape from predators, they also provide connection between outlying populations and the main corridor, permitting an increase in gene flow among populations.

These linkages among habitat types can extend for miles between primary habitat areas and occur on a large scale throughout California. Habitat linkages facilitate movement among populations located in discrete areas and populations located within larger habitat areas. The mosaic of habitats found within a large-scale landscape results in wildlife populations that consist of discrete sub-populations comprising a large single population, which is often referred to as a meta-population. Even where patches of pristine habitat are fragmented, such as occurs with coastal scrub, the movement between wildlife populations is facilitated through habitat linkages, migration corridors and movement corridors. Depending on the condition of the corridor, genetic flow between populations may be high in frequency, thus allowing high genetic diversity within the population, or may be low in frequency. Potentially low frequency genetic flow may lead to complete isolation, and if pressures are strong, potential extinction (McCullough 1996; Whittaker 1998).

The undeveloped nature of the Davidson Subdivision study area provides a limited movement corridor for common mammal species, such as coyote, within the local vicinity of the study area in eastern portion of East Antioch. Wildlife movement is limited in this area due to the increasing development, such as the residential development occurring on the western and southern borders of the study area, the residential development approved and planned immediately north of the study area, the commercial development along Lone Tree Way, and opening of the State Route 4 Bypass freeway along the entire easterly project boundary. The Antioch Creek may provide a suitable movement corridor for small to moderate sized animals; however, Antioch Creek does not connect to any other open space lands, and is separated from the project site by the new 6-lane freeway.

4.0 SPECIAL-STATUS SPECIES AND NATURAL COMMUNITIES

Certain plants and wildlife species are designated as having special status due to their overall rarity, endangerment, restricted distribution, and/or unique habitat requirements. In general, special-status is a combination of these factors that leads to the designation of a species as sensitive. The Federal Endangered Species Act (FESA), enacted by Congress in 1973, outlines the procedures whereby species are listed as endangered or threatened and established a program for the conservation of such species and the habitats in which they occur. Many individual states have enacted their own listing procedures to provide for the protection of additional locally sensitive biological resources. The California Endangered Species Act (CESA) of 1984 amends

the California Fish and Game Code to protect species deemed to be locally endangered and essentially expands the number of species protected under the FESA.

The CDFG has also compiled a list of "Special Plants" (CDFG 2007a) and "Special Animals" (CDFG 2007b) which include California Special Concern species. These designations are given to plant species whose communities are seriously threatened, and to wildlife species whose breeding populations are in serious decline. Although these species may be abundant elsewhere they are considered to be at some risk of extinction in California. Although Special Concern species are afforded no official legal status under FESA or CESA, they may receive special consideration during the planning stages of certain development projects and adverse impacts may be deemed significant under the California Environmental Quality Act (CEQA).

4.1 Special-Status Vegetation Communities

Based on a review of the CNDDDB (CNDDDB 2007), a total of 6 special-status communities may have potential to occur within the region, including alkali meadow, alkali seep, cis-montane alkali marsh, coastal brackish marsh, coastal and valley freshwater marsh, and stabilized interior dunes. Only one of these communities occurs on the site, the coast and valley freshwater marsh.

4.2 Special-Status Plant Species

Special-status plant species include those listed as Endangered, Threatened, Rare or Candidates for listing by the USFWS (2007), the CDFG (2007a), the CNDDDB (2007) and the CNPS (Skinner and Pavlik 1999). The CNPS listing is sanctioned by the CDFG and serves essentially as their list of "candidate" plant species.

Based on a review of the CNDDDB (CNDDDB 2007), and general and personal knowledge of the flora of eastern Contra Costa County, a total of 37 special-status plant species were reviewed, but only 14 were determined to have at least some potential for occurring in the study area based on the vegetation communities present (Appendix A). None of these target species were detected during the reconnaissance survey and none are considered to occur within the study area due to the highly disturbed nature of the site.

As discussed in the Draft EIR for *Future Urbanization Area #2 Specific Plan* (Mundie & Associates 1995) and the *Lindsey Basin Biological Constraints Analysis* (ESA 1994), five special-status plant species are identified as having some potential to occur within the study area. These include diamond-petaled California poppy (*Eschscholzia rhombipetala*), showy madia (*Madia radiata*), fragrant fritillary (*Fritillaria liliacea*), stinkbells (*Fritillaria agrestis*), and caper-fruited tropidocarpum (*Tropidocarpum capparideum*). In addition, 10 other species were evaluated for their potential to occur within the study area based on the habitat present. See Appendix A. None of these species are considered to have any potential to be present within the study area due to a lack of suitable habitat and the high level of disturbance.

The CNDDDB records for the Antioch North, Antioch South, Brentwood, and Jersey Island quadrangles include several special-status plant species that are known to only occur within marsh habitat, including Delta tule pea (*Lathyrus jepsonii* var. *jepsonii*), Mason's lilaeopsis (*Lilaeopsis masonii*), soft bird's beak (*Cordylanthus mollis* ssp. *mollis*), and Suisun marsh aster (*Aster lentus*). However, these species are restricted to waterways of the Sacramento-San Joaquin Delta system, and none are considered to have any potential to occur within the study area. The isolated remnant freshwater marsh on site does not provide suitable habitat for these species. Two other special-status plant species, Antioch dunes evening primrose (*Oenothera deltoides* ssp. *howellii*) and Contra Costa wallflower (*Erysimum capitatum* ssp. *angustatum*) are also known

from the sand dunes in the vicinity of Antioch. Neither of these species is considered to have any potential to occur within the study area due to lack of suitable habitat.

Below are descriptions of those species that are prominent in today's regulatory environment based on the location of the study area and the habitats present on the site.

Big tarplant (*Blepharizonia plumosa ssp. plumosae*) - a CNPS List B annual herb that occurs in valley/foothill grasslands on dry sites. This species may be extant in Alameda and possibly Contra Costa counties. This species blooms from July through October and was not observed on the site during the surveys conducted in 1995 and 2003 (Mundie and Associates 1995, Michael Brandman Associates 2003).

Diablo helianthella (*Helianthella castanea*) - a federal species of concern and a CNPS List 1B perennial herb that occurs in broadleaf upland forest, chaparral, cismontane woodland, coastal scrub, riparian woodland, and Valley/foothill grassland. This species blooms April through June and was not observed during the surveys conducted in 1995 and 2003 (Mundie and Associates 1995, Michael Brandman Associates 2003).

Carquinez goldenbush (*Isocoma arguta*) - is a CNPS List 1B species that occurs in valley/foothill grasslands on alkaline soils. This species blooms August through December and was not observed during the surveys conducted in 1995 and 2003 (Mundie and Associates 1995, Michael Brandman Associates 2003).

Hoover's cryptantha (*Cryptantha hooveri*) - a CNPS List 1B species that occurs in valley/foothill grasslands. This species blooms April through May and was not observed during the surveys conducted in 1995 and 2003 (Mundie and Associates 1995, Michael Brandman Associates 2003).

Diamond-petaled California poppy (*Eschscholzia rhombipetala*) - a federal species of concern and a CNPS List 1A annual herb that occurs in valley/foothill grassland on clay soils. This species blooms March through April and was not observed during the surveys conducted in 1995 and 2003 (Mundie and Associates 1995, Michael Brandman Associates 2003).

4.3 Special-Status Wildlife Species

Special-status animal species include those protected under FESA, CESA and Section 15380(d) of the California Environmental Quality Act (CEQA). The USFWS officially lists species as either Threatened (FT), Endangered (FE), or as candidates (FC) for listing. Additional species receive federal protection under the Bald Eagle Protection Act (e.g., bald eagle, golden eagle), and the Migratory Bird Treaty Act (MBTA). In addition, many other species are considered by the CDFG to be Special Concern species (CSC); these are listed in Remsen (1978), Williams (1986), and Jennings and Hayes (1994). Although such species are afforded no official legal status, they may receive special consideration during the planning stages of certain development projects. The CDFG further classifies some species under the following categories: "fully protected", "protected fur-bearer", "protected amphibian", and "protected reptile". The designation "protected" indicates that a species may not be taken or possessed except under special permit from the CDFG; "fully protected" indicates that a species can be taken for scientific purposes by permit only.

A total of 45 special-status animal species have potential to be present within the study area (CDFG 2007). A complete list of wildlife species, including their potential to occur within the

study area, their legal status and habitat affinities, is included in Appendix B. Several special-status animal species have potential to occur within the Davidon Subdivision study area, including white-tailed kite (*Elanus leucurus*), American kestrel (*Falco sparverius*), loggerhead shrike (*Lanius ludovicianus*), and other passerine species. One species, the western burrowing owl (*Athene cunicularia hypugea*), is known to occur within the study area. Two species of concern, the loggerhead shrike and white-tailed kite, were observed nesting on the V. Jacuzzi property in 2005 (CNDDDB 2007).

The following is a discussion of species that have either a low or moderate potential to occur within the study area, and/or are species that are prominent in today's regulatory environment. Special-status wildlife species associated with habitats not present within the study area, such as salt marsh habitat, vernal pools, interior dunes, and freshwater marshes, are not discussed in this report. These species include vernal pool fairy shrimp (*Branchinecta lynchi*), mid-valley fairy shrimp (*Branchinecta mesovalliensis*), San Joaquin dune beetle (*Coelus gracilis*), Antioch efferian robberfly (*Efferia antiochi*), red-headed sphecid wasp (*Euececeris ruficeps*), curved-foot hygrotis beetle (*Hygrotus curvipes*), vernal pool tadpole shrimp (*Lepidurus packardii*), California linderiella (*Linderiella occidentalis*), molestan blister beetle (*Lytta molesta*), Sacramento perch (*Archoplites interruptus*), delta smelt (*Hypomesus transpacificus*), western pond turtle (*Emys marmorata*), giant garter snake (*Thamnophis gigas*), saltmarsh common yellow-throat (*Geothlypis trichas sinuosa*), California black rail (*Laterallus jamaicensis coturniculus*), Suisun song sparrow (*Melospiza melodia maxillaris*), double-crested cormorant (*Phalacrocorax auritus*), and bank swallow (*Riparia riparia*).

4.2.1 Federal and State Threatened and Endangered Wildlife Species

San Joaquin kit fox (*Vulpes macrotis mutica*, SJKF), a federally listed Endangered and State listed Threatened species, are associated with open habitats, such as arid grasslands, alkali sinks, and open woodlands of the San Joaquin Valley and in surrounding foothills. Reports have shown that SJKF will use the edges of orchards for denning, while foraging in adjacent grassland areas. Kit fox are usually associated with loose textured soils that are suitable for excavating dens, with badgers and coyotes sometimes initiating the excavation. Dens have been found on flatter slopes, suggesting a preference for deep, friable soils. Den entrances are typically 5 to 10 inches in diameter, with three- to six-foot ramps formed from diggings, although dens in this species' northern range often lack ramps or other signs of use (Orloff, *et al.* 1986). Occurrences of populations of SJKF are thought to be related to the availability of denning sites, particularly natal denning sites, which are often moved several times throughout the season. Manmade features, such as culverts and roadbeds, are occasionally used for dens. San Joaquin kit fox prey includes kangaroo rats, black-tailed hare, and ground squirrels.

Study Area Occurrence. Ground squirrel burrows (approximately four inches in diameter extending 2.5 feet) were observed within the study area, which could provide potentially suitable denning habitat for San Joaquin kit fox. However, no occupied denning habitat occurs on the site. No scat, tracks or other sign were observed on site. The closest reported sightings of San Joaquin kit fox are located approximately nine miles to the west, at Black Diamond Mines (Bell 1992). Surveys conducted by H.T. Harvey in 1994 (Kaiser Site), by McGinnis in 1990 and 1991 (Lone Tree Valley) in areas east of the Black Diamond Mines produced negative results (H.T. Harvey and Associates 1997). However, construction and operation of Segment 1 of the Highway 4 Bypass freeway and residential and commercial buildings areas along Lone Tree Way precludes the presence of this species in this area. Therefore, no suitable habitat occurs within the study area for San Joaquin kit fox.

Swainson's hawk (*Buteo swainsonii*, SH), State listed Threatened and protected under the Migratory Bird Treaty Act and California Fish and Game Code 3503.5, once found throughout the lowland basin of California, but are now restricted to portions of the Central Valley where suitable nesting and foraging habitat are still available. Swainson's hawks prefer to nest along the periphery of riparian systems, but will also use lone trees or groves of trees in agricultural fields (CDFG 1990). Valley oak (*Quercus lobata*), Fremont cottonwood (*Populus fremontii*), walnut (*Juglans hindsii*) and large willow (*Salix* sp.) are the tree species most commonly used. Swainson's hawks require large open grasslands with abundant prey, such as small mammals and insects. Over 85 % of SH territories in the Central Valley are in riparian systems adjacent to suitable foraging habitats (Barnes 1994).

Study Area Occurrence. This species has been reported nesting within two miles southeast of the Davidson Subdivision study area (CNDDDB 2007). However, no suitable nesting trees occur in the study area.

The **California red-legged frog** (*Rana draytonii*, CRF) is listed by the USFWS as Threatened and is classified by the CDFG as a California Species of Special Concern. It breeds primarily in ponds, but will also breed in slow moving streams, or deep pools in intermittent streams. Inhabited ponds are typically permanent, at least three feet in depth, and contain emergent and shoreline vegetation. Sufficient pond depth and shoreline cover are both critical, because they provide means of escape from predators for the frogs. Non-breeding CRF have been found in both aquatic and upland habitats. The majority of individuals prefer dense, shrubby or emergent vegetation, closely associated with deep (>0.7 meters) still, or slow moving water. However, some individuals use habitats that are removed from aquatic habitats, seeking cover under coyote brush (*Baccharis pilularis*) and non-native grasslands (Fellers and Kleeman 2007, Tatarian 2005). Aestivation habitat can occur in areas up to 300 feet from a stream corridor or pond and includes natural features, such as boulders, rocks, trees, shrubs, and logs.

Study Area Occurrence: California red-legged frog is considered to have no potential to occur within the study area, based on the lack of suitable habitat on the site or within one mile of the site. No movement or dispersal corridors or hydrologic connection occurs between the project site and known locations of CRF.

The **California tiger salamander** (*Ambystoma californiense*, CTS) is federally listed Threatened, and a California Special Concern species. California tiger salamander inhabits grassland and oak savanna habitats in the valleys and low hills of central and coastal California. Habitat conversion has eliminated the species from much of its former range (Shaffer, *et al.* 1993; Fisher and Shaffer 1996). Adults spend most of their lives underground, typically in the burrows of ground squirrels and other animals (Stebbins and Cohen 1997, Jennings 1996). During winter rains between November and March, adults emerge from underground retreats to feed, court and breed (Loredo and Van Vuren 1996). Ponds must contain water for at least 3.5 months to allow CTS larvae to complete their development. Following transformation, juvenile salamanders seek refugia, typically mammal burrows, where they remain until the next winter rains (Stebbins 1985; Jennings 1996).

Study Area Occurrence: The California tiger salamander is considered to have no potential for occurrence within the study area due to the lack of suitable breeding habitat on the site, together with the site's disconnection from known occurrences. The closest report sighting of CTS occurs approximately four miles southwest of the study area (CNDDDB 2007). Residential and commercial development occurs between the study area and the reported sighting.

Valley Elderberry Longhorn Beetle (*Desmocerus californicus dimorphus*, VELB), a federally-listed Threatened species, is a red and black wood-boring insect, occurs throughout the California Central Valley and foothills of the Coast Ranges and Sierras, between the elevations of 0 to 3,000 ft. The host plant, blue elderberry (*Sambucus mexicanus*), is typically associated with riparian habitats and adjacent upland habitats. The one- to two-year life cycle of the VELB is dominated by the larval stage of the insect, where it resides in the trunk and limbs of the blue elderberry. Emergence of adults occurs from late March through June, and evidence of occupancy in an elderberry is shown by the emergence hole of the adult. Today less than 4% of the historical 400,000 acres of riparian forest remain (USFWS 1990).

Study Area Occurrence: The VELB is considered to have no potential for occurrence within the study area due to the lack of suitable habitat on the site - no elderberry trees were observed on site.

4.2.2 Other Special-Status Wildlife Species

Bat Species (including pallid bat (*Antrozous pallidus*), small-footed myotis (*Myotis ciliolabrum*), long-eared myotis (*Myotis evotis*), fringed myotis (*Myotis thysanodes*), Yuma myotis (*Myotis yumanensis*), and long-legged myotis (*Myotis volans*)), are listed as federal Species of Concern and California Special Concern species. Of the 25 bat species in California, approximately 60% (15 species) use trees as an important part of their roosting habitat (Brown 1996). Species that use trees as well as other structures include pallid bat (*Antrozous pallidus*), western small-footed (*Myotis ciliolabrum*), western long-eared myotis (*Myotis evotis*), fringed bat (*Myotis thysanodes*), and long-legged bat (*Myotis volans*). Day roost selection is governed by several factors, such as temperature, roost configuration, lack of disturbance from people and predators, and proximity to foraging habitat and/or water (Brown 1996). Trees typically used by bats require structurally complex forests, heterogeneous age structure, large component of old trees (>25 inch DBH) and >40 feet in height), with emergent canopy or gap providing sun exposure and snags of various stages, although smaller trees with suitable cavities are also used.

Study Area Occurrence. No suitable roosting habitat occurs on the site for special status bat species.

The **western burrowing Owl** (BUOW) is a federal and California Special Concern species and is protected under the Migratory Bird Treaty Act. The BUOW is small, and long-legged, with dull brown plumage that is barred and spotted with white. Burrowing owls are typically observed on the ground, at or near a burrow, or on elevated areas, such as dirt mounds or fence posts that are used as observational or hunting perches. Three habitat characteristics that comprise burrowing owl habitat include openness (lack of canopy cover), short vegetation, and burrow availability. Suitable habitat may also include areas with trees and shrubs, as long as the canopy covers less than 30 percent of the ground surface (CDFG 1995, CBOC 1993). Vegetation height has been identified as a limiting factor in occupancy (Coulombe 1971, Wesseman 1985). Owls have been reported foraging up to one mile from breeding areas (Haug and Oliphant 1990). Long distance movement of BUOW of over 53 km has been reported for birds in Carrizo Plain, near Bakersfield (Rosier, et al 2006). Although similar movements have been reported for birds in Canada, movement was attributed to habitat fragmentation, not experienced on the Carrizo plain (Rosier, et al 2006).

Study Area Occurrence. This species has been observed in the southwestern corner of the study area since 2005 (CNDDDB 2007). Please refer to Table 1 for a synopsis of the number of owls observed on the site.

Table: Number of BUOW observed in the southwestern portion of Park Ridge Estates

| Date (Reference) | Number of BUOW | Banded | Exclusion Date |
|---------------------------------|----------------|--------|-----------------|
| 8/5/05 ⁽¹⁾ | 8 | no | none |
| 9/1 – 9/7/05 ⁽²⁾ | 9 | 7 | none |
| 9/23 – 9/28/05 ⁽³⁾ | 4 | 4 | 9/23 – 9/28/05 |
| 2/6/06 – 3/10/06 ⁽⁴⁾ | 3 | 1 | 2/6 – 3/10/06 |
| 3/19/06 ⁽⁵⁾ | 2 | no | none |
| 2/27/07 ⁽⁵⁾ | 1 | no | 2/13/ - 3/15/07 |
| 9/20/07 ⁽⁵⁾ | 1 | no | none |

Notes:

1 = Wildlife Research Associates 2005.

2 = Albion Environmental 2005a.

3 = Albion Environmental 2005b.

4 = Wildlife Research Associates 2006.

5 = Wildlife Research Associates 2007a.

In August 2005, 3 adults and 5 babies, with down on their heads, were observed on the site during focused surveys in the southwestern portion of the site (Wildlife Research Associates 2005). Focused surveys for BUOW were conducted only in this area and not of the entire site. In a follow-up survey in September, a total of 9 BUOW were observed in the southwestern portion (Albion 2005a). Of these 9, two adults were banded, and 5 of the 7 juveniles were banded (Albion 2005a) at the request of CDFG.

On February 6, 2006, three BUOW, of which one was banded, were observed in the southwestern portion of the site (Wildlife Research Associates 2006). Under coordination with CDFG, these owls were excluded and the burrows were collapsed. No additional surveys for BUOW on the rest of the site were conducted. No collapse of burrows were conducted in the northwestern portion of the site. In February of 2007, one BUOW was observed in the southwest area and was excluded. In September 2007, another owl was observed in a new set of burrows in the southwestern central portion of the site. This owl was not excluded, nor were the burrows collapsed.

In 2006, three pairs of BUOW were observed in the northwestern portion of the site. In 2007, 4 pairs were observed (CNDDDB 2007). None of the BUOW appeared to be banded.

Previous Mitigation: As part of the exclusion and banding procedure conducted in 2005 on the Davidon project site, mitigation for the 1 pair and 1 unpaired resident owl was implemented in August of 2006. A Purchase Agreement was completed for 19.5 credits (acres of occupied habitat credit) purchased by Davidon for the Jacuzzi Ranch (Park Ridge) Project in Antioch in the

CDFG-approved Haera Conservation Bank, operated by Wildlands, Inc. Copies of the executed Agreement were provided by the project sponsor to the City of Antioch and CDFG. The 19.5 conservation bank credits correspond to the adopted CDFG policy (based on the Burrowing Owl Survey Protocol and Mitigation Guidelines report prepared in April of 1993 by the California Burrowing Owl Consortium) of requiring 1.5 times 6.5 acres (9.75 acres) of replacement occupied habitat for each pair or single adult bird affected (1.5 X 6.5 acres X 2 pair or single individuals = requirement for 19.5 acres of occupied replacement habitat).

Although 7 of the 9 BUOW were banded, which allowed for tracking of those individuals, only one owl was observed in February 2006 in the southwestern corner. After exclusion in 2006, subsequent sightings of them have not been reported on the Park Ridge project site or in the vicinity (Barclay, pers. comm. 2007). None of the BUOW observed on the Park Ridge Estate site after February 2006 appeared to be banded. As a result, it is unclear where those originally banded on the project site have moved to, and whether the birds subsequently observed on the project site have migrated from the Bypass right-of-way or another site for which mitigation have been provided. Additionally, due to their mobility and use of many different burrows within a complex, the number of birds currently using the southwestern and northwestern corners of the site is unknown.

Raptors (birds of prey) (including white-tailed kite (*Elanus leucurus*), American kestrel (*Falco americanus*), northern harrier (*Circus cyaneus*) and red-tailed hawk (*Buteo jamaicensis*)) are Protected under the Federal Migratory Bird treaty Act and Fish and Game Code 3503.5 and 3511. Nest structures for raptor species range from stick nests to ground nesting. Remnant orchard trees located individually throughout the study area once provided potential nesting habitat for a limited number of the raptor species listed above.

Study Area Occurrence. White tailed kite and kestrels were observed nesting on the Deliza Ranch property in 2005 (CNDDDB 2007). There is a high likelihood that these birds may nest within the same area in the future. The remaining grasslands on the site provide nesting habitat for northern harrier.

Passerines (perching birds) (including loggerhead shrike (*Lanius ludovicianus*), Say's phoebe (*Sayornis saya*), mourning dove (*Zenaida macroura*) and ground-nesting species, such as western meadowlark, (*Sturnella neglecta*), and horned lark (*Eremophila alpestris actia*), are protected under the Federal Migratory Bird Treaty Act and Fish and Game Code 3503.5. Several of these species, including western meadowlark and horned lark, breed in open grasslands throughout the Central Valley and adjacent foothills and along the central and southern California coast region. These species typically prefer shorter, less dense grasses and areas with some bare ground. California horned lark often forms flocks in the summer and winter months, foraging and roosting in cultivated fields and along dirt roads and feeding on insects and seeds. Tree nesting species, such as loggerhead shrike and mourning dove, prefer densely vegetated, isolated trees and shrubs and occasionally man-made structures are typically used for nesting. Loggerhead shrikes feed on a variety of small prey, including arthropods, small mammals, amphibians, reptiles and birds (Yosef 1996). Since it lacks talons, it often impales prey on thorns or barbed wire. In California, the species does not migrate and is resident year-round. Pairs maintain territories during the breeding season and individuals maintain territories during the winter (Yosef 1996).

Study Area Occurrence. These passerines may nest throughout the study area in grasslands and in individual trees. Loggerhead shrikes once nested within almond trees, which are annually

trimmed. Unless tree structures are removed completely, , there is a high likelihood this species will nest on the site. The willow trees located at the freshwater marsh may also provide nesting habitat for passerines.

5.0 IMPACTS AND MITIGATION MEASURES

This section summarizes the potential temporary biological impacts from construction activities within the study area. The analysis of these impacts is based on a single reconnaissance-level survey of the study area, focused BUOW surveys at the southwest corner of the project site, a review of existing databases and literature, and personal professional experience with biological resources of the region. Potential impacts to special-status biotic resources, namely to individual special-status animal species may occur from the proposed project. Mitigation for these biological impacts to avoid adverse effects on the environment, are provided below.

Assessing impacts and creating mitigation measures for western burrowing owl were based on the CDFG *Staff Report on Burrowing Mitigation* (CDFG 1995) which is based on the *Burrowing Owl Survey Protocol and Mitigation Guidelines* created by the California Burrowing Owl Consortium (CBOC 1993).

Impact 5.1. The **San Joaquin kit fox** has no potential for occurrence on-site, and based on the presumed presence of extremely low numbers in the region and the physical distance and urban separation of the site from known San Joaquin kit fox habitat, no suitable habitat for this species occurs on the study site. Although ground squirrel burrows, which could provide potentially suitable denning habitat, were observed on site, no burrows showed signs of San Joaquin kit fox activity (i.e., large dirt ramps from excavation, cleared vegetation, tracks, scat, etc). Therefore, construction within the grasslands would not result in any temporary direct or indirect impacts to San Joaquin kit fox individuals and/or habitat.

This is a less-than-significant impact. No mitigation measures are required.

Impact 5.2. The proposed project could result in disturbance of potential **raptor nesting** habitat on the adjacent Deliza Ranch lands and within the study area. Disturbance during the nesting season (February 1 through August 31) may result in the potential nest abandonment and mortality of young.

Mitigation Measure 5.2: To avoid “take” and/or further evaluate presence or absence of raptors, the following measures are recommended:

- A. A pre-construction nesting bird survey of the individual trees and grasslands throughout the study area shall be performed by a qualified biologist. If no nesting birds are observed no further action is required and grading may occur within one week of the survey to prevent “take” of individual birds that may have begun nesting after the survey.
- B. If birds are observed nesting on site after February 1 it should be assumed that they are nesting adjacent to the site. The CDFG Central Coast Regional office allows grading to occur if nesting birds are observed on site, providing that a 300-foot buffer zone is created around the observed nest to prevent disturbance and ultimately “take” of young.

Impact 5.3. The proposed project was found in 2005 to result in the removal of occupied **BUOW nesting** habitat within the non-native grasslands in the southwestern corner of the site. The

habitat area was found to have been occupied in 2005 by one pair and one individual adult owl, along with dependent juvenile owls. Mitigation for this impact was implemented in 2006 through the purchase of credits in a CDFG-authorized mitigation bank correlating with 19.5 acres of occupied replacement habitat. Subsequent follow-up surveys conducted in 2006 and 2007 have identified burrow complexes in northwestern and southwestern areas of the site which appear to support a current population of owls. Disturbance to these areas during the nesting season (February 1 through August 31) may result in the potential nest abandonment and mortality of young, resulting in “take” of individuals.

Mitigation 5.3. Established procedures provide for mitigation of lost nesting BUOW habitat either on-site or off-site. Mitigation Measure No. 2 of the CDFG *Staff Report on Burrowing Owl Mitigation* (CDFG 1995) states the following:

“To offset the loss of foraging and burrow habitat on the project site, a minimum of 6.5 acres of foraging habitat, (calculated on a 100-m (approx. 300 ft.) foraging radius around the burrow) per pair or unpaired resident bird, should be acquired and permanently protected. The protected lands should be adjacent to occupied burrowing owl habitat and at a location acceptable to the Department. *Protection of additional habitat acreage per pair or unpaired resident bird may be applicable in some instances.* The California Burrowing Owl Consortium has also developed mitigation guidelines (CBOC 1993) that can be incorporated by CEQA lead agencies and which are consistent with this staff report.”

The California Burrowing Owl Consortium *Burrowing Owl Survey Protocol and Mitigation Guidelines* (CBOC 1993) state the following:

“Off-site habitat must be suitable burrowing owl habitat, as defined in the *Burrowing Owl Survey Protocol*, and the site approved by CDFG. Land should be purchased and/or placed in a conservation easement in perpetuity and managed to maintain suitable habitat. Off-site mitigation should use one of the following ratios:

1. Replacement of occupied habitat with occupied habitat: 1.5 times 6.5 (9.75) acres per pair or single bird.
2. Replacement of occupied habitat with habitat contiguous to currently occupied habitat: 2 times 6.5 (13.0) acres per pair or single bird.
3. Replacement of occupied habitat with suitable unoccupied habitat: 3 times 6.5 (19.5) acres per pair or single bird.”

Based on the foregoing, the project sponsor entered into discussions with the City of Antioch (Lead Agency under CEQA) and CDFG in 2005-2006 to consider the feasibility of using a minimum of 13 acres (6.5 acres X 2 pair or unpaired individual owls) of the on-site open space area as a protected mitigation site. Following review and comment from the City and CDFG staff, it was determined that a number of long-term operational constraints made the on-site mitigation option less desirable than an off-site option. As a result, 19.5 credits for occupied habitat within a CDFG-authorized mitigation bank at an off-site location were purchased (1.5 X 6.5 acres X 2 pair or unpaired individual owls) and reported as mitigation for loss of occupied nesting habitat identified in 2005-2006 in the southwestern corner. No exclusion or eradication effort was conducted of the potential habitat (ground squirrel burrows) subsequently identified in the NW corner of the entire site. As a result, these areas currently remain available for use by BUOW.

Impact 5.4. The proposed project could result in “take” of individuals or pairs of BUOW nesting within the Park Ridge Estates project site.

Mitigation 5.4. To avoid “take” of individual BUOW nesting on site, the following measures are recommended:

- A. If ground disturbance must occur within the nesting season (February 1 to August 31), a pre-construction nesting burrowing owl survey following CDFG protocols should be performed by a qualified biologist prior to disturbance. Protocol surveys include conducting four crepuscular (early morning or late evening) surveys. If owls are found but no courtship behavior is observed then exclusion of the owls from the burrows may occur. Any early season active nests, as shown by courtship behavior or food transfers between adults, must not be disturbed until the young have fledged.
- B. Ground squirrel burrows within the area of proposed ground disturbance will have exclusion devices put on them for 48 hours to ensure any owls have left the burrows before excavation.
- C. All burrows with active nests with owls exhibiting courtship behavior or food transference shall be identified by flagging and be protected by a no disturbance buffer zone of 75 meters (approximately 250 feet). No further disturbance to these areas shall occur until the young have fledged and exclusion has been implemented.
- D. Areas of bare ground or with grass less than six inches in height may attract burrowing owls during the winter season. If construction is to occur after a period of inactivity and soil is left barren, a burrowing owl habitat evaluation to determine occupancy of the site should be conducted prior to ground disturbance the following season.

Impact 5.5. The proposed project could result in the removal of potential passerine nesting habitat in the non-native grasslands and trees along the southern and northern boundaries, although no focused surveys for nesting passerines have been conducted within the study area. Disturbance during the nesting season may result in the potential nest abandonment and mortality of young.

Mitigation Measure 5.5: The BUOW Conservation Area will provide nesting passerine habitat. To avoid “take” and/or further evaluate presence or absence of passerines, the following measures are recommended:

- Grading within the grasslands should be conducted outside the nesting season, which occurs between approximately February 1 and August 15.
- If grading before February 1 is infeasible and groundbreaking must occur within the breeding season, a pre-construction nesting bird survey of the grasslands and adjacent trees shall be performed by a qualified biologist. If no nesting birds are observed no further action is required and grading shall occur within one week of the survey to prevent “take” of individual birds that may have begun nesting after the survey.
- If birds are observed on site after February 1 it will be assumed that they are nesting on site or adjacent to the site and ground breaking will have to be delayed until after the young have fledged, as determined by bird surveys by a qualified biologist, or after the nesting season.
- The CDFG Central Coast Regional office does allow grading to occur if nesting birds are observed on site, providing that a 100 foot buffer zone is created around the

observed nest. Because nests may occur in the middle of the grading area, this method is not advised.

- Nesting bird surveys for raptors and passerines may occur at the same time, after February 1.

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Appendix C

Burrowing Owl Banding Report



ALBION ENVIRONMENTAL, INC.
NATURAL AND CULTURAL RESOURCES CONSULTANTS

1414 SOQUEL AVENUE, SUITE 205
SANTA CRUZ, CALIFORNIA 95062

TELEPHONE (831) 469-9128
FACSIMILE (831) 469-9137

September 12, 2005

Richard T. Loewke, AICP
Urban & Environmental Planning
55 Oak Trail Court
Alamo, CA 94507

Dear Mr. Loewke:

I am writing with a final report on burrowing owl (*Athene cunicularia*) banding at the Davidon site in Antioch. The Davidon site is located immediately east of Canada Valley Road approximately 0.4 miles north of Lone Tree Way in the City of Antioch, Contra Costa County. The site supports mixed herbaceous vegetation ranging up to 5 feet tall in places. Owls were using burrows on the east-facing slope of a small hill that extends east from Canada Valley Road just south of a short dead-end spur on the as-yet-to-be-constructed Jacuzzi Drive. I also observed owls roosting at burrows in a low ridge of rocky debris approximately 150 feet southeast of the small hill and at a small burrow complex on the opposite slope approximately 400 feet to the east.

I saw a total of 9 burrowing owls, 2 adults and 7 juveniles, when I briefly monitored their behavior and evaluated opportunities to capture them on August 29th and 30th. I did not observe the owls retreating down burrows, either voluntarily or when provoked, so there were no opportunities to capture them using one-way doors and enclosures. I also closely monitored the owls throughout the day on September 2 and did not see them retreat down burrows for extended periods. Based on their behavior I decided to capture them for banding using other raptor traps including a bow net, dho-gazza and bal-chatri.

We (myself or my employee Lindsay Harman) spent 4 evenings trapping - September 1, 2, 6 and 7, 2005. We captured and banded a total of 7 burrowing owls; 2 adults and 5 juveniles. Age was determined by molt and plumage condition. Below are the band numbers, ages and banding dates. Each captured owl was banded with a standard bird band issued by the U.S. Geological Survey Bird Banding Laboratory (i.e., federal band) and a red metal color band with alphanumeric code manufactured by Acraft Sign and Nameplate Company. The red color bands, which can be read with binoculars or spotting scope, enable individual identification without having the bird in the hand as is necessary to read the federal band number. Each owl was released immediately after it was banded and no owls were injured during trapping.

| Federal Band No. | Color Band No. (type 1*) | Age | Date Banded |
|------------------|--------------------------|----------|-------------|
| 934-13876 | Red VK | Juvenile | 9/1/05 |
| 934-13877 | Red WK | Juvenile | 9/2/05 |
| 934-13878 | Red XK | Adult | 9/6/05 |
| 934-13879 | Red YK | Juvenile | 9/6/05 |
| 934-13880 | Red AM | Juvenile | 9/7/05 |
| 934-13881 | Red BM | Juvenile | 9/7/05 |
| 934-13882 | Red CM | Adult | 9/7/05 |

*Type 1 refers to the orientation of the characters on the color band, in this case side-by-side.

As required by my federal and state authorizations to capture and band burrowing owls I will be submitting these banding records to the Bird Banding Laboratory and to the Department of Fish and Game with my annual report of activities. I have also submitted a field observation form of my burrowing owl observations and bandings to the California Natural Diversity Database.

Thank you for asking me to band these burrowing owls. Please contact me if you have any questions about my report.

Sincerely,

A handwritten signature in cursive script that reads "Jack Barclay". The signature is written in black ink and is positioned above the printed name and title.

Jack Barclay
Ornithologist, Vice-President
Master Banding Permit No. 23371
CDFG Burrowing Owl Research MOU June 9, 2000
CDFG Scientific Collecting Permit No. 004413

Appendix D

Burrowing Owl Survey Protocol & Mitigation Guidelines

BURROWING OWL SURVEY PROTOCOL
AND MITIGATION GUIDELINES

Prepared by:

The California Burrowing Owl Consortium

April 1993

INTRODUCTION

The California Burrowing Owl Consortium developed the following Survey Protocol and Mitigation Guidelines to meet the need for uniform standards when surveying burrowing owl (*Speotyto cunicularia*) populations and evaluating impacts from development projects. The California Burrowing Owl Consortium is a group of biologists in the San Francisco Bay area who are interested in burrowing owl conservation. The following survey protocol and mitigation guidelines were prepared by the Consortium's Mitigation Committee. These procedures offer a decision-making process aimed at preserving burrowing owls in place with adequate habitat.

California's burrowing owl population is clearly in peril and if declines continue unchecked the species may qualify for listing. Because of the intense pressure for development of open, flat grasslands in California, resource managers frequently face conflicts between owls and development projects. Owls can be affected by disturbance and habitat loss, even though there may be no direct impacts to the birds themselves or their burrows. There is often inadequate information about the presence of owls on a project site until ground disturbance is imminent. When this occurs there is usually insufficient time to evaluate impacts to owls and their habitat. The absence of standardized field survey methods impairs adequate and consistent impact assessment during regulatory review processes, which in turn reduces the possibility of effective mitigation.

These guidelines are intended to provide a decision-making process that should be implemented wherever there is potential for an action or project to adversely affect burrowing owls or the resources that support them. The process begins with a four-step survey protocol to document the presence of burrowing owl habitat, and evaluate burrowing owl use of the project site and a surrounding buffer zone. When surveys confirm occupied habitat, the mitigation measures are followed to minimize impacts to burrowing owls, their burrows and foraging habitat on the site. These guidelines emphasize maintaining burrowing owls and their resources in place rather than minimizing impacts through displacement of owls to an alternate site.

Each project and situation is different and these procedures may not be applicable in some circumstances. Finally, these are not strict rules or requirements that must be applied in all situations. They are guidelines to consider when evaluating burrowing owls and their habitat, and they suggest options for burrowing owl conservation when land use decisions are made.

Section 1 describes the four phase Burrowing Owl Survey Protocol. Section 2 contains the Mitigation Guidelines. Section 3 contains a discussion of various laws and regulations that protect burrowing owls and a list of references cited in the text.

We have submitted these documents to the California Department of Fish and Game (CDFG) for review and comment. These are untested procedures and we ask for your comments on improving their usefulness.

SECTION 1 BURROWING OWL SURVEY PROTOCOL

PHASE I: HABITAT ASSESSMENT

The first step in the survey process is to assess the presence of burrowing owl habitat on the project site including a 150-meter (approx. 500 ft.) buffer zone around the project boundary (Thomsen 1971, Martin 1973).

Burrowing Owl Habitat Description

Burrowing owl habitat can be found in annual and perennial grasslands, deserts, and scrublands characterized by low-growing vegetation (Zarn 1974). Suitable owl habitat may also include trees and shrubs if the canopy covers less than 30 percent of the ground surface. Burrows are the essential component of burrowing owl habitat: both natural and artificial burrows provide protection, shelter, and nests for burrowing owls (Henny and Blus 1981). Burrowing owls typically use burrows made by fossorial mammals, such as ground squirrels or badgers, but also may use man-made structures, such as cement culverts; cement, asphalt, or wood debris piles; or openings beneath cement or asphalt pavement.

Occupied Burrowing Owl Habitat

Burrowing owls may use a site for breeding, wintering, foraging, and/or migration stopovers. Occupancy of suitable burrowing owl habitat can be verified at a site by an observation of at least one burrowing owl, or, alternatively, its molted feathers, cast pellets, prey remains, eggshell fragments, or excrement at or near a burrow entrance. Burrowing owls exhibit high site fidelity, reusing burrows year after year (Rich 1984, Feeney 1992). A site should be assumed occupied if at least one burrowing owl has been observed occupying a burrow there within the last three years (Rich 1984).

The Phase II burrow survey is required if burrowing owl habitat occurs on the site. If burrowing owl habitat is not present on the project site and buffer zone, the Phase II burrow survey is not necessary. A written report of the habitat assessment should be prepared (Phase IV), stating the reason(s) why the area is not burrowing owl habitat.

PHASE II: BURROW SURVEY

1. A survey for-burrows and owls should be conducted by walking through suitable habitat over the entire project site and in areas within 150 meters (approx 500 ft.) of the project impact zone. This 150-meter buffer zone is included to account for adjacent burrows and foraging habitat outside the project area and impacts from factors such as noise and vibration due to heavy equipment which could impact resources outside the project area.

2. Pedestrian survey transects should be spaced to allow 100 percent visual coverage of the ground surface. The distance between transect center lines should be no more than 30 meters (approx. 100 ft.), and should be reduced to account for differences in terrain, vegetation density, and ground surface visibility. To efficiently survey projects larger than 100 acres, it is recommended that two or more surveyors conduct concurrent surveys. Surveyors should maintain a minimum distance of 50 meters (approx. 160 ft.) from any owls or occupied burrows. It is important to minimize disturbance near occupied burrows during all seasons.
3. If burrows or burrowing owls are recorded on the site, a map should be prepared of the burrow concentration areas. A breeding season survey and census (Phase III) of burrowing owls is the next step required.
4. Prepare a report (Phase IV) of the burrow survey stating whether or not burrows are present.
5. A preconstruction survey may be required by project-specific mitigations no more than 30 days prior to ground disturbing activity.

PHASE III: BURROWING OWL SURVEYS, CENSUS AND MAPPING

If the project site contains burrows that could be used by burrowing owls, then survey efforts should be directed towards determining owl presence on the site. Surveys in the breeding season are required to describe if, when, and how the site is used by burrowing owls. If no owls are observed using the site during the breeding season, a winter survey is required.

Survey Methodology

A complete burrowing owl survey consists of four site visits. During the initial site visit examine burrows for owl sign and map the locations of occupied burrows. Subsequent observations should be conducted from as many fixed points as necessary to provide visual coverage of the site using spotting scopes or binoculars. It is important to minimize disturbance near occupied burrows during all seasons. Site visits must be repeated on four separate days. Conduct these visits from two hours before sunset to one hour after or from one hour before to two hours after sunrise. Surveys should be conducted during weather that is conducive to observing owls outside their burrows. Avoid surveys during heavy rain, high winds (> 20 mph), or dense fog.

Nesting Season Survey. The burrowing owl nesting season begins as early as February 1 and continues through August 31 (Thomsen 1971, Zam 1974). The timing of nesting activities may vary with latitude and climatic conditions. If possible, the nesting season survey should be conducted during the peak of the breeding season, between April 15 and July 15. Count and map all burrowing owl sightings, occupied burrows, and burrows with owl sign. Record numbers of pairs and juveniles, and behavior such as courtship and copulation. Map the approximate territory boundaries and foraging areas if known.

Survey for Winter Residents (non-breeding owls). Winter surveys should be conducted between December 1 and January 31, during the period when wintering owls are most likely to be present. Count and map all owl sightings, occupied burrows, and burrows with owl sign.

Surveys Outside the Winter and Nesting Seasons. Positive results, (i.e., owl sightings)- outside of the above survey periods would be adequate to determine presence of owls on site. However, results of these surveys may be inadequate for mitigation planning because the numbers of owls and their pattern of distribution may change during winter and nesting seasons. Negative results during surveys outside the above periods are not conclusive proof that owls do not use the site.

Preconstruction Survey. A preconstruction survey may be required by project-specific mitigations and should be conducted no more than 30 days prior to ground disturbing activity.

PHASE IV: RESOURCE SUMMARY, WRITTEN REPORT

A report should be prepared for CDFG that gives the results of each Phase of the survey protocol, as outlined below.

Phase I: Habitat Assessment

1. Date and time of visit(s) including weather and visibility conditions; methods of survey.
2. Site description including the following information: location, size, topography, vegetation communities, and animals observed during visit(s).
3. An assessment of habitat suitability for burrowing owls and explanation.
4. A map of the site.

Phase II: Burrow Survey

1. Date and time of visits including weather and visibility conditions; survey methods including transect spacing.
2. A more detailed site description should be made during this phase of the survey protocol including a partial plant list of primary vegetation, location of nearest freshwater (on or within one mile of site), animals observed during transects.
3. Results of survey transects including a map showing the location of concentrations of burrow(s) (natural or artificial) and owl(s), if present.

Phase III: Burrowing Owl Surveys, Census and Mapping

1. Date and time of visits including weather and visibility conditions; survey methods including transect spacing.
2. Report and map the location of all burrowing owls and owl sign. Burrows occupied by owl(s) should be mapped indicating the number of owls at each burrow. Tracks, feathers, pellets, or other items (prey remains, animal scat) at burrows should also be reported.
3. Behavior of owls during the surveys should be carefully recorded (from a distance) and reported. Describe and map areas used by owls during the surveys. Although not required, all behavior is valuable to document including feeding, resting, courtship, alarm, territorial, parental, or juvenile behavior.
4. Both winter and nesting season surveys should be summarized. If possible include information regarding productivity of pairs, seasonal pattern of use, and include a map of the colony showing territorial boundaries and home ranges.
5. The historical presence of burrowing owls on site should be documented, as well as the source of such information (local bird club, Audubon society, other biologists, etc.).

Burrowing: Owl Survey Protocol

April 1993

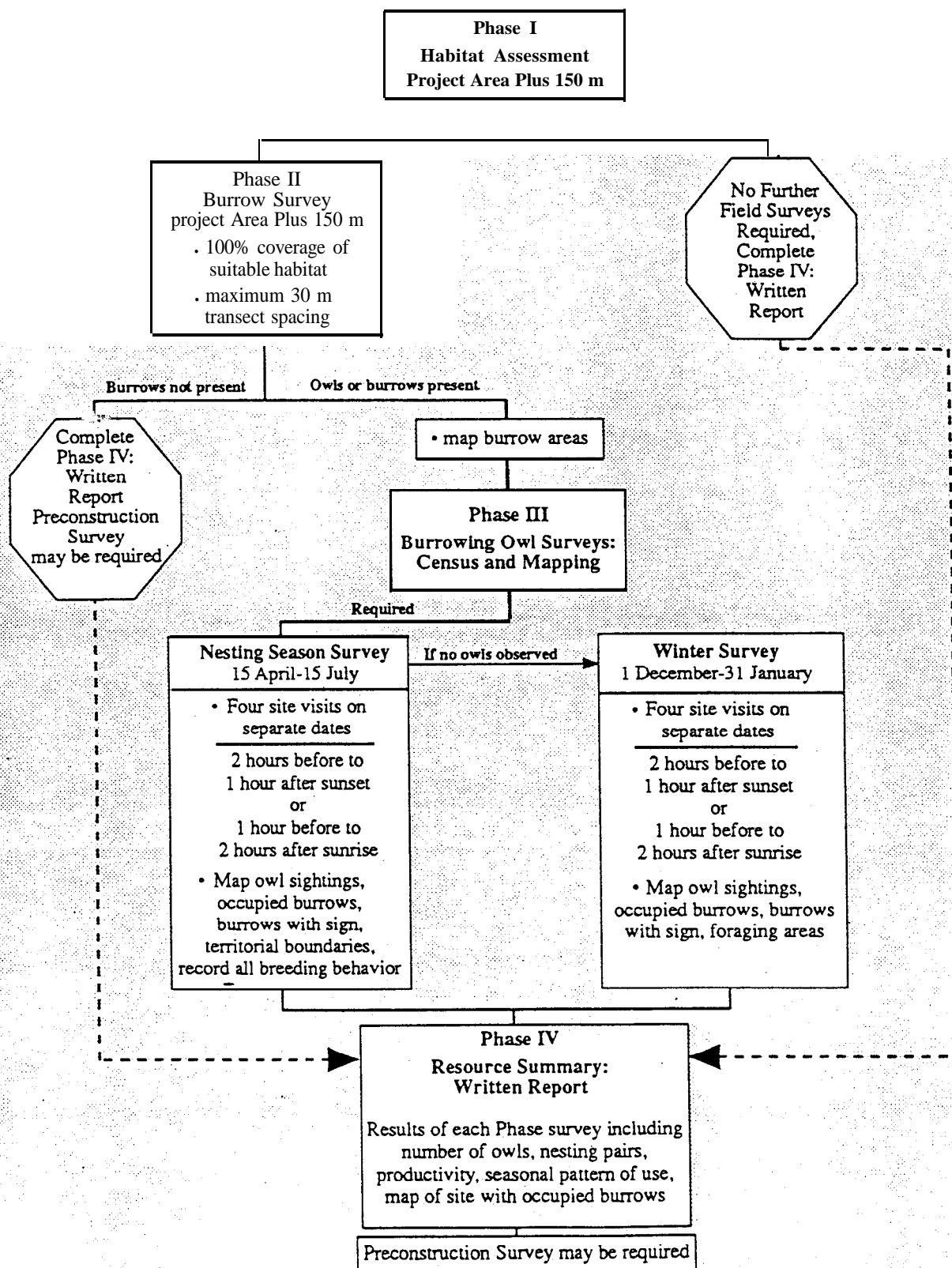


Figure 1.

SECTION 2 BURROWING OWL MITIGATION GUIDELINES

The objective of these mitigation guidelines is to minimize impacts to burrowing owls and the resources that support viable owl populations. These guidelines are intended to provide a decision-making process that should be implemented wherever there is potential for an action or project to adversely affect burrowing owls or their resources. The process begins with a four-step survey protocol (see *Burrowing Owl Survey Protocol*) to document the presence of burrowing owl habitat, and evaluate burrowing owl use of the project site and a surrounding buffer zone. When surveys confirm occupied habitat, the mitigation measures described below are followed to minimize impacts to burrowing owls, their burrows and foraging habitat on the site. These guidelines emphasize maintaining burrowing owls and their resources in place rather than minimizing impacts through displacement of owls to an alternate site.

Mitigation actions should be carried out prior to the burrowing owl breeding season, generally from February 1 through August 31 (Thomsen 1971, Zarn 1974). The timing of nesting activity may vary with latitude and climatic conditions. Project sites and buffer zones with suitable habitat should be resurveyed to ensure no burrowing owls have occupied them in the interim period between the initial surveys and ground disturbing activity. Repeat surveys should be conducted not more than 30 days prior to initial ground disturbing activity.

DEFINITION OF IMPACTS

1. Disturbance or harassment within 50 meters (approx. 160 ft.) of occupied burrows.
2. Destruction of burrows and burrow entrances. Burrows include structures such as culverts, concrete slabs and debris piles that provide shelter to burrowing owls.
3. Degradation of foraging habitat adjacent to occupied burrows.

GENERAL CONSIDERATIONS

1. Occupied burrows should not be disturbed during the nesting season, from February 1 through August 31, unless the Department of Fish and Game verifies that the birds have not begun egg-laying and incubation or that the juveniles from those burrows are foraging independently and capable of independent survival at an earlier date.
2. A minimum of 6.5 acres of foraging habitat, calculated on a 100-m (approx. 300 ft.) foraging radius around the natal burrow, should be maintained per pair (or unpaired resident single bird) contiguous with burrows occupied within the last three years (Rich 1984, Feeney 1992). Ideally, foraging habitat should be retained in a long-term conservation easement.

3. When destruction of occupied burrows is unavoidable, burrows should be enhanced (enlarged or cleared of debris) or created (by installing artificial burrows) in a ratio of 1:1 in adjacent suitable habitat that is contiguous with the foraging habitat of the affected owls.
4. If owls must be moved away from the disturbance area, passive relocation (see below) is preferable to trapping. A time period of at least one week is recommended to allow the owls to move and acclimate to alternate burrows.
5. The mitigation committee recommends monitoring the success of mitigation programs as required in Assembly Bill 3180. A monitoring plan should include mitigation success criteria and an annual report should be submitted to the California Department of Fish and Game.

AVOIDANCE

Avoid Occupied Burrows

No disturbance should occur within 50 m (approx. 160 ft.) of occupied burrows during the non-breeding Season of September 1 through January 31 or within 75 m (approx. 250 ft.) during the breeding Season of February 1 through August 31. Avoidance also requires that a minimum of 6.5 acres of foraging habitat be preserved contiguous with occupied burrow sites for each pair of breeding burrowing owls (with or without dependent young) or single unpaired resident bird (Figure 2).

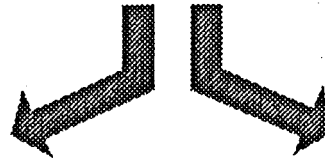
MITIGATION FOR UNAVOIDABLE IMPACTS

On-site Mitigation

On-site passive relocation should be implemented if the above avoidance requirements cannot be met. Passive relocation is defined as encouraging owls to move from occupied burrows to alternate natural or artificial burrows that are beyond 50 m from the impact zone and that are within or contiguous to a minimum of 6.5 acres of foraging habitat for each pair of relocated owls (Figure 3). Relocation of owls should only be implemented during the non-breeding season. On-site habitat should be preserved in a conservation easement and managed to promote burrowing owl use of the site.

Owls should be excluded from burrows in the immediate impact zone and within a 50 m (approx. 160 ft.) buffer zone by installing one-way doors in burrow entrances: One-way doors should be left in place 48 hours to insure owls have left the burrow before excavation. One alternate natural or artificial burrow should be provided for each burrow that will be excavated in the project impact zone. The project area should be monitored daily for one week to confirm owl use of alternate burrows before excavating burrows in the immediate impact zone. Whenever possible, burrows should be excavated using hand tools and refilled to prevent reoccupation. Sections of flexible plastic pipe or burlap bags should be inserted into the tunnels

AVOIDANCE



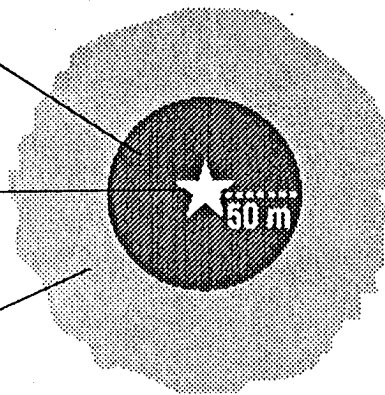
Non-breeding season

1 Sept. - 31 Jan.

No impacts within
50 m of occupied
burrow

Occupied
burrow

Maintain
at least 6.5 acres
foraging habitat



Breeding season

1 Feb. - 31 Aug.

No impacts within
75 m of occupied
burrow

Occupied
burrow

Maintain
at least 6.5 acres
foraging habitat

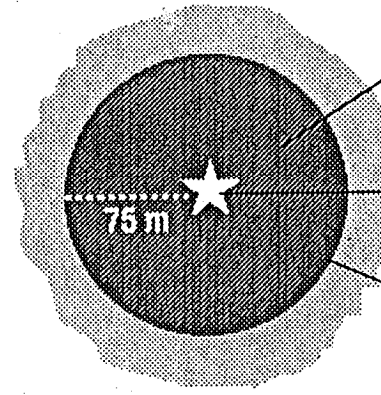


Figure 2. Burrowing owl mitigation guidelines.

ON-SITE MITIGATION IF AVOIDANCE NOT MET

(More than 6.5 acres suitable habitat available)

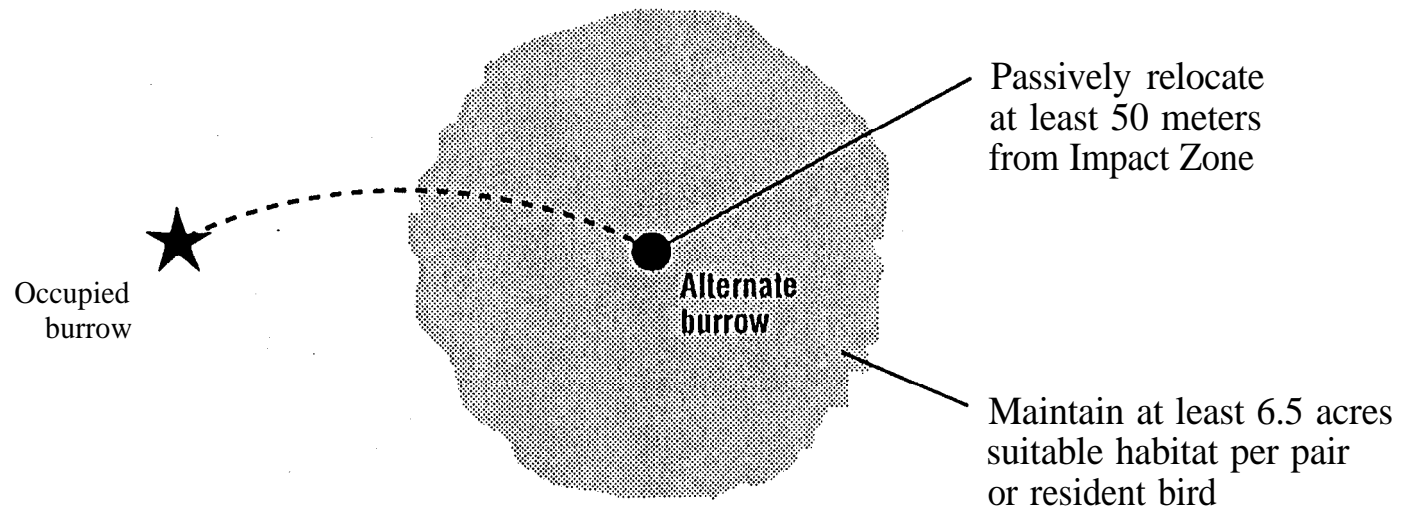


Figure 3. Burrowing owl mitigation guidelines.

during excavation to maintain an escape route for any animals inside the burrow.

Off-site Mitigation

If the project will reduce suitable habitat on-site below the threshold level of 6.5 acres per relocated pair or single bird, the habitat should be replaced off-site. Off-site habitat must be suitable burrowing owl habitat, as defined in the *Burrowing Owl Survey Protocol*, and the site approved by CDFG. Land should be purchased and/or placed in a conservation easement in perpetuity and managed to maintain suitable habitat. Off-site mitigation should use one of the following ratios:

1. Replacement of occupied habitat with occupied habitat: 1.5 times 6.5 (9.75) acres per pair or single bird.
2. Replacement of occupied habitat with habitat contiguous to currently occupied habitat: 2 times 6.5 (13.0) acres per pair or single bird.
3. Replacement of occupied habitat with suitable unoccupied habitat: 3 times 6.5 (19.5) acres per pair or single bird.

SECTION 3 LEGAL STATUS

The burrowing owl is a migratory bird species protected by international treaty under the Migratory Bird Treaty Act (MBTA) of 1918 (16 U.S.C. 703-711). The MBTA makes it unlawful to take, possess, buy, sell, purchase, or barter, any migratory bird listed in 50 C.F.R. Part 10, including feathers or other parts, nests, eggs, or products, except as allowed by implementing regulations (50 C.F.R. 21). Sections 3503, 3503.5, and 3800 of the California Department of Fish and Game Code prohibit the take, possession, or destruction of birds, their nests or eggs. Implementation of the take provisions requires that project-related disturbance at active nesting territories be reduced or eliminated during critical phases of the nesting cycle (March 1 - August 15, annually). Disturbance that causes nest abandonment and/or loss of reproductive effort (e.g., killing or abandonment of eggs or young) or the loss of habitat upon which the birds depend is considered “taking” and is potentially punishable by fines and/or imprisonment. Such taking would also violate federal law protecting migratory birds (e.g., MBTA).

The burrowing owl is a Species of Special Concern to California because of declines of suitable habitat and both localized and statewide population declines. Guidelines for the Implementation of the California Environmental Quality Act (CEQA) provide that a species be considered as endangered or “rare” regardless of appearance on a formal list for the purposes of the CEQA (Guidelines, Section 15380, subsections b and d). The CEQA requires a mandatory findings of significance if impacts to threatened or endangered species are likely to occur (Sections 21001(c), 21083. Guidelines 15380, 15064, 15065). Avoidance or mitigation must be presented to reduce impacts to less than significant levels.

CEQA AND SUBDIVISION MAP ACT

CEQA Guidelines Section 15065 directs that a mandatory finding of significance is required for projects that have the potential to substantially degrade or reduce the habitat of, or restrict the range of a threatened or endangered species. CEQA requires agencies to implement feasible mitigation measures or feasible alternatives identified in EIR’s for projects which will otherwise cause significant adverse impacts (Sections 21002, 21081, 21083; Guidelines, sections 15002, subd. (a)(3), 15021, subd. (a)(2), 15091, subd. (a).).

To be legally adequate, mitigation measures must be capable of “avoiding the impact altogether by not taking a certain action or parts of an action”; “minimizing impacts by limiting the degree or magnitude of the action and its implementation”; “rectifying the impact by repairing, rehabilitating or restoring the impacted environment”; “or reducing or eliminating the impact over time by preservation and maintenance operations during the life of the action.” (Guidelines, Section 15.370).

Section 66474 (e) of the Subdivision Map Act states “a legislative body of a city or county shall deny approval of a tentative map or parcel map for which a tentative map was not required, if

it makes any of the following findings:... (e) that the design of the subdivision or the proposed improvements are likely to cause substantial environmental damage or substantially and avoidably injure fish and wildlife or their habitat". In recent court cases, the court upheld that Section 66474(e) provides for environmental impact review separate from and independent of the requirements of CEQA (Topanga Assn. for a Scenic Community v. County of Los Angeles, 263 Cal. Rptr. 214 (1989).). The finding in Section 66174 is in addition to the requirements for the preparation of an EIR or Negative Declaration.

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Appendix E

CDFG Staff Report on Burrowing Owl Mitigation

M e m o r a n d u m

: "Div. Chiefs - IFD, BDD, NED, & WMD
Reg. Mgrs. - Regions 1, 2, 3, 4, & 5

Date : October 17, 1995

From : Department of Fish and Game

Subject :
Staff Report on Burrowing Owl Mitigation

I am hereby transmitting the Staff Report on Burrowing Owl Mitigation for your use in reviewing projects (California Environmental Quality Act [CEQA] and others) which may affect burrowing owl habitat. The Staff Report has been developed during the last several months by the Environmental Services Division (ESD) in cooperation with the Wildlife Management Division (WMD) and regions 1, 2, and 4. It has been sent out for public review and redrafted as appropriate.

Either the mitigation measures in the staff report may be used or project specific measures may be developed. Alternative project specific measures proposed by the Department divisions/regions or by project sponsors will also be considered. However, such mitigation measures must be submitted to ESD for review. The review process will focus on the consistency of the proposed measure with Department, Fish and Game Commission, and legislative policy and with laws regarding raptor species. ESD will coordinate project specific mitigation measure review with WMD.

If you have any questions regarding the report, please contact Mr. Ron Rempel, Supervising Biologist, Environmental Services Division, telephone (916) 654-9980.

COPY Original signed by
C.F. Raysbrook

C. F. Raysbrook
Interim Director

Attachment

cc: Mr. Ron Rempel
Department of Fish and Game
Sacramento

STAFF REPORT ON BURROWING OWL MITIGATION

Introduction

The Legislature and the Fish and Game Commission have developed the policies, standards and regulatory mandates to protect native species of fish and wildlife. In order to determine how the Department of Fish and Game (Department) could judge the adequacy of mitigation measures designed to offset impacts to burrowing owls (*Speotyto cunicularia*; A.O.U. 1991) staff (WMD, ESD, and Regions) has prepared this report. To ensure compliance with legislative and commission policy, mitigation requirements which are consistent with this report should be incorporated into: (1) Department comments to Lead Agencies and project sponsors pursuant to the California Environmental Quality Act (CEQA); and (2) other authorizations the Department gives to project proponents for projects impacting burrowing owls.

This report is designed to provide the Department (including regional offices and divisions), CEQA Lead Agencies and project proponents the context in which the Environmental Services Division (ESD) will review proposed project specific mitigation measures. This report also includes preapproved mitigation measures which have been judged to be consistent with policies, standards and legal mandates of the Legislature, the Fish and Game Commission and the Department's public trust responsibilities. Implementation of mitigation measures consistent with this report are intended to help achieve the conservation of burrowing owls and should compliment multi-species habitat conservation planning efforts currently underway. The *Burrowing Owl Survey Protocol and Mitigation Guidelines* developed by The California Burrowing Owl Consortium (CBOC 1993) were taken into consideration in the preparation of this staff report as were comments from other interested parties.

A range-wide conservation strategy for this species is needed. Any range-wide conservation strategy should establish criteria for avoiding the need to list the species pursuant to either the California or federal Endangered Species Acts through preservation of existing habitat, population expansion into former habitat, recruitment of young into the population, and other specific efforts.

California's burrowing owl population is clearly declining and, if declines continue, the species may qualify for listing. Because of the intense pressure for urban development within suitable burrowing owl nesting and foraging habitat (open, flat and gently rolling grasslands and grass/shrub lands) in California, conflicts between owls and development projects often occur. Owl survival can be adversely affected by disturbance and foraging habitat loss even when impacts to individual birds and nests/burrows are avoided. Adequate information about the presence of owls is often unavailable prior to project approval. Following project approval there is no legal mechanism through which to seek mitigation other than avoidance of occupied burrows or nests. The absence of standardized survey methods often impedes consistent impact assessment.

Burrowing Owl Habitat Description

Burrowing owl habitat can be found in annual and perennial grasslands, deserts, and arid scrublands characterized by low-growing vegetation (Zarn 1974). Suitable owl habitat may also include trees and shrubs if the canopy covers less than 30 percent of the ground surface. Burrows are the essential component of burrowing owl habitat. Both natural and artificial burrows provide protection, shelter, and nests for burrowing owls (Henny and Blus 1981). Burrowing owls typically use burrows made by fossorial mammals, such as ground squirrels or badgers, but also may use man-made structures such as cement culverts; cement, asphalt, or wood debris piles; or openings beneath cement or asphalt pavement.

Occupied Burrowing Owl Habitat

Burrowing owls may use a site for breeding, wintering, foraging, and/or migration stopovers. Occupancy of suitable burrowing owl habitat can be verified at a site by detecting a burrowing owl, its molted feathers, cast pellets, prey remains, eggshell fragments, or excrement at or near a burrow entrance. Burrowing owls exhibit high site fidelity, reusing burrows year after year (Rich 1984, Feeney 1992). A site should be assumed occupied if at least one burrowing owl has been observed occupying a burrow there within the last three years (Rich 1984).

CEQA Project Review

The measures included in this report are intended to provide a decision-making process that should be implemented whenever there is potential for an action or project to adversely affect burrowing owls. For projects subject to the California Environmental Quality Act (CEQA), the process begins by conducting surveys to determine if burrowing owls are foraging or nesting on or adjacent to the project site. If surveys confirm that the site is occupied habitat, mitigation measures to minimize impacts to burrowing owls, their burrows and foraging habitat should be incorporated into the CEQA document as enforceable conditions. The measures in this document are intended to conserve the species by protecting and maintaining viable populations of the species throughout their range in California. This may often result in protecting and managing habitat for the species at sites away from rapidly urbanizing/developing areas. Projects and situations vary and mitigation measures should be adapted to fit specific circumstances.

Projects not subject to CEQA review may have to be handled separately since the legal authority the Department has with respect to burrowing owls in this type of situation is often limited. The burrowing owl is protected from "take" (Section 3503.5 of the Fish and Game Code) but unoccupied habitat is likely to be lost for activities not subject to CEQA.

Legal Status

The burrowing owl is a migratory species protected by international treaty under the Migratory Bird Treaty Act (MBTA) of 1918 (16 U.S.C. 703-711). The MBTA makes it unlawful to take, possess, buy, sell, purchase, or barter any migratory bird listed in 50 C.F.R. Part 10, including feathers or other parts, nests, eggs, or products, except as allowed by implementing regulations (50 C.F.R. 21). Sections 3505, 3503.5, and 3800 of the California Department of Fish and Game Code prohibit the take, possession, or destruction of birds, their nests or eggs. To avoid violation of the take provisions of these laws generally requires that project-related disturbance at active nesting territories be reduced or eliminated during the nesting cycle (February 1 to August 31). Disturbance that causes nest abandonment and/or loss of reproductive effort (e.g., killing or abandonment of eggs or young) may be considered “take” and is potentially punishable by fines and/or imprisonment.

The burrowing owl is a Species of Special Concern to California because of declines of suitable habitat and both localized and statewide population declines. Guidelines for the Implementation of the California Environmental Quality Act (CEQA) provide that a species be considered as endangered or “rare” regardless of appearance on a formal list for the purposes of the CEQA (Guidelines, Section 15380, subsections b and d). The CEQA requires a mandatory findings of significance if impacts to threatened or endangered species are likely to occur (Sections 21001 (c), 2103; Guidelines 15380, 15064, 15065). To be legally adequate, mitigation measures must be capable of “avoiding the impact altogether by not taking a certain action or parts of an action”; “minimizing impacts by limiting the degree or magnitude of the action and its implementation”; “rectifying the impact by repairing, rehabilitating or restoring the impacted environment”; “or reducing or eliminating the impact over time by preservation and maintenance operations during the life of the action” (Guidelines, Section 15370). Avoidance or mitigation to reduce impacts to less than significant levels must be included in a project or the CEQA lead agency must make and justify findings of overriding considerations.

Impact Assessment

Habitat Assessment

The project site and a 150 meter (approximately 500 ft.) buffer (where possible and appropriate based on habitat) should be surveyed to assess the presence of burrowing owls and their habitat (Thomsen 1971, Martin 1973). If occupied habitat is detected on or adjacent to the site, measures to avoid, minimize, or mitigate the project’s impacts to the species should be incorporated into the project, including burrow preconstruction surveys to ensure avoidance of direct take. It is also recommended that preconstruction surveys be conducted if the species was not detected but is likely to occur on the project site.

Burrowing Owl and Burrow Surveys

Burrowing owl and burrow surveys should be conducted during both the wintering and nesting seasons, unless the species is detected on the first survey. If possible, the winter survey should be conducted between December 1 and January 31 (when wintering owls are most likely to be present) and the nesting season survey should be conducted between April 15 and July 15 (the peak of the breeding season). Surveys conducted from two hours before sunset to one hour after, or from one hour before to two hours after sunrise, are also preferable.

Surveys should be conducted by walking suitable habitat on the entire project site and (where possible) in areas within 150 meters (approx. 500 ft.) of the project impact zone. The 150-meter buffer zone is surveyed to identify burrows and owls outside of the project area which may be impacted by factors -such as noise and vibration (heavy equipment, etc.) during project construction. Pedestrian survey transects should be spaced to allow 100 percent visual coverage of the ground surface. The distance between transect center lines should be no more than 30 meters (approx. 100 ft.) and should be reduced to account for differences in terrain, vegetation density, and ground surface visibility. To effectively survey large projects (100 acres or larger), two or more surveyors should be used to walk adjacent transects. To avoid impacts to owls from surveyors, owls and/or occupied burrows should be avoided by a minimum of 50 meters (approx. 160 ft.) wherever practical. Disturbance to occupied burrows should be avoided during all seasons.

Definition of Impacts

The following should be considered impacts to the species:

- Disturbance within 50 meters (approx. 160 ft.) Which may result in harassment of owls at occupied burrows;
- Destruction of natural and artificial burrows (culverts, concrete slabs and debris piles that provide shelter to burrowing owls); and
- Destruction and/or degradation of foraging habitat adjacent (within 100 m) of an occupied burrow(s).

Written Report

A report for the project should be prepared for the Department and copies should be submitted to the Regional contact and to the Wildlife Management Division Bird and Mammal Conservation Program. The report should include the following information:

- Date and time of visit(s) including name of the qualified biologist conducting surveys, weather and visibility conditions, and survey methodology;
- Description of the site including location, size, topography, vegetation communities, and animals observed during visit(s);
- Assessment of habitat suitability for burrowing owls;
- Map and photographs of the site;
- Results of transect surveys including a map showing the location of all burrow(s) (natural or artificial) and owl(s), including the numbers at each burrow if present and tracks, feathers, pellets, or other items (prey remains, animal scat);
- Behavior of owls during the surveys;
- Summary of both winter and nesting season surveys including any productivity information and a map showing territorial boundaries and home ranges; and
- Any historical information (Natural Diversity Database, Department regional files? Breeding Bird Survey data, American Birds records, Audubon Society, local bird club, other biologists, etc.) regarding the presence of burrowing owls on the site.

Mitigation

The objective of these measures is to avoid and minimize impacts to burrowing owls at a project site and preserve habitat that will support viable owls populations. If burrowing owls are detected using the project area, mitigation measures to minimize and offset the potential impacts should be included as enforceable measures during the CEQA process.

Mitigation actions should be carried out from September 1 to January 31 which is prior to the nesting season (Thomsen 1971, Zam 1974). Since the timing of nesting activity may vary with latitude and climatic conditions, this time frame should be adjusted accordingly. Preconstruction surveys of suitable habitat at the project site(s) and buffer zone(s) should be conducted within the 30 days prior to construction to ensure no additional, burrowing owls have established territories since the initial surveys. If ground disturbing activities are delayed or suspended for more than 30 days after the preconstruction survey, the site should be resurveyed.

Although the mitigation measures may be included as enforceable project conditions in the CEQA process, it may also be desirable to formalize them in a Memorandum of Understanding (MOU) between the Department and the project sponsor. An MOU is needed when lands (fee title or conservation easement) are being transferred to the Department.

Specific Mitigation Measures

1. Occupied burrows should not be disturbed during the nesting season (February 1 through August 31) unless a qualified biologist approved by the Department verifies through non-invasive methods that either: (1) the birds have not begun egg-laying and incubation; or (2) that juveniles from the occupied burrows are foraging independently and are capable of independent survival.
2. To offset the loss of foraging and burrow habitat on the project site, a minimum of 6.5 acres of foraging habitat (calculated on a 100 m {approx. 300 ft.} foraging radius around the burrow) per pair or unpaired resident bird, should be acquired and permanently protected. The protected lands should be adjacent to occupied burrowing owl habitat and at a location acceptable to the Department. *Protection of additional habitat acreage per pair or unpaired resident bird may be applicable in some instances.* The CBOC has also developed mitigation guidelines (CBOC 1993) that can be incorporated by CEQA lead agencies and which are consistent with this staff report.
3. When destruction of occupied burrows is unavoidable, existing unsuitable burrows should be enhanced (enlarged or cleared of debris) or new burrows created (by installing artificial burrows) at a ratio of 2:1 on the protected lands site. One example of an artificial burrow design is provided in Attachment A.
4. If owls must be moved away from the disturbance area, passive relocation techniques (as described below) should be used rather than trapping. At least one or more weeks will be necessary to accomplish this and allow the owls to acclimate to alternate burrows.
5. The project sponsor should provide funding for long-term management and monitoring of the protected lands. The monitoring plan should include success criteria, remedial measures, and an annual report to the Department.

Impact Avoidance

If avoidance is the preferred method of dealing with potential project impacts, then no disturbance should occur within 50 meters (approx. 160 ft.) of occupied burrows during the nonbreeding season of September 1 through January 31 or within 75 meters (approx. 250 ft.) during the breeding season of February 1 through August 31. Avoidance also requires that a minimum of 6.5 acres of foraging habitat be *permanently* preserved contiguous with occupied burrow sites for each pair of breeding burrowing owls (with or without dependent young) or single unpaired resident bird. The configuration of the protected habitat should be approved by the Department.

Passive Relocation - With One-Way Doors

Owls should be excluded from burrows in the immediate impact zone and within a 50 meter (approx. 160 ft.) buffer zone by installing one-way doors in burrow entrances. One-way doors (e.g., modified dryer vents) should be left in place 48 hours to insure owls have left the burrow before excavation. Two natural or artificial burrows should be provided for each burrow in the project area that will be rendered biologically unsuitable. The project area should be *monitored daily for one* week to confirm owl use of burrows before excavating burrows in the immediate impact zone. Whenever possible, burrows should be excavated using hand tools and refilled to prevent reoccupation. Sections of flexible plastic pipe should be inserted into the tunnels during excavation to maintain an escape route for any animals inside the burrow.

Passive Relocation - Without One-Way Doors

Two natural or artificial burrows should be provided for each burrow in the project area that will be rendered biologically unsuitable. The project area should be *monitored daily until the owls have relocated to the new burrows*. The formerly occupied burrows may then be excavated. Whenever possible, burrows should be excavated using hand tools and refilled to prevent reoccupation. Sections of flexible plastic pipe should be inserted into burrows during excavation to maintain an escape route for any animals inside the burrow.

Projects Not Subject to CEQA

The Department is often contacted regarding the presence of burrowing owls on construction sites, parking lots and other areas for which there is no CEQA action or for which the CEQA process has been completed. In these situations, the Department should seek to reach agreement with the project sponsor to implement the specific mitigation measures described above. If they are unwilling to do so, passive relocation without the aid of one-way doors is their only option based upon Fish and Game Code 3503.5.

Literature Cited

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- Thomsen, L. 1971. Behavior and ecology of burrowing owls on the Oakland Municipal Airport. *Condor* 73:177-192.
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Reproductive Success of Burrowing Owls Using Artificial Nest Burrows in Southeastern Idaho

by Bruce Olenick

Artificial nest burrows were implanted in southeastern Idaho for burrowing owls in the spring of 1986. These artificial burrows consisted of a 12" x 12" x 8" wood nesting chamber with removable top and a 6 foot corrugated and perforated plastic drainage pipe 6 inches in diameter (Fig. 1). Earlier investigators claimed that artificial burrows must provide a natural dirt floor to allow burrowing owls to modify the nesting tunnel and chamber. Contrary to this, the artificial burrow introduced here does not allow owls to modify the entrance or tunnel. The inability to change the physical dimensions of the burrow tunnel does not seem to reflect the owls' breeding success or deter them from using this burrow design.

In 1936, 22 artificial burrows were inhabited. Thirteen nesting attempts yielded an average clutch size of 8.3 eggs per breeding pair. Eight nests successfully hatched at least 1 nestling. In these nests, 67 of 75 eggs hatched (59.3%) and an estimated 61 nestlings (91.0%) fledged. An analysis of the egg laying and incubation periods showed that incubation commenced well after egg lay-

ing began. Average clutch size at the start of incubation was 5.6 eggs. Most eggs tended to hatch synchronously in all successful nests.

Although the initial cost of constructing this burrow design may be slightly higher than a burrow consisting entirely of wood, the plastic pipe burrow offers the following advantages: (1) it lasts several field seasons without rotting or collapsing; (2) it may prevent or retard predation; (3) construction time is min-

imal; (4) it is easy to transport, especially over long distances; and (5) the flexible tunnel simplifies installation. The use of this artificial nest burrow design was highly successful and may prove to be a great resource technique for future management of this species.

For additional information on constructing this artificial nest burrow, contact Bruce Olenick, Department of Biology, Idaho State University, Pocatello, ID 83209.

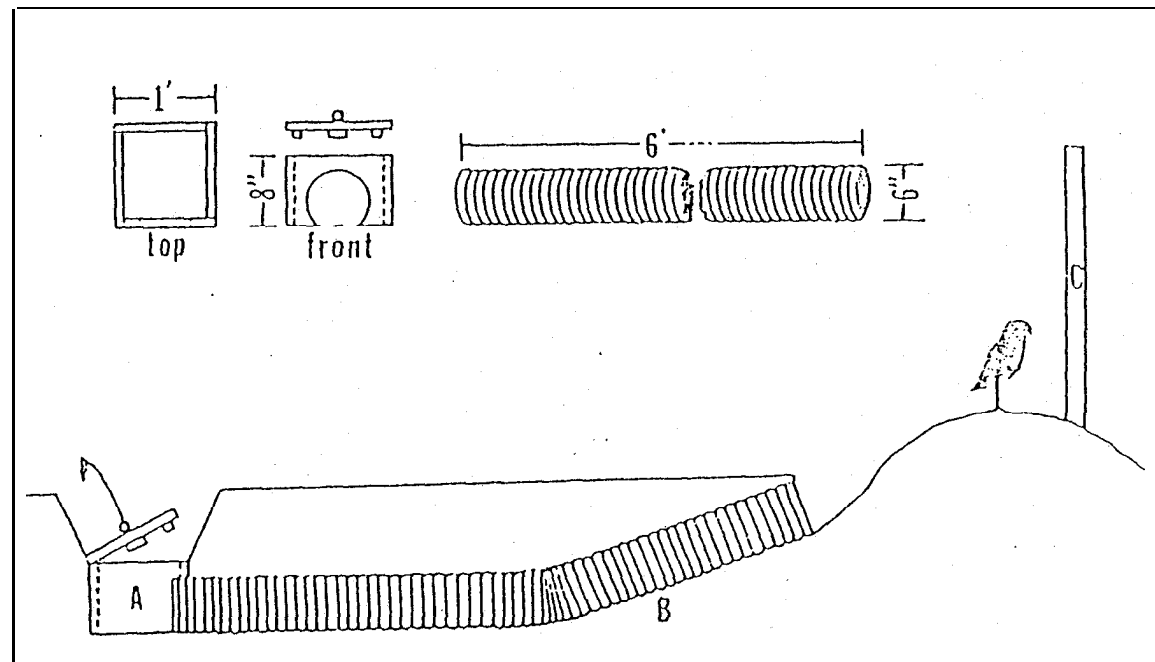


fig. 1 Artificial nest burrow design for burrowing owls Entire unit (including nest chamber) is buried 12" -- 18" below ground for maintaining thermal stability of the nest chamber. A= nest chamber, B = plastic pipe. C = perch.

Appendix F

Albion Report on Burrowing Owl Site Eviction



October 4, 2005

Jack Hall
Community Development Manager
Shea Homes
2580 Shea Center Drive
Livermore, CA. 94551

Summary report on burrowing owl eviction from the Davidon/Shea project site in Antioch, CA.

Dear Mr. Hall:

This is a summary report on the results of the burrowing owl (*Athene cunicularia*) passive relocation activities that Albion biologists Jack Barclay and Lindsay Harman carried out on the Davidon/Shea project site in Antioch on September 23, 26 and 28, 2005. The project site is located on the east side of Canada Valley Road approximately 0.4 miles north of Lone Tree Way in Antioch. The purpose of our work was to passively relocate burrowing owls from the Davidon/Shea project area to ensure no owls were present or harmed during initial grading. Prior to beginning the passive relocation we requested the limits of the work area be marked in the field so we could accurately determine the areas that needed to be treated with one-way door exclusion devices.

We observed four burrowing owls on the project area when we began passive relocation activities on September 23, 2005. We had previously documented 9 burrowing owls on the site and had captured and banded 7 of them between September 1-7. The owls had been using numerous burrows and roosts on the site but often they were on the rocky berm running through the center of the project area along the west side of the creek. This berm has many rock piles that provided shade and cover for the burrowing owls. The four burrowing owls flew to various burrow locations in the surrounding habitat as we surveyed the site and all four owls flew off the project area as we began installing one-way doors.

We walked the entire project area and installed one-way doors in all burrows and cavities potentially suitable for burrowing owl occupancy. We installed 41 one-way doors in 4 locations on the project area; on the hill in the northwest corner of the property, along the rocky berm parallel to the west side of creek, in a soil pile on the east side of the creek and on the slope at the northeast portion of the project site. We left all burrows outside the limits of grading open to help facilitate owls moving off of the project site. Leaving open burrows adjacent to the project area provided cover for the owls while they are transitioning to new burrow locations. Because of the close proximity of burrows we recommended that the work area be clearly marked or fenced to ensure ground disturbing activity stayed inside the marked limits of grading.

I returned to the site on September 26 to determine if owls had left the site. Grading was scheduled to begin if all one-way doors were still intact and owls were not observed using burrows on the project area. After inspecting the site I observed three owls still using the rocky berm in the center of the project area. As I approached they flew off the project area and I inspected the area for available burrows. Owls were still roosting on the berm but only appeared to be using the rocks for shade or cover because I did not observe any new burrows or cavities and all the one-way doors were still intact. After the site was clear of owls and all cavities were inspected I began removing one-way

doors in preparation for grading, which was to begin immediately. As I finished removing the one-way doors on the berm, one owl from off the site flew into the berm and disappeared down one of the burrows. Such activity is unusual and if I thought an owl might return to the berm immediately before it was to be graded I would not have removed the doors. After the owl disappeared, I immediately explained to the contractor that he should not grade that portion of the site. I reinstalled 9 one-way doors in the area where the owl disappeared and put flagging around this area to prevent any ground disturbance. I also explained to the contractor that these new one-way doors should be left in place for 48 hours and the area should be surveyed again on September 28. I monitored grading on the remaining portion of the site.

Jack and I returned on September 28, 2005 to inspect the work area and the one-way doors in the exclusion area (berm). We surveyed the berm, inspected each one-way door, looked for newly opened burrows, and checked for any newly created cavities. We did not observe any burrowing owls in the exclusion zone. After thoroughly inspecting the site we concluded that all suitable burrows and cavities were still closed and grading could begin in this area. We monitored grading of this remaining portion of the project area.

In summary, the eviction of burrowing owls from project area was successful, although it was delayed for 48 hours because one owl was very persistent at wanting to continue to use the rocky berm. After careful inspection of one-way doors, reinstalling one-way doors on the rocky berm and carefully monitoring the site prior to and during grading we concluded that burrowing owls had vacated the areas to be graded and no owls were harmed during the initial grading. Please contact me if you have any questions about this report.

Sincerely,

A handwritten signature in cursive script that reads "Lindsay Harman".

Lindsay Harman
Wildlife Biologist

Appendix G

City Council RDA Allocation
Resolution No. 2004/118

**STAFF REPORT TO THE RDA COMMITTEE FOR CONSIDERATION AT THE
MEETING OF JUNE 28, 2004**

Prepared by: Tina Wehrmeister, Senior Planner
Approved by: Joseph G. Brandt, Director of Community Development
Date: June 24, 2004
Subject: Davidon / Jacuzzi Property

PROJECT INFORMATION

Applicant: Davidon Homes

Owner: Tristar Land Investment Corporation

Location: 170 acres generally located west of the future State Route 4 Bypass and north of the McBail residential project being developed north of Lone Tree Way (a portion of the former Jacuzzi family properties – see Attachment A for vicinity map). (APN: 053-060-021, and portion of 053-072-013)

General Plan / Zoning: The site is part of the East Lone Tree Specific Plan (FUA 2) and is designated for low and medium low density residential with open space areas as shown in the Specific Plan (see Attachment B). The Specific Plan allows a maximum of four dwelling units per acre (6,000 square foot minimum lot area) for low-density areas and six dwelling units per acre (4,000 square foot minimum lot area) for medium low density areas.

The General Plan states that the project area should be developed consistent with the Low and/or Medium Density Residential land use category which allows four and six dwelling units to the acre respectively.

Requested Allocations: The applicant has amended the number of requested allocations from 579 to 562 and will discuss the yearly break down of allocations at the RDAC meeting. The site plan has not been amended. The lot reduction will be reflected in future entitlement applications.

PROJECT DESCRIPTION / BACKGROUND

The project consists of a mix of low and medium density residential lots with minimum lot sizes of 6,000 s.f. (8,217 s.f. average size) and 5,000 s.f. (6,566 s.f. average size) respectively. It should be noted that the 5,000 s.f. minimum lots exceed the minimum allowed by the Specific Plan which is 4,000 s.f. in Medium Low Density Areas. The applicant is proposing 27 acres of open space including trails with connections to the subdivision. In addition, an 8 acre neighborhood park is shown with five of the eight acres developed similar to other neighborhood parks. The Specific Plan envisioned a fully developed 8-acre neighborhood park at this location, but this type of detail will be resolved at the Tentative Map/Planned Development entitlement level.

The applicant was denied a request for 549 units in the first round of the RDA process last year. The 2003 plan included a third high school site. At that time, the Council felt that the applicant did not provide an acceptable level of community benefit noting that the project was not offering to front infrastructure costs for the employment / commercial portion of Future Urban Area 2 despite requirements contained in the specific plan; that the proposal did not provide a sufficient variety in product or street design; and that the applicant was not providing any other significant community benefit other than the high school site which was to be located on acreage previously slated for open space.

SURROUNDING LAND USES

The project is bounded by existing single family residential development on the west, the McBail single family residential development in construction to the south, the future State Route 4 Bypass on the east, and Laurel Rd and the proposed Bixby residential development to the north.

SITE PLANNING & DEVELOPMENT ISSUES

Open Space: The applicant shows the ridgeline open space area as was offered to the City as a gift from the Jacuzzi family. A copy of the agreement is attached (see Attachment C). The land was never officially accepted by the City. A condition of future entitlements for the project would require that the applicant take the necessary steps to annex the property into Lighting and Landscape District 10 to assure proper fire protection, access, public liability protection, and maintenance. The applicant would be required to install trails as shown on the plans and could, as a community benefit, provide such items as bench seating, look out areas, and waste receptacles.

Neighborhood Park: The East Lone Tree Specific Plan requires an eight acre active community park. Future entitlement plans would need to reflect this requirement. The plans currently show a five acre active park. The neighborhood park improvements would be eligible for reimbursement. As an additional community benefit, the applicant could offer to not request reimbursement, allowing the City to utilize the funds to improve other neighborhood parks.

Specific Plan Financing Requirements: The East Lone Tree Specific Plan and its corresponding Financial Plan intended that funding for major infrastructure links in the employment areas east of the State Route 4 Bypass be fronted by residential development on the west side of the Bypass with possible reimbursement, at Council's discretion, for some or all of those funds (see Attachment D for a summary of infrastructure requirements contained in the Specific and Financial plans).

The applicant is offering a non-reimbursable Community Facilities District (CFD) lien of up to \$15,000 per residential lot for construction of the infrastructure identified by the Financial Plan (see Attachment E). This offer, along with the participation of the other property owners north of McBail in the CFD, will be adequate to construct the remaining infrastructure improvements north of the McBail properties. If the CFD is not formed, it is estimated that the offer will be adequate to construct full four lane Slatten Ranch Rd. from the McBail north boundary to Laurel Rd with sewer and water OR two lane Slatten Ranch Rd. and the East Antioch Creek improvements needed to move the employment / regional retail areas out of the flood zone.

This offer will provide the necessary funding to construct Slatten Ranch Rd. from the northern McBail property line to Laurel Road and the State Route 4 Bypass interchange. Staff believes this link is critical in order to attract regional retail and employment users to the area. Currently, the development interest in the area has been from large regional retail entities which would provide significant revenues to the City. Without the completion of Slatten Ranch Rd., it is likely that those retail entities will locate in the area however, most likely in Oakley or Brentwood (see last paragraph of Attachment F, EPS market study).

It should be noted that the applicant's offer is non-reimbursable. This is over and above the specific plan requirement which discusses possible reimbursement to residential developers.

The above offer is contingent upon the execution of a Development Agreement providing that Davidon has no further obligation to construct additional off-site infrastructure that is not project related and that bonds will be sold and CFD assessment will be payable only as necessary to complete the improvements concurrent with the completion of the State Route 4 Bypass.

Should a CFD not be established, and an alternative funding mechanism acceptable to both Davidon and the City not be devised, or should the Development Agreement not be entered into, any allocation of residential units under the RDA process would be void.

State Route 4 Bypass Noise Issues: It has recently been determined that noise from the future Bypass may exceed the City's noise standards for residential development. The Community Development Department will address this issue in the near future before the Planning Commission and City Council. Most likely, it will be requested that

the noise standards in the General Plan be amended to be consistent with the State standards along freeways. This issue may impact site planning during the entitlement process for this project.

SUMMARY OF PROJECT BENEFITS

Below is a brief description of the community benefits provided by the project and their timing; organized by each evaluation category approved by the City Council. The maximum possible points for each category are shown in the table, but no points have been assigned. The applicant's description of the project and community benefits is attached to the plan set (note that Attachment E modifies the community benefit offer). Only items that can be considered above and beyond typical development requirements are included in the table below.

| CATEGORY | POINTS POSSIBLE | COMMITTEE NOTES |
|--|----------------------------|----------------------------|
| A. PHYSICAL IMPROVEMENTS | 200 POINTS | NOTES |
| A-1 Traffic and Transportation | 75 points | |
| <ul style="list-style-type: none">• Non-reimbursable Community Facilities District (CFD) lien of up to \$15,000 per residential lot for construction of the infrastructure identified by the East Lone Tree Specific Plan and Financial Plan. | | |
| A-2 Utilities and Infrastructure | 75 points | |
| <ul style="list-style-type: none">• See above | | |
| A-3 Open Space and Parks | 25 points | |
| <ul style="list-style-type: none">• The project is providing 27 acres of passive open space and 8 acres of park land, five acres to be developed. These facilities are required by an offer of dedication of land to the City by previous owners and the specific plan respectively. | | |
| A-4 Natural Features | 25 points | |
| <ul style="list-style-type: none">• The applicant references the 27 acres of passive open space for this category.• This acreage was previously offered to the City and is not considered a benefit over and above standard requirements by staff. | | |

| CATEGORY | POINTS POSSIBLE | COMMITTEE NOTES |
|---|-------------------|-----------------|
| B. DESIGN | 100 POINTS | |
| B-1 Site Design | 25 points | |
| <ul style="list-style-type: none"> The applicant is providing 5,000 and 6,000 s.f. lot types and states that many of the lots exceed the minimums. | | |
| B-2 Architecture and Design Quality | 25 points | |
| <ul style="list-style-type: none"> The applicant submitted working architectural plans, which were included in the plans distributed to the RDAC. The applicant notes that they are developing two distinct product lines and that design updates may occur during the life of the project. Staff feels that the architecture is typical of homes currently under construction in Antioch. | | |
| B-3 Energy and Efficiency | 25 points | |
| <ul style="list-style-type: none"> The applicant states that dual pane windows, tech shield roof sheathing, re-circulating hot water systems, and energy saver furnaces, air conditioners, and appliances will be installed as standard features on all homes. The applicant states that developer installed front yard landscaping will utilize water saving techniques and plant materials. | | |
| B-4 Public Safety | 25 points | |
| <ul style="list-style-type: none"> The applicant states that Class A fire resistant roof materials will be utilized on all homes. Class C roof material is the minimum required by the Building Code for residences. The Class A materials offered by the applicant is less flammable. As a standard feature, homes will be wired for security systems with an option for digital surveillance. | | |
| C. ADDITIONAL COMMUNITY BENEFITS AND CONTRIBUTIONS | 200 POINTS | |
| C-1 School Mitigation | 60 points | |
| <ul style="list-style-type: none"> The project will participate in the new AUSD CFD 2004-1. | | |

| CATEGORY | POINTS POSSIBLE | COMMITTEE NOTES |
|---|--------------------|--------------------|
| C-2 Economic Development Benefits | 60 points | |
| <ul style="list-style-type: none">The non-reimbursable infrastructure funding offer will provide the necessary improvements to attract regional retail and employment projects to FUA2. Future regional retail projects in particular will provide significant sales tax revenue to the City. | | |
| C-3 Contributions to Special Projects | 80 points | |
| <ul style="list-style-type: none">None | | |
| TOTAL POINTS (500 points possible) | | |

RECOMMENDATION

According to the RDA Ordinance, one of the primary objectives of this process is to implement the City's goal that new residential developments make positive contributions to the community, and not just mitigate impacts. The community benefits offered by Davidon Homes are significant in boosting the City's ability to attract regional retail and employment development in FUA2.

Staff recommends that the RDAC recommend approval of allocations for this project.

ATTACHMENTS

- A. Vicinity Map
- B. East Lone Tree Specific Plan Land Use Map
- C. Jacuzzi Open Space Agreement
- D. FUA 2 Commercial/Employment Infrastructure Requirements
- E. Letter from applicant dated June 23, 2004 modifying offer
- F. Excerpt from EPS Antioch Retail Market Study

**RESIDENTIAL DEVELOPMENT ALLOCATION COMMITTEE
RECOMMENDATION FOR APPROVAL OF ALLOCATION OF RESIDENTIAL UNITS
FOR THE DAVIDON / JACUZZI PROPERTIES RESIDENTIAL DEVELOPMENT**

WHEREAS, the Residential Development Allocation Committee (RDAC) of the City of Antioch did receive an application from Davidon Homes for the approval of 562 residential development allocations for a 170 acre project generally located west of the future State Route 4 Bypass and north of the McBail residential project being developed north of Lone Tree Way (APN: 053-060-021, and portion of 053-072-013) (RDA-04-01); and

WHEREAS, the approval of residential development allocations does not constitute an entitlement to develop a project and the allocation process is not subject to the provisions of the California Environmental Quality Act; and

WHEREAS, the RDAC duly gave notice of public meeting as required by law; and

WHEREAS, on June 28, 2004 the RDAC duly held a public meeting, received and considered evidence, both oral and documentary; and

WHEREAS, it is hereby understood that any contributions, mitigations, and other benefits that were agreed to as part of this allocation process shall be incorporated into future entitlement submittal(s).

NOW THEREFORE BE IT RESOLVED that the RDAC does hereby recommend that Davidon Homes be granted 562 residential development allocations **insert yearly break down** subject to the following items and community benefits that the applicant has agreed to provide:

1. That the overall project description, facilities, layout, and phasing shall be substantially in conformance with the plans reviewed by the RDAC.
2. That the applicant shall provide dual pane windows, tech shield roof sheathing, re-circulating hot water systems, Class A fire resistant roofs, prewired security alarm systems, and energy saver furnaces, air conditioner, and appliances as standard features on all homes.
3. That front yard landscaping shall utilize water saving techniques and plant materials.
4. That the applicant shall contribute a non-reimbursable Community Facilities District (CFD) lien of up to \$15,000 per residential lot for construction of infrastructure identified by the East Lone Tree Financial Plan. This offer is contingent on the successful formation of a CFD that will provide for the construction of all such infrastructure with fair and reasonable liens on the other

properties in FUA 2. Fair and reasonable liens shall be determined by a study by EPS which is presently being conducted.

The City and Davidon Homes shall enter into a Development Agreement (DA) which shall provide the framework for entitlement of 562 single family units. Davidon understands that RDA approval is not an entitlement and the plat provided for the RDA process showing 579 units shall be revised as part of the tentative map process. The DA shall further provide that Davidon has an obligation to construct additional off-site infrastructure that is not directly project related. The DA shall also confirm that bonds will be sold and CFD assessments will be payable only as necessary to complete the improvements approximately concurrent with the completion of the State Route 4 Bypass.

5. That Davidon Homes shall participate in the new AUSD CFD 2004-1.

* * * * *

I HEREBY CERTIFY that the foregoing resolution was passed and adopted by the Residential Development Allocation Committee of the City of Antioch, County of Contra Costa, State of California at a regular meeting of said Residential Development Allocation Committee held on the 28th day of June, 2004 by the following vote:

Victor Carniglia
Secretary to the RDAC

**RESIDENTIAL DEVELOPMENT ALLOCATION COMMITTEE
RECOMMENDATION FOR APPROVAL OF ALLOCATION OF RESIDENTIAL UNITS
FOR THE DAVIDON / JACUZZI PROPERTIES RESIDENTIAL DEVELOPMENT**

WHEREAS, the Residential Development Allocation Committee (RDAC) of the City of Antioch did receive an application from Davidon Homes for the approval of 562 residential development allocations for a 170 acre project generally located west of the future State Route 4 Bypass and north of the McBail residential project being developed north of Lone Tree Way (APN: 053-060-021, and portion of 053-072-013) (RDA-04-01); and

WHEREAS, the approval of residential development allocations does not constitute an entitlement to develop a project and the allocation process is not subject to the provisions of the California Environmental Quality Act; and

WHEREAS, the RDAC duly gave notice of public meeting as required by law; and

WHEREAS, on June 28, 2004 the RDAC duly held a public meeting, received and considered evidence, both oral and documentary; and

WHEREAS, it is hereby understood that any contributions, mitigations, and other benefits that were agreed to as part of this allocation process shall be incorporated into future entitlement submittal(s).

NOW THEREFORE BE IT RESOLVED that the RDAC does hereby recommend that Davidon Homes be granted 562 residential development allocations over four years (2005 – 125; 2006 – 150; 2007 – 150; 2008 – 137) subject to the following items and community benefits that the applicant has agreed to provide:

1. That the overall project description, facilities, layout, and phasing shall be substantially in conformance with the plans reviewed by the RDAC.
2. That the applicant shall provide dual pane windows, tech shield roof sheathing, re-circulating hot water systems, Class A fire resistant roofs, prewired security alarm systems, and energy saver furnaces, air conditioner, and appliances as standard features on all homes.
3. That front yard landscaping shall utilize water saving techniques and plant materials.
4. That the applicant shall contribute a non-reimbursable Community Facilities District (CFD) lien of up to \$15,000 per residential lot for construction of infrastructure identified by the East Lone Tree Financial Plan. This offer is contingent on the successful formation of a CFD that will provide for the construction of all such infrastructure with fair and reasonable liens on the other

properties in FUA 2. Fair and reasonable liens shall be determined by a study by EPS which is presently being conducted.

The City and Davidon Homes shall enter into a Development Agreement (DA) which shall provide the framework for entitlement of 562 single family units. Davidon understands that RDA approval is not an entitlement and the plat provided for the RDA process showing 579 units shall be revised as part of the tentative map process. The DA shall further provide that Davidon has no obligation to construct additional off-site infrastructure that is not directly project related. The DA shall also confirm that bonds will be sold and CFD assessments will be payable only as necessary to complete the improvements approximately concurrent with the completion of the State Route 4 Bypass.

5. That Davidon Homes shall participate in the new AUSD CFD 2004-1.

* * * * *

I HEREBY CERTIFY that the foregoing resolution was passed and adopted by the Residential Development Allocation Committee of the City of Antioch, County of Contra Costa, State of California at a regular meeting of said Residential Development Allocation Committee held on the 28th day of June, 2004 by the following vote:

AYES: Azevedo, Henry

NOES: Mayor Freitas, Conley

Victor Carniglia
Secretary to the RDAC

**STAFF REPORT TO THE CITY COUNCIL
FOR CONSIDERATION AT THE MEETING OF SEPTEMBER 14, 2004**

Prepared by: Tina Wehrmeister, Senior Planner
Reviewed by: Victor Carniglia, Deputy Director of Community Development
Approved by: Joseph G. Brandt, Director of Community Development
Date: September 3, 2004
Subject: RDA-04-1 Davidon / Jacuzzi Property

RECOMMENDATION

It is recommended that the City Council approve an allocation of 562 single family residential units over four years (2005 – 125; 2006 – 150; 2007 – 150; 2008 – 137), subject to conditions in the attached resolution.

BACKGROUND / DISCUSSION

Davidon Homes requests an allocation of 562 single family residential units over four years (2005 – 125; 2006 – 150; 2007 – 150; 2008 – 137) under the Residential Development Allocation Program. The site is approximately 170 acres and is generally located west of the future State Route 4 Bypass and north of the McBail residential project being developed north of Lone Tree Way (APN: 053-060-021, and portion of 053-072-013).

The RDAC reviewed this application on June 28, 2004. RDA applications are required to achieve at least 50% of the total points possible to be eligible to receive an allocation. The project received an overall score of 59% (298 out of 500). The RDAC did not take an action on the project as the vote was split (Noes – Freitas, Conley; Ayes – Azevedo, Henry).

There was some concern expressed at the RDAC meeting regarding the CFD lien offer which was worded as up to \$15,000 per unit. The applicant has attempted to address this concern with a revised community benefit offer (see Attachment “D”). The applicant is now offering a firm \$15,000 per unit. Additionally, any future reimbursement owed to Davidon for infrastructure improvements funded by the CFD is offered to the City for additional community benefit improvements. The applicant has also submitted new enhanced architectural renderings of the two products proposed for the development. The Design Review Board will review architecture as part of the entitlement process however; any architectural features that the Council considers a community enhancement should be made a part of the RDA resolution.

The Planning Commission recommended approval of allocations for this project on July 21, 2004. Minutes from this meeting are attached.

An RDA approval is a non-entitlement action. The purpose of the RDA process is to determine the number of units a developer may submit for entitlement. The RDA process should not be construed as an approval of subdivision design or density. Future entitlement applications may require significant redesign and layout departure from the RDA map. Future entitlement applications may be denied or may be approved for fewer units than the RDA approval.

FINANCIAL IMPACT

The applicant is offering a community benefit contribution of \$15,000 per residential unit for construction of infrastructure identified by the East Lone Tree Financial Plan (ELTSP). This offer could provide the majority of funding necessary to construct the full four lanes of Slatten Ranch Road from the northern McBail property line to Laurel Road and the State Route 4 Bypass interchange. Ultimately, these funds will be combined with other funds from residential, commercial and employment developments in the ELTSP area to construct all “backbone” infrastructure improvements in that area. Staff believes construction of the Slatten Ranch Road link is critical in order to attract regional retail and employment users to the area. Currently, the development interest in the area has been from large regional retail entities which would provide significant sales tax revenues to the City. A conservative estimate of the amount of sales tax the area north of Slatten Ranch may generate is \$1.8 to \$2 million/yr.

Additional funds may be generated for community benefit / enhancement use pending future studies regarding the reimbursement of CFD improvements.

OPTIONS

1. Continue the item for further discussion.
2. Deny the request for residential development allocations.

ATTACHMENTS

- A: June 28, 2004 RDAC Staff Report
- B: Planning Commission minutes
- C: RDAC Scoring
- D: Revised Offer

RESOLUTION NO. 2004/118

RESOLUTION OF THE CITY COUNCIL OF THE CITY OF ANTIOCH APPROVING AN ALLOCATION OF RESIDENTIAL UNITS FOR THE DAVIDON / JACUZZI SUBDIVISION

WHEREAS, the City Council of the City of Antioch did receive an application from Davidon Homes for the approval of development allocations for 562 single family residential units over four years (2005 – 125; 2006 – 150; 2007 – 150; 2008 – 137) for an approximately 170 acre site generally located west of the future State Route 4 Bypass and north of the McBail residential project being developed north of Lone Tree Way (APN: 053-060-021, and portion of 053-072-013) (RDA-04-1); and

WHEREAS, the City Council did receive a recommendation for approval of residential allocations for this project from the Planning Commission; and

WHEREAS, the approval of residential development allocations does not constitute an entitlement to develop a project. The City may deny a future entitlement application, or approve such an application for fewer units than the 562 allocations requested; and

WHEREAS, the allocation process is not subject to the provisions of the California Environmental Quality Act; and

WHEREAS, the City Council duly gave notice of public meeting as required by law; and

WHEREAS, on September 14, 2004 the City Council duly held a public meeting, received and considered evidence, both oral and documentary; and

WHEREAS, it is hereby understood that any contributions, mitigations, and other benefits that were agreed to as part of this allocation process shall be incorporated into future entitlement submittal(s).

NOW THEREFORE BE IT RESOLVED that the City Council does hereby APPROVE 562 single family residential units over four years (2005 – 125; 2006 – 150; 2007 – 150; 2008 – 137), subject to the following items and community benefits that the applicant has agreed to provide:

1. That the applicant shall provide dual pane windows, tech shield roof sheathing, re-circulating hot water systems, Class A fire resistant roofs, prewired security alarm systems, and energy saver furnaces, air conditioner, and appliances as standard features on all homes.
2. That front yard landscaping shall utilize water saving techniques and plant materials.
3. That the applicant shall contribute a non-reimbursable Community Facilities District (CFD) lien of \$15,000 per residential lot for construction of infrastructure identified by the East Lone Tree Financial Plan. This offer is contingent on the successful formation of a CFD that will provide for the construction of all such infrastructure with

fair and reasonable liens on the other properties in FUA 2. Fair and reasonable liens shall be determined by a study by EPS which is presently being conducted.

4. The City and Davidon Homes shall enter into a Development Agreement (DA) which shall provide the framework for entitlement of the project. Davidon understands that RDA approval is not an entitlement and the plat provided for the RDA process showing 579 units shall be revised as part of the tentative map process. The DA shall further provide that Davidon has no obligation to construct additional off-site infrastructure that is not directly project related. The DA shall also confirm that bonds will be sold and CFD assessments will be payable only as necessary to complete the improvements approximately concurrent with the completion of the State Route 4 Bypass.
5. Upon finalization of the CFD, the City may determine that Davidon's contribution has exceeded that required for completion of East Lone Tree Specific Plan infrastructure. In this case, the excess funds shall be available for application to other projects enhancing the economic development of Antioch. The use of any excess funds shall be at the direction of the City Council.
6. That Davidon Homes shall participate in the new AUSD CFD 2004-1.

* * * * *

I HEREBY CERTIFY that the foregoing resolution was passed and adopted by the City Council of the City of Antioch at a regular meeting thereof, held on the 14th day of September, 2004 by the following vote.

AYES: Council Members Davis, Conley and Simonsen

NOES: Mayor Freitas and Council Member Kalinowski

ABSENT: None

L. JOLENE MARTIN, City Clerk

Appendix H

USACE and CDFG Jurisdictional Determinations



REPLY TO
ATTENTION OF

DEPARTMENT OF THE ARMY
U.S. ARMY ENGINEER DISTRICT, SACRAMENTO
CORPS OF ENGINEERS
1325 J STREET
SACRAMENTO, CALIFORNIA 95814-2922

December 9, 2003

Regulatory Branch (200200674)

Richard Loewke
Richard Loewke AICP Planning Consultant
55 Oak Trail Court
Alamo, California 94507-2502

Dear Mr. Loewke:

This letter concerns the 10/8/02 wetland delineation for the proposed Rolling Hills Ranch project site submitted to this office for verification on your behalf. This site is located in Section 34, Township 2 North, Range 2 East, MDB&M, Contra Costa County, California.

Based on the available information the 0.17-acre wetland, identified as temporary swale in your October 8, 2002, Request for Verification of Non-Jurisdictional Status of Swale Located on Property in Antioch, is isolated with no apparent interstate commerce connection. This wetland is not currently regulated by the Corps under the Clean Water Act. This disclaimer of jurisdiction is only for Section 404 of the Federal Clean Water Act. Other Federal, State, and local laws may apply to your activities. In particular, you may need authorization from the California State Water Resources Control Board and/or the U.S. Fish and Wildlife Service.

This verification is valid for five years from the date of this letter unless new information warrants revision of the determination before the expiration date. A notice of appeal options is enclosed. You should provide a copy of this to all other affected parties. Please refer to identification number 200200674 in any future correspondence concerning this project. If you have any questions, please write to William Guthrie at the letterhead address, or email William.H.Guthrie@usace.army.mil, or telephone 916-557-5269.

Sincerely,

Michael Finan
Chief, Delta Office

Enclosure(s)

Copy furnished without enclosure(s):

George Day, Storm Water and Water Quality Certification Unit, Central Valley Regional
Water Quality Control Board, 3443 Routier Road, Suite A, Sacramento, California
95827-3003

Oscar Balaguer, Chief, Water Quality Certification Unit, California State Water Resources
Control Board, 1001 I Street, Sacramento, California 95814

Michael Wood, Michael Wood Biological Consulting, 65 Alta Hill Way, Walnut Creek,
California 94595

January 22, 2003

California Department of Fish and Game
Central Coast Region 3
P. O. Box 47
Yountville, CA 94599

Warden Nicole Kozicki
P. O. Box 284
Moraga, CA 94556

SUBJECT: 1603 Notification #R3-2002-0917 – Acceptance of CDFG Mitigation

Dear Nicole and Department Staff:

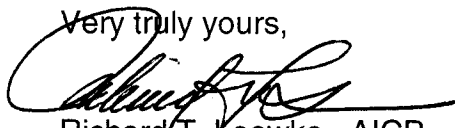
The above referenced Section 1603 Notification package was originally transmitted to you on October 30, 2002. The application identified the planned removal of a temporary drainage swale measuring 0.17 acres, located on property owned by Davidon Homes in Southeast Antioch. Following initial review of these materials, a field visit was conducted on November 19, 2002 by Warden Nicole Kozicki and Dick Loewke. This meeting resulted in Warden Kozicki's determination that the subject temporary swale currently provides water filtering benefits, which may be replaced in kind. Specifically, Warden Kozicki recommended that the property owner agree, as part of planned development on this 160-acre site, to replace the swale by means of one of the following alternatives:

- (a) Inclusion of 0.17 acres of replacement open drainage course(s) within the project boundaries having similar filtering benefits.
- (b) Inclusion of an integrated storm drainage system filtering mechanism which employs low flow soil percolation through rock layers.

Details of the selected alternative (or combination thereof) shall be included on the project improvement plans, and submitted to Warden Kozicki for review and approval prior to commencement of work. This water filtering feature may be referenced as part of the independent submittal and permit requirements of the Regional Water Quality Control Board.

Thank you for your assistance and guidance in this matter.

Very truly yours,


Richard T. Loewke, AICP
Planning Consultant

AGREED TO BY DAVIDON HOMES:

1600 South Main Street, Suite 150
Walnut Creek, CA 94596
Tel.: (925) 945-8000

By: 

Jeff Thayer

Date

Cc: Victor Carniglia, City of Antioch

October 30, 2002

California Department of Fish & Game Warden Nicole Kozicki
Central Coast Region 3 P. O. Box 284
P. O. Box 47 Moraga, CA 94556
Yountville, CA 94599

**SUBJECT: Section 1603 Notification for Davidon Homes Property Located in
Southeast Antioch, Contra Costa County**

Dear Nicole and Department Staff:

Attached please find a completed Notification of Lake or Streambed Alteration form and Project Questionnaire involving a very small portion of the Davidon Homes property located immediately east of the intersection of Canada Valley Road and Vista Grande in southeast Antioch. These forms supplement the detailed information previously forwarded to the USACE for wetland delineation verification and determination of non-jurisdiction.

The attached CDFG forms have been tentatively completed, pursuant to my earlier discussions with Nicole. At issue is the planned removal of a temporary swale, measuring 0.17 acres in area, which currently conveys storm drainage from Canada Valley Road to East Antioch Creek. As detailed in the attached October 8, 2002 letter to the USACE, the swale was constructed approximately 3 years ago to carry City storm drainage across the southwest corner of my client's property. Pursuant to an agreement with the City of Antioch, water will no longer discharge into the swale beginning next year when Canada Valley Road is extended south to connect with Lone Tree Way (see maps included in USACE package). Davidon Homes plans to concurrently develop the southwest corner of their 150-acre parcel where the swale is now located, in accordance with the City's adopted East Lone Tree Specific Plan and project-level EIR.

As detailed in the report from biologist Michael Wood (included in the attached USACE package), the swale currently satisfies vegetation, soils and hydrology criteria to classify it as an isolated wetland. However, as Canada Valley Road is completed to the south, the continued discharge of storm water will be eliminated, thereby allowing the swale area to revert to its historical dry condition. Based on these facts and the materials included in the USACE submittal, I do not believe the removal of this 0.17-acre artificial swale would "substantially divert or obstruct the natural flow or substantially change the bed, channel or bank of any river, stream or lake designated by the department" as regulated under Section 1603(a) of the Fish and Game Code.

As noted in the attached documentation, no special status plants or animals have been identified on this site or in the vicinity of this site. The City's previous EIR also failed to identify any sensitive biological resources within this area. In addition, a number of focused biological surveys recently completed in cooperation with your department, as part of the nearby East Antioch Creek Channel relocation project (CDFG Agreement #2000-573), also confirmed the absence of special resources.

Nicole Kozicki / CDFG
October 30, 2002
Page 2

I have completed the attached forms for your review and formal determination. Should you concur that work within this swale area does not warrant the issuance of a Section 1603(g) Agreement, please provide me with your written verification. Alternatively, if you have further questions, or if you would like to arrange to meet at the site, please call me as soon as possible. Thank you in advance for your review of the attached documentation.

Sincerely,



Richard T. Loewke, AICP

COPY: Mr. Jeff Thayer
Davidon Homes
1600 South Main Street #150
Walnut Creek, CA 94596

| For Department Use Only | | | | |
|-------------------------|-----------------|----------------|--|-----------------|
| Notification Number: | | Date Received: | | Date Completed: |
| Fees Enclosed? | Yes \$ _____ No | | | |
| Action Taken/Notes: | | | | |

STATE OF CALIFORNIA
THE RESOURCES AGENCY
DEPARTMENT OF FISH AND GAME

NOTIFICATION OF LAKE OR STREAMBED ALTERATION

(See attachment/enclosure for instructions)

| Notification Type | |
|--|---|
| <input type="checkbox"/> 1601 (Public) | <input type="checkbox"/> Timber Harvest Plan (No. _____) |
| <input checked="" type="checkbox"/> 1603 (Private) | <input type="checkbox"/> Commercial Gravel Extraction (No. _____) |
| | <input type="checkbox"/> Water Application (No. _____) |

| Applicant Information | | | |
|---------------------------------------|------------------------------|---|---|
| | Name | Address | Telephone/FAX |
| Applicant: | Richard T. Loewke, ACP | 55 Oak Trail Ct. Alamo, CA 94507 | Business: (925) Fax: (925) 256-0140 |
| Operator: | JEFF Thayer Davidon Homes | 1600 South Main St Walnut Creek, CA 94596 | Business: (925) 945-8000 Fax: (925) 256-0140 |
| Contractor: (if known) | | | Business: Fax: |
| Contact Person: (if not applicant) | | | Business: Fax: |
| Property Owner: | Davidon Homes | 1600 South Main St Walnut Creek, CA 94596 | Business: (925) 945-8000 Fax: (925) 256-0140 |

| Project Location | | | | | |
|---------------------------------|--|-------|--------------------------|--------------------|--|
| Location Description: | Immediately east of intersection of Canada Valley Road and Vista Grande in southeast Amador (see attached maps). | | | | |
| County | | | Assessor's Parcel Number | | |
| Contra Costa | | | 053-060-008 | | |
| USGS Map | Township | Range | Section | Latitude/Longitude | |
| | 2N | 2E | 34 (SW 1/4 Section) | | |
| Name of River, Stream, or Lake: | N/A | | | | |
| Tributary To? | N/A | | | | |

NOTIFICATION OF LAKE OR STREAMBED ALTERATION

(Continued)

Name of Applicant: Richard T. Weawe, AICP

Project Description

| | | | | | | |
|----------------------|---|---------------------------|----------------|---------------|-------------------|---|
| Project Name: | <u>Davidson Homes Property Wale / Southeast Antioch</u> | | | | | |
| Proposed Start Date: | <u>Nov '02</u> | Proposed Completion Date: | <u>Nov '02</u> | Project Cost: | <u>\$ 1,000 ±</u> | Number of Stream Encroachments: (Timber Harvest Plans only) |

Describe project below: (Attach separate pages if necessary)

Please review letter to CDFG dated 10/30/02, and Oct 8, 2002 Submittal for wetland delineation to USACE. Project involves removal of small (0.17-acre) Swale which currently conveys City storm drain discharge from Canada Valley Road. Swale is plastic-lined surface created 3+ yrs. ago under agreement between property owners and City of Antioch.

☒ Continued on separate page(s)

Attachments/Enclosures

Attach or enclose the required documents listed below and check the corresponding boxes.

| | | |
|---|---|--|
| <input checked="" type="checkbox"/> Project description | <input checked="" type="checkbox"/> Map showing project location, including distances and/or directions from nearest city or town | <input type="checkbox"/> Construction plans and drawings pertaining to the project |
|---|---|--|

Attach or enclose the documents listed below, if complete, and check the corresponding boxes.

| | | | |
|---|--|---|--|
| Completed CEQA documents: | <input type="checkbox"/> Negative Declaration | <input checked="" type="checkbox"/> Environmental Impact Report | <input type="checkbox"/> Notice of Exemption |
| | <input type="checkbox"/> Mitigated Negative Declaration | | <input type="checkbox"/> Notice of Determination |
| Copies of applicable local, State, or federal permits, agreements, or other authorizations: | <input checked="" type="checkbox"/> Local. Describe: <u>City Specific Plan for East Line Tree Area</u> | | |
| | <input checked="" type="checkbox"/> Federal. Describe: <u>Pending Verification of Wetlands / Non Jurisdiction from ACE</u> | | |

I hereby certify that all information contained in this notification is true and correct and that I am authorized to sign this document. I understand that in the event this information is found to be untrue or incorrect, I may be subject to civil or criminal prosecution and the Department may consider this notification to be incomplete and/or cancel any Lake or Streambed Alteration Agreement issued pursuant to this notification. I understand that this notification is valid only for the project described herein and that I may be subject to civil or criminal prosecution for undertaking a project that differs from the one described herein, unless I have notified the Department of that project in accordance with section 1601 or 1603 of the Fish and Game Code.

I understand that a Department representative may need to inspect the property where the project described herein will take place before issuing a Lake or Streambed Alteration Agreement pursuant to this notification. In the event the Department determines that a site inspection is necessary, I hereby authorize the Department to enter the property where the project described herein will take place to inspect the property at any reasonable time and certify that I am authorized to grant the Department permission to access the property.

☐ I request the Department to first contact me at (insert telephone number) _____ to schedule a date and time to enter the property where the project described herein will take place and understand that this may delay the Department's evaluation of the project described herein.

Richard T. Weawe
Operator or Operator's Representative

10/30/02
Date



Lake and Streambed Alteration Program

Project Questionnaire

Please complete the following questionnaire and submit it with your notification package to expedite the Department's review of your proposed project or activity.
Please attach or enclose any additional information or documents that support or relate to your response.

| | Yes | Maybe/ Uncertain | No | Please explain if you responded "yes" or "maybe/uncertain" |
|---|-----|---------------------|----|--|
| 1. Will the project or activity involve work on the bank of a river, stream, or lake? | | | X | Affected area is a very shallow man-made swale which has an underlying plastic lining |
| 2. If you answered "yes" to #1, will the project or activity involve any of the following: | n/a | | | |
| a. Removal of any vegetation? | | | | |
| b. Excavation of the bank? | | | | |
| c. Placement of piers? | | | | |
| d. Placement of bank protection or stabilization structures or materials (e.g., gabions, rip-rap, concrete slurry/sacks)? | | | | |
| 3. Will the project or activity take place in, adjacent to, or near a river that has been designated as "wild and scenic" under state or federal law? | | | X | Nearest water course is the East Antioch Creek Flood Control Channel (CDEP Agreement #200-073) |
| 4. Will the project or activity involve work in the bed or channel of a river, stream, or lake? | | | X | |
| 5. Will the project or activity involve the placement of any permanent or temporary structure in a river, stream, or lake? | | | X | |

| | Yes | Maybe/ Uncertain | No | Please explain if you responded "yes" or "maybe/uncertain" |
|---|-----|---------------------|----|--|
| 6. Will the project involve the use of material from a streambed? | | | X | |
| 7. Will the project or activity result in the disposal or deposition of debris, waste, or other material in a river, stream, or lake? | | | X | |
| a. If you answered "yes" to #7, describe the material that will be disposed of or deposited in the river stream, or lake: | N/A | | | |
| 8. Will any type of equipment be used in a river, stream, or lake? | | | X | |
| a. If you answered "yes" to #8, describe the type of equipment that will be used: | N/A | | | |
| 9. Does the project or activity area flood or periodically become inundated with water? | X | | | This site currently carries storm drainage discharge from Pipe in Canyon Valley Road. For a distance of 1450', this discharge will end when roadway is extended. |
| 10. Will water need to be diverted from a river, stream, or lake for the project or activity? | | | X | |
| 11. If you answered "yes" to #10, please answer the following: N/A | | | | |
| a. Will this be a temporary diversion? | | | | |
| b. Will water quality be affected by the deposition of silt, an increase in water temperature, a change in the pH level, or in some other way? | | | | |
| c. Will the water be diverted by means of a dam, reservoir, or other water impoundment structure? | | | | |
| 12. Will the project or activity be done pursuant to a water right application or permit? | | | X | |
| 13. a. Has a wildlife assessment or study been completed for the area where or near where the project or activity will take place? (If "yes", attach or enclose a copy of the assessment or study.) | X | | | Completed as part of EIR for Antelope Valley Tree Planting Area. See Attached Documentation. No Special Status plants or animals identified (See letter). |

| | Yes | Maybe/ Uncertain | No | Please explain if you responded "yes" or "maybe/uncertain" |
|--|--|---------------------|----|---|
| 14. Will the project or activity affect fish, amphibians, insects, or other aquatic resources? | | | X | No evidence of any special status plants, grasslands pursuant to project level EIR. |
| 15. Will the project or activity affect terrestrial wildlife? | | | X | This small Exotic (0.17 acre) is maintained periodically (By vegetation removal) and is temporary in nature (Bureau) See 13, 14 & 15 above |
| 16. Are any endangered or rare plant species thought or known to occur in the area where the proposed project or activity will take place? | | | X | " |
| 17. Are any endangered or threatened fish, bird, or animal species thought or known to occur in the area where the proposed project or activity will take place? | | | X | " |
| 18. Have you contacted any other local, State, or federal agency regarding the project or activity? | X | | | A wetland delineation was completed and filed with the USACE on 10/8/02. |
| a. If you answered "yes" to #18, please list the names of the agencies you have contacted: | Copy of the request for verification and non-jurisdictional determination is attached. | | | |
| 19. Have you applied for or obtained any permit, agreement, or other authorization for your project or activity from any government agency? | X | | | A specific plan and project-level EIR were approved by the City of Antioch in 1996, followed by adoption of a Utility Service Financial Plan in 1998. |
| a. If you answered "yes" to #19, please list the names or describe the permit, agreement, or authorization you have applied for or obtained: | X | | | See #19 above. |
| 20. Have any environmental documents pertaining to your project or activity been prepared? | X | | | |
| a. If you answered "yes" to #20, please list the environmental documents that have been prepared: | | | | |

I hereby certify that all information contained in this notification is true and correct and that I am authorized to sign this document. I understand that in the event this information is found to be untrue or incorrect, I may be subject to civil or criminal prosecution and the Department may consider this notification to be incomplete and/or cancel any Lake or Streambed Alteration Agreement Issued pursuant to this notification.



Operator or Operator's Representative

10/30/02

Date

October 8, 2002

Michael Finan
Chief, Delta Office
U.S. Army Corps of Engineers
1325 J Street
Sacramento, CA 95814-2922

**SUBJECT: Request for Verification of Non-Jurisdictional Status of Swale
Located on Property in Antioch, Contra Costa County**

Dear Mr. Finan:

This request involves review of a draft wetland delineation report recently completed for a very small (0.17-acre) isolated area located immediately adjacent to the intersection of Canada Valley Road and Vista Grande in southeastern Antioch. The site is located in Section 34, Township 2 North, Range 2 East, MDBM, Antioch, Contra Costa County. Attached to this cover letter are the following documents for your further review:

1. Regional Location Map.
2. Map of Southeast Antioch showing location of East Lone Tree Planning Area.
3. Map of East Lone Tree Planning Area showing delineation area and recent USACE non-jurisdiction determination areas as discussed below.
4. September 13, 2002 Wetland Delineation Report by Michael Wood, Biologist.
5. USACE Determination Letter of 10/16/01 for Lindsey Basin (#200100337).
6. USACE Determination Letter of 4/25/00 for East Antioch Channel (#200000110).
7. Excerpts from East Lone Tree Specific Plan project EIR, certified by the City of Antioch.

Your office has twice recently been involved in the review and verification of wetland delineations for adjoining properties, located north of Lone Tree Way and West of Empire Avenue in the City of Antioch. In both of the above referenced cases, representatives of your office met in the field with my team of planners and biologists. In both cases, your office determined that jurisdictional waters of the U.S. were not present.

The subject property is a very small and isolated temporary drainage swale, located immediately to the east of the intersection of Canada Valley Road and Vista Grande in southeast Antioch. The swale was originally created approximately 3 years ago (subject to a drainage release to the City of Antioch), as a plastic-lined discharge course to carry storm water from a temporary 48" RCP outlet on the east side of Canada Valley Road.

Cattle grazing has been responsible for the demise of the original plastic liner, allowing cattails and other non-native vegetation to periodically grow within the saturated soils on the swale. The property owner has, however, made various subdrain and rock lining improvements to the swale, and has consistently bladed the surface of the swale since its liner deteriorated. As discussed in the report from Mr. Wood, however, cattails and other non-native vegetation continue to emerge from the saturated soils within this 0.17-acre swale.

Michael Finan / Davidon Swale
October 8, 2002
Page 2

The City of Antioch is planning to extend Canada Valley Road south to connect with Lone Tree Way in the next several months, as called for in the specific plan. Once complete, this improvement will extend the 48" storm drain trunk line which currently discharges onto the subject property. Completion of the trunk line will remove all water from the swale, thereby eliminating the need for the swale.

As a condition of subdivision approval (called out in the City's project EIR as a verification requirement), the property owner, Davidon Homes, is obligated to obtain verification of non-jurisdiction from the Corps. We therefore request that you review this documentation and issue a written determination with respect to jurisdiction. If I can be of assistance in answering any questions, or if your staff would like to arrange a meeting in the field, please do not hesitate to call me at 9925) 831-8016 (or via e-mail at LoewkeAICP@cs.com).

Sincerely,

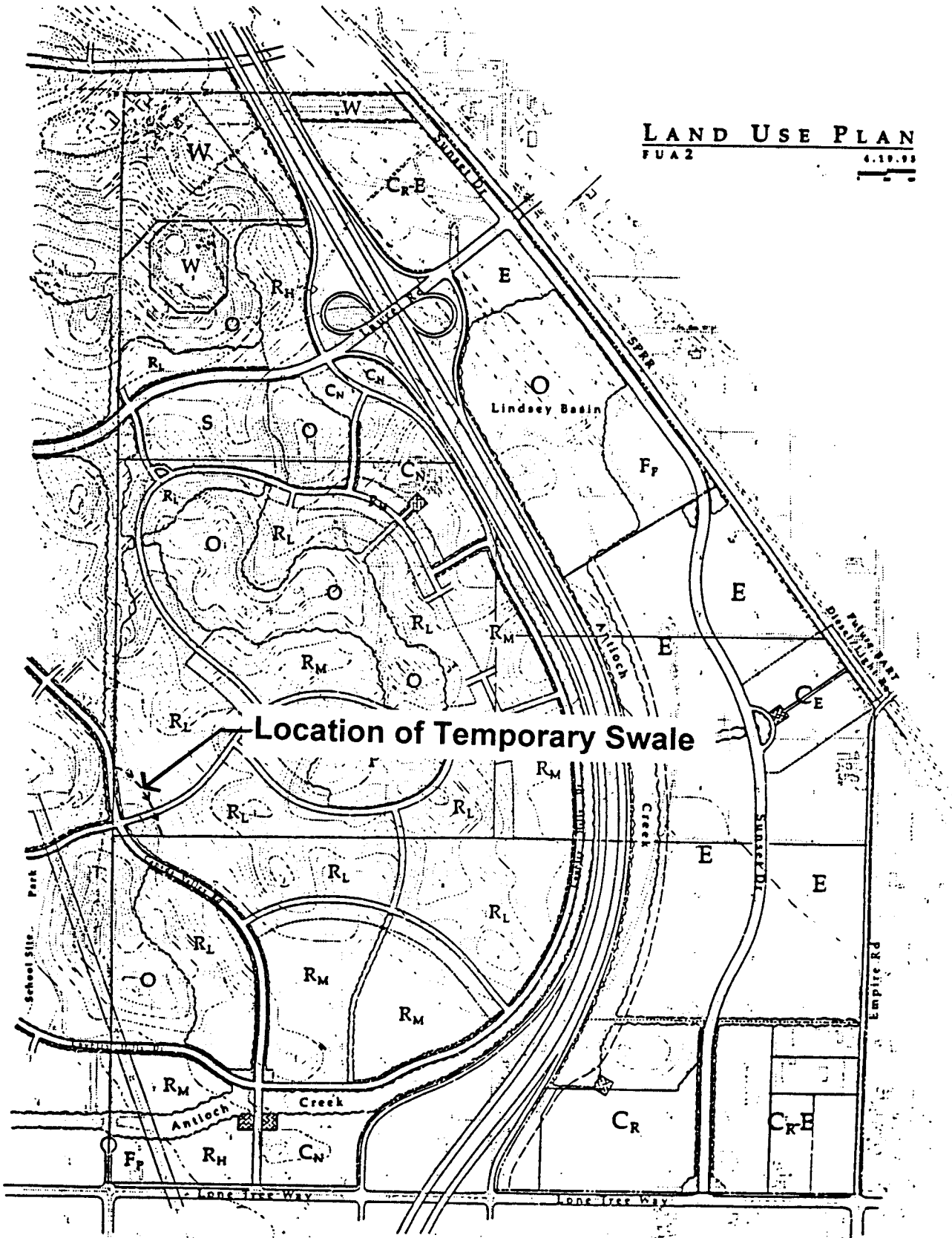
A handwritten signature in dark ink, appearing to read "Richard T. Loewke", with a stylized flourish at the end.

Richard T. Loewke, AICP

Cc: Jeff Thayer, Davidon Homes
Nicole Kozicki, CDFG
Mike Wood, Biological Consulting

LAND USE PLAN
FUA 2

4.19.93
2-2



**Adopted 1996 City of Antioch
East Lone Tree Specific Plan**

b. Mitigation Measures

The following mitigation measure is hereby adopted and will be implemented as provided in the Mitigation Monitoring Program:

- I5. Development applicants shall coordinate with the pipeline and irrigation companies and appropriate Health and Safety Agencies with regard to the design, timing, access and easement requirements related to respective utility relocation.

c. Findings

Based on the Final Environmental Impact Report (FEIR) and the entire record before this City Council, this City Council finds that:

- i. The adoption of mitigation measure I5 would reduce the potential of infrastructure-related impacts to a less-than significant level.

Vegetation and Wildlife

Impact J1: Wetland habitats within the planning area would be lost or periodically modified by development envisioned by the proposed plan.

a. Description

This Project Impact is discussed on Page 144 of the Draft Environmental Impact Report (DEIR).

b. Mitigation Measures

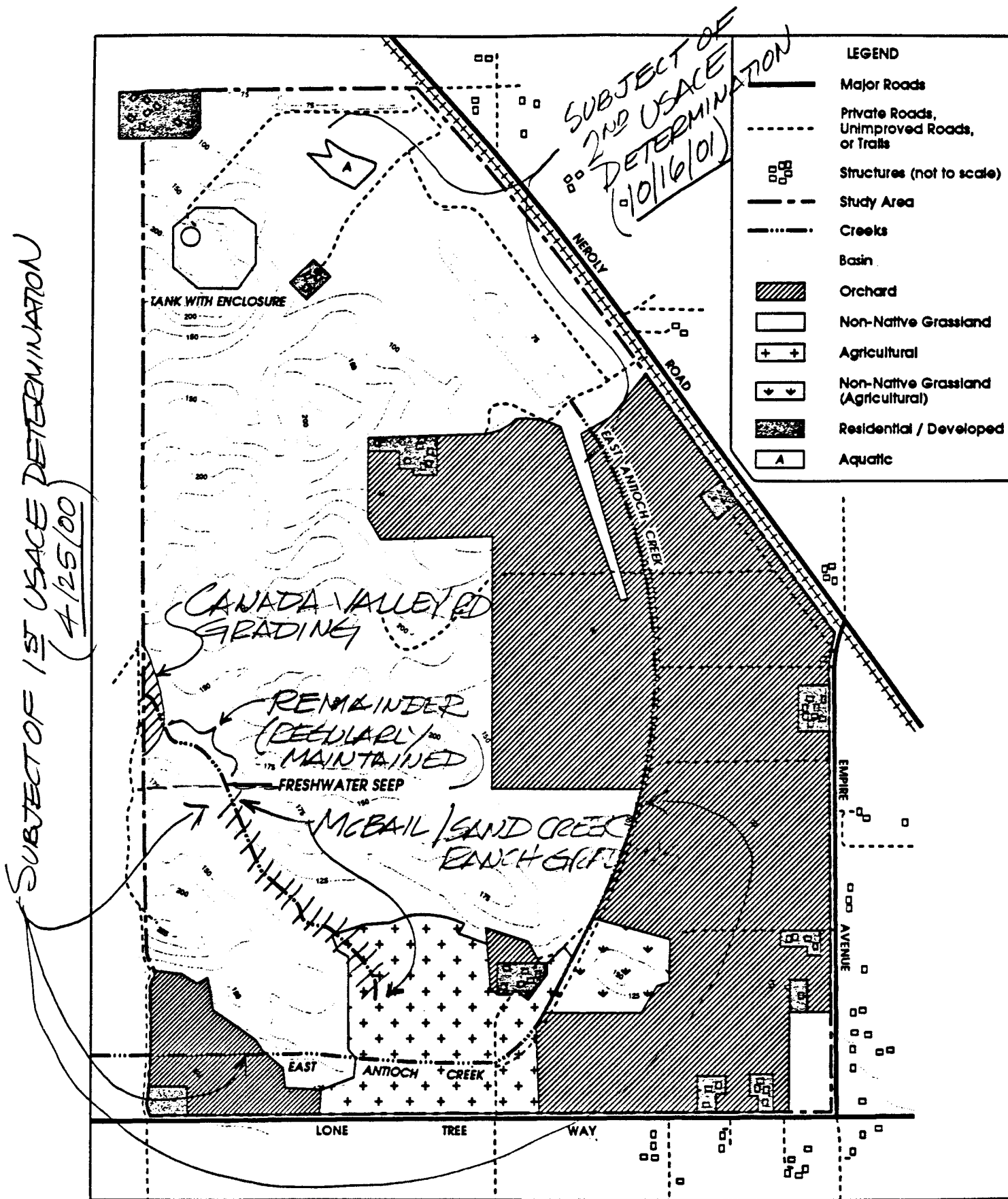
The following mitigation measure is hereby adopted and will be implemented as provided in the Mitigation Monitoring Program:

- J1. The developer of any subsequent project(s) shall be required to have a formal wetland delineation undertaken and verified by the Army Corps of Engineers. Based on the findings of that delineation, the developer may be required to have a wetland replacement plan prepared by a biologist qualified to prepare such plans, and shall commit to its implementation in a manner, and on a schedule, acceptable to the Corps and to the City of Antioch.

c. Findings

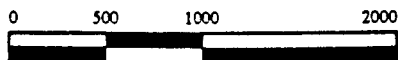
Based on the Final Environmental Impact Report (FEIR) and the entire record before this City Council, this City Council finds that:

- i. The adoption of mitigation measure J1 would reduce the potential of vegetation and wildlife-related impacts to a less-than significant level.



Source: H. T. Harvey & Associates

Figure 30



Biotic Habitats

Michael K. Wood
Biological Consulting

65 Alta Hill Way
Walnut Creek, CA 94595
Tel: (925) 899-1282
Fax: (925) 939-4026
e-mail: wood-biological@mindspring.com

September 13, 2002

Dick Loewke
55 Oak Trail Ct.
Alamo, CA 94507

Re: Wetland Delineation, Southwest Corner of Rolling Hills Ranch

Dear Dick:

At your request, I have completed a preliminary jurisdictional determination of the western portion of the Rolling Hills Ranch site. The study area is located near the intersection of Canada Valley Road and Vista Grande Drive in eastern Antioch (Figure 1). The study area was restricted to the rock-lined drainage channel situated just east of Canada Valley Road and drains roughly from north to south, and exiting onto the McBail property.

METHODS

A routine wetlands delineation and preliminary jurisdictional determination was performed by biologist Michael Wood on August 29, 2002. The survey was conducted in accordance with the procedures outlined in the U.S. Army Corps of Engineers' (USACE) Wetlands Delineation Manual (Environmental Laboratory 1987). Based on topography and the presence or absence of field indicators including vegetation, hydrology and soils, the limits of potential jurisdictional waters of the U.S. was determined. The extent of potential wetlands and waters of the U.S. was mapped on a 1" = 50' scale topographic map (enclosed).

Documentation reviewed as part of this analysis includes *Draft Environmental Impact Report, Future Urbanization Area #2 Specific Plan, Antioch, California* (Mundie & Associates 1995), *Biological Constraints Analysis for East Antioch Creek Corridor through the McBail Property, Contra Costa County, California* (Sycamore Associates 2000), *Wetland Delineation and Preliminary Jurisdictional Determination for the Lindsey Basin Expansion Project* (Michael Wood Biological Consulting 2001), and jurisdictional determination letters for the East Antioch Creek Flood Control Channel and Lindsey Basin Expansion Project (USACE 2000, 2001, respectively).

SETTING AND SITE DESCRIPTION

The study area is situated in an open field adjacent to recent residential subdivision development (Figure 2). Lands to the west have been graded and filled to accommodate the southward extension of Canada Valley Road. The Jacuzzi property has been used historically for the grazing of cattle. Cattle have been recently excluded from the study area by construction of a barbed-wire fence. Vegetation on the Jacuzzi property and surrounding, undeveloped lands is characteristic of eastern Contra Costa County, consisting predominantly of non-native annual grassland. Topography of the site consists of low, rolling hills.

The focus of this effort is a recently evolved drainage channel at the western edge of the Jacuzzi property. A temporary 48" reinforced concrete pipe (RCP) outfall leads onto the Jacuzzi property, conveying storm water from beneath Canada Valley Road. The outfall is situated near the northern, or upstream, end of the drainage channel. The outfall is due to be closed as the roadway is extended to the south later this year.

Vegetation

The Jacuzzi property is dominated by non-native annual grassland. Non-native annual grassland is typically of heavily grazed areas. Characteristic non-native species detected on site include ripgut brome (*Bromus diandrus*), wild oats (*Avena fatua*), Italian ryegrass (*Lolium multiflorum*), bur-clover (*Medicago polymorpha*), yellow star thistle (*Centaurea solstitialis*), bristly ox-tongue (*Picris echioides*), field bindweed (*Convolvulus arvensis*), curly dock (*Rumex crispus*), and filaree (*Erodium* spp.), among others.

Vegetation within the channel consists of a more or less continuous band of freshwater marsh vegetation that has recently evolved on the site. The dominant species is cattails (*Typha latifolia* and *T. angustifolia*). Also present in the channel are three-square (*Scirpus americanus*), toad rush (*Juncus bufonius*), northern willow herb (*Epilobium ciliatum*), water speedwell (*Veronica anagallis-aquatica*), umbrella sedge (*Cyperus eragrostis*), and loosestrife (*Lythrum hyssopifolia*). A single sapling of red willow (*Salix laevigata*) is also present. Vegetation on the slopes leading to the channel is ruderal, and dominated by bristly ox-tongue.

No woody vegetation is present within the study area or its vicinity.

Non-native annual grassland to the California annual grassland series as described in Sawyer and Keeler-Wolf (1995), and would be classified as an upland habitat following Cowardin, *et al.* (1979). Freshwater marsh conforms to the cattail series as described in Sawyer and Keeler-Wolf (1995) and would be classified as a palustrine persistent emergent freshwater wetland following Cowardin, *et al.* (1979).

Soils

Soils within the study area are mapped as Diablo clay, 9-15 percent slopes (USDA 1977). The Diablo series consists of well-drained soils underlain by calcareous, soft, fine-grained sandstone and shale. These soils are on uplands with slopes ranging from 9 to 50 percent and at elevations from 400 to 1,200 feet above mean sea level. The average annual temperature is

59° F, average annual rainfall is 12-25 inches, and the average frost-free period is 260-300 days per year. The soils are generally moist to a depth of 30 inches from November to May and are dry from June to mid-October in most years. The natural vegetation consists primarily of annual grasses and forbs with a few scattered oaks.

The specific mapping unit occurring onsite, Diablo clay, 9 to 15 percent slopes, has slow permeability in the subsoil, run-off is slow to medium and the hazard of erosion is slight to moderate where the soil is bare. No water table was within the depth of observation, usually five feet (USDA 1977). The presence of this soil type was confirmed in the field. The Diablo series is classified as a Chromic Pelloxerert. Included in this soil unit are areas of Cropley clay and Altamont clay. Diablo clay, 9 to 15 percent slopes is not considered a hydric soil type (USDA 1991, 1992).

Hydrology

The focus of the present study is an unnamed drainage channel located at the western edge of the property. The drainage channel contained a small amount of standing water at the time of the present survey, and soils beneath the surface were moist to the touch. The channel is presumed to be ephemeral in nature.

The drainage channel is not part of a natural creek. It does not appear in aerial photos prior to 1970 and is believed to have evolved following construction of the adjacent residential development. Around 1990, a storm water detention basin was constructed on adjacent land immediately upslope of the study area (D. Loewke, pers. comm.) The basin discharged onto the Jacuzzi property. Surface flows drained overland onto the McBail property before disappearing underground. The basin was removed in 1998. As part of the construction of the adjacent residential subdivision and the extension of Canada Valley Road, a 48" storm drain outfall was constructed at the western boundary of the Jacuzzi property. The outfall empties into the drainage channel, near its northern, or upstream end. Interestingly, freshwater marsh vegetation extends approximately 60 feet upstream of the outfall, indicating that it might not be the sole source of water. However, there is no evidence of surface water leading to the upstream end of the cattail habitat.

The drainage channel itself covers approximately 450 linear feet and varies in width (at the tops of bank) from 5-15 feet. It is shallowly to barely incised, ranging in depth from 0.5-1.5 feet. The channel has developed as a result of periodic maintenance, which has occurred over the past four years (since the detention basin was removed.) Beneath the channel, two perforated drainpipes were installed over a plastic liner, and covered with rock. The plastic liner appears to have deteriorated. Three 36" diameter corrugated steel pipes (CSP) are installed near the middle of the channel to accommodate vehicle access onto the property.

The channel exists the property at the McBail Ranch, where it meanders and ultimately dissipates into the ground. Sheet flow from the surrounding lands ultimately reach East Antioch Creek. East Antioch Creek is an artificial flood control channel draining the Lone Tree Valley. Storm flows are directed into the Lindsey Basin, an artificial flood control basin built around 1994 by the Contra Costa County Flood Control District.

RESULTS

Based on an evaluation of the existing conditions within the study area, vegetation within the drainage channel appears to meet the federal definition of a wetland (see below). A total of 7,575 square feet of wetland habitat (emergent freshwater marsh) is currently present within the study area.

Based on review of historical aerial photographs and interviews with persons familiar with the history of the site, the existing wetland is believed to have only recently developed due presumably to man-caused alterations of the surface hydrology. However, even though the presumed original source of water causing the development of this wetland, the storm water detention basin, was removed around 1998, the habitat has persisted. It can therefore be presumed that the freshwater marsh will continue to persist, therefore representing a “new existing condition.” As such, impacts to this habitat may be regulated by several agencies (see discussion, below.)

PERMITTING IMPLICATIONS

Because the drainage channel is not connected to a natural watercourse and is isolated, it is believed to fall outside of the jurisdiction of the USACE. In 2001, the Supreme Court ruled that the U.S. Army Corps of Engineers (USACE) cannot evoke the Commerce Clause (migratory bird rule) in claiming jurisdiction over isolated wetlands (Solid Waste Agency of Northern Cook County [SWANCC] v. USACE). Based on our experience, we do not believe that impacts to the isolated wetlands on site would be regulated under Section 404 of the Clean Water Act. This is supported by recent determination made by the USACE-Sacramento District that the agency does not have jurisdiction over the nearby East Antioch Creek (2000) or the Lindsey Basin (2001). Nonetheless, the USACE should be contacted to make a formal jurisdictional determination.

Irrespective of federal jurisdiction, impacts to wetlands, including isolated wetlands, are regulated pursuant to state law. Specifically, Section 1600 *et seq.* and the Porter-Cologne Act provide authority for the California Department of Fish and Game (CDFG), the State Water Resources Control Board (SWRB), and the Regional Water Quality Control Board (RWQCB) to regulate impacts to wetlands and waters of the state.

Some general background information regarding wetlands and the agencies involved in their regulation is provided below.

U.S. Army Corps of Engineers

Section 404 of the Clean Water Act (CWA) of 1972 regulates activities that result in the discharge of dredged or fill material into waters of the U.S., including wetlands. The primary intent of the CWA is to authorize the U.S. Environmental Protection Agency (EPA) to regulate water quality through the restriction of pollution discharges. The USACE has the principal authority to regulate discharges of dredged or fill material into waters of the U.S.

Waters of the U.S. are defined as 1) waters used in interstate or foreign commerce, 2) waters subject to the ebb and flow of tide, 3) all interstate waters including interstate wetlands, intrastate lakes, rivers, streams, mudflats, sand flats, wetlands, sloughs, prairie potholes, wet meadows, playa lakes, natural ponds, the use, degradation, or destruction of which could affect interstate or foreign commerce, and 4) areas that are or could be used for recreation by interstate or foreign travelers, fish or shellfish that is sold in interstate or foreign commerce, or industrial purposes in interstate commerce. The Environmental Protection Agency (EPA) has expanded the definition of "waters" to include waters used to irrigate crops sold in interstate commerce, and habitats that are used by birds protected by treaty or birds that cross state lines, and habitat for endangered species (51 FR 41217), as well as impoundments of "waters", tributaries of "waters", and territorial seas (§328.3(a)(4),(5),(6)).

Wetlands, a subset of waters of the U.S., are defined as "those areas that are inundated or saturated by surface or ground water at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions" (§404 Clean Water Act). Indicators of all three wetlands parameters (hydric soils, hydrophytic vegetation, wetlands hydrology) must be present for a site to be classified as a wetland (Environmental Laboratory 1987).

Projects that result in impacts of less than one-half acre (or one-third acre for certain transportation projects) and/or less than 300 linear feet (or 200 linear feet for certain transportation projects) may be authorized under one of the existing USACE Nationwide Permits (NWP) if they meet all of the Nationwide Permit General Conditions. If the project falls under the NWP program and will result in greater than 0.10 acre of impacts, a pre-construction notification (PCN) must be submitted to the USACE prior to discharging fill. The NWP General Conditions require that the project include provisions for the protection of federally- or state-listed Endangered or Threatened species, water quality management and construction practices that do not disrupt movement of aquatic life, among other requirements. Additional regional requirements for maintaining upland buffer areas between authorized projects and open waters or streams may be conditions for granting any USACE permit. Therefore, activities authorized under NWPs are often those projects that have minimal impacts to wetlands, waters and special-status species. If no state- or federally-listed Endangered or Threatened species have the potential to occur in the project area, processing of NWPs frequently takes 30 to 60 days. When listed species may be present in the project area, the review and negotiation process may take up to six months or more.

California Department of Fish and Game

The CDFG exercises jurisdiction over wetland and riparian resources associated with rivers, streams, and lakes under California Fish and Game Code Sections 1600 to 1607. The CDFG has the authority to regulate work that will substantially divert, obstruct, or change the natural flow of a river, stream, or lake; substantially change the bed, channel, or bank of a river, stream, or lake; or use material from a streambed. California Department of Fish and Game's jurisdictional area along a river, stream or creek is usually bounded by the top-of-bank or the outermost edges of riparian vegetation. Typical activities regulated by CDFG under Sections 1600-1607 authority include installing outfalls, stabilizing banks, implementing flood control

projects, construction river and stream crossings, diverting water, damming streams, gravel mining, and logging operations.

Prior to undertaking any activity that will impact any of the above biological resources, a Streambed Alteration Permit must be obtained from CDFG. An application for a Streambed Alteration Permit usually requires a complete project description, a biological assessment of the project site, analyses of direct, indirect and cumulative impacts, a technically-defensible biological mitigation and monitoring plan, a documented history of project alternatives and efforts to avoid and minimize impacts, a relevant California Environmental Quality Act (CEQA) document, and a Notice of Determination that demonstrates the project has complied with CEQA. The CDFG has authority to reopen CEQA if impacts to resources over which it has jurisdiction have not been adequately addressed.

Regional Water Quality Control Board

Pursuant to Section 401 of the Clean Water Act and EPA 404(b)(1) Guidelines, an applicant for a federal permit to conduct any activity which may result in discharge into navigable waters must provide a certification from the Regional Water Quality Control Board (RWQCB) that such discharge will comply with the state water quality standards (Cal. Code Regs. tit. 23, §§3830 *et seq.*). The RWQCB has a policy of no net loss of wetlands in effect and typically requires mitigation for all impacts to wetlands before it will issue a water quality certification or waiver thereof.

Under the Porter-Cologne Water Quality Control Act (Cal. Water Code §§13000-14920), the RWQCB is authorized to regulate the discharge of waste that could affect the quality of the State's waters. "Waste" is broadly defined by the Porter-Cologne Act to include "sewage and any and all other waste substances, liquid, solid, gaseous, or radioactive, associated with human habitation, or of human or animal origin, or from any producing, manufacturing, or processing operation of whatever nature...." (Cal. Water Code §13050). Concentrated silt or sediment associated with human habitation and harmful to the aquatic environment is "waste" under this section. In addition, the California Attorney General has interpreted this definition to include extraction of sand, gravel or other minerals from a streambed, because it may cause an increase in turbidity and silt in the waters of the stream downstream from the operations. Therefore, even if a project does not require a federal permit (*i.e.*, a Nationwide Permit for the USACE), it may require review and approval of the RWQCB.

When reviewing applications, the RWQCB focuses on ensuring that projects do not adversely affect the "beneficial uses" associated with waters of the state. Generally, the RWQCB defines beneficial uses to include all of the resources, services and qualities of aquatic ecosystems and underground aquifers that benefit the state of California. Numerous beneficial uses have been identified, including agricultural supply, wildlife habitat, recreation, groundwater recharge, and municipal and domestic water supply. In most cases, the RWQCB seeks to protect these beneficial uses by requiring the integration water quality control measures into projects that will result in discharge into waters of the state. For most construction projects, RWQCB requires the use of construction and post-construction Best Management Practices (BMPs). In many cases, proper use of BMPs, including detention ponds, grassy swales, sand filters,

modified roof drains, and other features, will speed project approval from RWQCB. Development setbacks from creek are also favored by RWQCB as they often lead to less creek-related impacts in the future. Proper integration of these and other features into project design will greatly decrease the necessary negotiation with RWQCB and speed the project approval process.

I hope this information allows you to move forward with your planning. If you have any questions, please don't hesitate to contact me.

Sincerely,

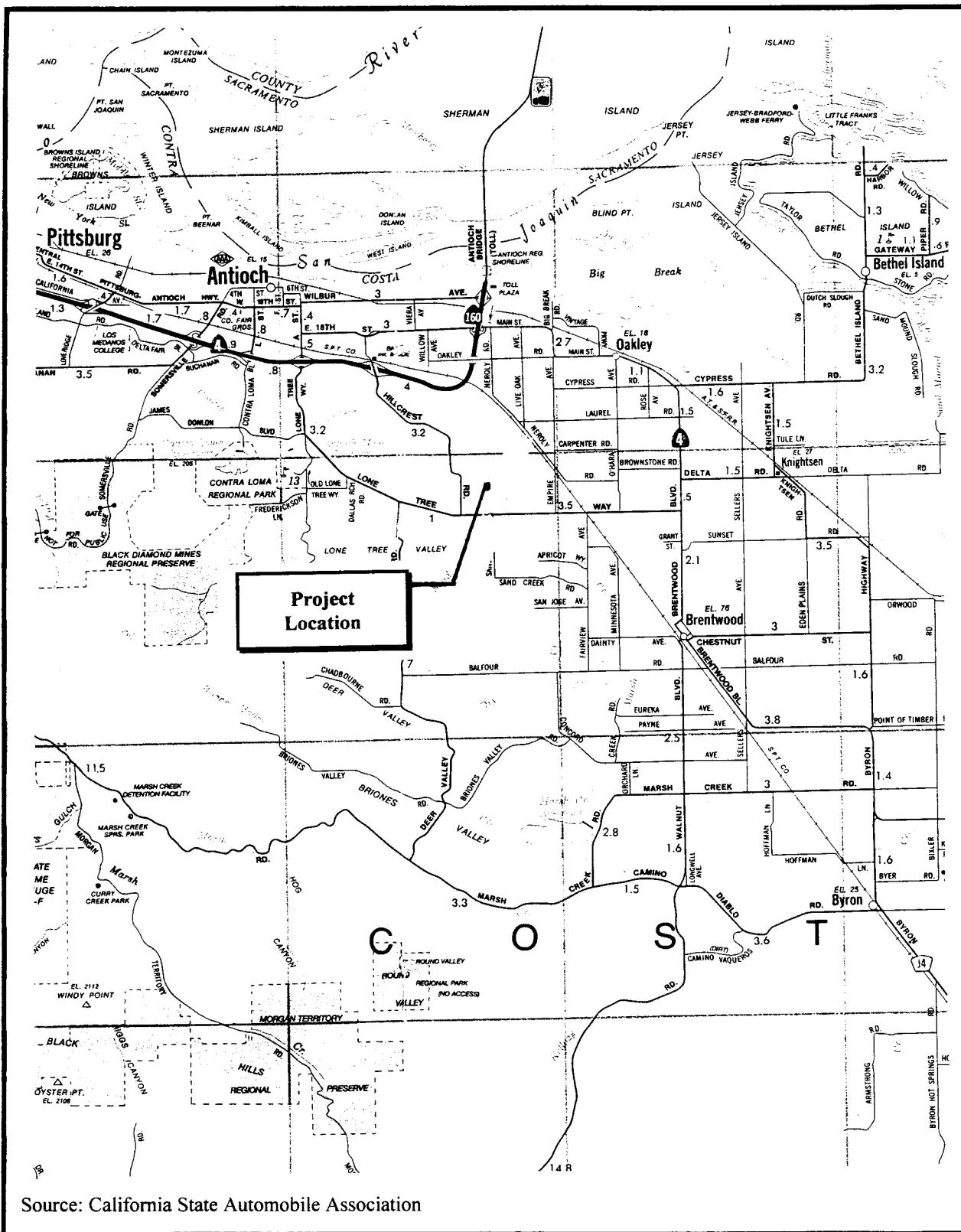


Michael Wood

Enclosures: Literature Cited, Data Forms, Figure 1 (Project Location), Figure 2 (Aerial Photograph of Project Vicinity), Preliminary Jurisdictional Determination Map

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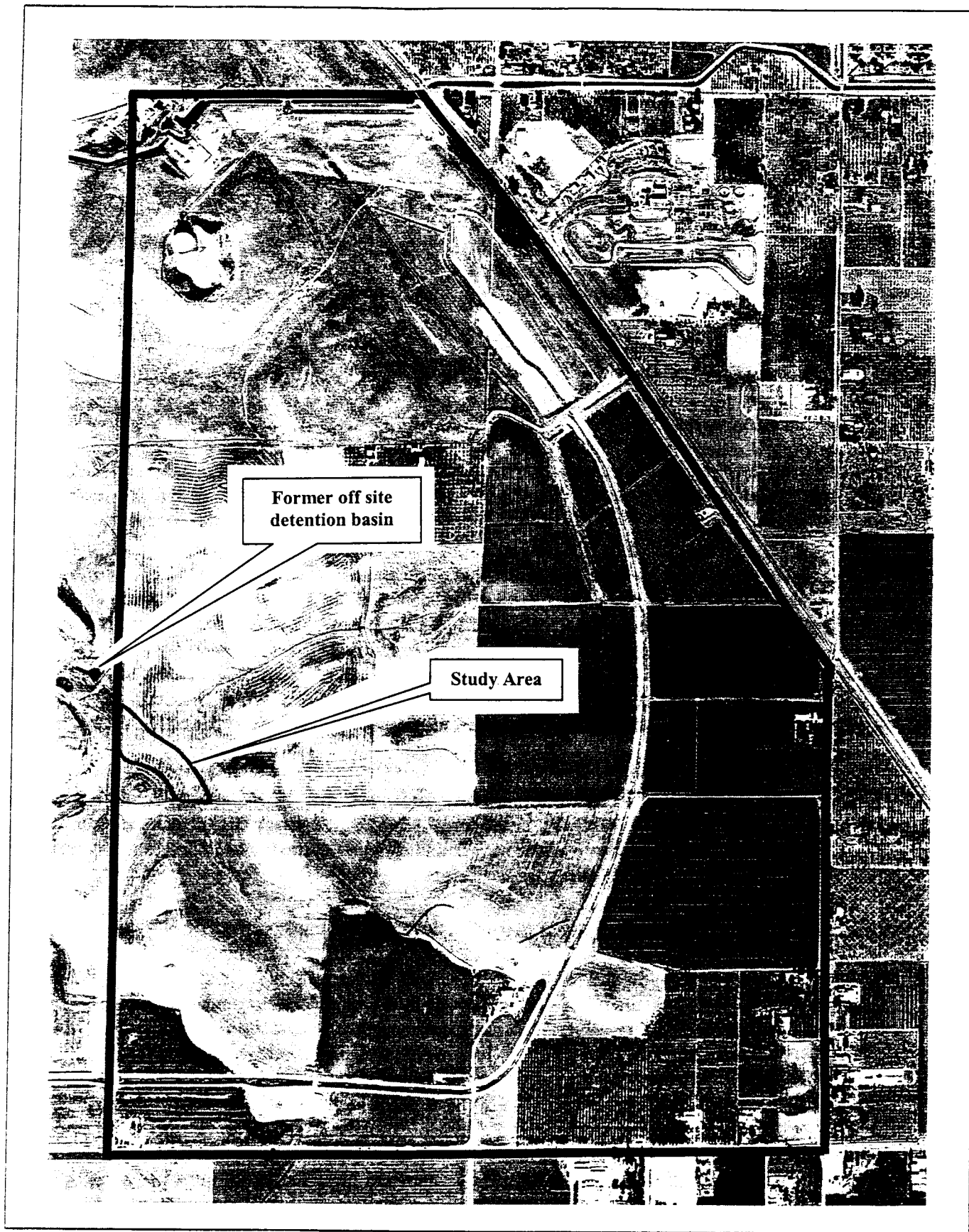
Michael Wood
Biological
Consulting

Figure 1. Project Location

NORTH

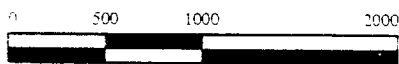


Scale 1" = 2.5 miles



Source: Mundie & Associates 1995
date of photo: July 1990

FIGURE 2
AERIAL PHOTOGRAPH OF PROJECT VICINITY



Antioch Future Urbanization Area #2

**DATA FORM
ROUTINE WETLAND DELINEATION
(1987 COE Wetlands Delineation Manual)**

Project/Site: Rolling Hills Ranch
Applicant/Owner: Jacuzzi
Investigator: Michael Wood (925) 899-1282

Date: 8/29/02
County: Contra Costa
State: California

Community ID: freshwater marsh

Do normal circumstances exist on the site? YES
Is the site significantly disturbed (Atypical Situation)? YES
Is the area a potential Problem Area? NO

Transect ID:
Plot ID: Sample Point # 1

VEGETATION

| <u>Dominant Species Present¹</u> | <u>% Cover²</u> | <u>Stratum</u> | <u>Indicator</u> | <u>Subdominant Species Present³</u> | <u>% Cover²</u> | <u>Stratum</u> | <u>Indicator</u> |
|---|----------------------------|----------------|------------------|--|----------------------------|----------------|------------------|
| 1. <i>Typha angustifolia</i> | 30 | herb | OBL | 1. <i>Cyperus eragrostis</i> | 15 | herb | OBL |
| 2. <i>Scirpus americanus</i> | 20 | herb | OBL | 2. <i>Juncus bufonius</i> | 8 | herb | FACW+ |
| 3. | | | | 3. <i>Lythrum hyssopifolia</i> | 5 | herb | FACW |
| 4. | | | | 4. <i>Picris echioides</i> | 12 | herb | FAC* |
| 5. | | | | 5. <i>Veronica anagallis-aquatica</i> | 3 | herb | OBL |
| 6. | | | | 6. <i>Polypogon monspeliensis</i> | 8 | herb | FACW+ |
| 7. | | | | 7. | | | |
| 8. | | | | 8. | | | |

Percent of Dominant Species that are OBL, FACW, or FAC (excluding FAC-): 100%

Remarks: Site is clearly dominated by strong wetland indicator species. Vegetation compositions is clearly distinct from adjacent uplands. Vegetation is presumed to have recently evolved on site as a result of modified hydrologic conditions following grading for a nearby housing development.

¹Dominance determined by the 50/20 Rule. ²Estimated absolute cover. ³Not considered for wetland determination.

HYDROLOGY

☐ Recorded data (describe in remarks)
☒ No recorded data available

Wetland Hydrology Indicators

Primary Indicators:

Field Observations:

Depth of surface water: 0 (inches)
Depth to free water in pit: >6 (inches)
Depth to saturated soil: >6 (inches)

☐ inundated
☐ saturated in upper 12 inches
☐ water marks
☐ drift lines
☒ sediment deposits
☒ drainage pattern in wetlands

Secondary Indicators:

☒ oxidized root channels in upper 12 inches
☐ water-stained leaves
☐ local soil survey data
☒ FAC neutral test
☒ other (see below)

Remarks:

Sample point is near top of watershed. Urban flows from residential development obviously contribute to surface hydrology of site. A 48" RCP outfall is located near upstream end of site, and 3 36" CSP culverts channel surface flows beneath a dirt road downstream. Algal mats present, as are deep vertical cracks in the soil. Channel was recently constructed and lined with coarse drainage rock, making it impossible to dig a 12" deep soil pit. Surface flows are conveyed off site via an unlined, open ditch. Standing water was present at the time of the survey.

**DATA FORM
ROUTINE WETLAND DELINEATION
(1987 COE Wetlands Delineation Manual)**

Project/Site: Rolling Hills Ranch
Applicant/Owner: Jacuzzi
Investigator: Michael Wood (925) 899-1282

Date: 8/29/02
County: Contra Costa
State: California

Community ID: ruderal upland

Do normal circumstances exist on the site? YES
Is the site significantly disturbed (Atypical Situation)? YES
Is the area a potential Problem Area? NO

Transect ID:
Plot ID: Sample Point # 2

VEGETATION

| <u>Dominant Species Present</u> ¹ | <u>% Cover</u> ² | <u>Stratum</u> | <u>Indicator</u> | <u>Subdominant Species Present</u> ³ | <u>% Cover</u> ² | <u>Stratum</u> | <u>Indicator</u> |
|--|-----------------------------|----------------|------------------|---|-----------------------------|----------------|------------------|
| 1. <i>Picris echioides</i> | 80 | herb | FAC* | 1. | | | |
| 2. <i>Lolium multiflorum</i> | 30 | herb | FAC* | 2. | | | |
| 3. | | | | 3. | | | |
| 4. | | | | 4. | | | |
| 5. | | | | 5. | | | |
| 6. | | | | 6. | | | |
| 7. | | | | 7. | | | |
| 8. | | | | 8. | | | |

Percent of Dominant Species that are OBL, FACW, or FAC (excluding FAC-): 100%

Remarks: Site is dominated by very marginal wetland indicator species. Vegetation compositions is not very distinct from adjacent non-native grassland (upland), but clearly distinct from adjacent freshwater marsh.

¹Dominance determined by the 50/20 Rule. ²Estimated absolute cover. ³Not considered for wetland determination.

HYDROLOGY

☐ Recorded data (describe in remarks)
☒ No recorded data available

Wetland Hydrology Indicators
Primary Indicators:

Field Observations:

Depth of surface water: 0 (inches)
Depth to free water in pit: >12 (inches)
Depth to saturated soil: >12 (inches)

☐ inundated
☐ saturated in upper 12 inches
☐ water marks
☐ drift lines
☐ sediment deposits
☐ drainage pattern in wetlands

Secondary Indicators:

☐ oxidized root channels in upper 12 inches
☐ water-stained leaves
☐ local soil survey data
☐ FAC neutral test
☐ other (see below)

Remarks:
No field indicators of wetland hydrology present.

PRELIMINARY
WETLAND DELINEATION
AND JURISDICTIONAL DETERMINATION
FOR THE JACUZZI PROPERTY,
CONTRA COSTA COUNTY, CALIFORNIA

August 29, 2002

Legend

Potential CDFG-Regulated Wetland



Total within study area:
7,575 sq. ft. (0.17 acre)

Prepared by:

Michael Wood Biological Consulting
65 Alta Hill Way
Walnut Creek, CA 94595
(925) 899-1282

NORTH



Scale 1" = 50 feet

SE

PLASTIC LINER

6"

18"

Limits of
Study Area

ft. 128.2

3 x 36" CSP
culverts beneath
dirt road

Ruderal freshwater
marsh

Property
Boundaries

McBAIL

Canada Valley Road

48" RCP
culvert outfall

DRIVE

EXISTING 36" RCP PIPE
EXISTING 24" RCP PIPE

JACUZZI

Appendix I

Future Urbanization Area #2 Specific Plan Mitigation Monitoring & Reporting Plan

CHAPTER II

MITIGATION MONITORING AND REPORTING

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|--|--|--|--|--|
| TRANSPORTATION | | | | |
| Intersection Improvements as described in the DEIR (Chapter III.B) | Developers of Specific Plan projects (shares to be determined at time of subsequent approvals) | City of Antioch, Community Development Department, Land Planning Services Division | Verify that appropriate contributions have been made by Specific Plan landowners | Requirement of Tentative Maps and/or Final Development Plans |
| Roadway Improvements as described in the DEIR (Chapter III.B) | Developers of Specific Plan projects (shares to be determined at time of subsequent approvals) | City of Antioch, Community Development Department, Land Planning Services Division | Verify that appropriate contributions have been made by Specific Plan landowners | Requirement of Tentative Maps and/or Final Development Plans |
| Signalizations as described in the DEIR (Chapter III.B) | Developers of Specific Plan projects (shares to be determined at time of subsequent approvals) | City of Antioch, Community Development Department, Land Planning Services Division | Verify that appropriate contributions have been made by Specific Plan landowners | Requirement of Tentative Maps and/or Final Development Plans |
| B10 Assure that subsequent plans provide for adequate access to onsite commercial and employment areas in a manner complying with the Specific Plan and with City of Antioch standards | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that project proposals adequately incorporate design features that meet City requirements and all applicable standards at the time individual projects are considered | Requirement of Final Development Plans |
| B11, 12, 13 Intersections, roadways, sidewalks and bike lanes shall be designed in subsequent plans to meet the City's standards | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that project proposals adequately incorporate design features that meet City requirements and all applicable standards at the time individual projects are considered | Requirement of Final Development Plans |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|---|--------------------------------------|--|--|--|
| TRANSPORTATION (cont'd) | | | | |
| B14 Provide for bicycle parking, showers at employment centers and connections to adjacent development | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that project proposals adequately incorporate design features that meet City requirements and all applicable standards at the time individual projects are considered | Requirement of Final Development Plans |
| B15, 16, 17 Provide site-specific layout and circulation design for school-related circulation, delivery access and parking, emergency vehicle access, and user parking | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that project proposals adequately incorporate design features that meet City requirements and all applicable standards at the time individual projects are considered | Requirement of Final Development Plans |
| B18 Implement a detailed construction traffic plan | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Conduct compliance investigations periodically during construction near and at the construction site during construction activity to verify achievement of traffic plan objectives | To be submitted with Use Permit applications |
| B19 To enhance the transit accessibility of the project: 1a The project shall be designed for pedestrian access to arterial and collector streets 1b Cul-de-sacs that back onto arterial and collector streets shall have a pedestrian/ bicycle link between the cul-de-sac and the main road 2 Bus turnouts and passenger shelters shall be provided on major streets to accommodate future transit service | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that project proposals adequately incorporate design features that meet City requirements and all applicable standards at the time individual projects are considered | Requirement of Final Development Plans |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|---|--------------------------------------|--|--|--|
| TRANSPORTATION (cont'd) | | | | |
| B20 Implement incentives for employment-bearing land uses to help assure that employment in FUA #2 shall be established in the same general time frame as housing | City of Antioch | City of Antioch, Community Development Department, Land Planning Services Division | | Requirement of Final Development Plans |
| AIR QUALITY | | | | |
| C1a The proposed project shall comply with the air quality policies of the <i>Antioch General Plan</i> by ensuring that the local circulation system will encourage and accommodate the use of transportation modes other than the automobile | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify compliance with the City's General Plan and that appropriate features have been incorporated into project plans | Requirement of Final Development Plans |
| C1b Antioch's Transportation Demand Management (TDM) ordinance shall be applied to all phases of the proposed project and include specific trip reduction goals and enforcement procedures | Developers of Specific Plan projects | City of Antioch, East County TDM Coordinator | Verify application of the City's TDM ordinance and that appropriate provisions have been incorporated into Specific Plan projects | Prior to issuance of building permits |
| C2 Control construction period fugitive dust in all phases of project development beyond the initial phase, using methods described in the DEIR (Chapter III.C) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Building Inspection Division | Conduct compliance investigations during construction to verify that fugitive dust is controlled according to mitigation specifications | Prior to issuance of grading permits and ongoing during construction |
| NOISE | | | | |
| D1a Limit hours of noise-generating construction activity to the hours of 8:00 AM to 5:00 PM. Trucks shall be restricted to major arterial roadways and shall avoid residential neighborhoods when possible | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Conduct occasional site visits to verify compliance. Respond to complaints alleging non-compliance. Record each site visit and complaint | During construction as needed |
| D1b Minimize equipment noise by properly muffling and maintaining all construction equipment | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Conduct occasional site visits to verify compliance. Respond to complaints alleging non-compliance. Record each site visit and complaint | During construction as needed |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|--|--------------------------------------|--|--|--|
| NOISE (cont'd) | | | | |
| D1c Protect sensitive receptors from excessive construction noise as described in the DEIR (Chapter III.C). | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Conduct occasional site visits to verify compliance. Respond to complaints alleging non-compliance. Record each site visit and complaint | During construction as needed |
| D2a Use open space buffer zones and/or noise barriers along roadways to reduce the CNEL to 60 dBA or less, as specified in the DEIR (Chapter III.D) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that noise attenuation features are incorporated into proposed projects consistent with approved plans | Requirement of Tentative Maps or Final Development Plans, as appropriate |
| D2b Site and design residences to meet interior noise standards, as specified in the DEIR (Chapter III.D) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that recommended mitigation measures are incorporated into proposed project | Requirement of Final Development Plans (site design) and prior to issuance of building permits (building design) |
| GEOLOGY, SOILS AND SEISMICITY | | | | |
| E1 A project grading plan shall be prepared by a licensed civil engineer pursuant to Uniform Building Code requirements for each Specific Plan project, consistent with the specifications of the DEIR (Chapter III.E) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Building Inspection Services Division | Review and approve grading plan; verify incorporation of recommended mitigation measures into proposed project | Requirement of Final Development Plans |
| E2 Site and building design shall take account of weak and/or expansive soils, consistent with the specifications of the DEIR (Chapter III.E) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Building Inspection Services Division | Verify incorporation of recommended mitigation measures into proposed project | Requirement of Final Development Plans (site design) and prior to issuance of building permits (building design) |
| E3a Site planning and building design shall incorporate provisions to reduce risk to life and property from seismic activity | Developers of Specific Plan projects | City of Antioch, Community Development Department, Building Inspection Services Division | (1) Verify that building plans incorporate provisions to reduce risk to life and property from seismic activity; (2) conduct site inspection during and upon completion of building construction | Prior to (1) issuance of building permits; (2) issuance of certificates of occupancy |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|---|--------------------------------------|--|---|--|
| GEOLOGY, SOILS AND SEISMICITY (cont'd) | | | | |
| E3b All buildings, underground utilities and other improvements shall be designed and constructed in accordance with seismic design criteria presented in the Uniform Building Code (see DEIR, Chapter III.E) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Building Inspection Services Division | (1) Verify compliance with Uniform Building Code seismic design criteria; (2) Conduct site inspection during and upon completion of building construction | Prior to (1) issuance of building permits; (2) issuance of certificates of occupancy |
| E4 Implement actions (described in DEIR, Chapter III.E) to protect the public from risks associated with natural gas extraction activities, for the duration of those activities | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify incorporation of recommended mitigation measures into proposed project | Prior to issuance of first building permit |
| FLOODING AND DRAINAGE | | | | |
| F1 Prepare and comply with Storm Water Pollution Prevention Plan, as described in the DEIR (Chapter III.F) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Engineering Services Division | Verify preparation of and compliance with the Storm Water Pollution Prevention Plan | Prior to (1) issuance of grading permits; (2) during construction; and (3) during operation of the project |
| F2 Defer development in the 100-year flood zone until capacity improvements have been provided for | Developers of Specific Plan projects | City of Antioch, Community Development Department, Engineering Services Division | Verify construction of improvements and appropriate contributions by Specific Plan landowners | Prior to issuance of building permits |
| F3 Construct needed facilities to detain runoff onsite to avoid increased downstream flooding, as specified in the DEIR (Chapter III.F) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Engineering Services Division | Verify construction of improvements and appropriate contributions by Specific Plan landowners | Prior to issuance of building permits |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|---|--------------------------------------|--|---|--|
| PUBLIC HEALTH AND SAFETY | | | | |
| G1 Implement measures to assure that site development not result in public safety hazards from accidental fuel releases, from release of asbestos in demolition activities, or from exposure to agriculture-related or other chemicals that may have been used or disposed of onsite (see DEIR, Chapter III.G) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review reports/findings of investigators and approve management and remediation plans | Prior to issuance of grading permits |
| G2 Implement accepted practices to alert the public to the risks of exposure to electromagnetic field (EMF) and to hazardous substances associated with electrical transmission. All existing transformers shall be checked for the presence of PCBs by PG&E. All metal structures or objects located adjacent to transmission line easements shall be properly grounded to prevent electrical shocks from persons or animals in contact with those objects. | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify compliance with measures to inform residents of EMF risks, inspection of transformers for PCB hazards and proper grounding of all metal objects in close proximity to electrical transmission line easements | EMF: Upon occupancy of residential units and at any future period when new information on EMF becomes available PCBs: During preparation and review of Final Development Plans Power lines: Prior to issuance of grading or building permits |
| G3 Comply with all policies, laws and regulations regarding use and storage of hazardous materials, as described in the DEIR (Chapter III.G) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify compliance with all applicable policies, laws and regulations, and adequacy of management practices | Prior to issuance of grading or building permits |
| G4 Conform with public safety standards with respect to location of residential and other development in the vicinity of operating and abandoned gas wells, as described in the DEIR (Chapter III.G) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review reports/findings of investigators and verify that development proposals comply with public safety standards | Requirement of Final Development Plans |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|--|---|--|--|--|
| PUBLIC SERVICES | | | | |
| H1 Incorporate Fire District planning and financing mechanisms into the Specific Plan and development process | City of Antioch in collaboration with CCCCFD | City of Antioch, Community Development Department, Land Planning Services Division | Verify that fee payments have been made, that CCCCFD concerns are addressed in project design, and that timing of development shall occur so as not to overburden CCCCFD resources | Requirement of Final Development Plans |
| H2 Specification of the appropriate water main sizes to deliver flows at the required rate | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review project proposals and plans to verify incorporation of specified improvements | Requirement of Final Development Plans |
| H3a Accommodate increased school enrollment by a variety of strategies, including provision of portable facilities, year-round education, double sessions and construction of new facilities | Developers of Specific Plan projects in consultation with the City of Antioch | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that proposed projects respond to the need for new and expanded school facilities that result from the development of those projects | Requirement of Final Development Plans |
| H3b Require the portions of FUA #2 that are within the AUSD to join the current AUSD Mello-Roos Community Facilities District or provide an alternate funding mechanism for construction of school facilities | Developers of Specific Plan projects in consultation with the City of Antioch | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that the boundaries of the current AUSD Mello-Roos CFD have been adjusted to include the Specific Plan area or that an alternate school funding mechanism is in place | Requirement of Final Development Plans |
| H3c Require the portions of FUA #2 that are within the BUESD to join the existing East Contra Costa County School Facilities Funding and Mitigation Agreement with the school district or provide an alternate funding mechanism for construction of elementary and middle school facilities | Developers of Specific Plan projects in consultation with the City of Antioch | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that the properties in the Specific Plan area have been added to the Agreement or that an alternate school funding mechanism is in place | Requirement of Final Development Plans |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|---|---|--|--|---|
| PUBLIC SERVICES (cont'd) | | | | |
| H3d Require the portions of FUA #2 that are within the LUHSD to join the existing East Contra Costa County School Facilities Funding and Mitigation Agreement with the school district or provide an alternative funding mechanism for construction of high school facilities | Developers of Specific Plan projects in consultation with the City of Antioch | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that the properties in the Specific Plan area have been added to the Agreement or that an alternate school funding mechanism is in place | Requirement of Final Development Plans |
| INFRASTRUCTURE | | | | |
| I1a Complete roadway improvements as specified in the DEIR (Chapter III.I) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify construction of improvements and appropriate contributions by Specific Plan landowners | At time of improvement project or prior to development review of individual project, whichever comes sooner |
| I1b Provide access and circulation routes to specific parcels | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify construction of improvements and appropriate contributions by Specific Plan landowners | At time of improvement project or prior to development review of individual project, whichever comes sooner |
| I1c Comply with City and State standards (or as modified by Specific Plan guidelines) in circulation and parking design and construction, including, but not limited to, parking standards, handicap requirements, fire equipment access, site distances, etc., as described in the DEIR (Chapter III.I) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Engineering Division | Verify compliance with City design and construction standards for parking and circulation | Requirement of Final Development Plans |
| I2a Construct water system improvements as described in the DEIR (Chapter III.I) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify construction of improvements and appropriate contributions by Specific Plan landowners | At time of improvement project or prior to development review of individual project, whichever comes sooner |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|--|--------------------------------------|--|--|--|
| INFRASTRUCTURE (cont'd) | | | | |
| 12b Compliance with City design and construction standards, including connections as required by the City of Antioch's ADCD, Engineering Department and internal water distribution plans meeting City standards for various land uses, fire flows and landscape needs (see DEIR, Chapter III.I) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Engineering Services Division | Verify compliance with City design and construction standards for domestic water supply | Requirement of Final Development Plans |
| 13a Extend sewer lines ranging in size from 8" to 12" | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify construction of improvements and appropriate contributions by Specific Plan landowners | At time of project construction |
| 13b Comply with City design and construction standards, including incorporating sewer connection requirements, manholes and any other needed improvements in the overall design and submitting those plans for City review and approval | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify compliance with City sewerage design and construction standards | Requirement of Final Development Plans |
| 13c Design the internal sewer collection system to address City, State and Federal standards regarding disposal of hazardous materials (from the commercial sites) and submitting plans for such systems to the appropriate responsible agency, as identified in the DEIR (Chapter III.G) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify compliance with City, State and Federal standards for the disposal of hazardous materials | Requirement of Final Development Plans |
| 14 Development applicants shall provide documentation to the City that electrical, natural gas, cable and telephone services can be provided for all phases of the project in a timely manner | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review documentation that specifies providers' ability to furnish utility services, including a schedule | Requirement of Final Development Plans |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|---|--------------------------------------|--|--|--|
| INFRASTRUCTURE (cont'd) | | | | |
| I5 Development applicants shall coordinate with the pipeline and irrigation companies and appropriate Health and Safety Agencies with regard to the design, timing, access and easement requirements related to respective utility relocation | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that development applicants have coordinated with all relevant entities regarding the design, timing, access and easement requirements involved in relocating existing oil pipelines and irrigation laterals | Requirement of Final Development Plans |
| VEGETATION AND WILDLIFE | | | | |
| J1 The developer of any subsequent project(s) shall be required to have a formal wetland delineation undertaken and verified by the Army Corps of Engineers, as specified in the DEIR (Chapter III.J) | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that a formal wetland delineation has been completed and verified by the Army Corps of Engineers, and if necessary, that a wetland replacement plan has been devised and implemented accordingly | Requirement of Tentative Maps and/or Final Development Plans |
| J2 Develop a site management plan, as specified in the DEIR (Chapter III.J) to prevent water quality degradation | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review and approve site management plan | Prior to the issuance of grading permits |
| J3 Construction activities during the nesting season (February through July) could disturb nesting raptors and shall be preceded by surveys conducted by a qualified ornithologist | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Verify that nesting surveys have been conducted by a qualified ornithologist and that nesting success will not be jeopardized by construction activities | Prior to the issuance of grading permits |

| Mitigation Measure | Responsibility for Implementation | Responsibility for Monitoring | Action by Monitor | Compliance |
|--|--------------------------------------|--|---|--|
| CULTURAL RESOURCES | | | | |
| K1a Initial ground-disturbing construction activities within the site boundaries shall be monitored by a qualified archeologist, as specified in the DEIR (Chapter IIIK). A qualified archeological monitor shall be present during excavation and grading at site CA-CCo-691H. | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Identify and assess potential historic archeological resources and determine appropriate response | During excavation and grading activities |
| K1b Section 7050.5(b) of the California Health and Safety Code shall be implemented in the event that human remains, or possible human remains, are located | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Confirm compliance with Section 7050.5(b) of the California Health and Safety Code | At the time human remains are discovered |
| VISUAL RESOURCES | | | | |
| L1 Site planning and grading plans shall respect the integrity of the ridge that is an important visual resource of the planning area | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Confirm that site planning and grading plans for individual projects comply with all applicable visual resource preservation guidelines, including those advocated in the Specific Plan | Requirement of Final Development Plans |
| L2a Utilize site plan review and design review to mitigate any adverse aesthetic impacts of the Specific Plan | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review proposed Final Development Plan to insure incorporation of Design Review Board recommendations | Requirement of Final Development Plans |
| L2b The City of Antioch shall take steps, as part of its participation in planning for the SR 4 Bypass, to assure that sound attenuation elements of the Bypass satisfy the city's design guidelines | Developers of Specific Plan projects | City of Antioch, Community Development Department, Land Planning Services Division | Review sound attenuation elements of the SR 4 Bypass project to ensure compliance with the City's design guidelines | Requirement of Final Development Plans |

Appendix J

City Council Resolution 2005/14
Amending General Plan Exterior Noise Levels

*Council
action*

RESOLUTION NO. 2005/14

**RESOLUTION OF THE CITY COUNCIL OF THE CITY OF ANTIOCH
APPROVING AN AMENDMENT TO THE GENERAL PLAN CHANGING THE
ALLOWABLE MAXIMUM EXTERIOR NOISE LEVEL FOR NEW SINGLE
FAMILY AND NEW MULTIPLE FAMILY RESIDENTIAL UNITS OUTDOOR
LIVING AREAS LOCATED ADJACENT TO A PLANNED EXPRESSWAY OR
BART/eBART DEVELOPMENT FROM 60 CNEL TO 65 CNEL AND FLEXIBLE
STANDARDS FOR EXISTING RESIDENTIAL OUTDOOR LIVING AREAS
ADJACENT TO PLANNED FREEWAY EXPANSION, PROVIDING THERE
WOULD BE NO SIGNIFICANT INCREASE IN CURRENT NOISE LEVELS.**

WHEREAS, the City Council of the City of Antioch did receive an application from the City of Antioch for the approval of an amendment to the Environmental Hazards section of the General Plan to modify the allowable maximum exterior noise level for new single family and new multiple family residential units outdoor living areas located adjacent to a planned expressway (State Route 4 Bypass) or any Bart/eBart development from 60 CNEL to 65 CNEL and to allow flexible noise levels at existing residential outdoor living areas adjacent to a planned freeway expansion (State Route 4) subject to no significant (5 CNEL or greater) increase (Citywide) (GP-04-3); and

WHEREAS, the City Council did receive a recommendation for approval of this project from the Planning Commission; and

WHEREAS, a Negative Declaration was prepared and circulated pursuant to the California Environmental Quality Act and no comments were received during the public review period; and

WHEREAS, the City Council duly gave notice of public meeting as required by law; and

WHEREAS, on February 8, 2005, the City Council duly held a public meeting, received and considered evidence, both oral and documentary; and

WHEREAS, recent traffic and noise analysis has shown that it is not practical to meet the City's maximum exterior residential noise standard of 60 CNEL without in many cases constructing sound walls in excess of ten to fifteen ft. in height or more; and

WHEREAS, the negative visual impacts created by such large sound walls outweigh the benefits that might be achieved by holding to the current 60 CNEL standard; and

WHEREAS, the City would benefit in having flexibility in applying the maximum exterior noise standards; and

WHEREAS, CALTRANS and other local communities utilize a maximum exterior noise level of 65-67 CNEL adjacent to freeways and expressways.

NOW THEREFORE BE IT RESOLVED that the City Council does hereby approve that the General Plan exterior noise standards be modified as shown in Exhibit A incorporated herein by reference.

* * * * *

I HEREBY CERTIFY that the foregoing resolution was passed and adopted by the City Council of the City of Antioch at a regular meeting thereof, held on the 8th day of February, 2005 by the following vote.

AYES: Council Members Davis, Kalinowski, Conley and Mayor Freitas

NOES: None

ABSENT: Council Member Simonsen


L. JOLENE MARTIN, City Clerk

Appendix K

City of Antioch Project Pipeline
August 15, 2008



CITY OF ANTIOCH PROJECT PIPELINE

Residential Projects

| Project Number(s) | Project | Applicant | Location | APN | Units | Site Size | Status | Planner |
|---|---|--|--|---|---|-----------|--|----------|
| RDA-03-07 PD-04-14 UP-04-30 AR-05-23 AR-07-17 | Almondridge East Tract 7906 | KB Associates 6700 Knoll Center Parkway Pleasanton, CA 92821 | Philips Lane | 051-200-053 | 81 SFD | 21 acres | In plan check Approved PC scheduled 6/18/08 CC approved 7/8/08 | Gentry |
| UP-03-24 V-04-07 | Baywoods Condo Conversion | AGI Capital Group 1375 Sutter St #300 San Francisco, CA 94109 | 2005 San Jose Drive | 076-440-032 | Convert 128 apts to condos | | PC approved Council approved 1 st phase completed 2 nd phase under construction | Gentry |
| AR-06-09 UP-01-25 | Black Diamond Ranch 7487, 8585, 8586 | Discovery Builders 4061 Port Chicago HWY #1 Concord, CA 94524 | Somersville Road and James Donlon | | Unit 1 58 SFD Unit 2 117 SFD Unit 3 105 SFD | | Built Under Const Under Const | Stahl |
| MDP-06-02 RDA-07-05 | Deer Valley Estates | Allied Investments 1033 Detroit Avenue Concord, CA 94520 | Off Deer Valley Road north of Kaiser | 057-02-002 | 136 SFD | 37.25 | MDP PC approved 1/16/08 | Morris |
| RDA-03-05 | Golden Bow Estates 8538 | Dhyanyoga Centers P.O. Box 3194 Antioch, CA 94531 | Off Lexington | 076-031-036 | 12 SFD | | Approved | Gentry |
| AR-04-40 | Hidden Glen 6909, 7505, 8387, 8388 | Arcadia Homes 115 Coleman Avenue San Jose, CA 95110 | Off Hillcrest at Hidden Glen | | Unit 1 89 SFD Unit 2 81 SFD Unit 3 111 SFD Unit 4 90 SFD | | Under Const Approved Approved Approved | Oshinsky |
| MDP-07-01 | Leung Master Development Plan (Sand Creek Estates) | Waters Fund II, LLC 150 Almaden Blvd, Ste 700 San Jose, CA 95113 | Southern boundary of Antioch, west of Deer Valley Road | 057-041-013 057-041-016 057-041-015 | 190 SFD | 160 acres | On hold | Oshinsky |
| | Meadow Creek Village | Albert D Seeno Construction | Off Lone Tree Way at | | Unit 1 55 SFD | | Built | Stahl |

Updated 8/15/2008

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| | 7862, 7947, 7967, 7971, 7897 | 4021 Port Chicago Highway Concord, CA 94524 | | | Unit 2 77 SFD Unit 3 108 SFD Unit 4 96 SFD Unit 5 97 SFD | | Built Built Built Under Const | |
| AR-03-33 | Mira Vista Hills 6708, 6921 | Albert D Seeno Construction 4021 Port Chicago Highway Concord, CA 94524 | Off James Donlon at east of Somersville | | Unit 13 95 SFD Unit 16 85 SFD | | Being Reviewed Under const | Stahl |
| UP-04-01 AR-07-07 | Monterra (Nelson Ranch) 6893, 8850, 8851 | Standard Pacific Housing 3825 Hopyard Road #195 Pleasanton, CA 94588 | Wild Horse Road | 052-061-039 | Unit 1 102 SFD Unit 2 128 SFD Unit 3 130 SFD | 145 acres | Under Construction | Morris |
| AR-04-45 | Oakley Knolls | Discovery Builders 4061 Port Chicago HWY #1 concord, CA 94524 | Off Oakley Road | 051-180-014 | 16 SFD | 5.5 acres | Approved | Gentry |
| | Oakley Meadows | Michelle Sidriean 4160 S. Royal Links Circle Antioch, CA 94509 | Off Oakley Road at | | 13 SFD | | Approved | Gentry |
| PD-08-03 AR-08-10 | Park Lake Apartments | Loving and Campos 345 Ygnacio Valley Road Walnut Creek, CA 94596 | James Donlon Blvd | 072-011-062 | 60 MFD | 3.28 acres | Incomplete | Morris |
| UP-08-04 AR-05-05 | Park Ridge | Davidon 1600 S Main Street Ste 150 Walnut Creek, CA 94596 | Canada Valley Road | 053-060-023 | 562 SFD | 171 Acres | In progress | Gentry |
| MDP-05-01 RDA-07-01 | Pulte Senior Housing | Pulte Homes 6210 Stone Ridge Mall 5 th Floor Pleasanton, CA 94588 | At the end of Heidorn Ranch Road | 057-030-001 057-050-013 | 550 +/- Del Webb adult community | 194 acres | Incomplete | Welch |
| PD-04-12 | Renaissance at Bluerock 8884 | KB Homes 6700 Knoll Center Parkway Pleasanton, CA 94566 | Bluerock and Lone Tree Way | | 86 SFD | | Under const | Morris |
| PDP-06-04 | Rivertown Village | Don Ladpidus 991 Solana court Mountainview, CA 94040 | 1700 4 th Street | 074-040-047 | 202 SFD | | PDP Processed | Oshinsky |
| RDA-07-03 PD-07-03 UP-08-05 AR-08-07 | Roddy Ranch | Roddy Ranch PBC, LLC 12885 Alcosta Blvd., Suite A San Ramon, CA 94583 | West of Deer Valley Road South of Empire Mine Road | 057-060-017 | 574 SFD +/- 126 multi family Hotel | | In progress | Gentry |
| RDA-04-03 | Sand Creek Active Adult Community | Topaz Creek Investors 275 Saratoga Ave #105 Santa Clara, CA 95050 | Empire Mine Road | 057-010-001 | 1500 SFD - senior | | Approved | Wehrmeister |
| AR-05-01 | Sand Creek Ranch | William Lyons Homes | Off Canada Valley Road | | 8640 69 SFD | | Built | Stahl |

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| | 8640, 8885, 8948 | 2603 Camino Ramon #150 San Ramon, CA 94583 | & Lone Tree Way | | 8885 42 SFD 8948 52 SFD | | Under Const Under Const | |
| AR-05-02 UP-08-06 AR-08-09 | Sand Creek Ranch Rivergate 8640, 8886, 8951 | Shea Homes 2580 Shea Center Drive Livermore, CA 94551 | Off Canada Valley Road & Lone Tree Way | | 8640 28 SFD 8886 30 SFD 8951 156 SFD | | Under Const Under Const Proposed unit mix change PC approved 7/2/08 DRB approved 7/9/08 Council scheduled 8/12/08 | Stahl |
| UP-04-28 | Sierra Vista 7722 | Suncrest Homes 300 H Street Antioch, CA 94509 | | 075-052-016 | 50 SFD | | Approved | |
| PDP-08-01 RDA-08-01 | Smith parcel | LCA Architects | Southeast Antioch off Deer Valley Road | 057-060-014 | 50 SFD and 8.5 acres of retail | | Accepted | |
| PDP-06-03 RDA-07-02 PD-08-01 UP-08-01 AR-08-03 | The Pointe | Discovery Builders 4061 Port Chicago Hwy #H Concord, CA 94520 | North of James Donlon at Somersville | | 72 SFD | | RDA approved 1/22/08 In Progress | Gentry |
| PDP-06-05 RDA-06-01 PD-08-03 UP-08-14 AR-08-12 | Tierra Villas | Mission Peak Homes 40480 Encyclopedia Circle Fremont, CA 94538 | 5020 Heidorn Ranch Road | 056-130-013 | 122 SFD | | RDA approved 1/22/08 Accepted | Morris |
| UP-08-07 | Vista Grande Mobile Estates | Vista Grande Mobile Estates 2901 Somersville Road Antioch, CA 94509 | 2901 Somersville Road | 076-010-029 | Addition of 6 new coach sites | | Incomplete | Stahl |
| PDP-07-03 RDA-07-04 | Wilbur Townhomes | Joseph Bosman 2281 Fairview Avenue Brentwood, CA 94513 | 701 & 810 Wilbur Avenue | 065-110-006 065-110-007 | 63 SFD | 5.36 acres | RDA approved 1/22/08 | Oshinsky |
| MDP-06-01 | Zeka Ranch Estates | Michael Milani 4071 Port Chicago Hwy Concord, CA 94520 | | | 314 SFD | 639 acres | Incomplete | Carniglia |

Commercial Projects

| Project Number(s) | Project | Application | Applicant | Location | APN | Bldg Sq Ft Description | Site Size | Status | Staff Report/Reso | Planner |
|----------------------------------|---|-------------|---|---|-------------|--|-----------|---|-------------------|----------|
| UP-07-07 | 1700 4 th Street/Fowler Property | | Trinity Property Consultants 851 81 st Avenue, Ste 300 Oakland, CA 94621 | 1700 4 th Street | 074-040-047 | Re-establish temp uses on property | | PC approved 8/1/07 | | Oshinsky |
| UP-08-02 | 1700 4 th Street/Fowler Property | | Ron Merritt 1666 Willow Pass Road Bay Point, CA 94565 | 1700 4 th Street | 074-040-047 | 10 year temporary use for warehouse and showroom | | PC approved | | Oshinsky |
| UP-06-08 AR-06-05 | 4 th Street Gift Shop | | Urban Impressions 812 5th Ave. #D Oakland, CA 94606 | 4 th Street near I Street | 066-131-011 | Construction of 2 story mixed use building | | PC approved 6/21/06 DRB approved 6/28/06 | | Stahl |
| UP-07-13 | Antioch Armory | | Allan Tong Antioch, CA 94509 | 625 W 3 rd Street | 066-062-007 | Sporting goods retail store for hunting, fishing, etc. | | PC approved 1/16/08 Under construction | | |
| UP-08-10 | Antioch High Scholl cell site | | NSA Wireless 12647 Alcosta Blvd #110 San Ramon, CA 94583 | 700 W 18 th Street | | New cell site located on Antioch High football field | | Incomplete | | Stahl |
| PD-04-09 UP-04-11 AR-04-09 | Antioch Surgical Center | | MS Walker & Associates, Inc 3551 Pegasus Drive Bakersfield, CA 93308 | 3500 Hillcrest Avenue | 052-370-010 | Construct 5500 sq ft outpatient surgery center | | PC approved 4/18/07 DRB approved 10/24/07 Council approved | | Oshinsky |
| UP-05-23 AR-06-08 | AUTOCARE 2000 | | Anthony Tabacco & Assoc. 7 Westwood Court Orinda, CA 94563 | 2700 Somersville Road | 074-123-013 | Additional 2300 sq ft auto service facility | 0.66 | PC approved 1/18/06 DRB approved 3/8/06 Approval extended 1/18/08 | | Stahl |
| UP-06-14 AR-06-12 | Bank of Agriculture | | Richard Miller 28 Marsala Way Napa, CA 94558 | Lone Tree Way at Country Hills | 055-071-080 | Subdivision of parcel and development of car wash and bank | 2.4 acres | PDP to PC 11/7/07 In progress | | Gentry |
| AR-05-13 | Bases Loaded | | Cyndi Karp 101 Corte del Pardo Walnut Creek, CA 94598 | Corner of 4 th Street and G Street | 066-142-008 | Construction of new restaurant and sports bar | 0.2 acres | DRB Approved Under construction | | Gentry |

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| UP-05-02 | Bluerock Business Center | | Reynolds & Brown 1200 Concord Ave #200 Concord, CA 94520 | Bleu Rock Drive at Lone Tree Way | 072-012-107 | | | Built | | Wehrmeister |
| PD-07-01 UP-07-06 AR-07-08 | Buchanan Crossings Shopping Center | | Catlin Properties 3620 Fair Oaks #150 Sacramento, CA 95864 | Buchanan Road at Somersville | 074-080-013 | 102,370 square foot shopping center | 13.5 acres | PC approved 7/2/08 CC scheduled 8/12/08 | | |
| AR-07-13 | Casino Building Remodel | | Joe Martinez 590 Garland Way Brentwood, CA 94513 | 101 H Street | 066-071-007 | Remodel exterior of building | | DRB scheduled 8/13/08 | | Gentry |
| AR-06-21 | Chevron Remodel | | Chevron, USA, 145 S. State College #400 Brea, CA 92821 | 3400 Hillcrest Avenue | 052-370-001 | Remodel of existing service station | | DRB approved 3/28/07 Under construction | | Stahl |
| AR-06-22 | Chevron Remodel | | Chevron, USA, 145 S. State College #400 Brea, CA 92821 | 4600 Lone Tree Way | 055-170-002 | Remodel of existing service station | | DRB Approved 3/28/07 Under construction | | Stahl |
| AR-07-14 | Chevron Remodel | | Johnson United 5201 Pentecost Drive Modesto, CA 95356 | 3201 Delta Fair Boulevard | 074-121-006 | Remodel of existing Chevron station | | DRB approved 1/9/08 Under Construction | | Stahl |
| Z-08-02 | City Gate Rezone | | Equus Group 1120 2 nd Street Brentwood, CA 94513 | | 051-200-026 | Rezone from PBC to PD | 15.94 acres | PC scheduled 8/13/08 CC scheduled 9/9/08 | | Gentry |
| AR-05-26 | Contra Loma Plaza new commercial pad | | Choi & Robles Architecture 1001 Marina Village Pkwy #S Alameda, CA 94501 | 3190 Contra Loma Blvd | 076-550-004 | New commercial pad | | Resubmitted DRB approved 11/28/07 | | Stahl |
| UP-07-01 AR-07-02 UP-07-11 AR-05-29 UP-05-34 | Costco Gas Station Costco Expansion & Bldg. Move Costco Relocation | | Costco 999 Lake Drive Issaquah, WA 98027 | Vern Roberts Circle at Crow Ct 2201 Verne Roberts Circle | 074-052-020 074-052-033 | New service station And relocate existing building Lot merger | 1.16 14 acres | Building permits issued Under construction | | Gentry |
| PD-05-03 UP-05-13 AR-05-12 | County Square Market | | Global Seven Inc. 410 Contra Costa Blvd. Pleasant Hill, CA 94523 | E Tregallas Road at Wildflower | 052-232-019 | New 30,860 sq ft market | | Under construction | | Oshinsky |
| UP-08-08 | County Square Market | | Global Seven Inc. 410 Contra Costa Blvd. Pleasant Hill, CA 94523 | E Tregallas Road at Wildflower | 052-232-019 | Increase in 2 nd floor office square footage | | In progress | | Oshinsky |

Updated 8/15/2008

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| UP-05-35 AR-06-07 | Deer Valley Business Park Parcel 1 + Bldgs N, O, P | | MS Walker & Associates, Inc 3551 Pegasus Drive Bakersfield, CA 93308 | SW Deer Valley at Country Hills | 055-071-071 | 16 single user/multi tenant bldgs 1800-7000 sq ft | 6 acres | DRB approved 1/17/07 Building permit plans being reviewed | | Gentry |
| UP-04-31 AR-04-43 V-06-06 | Deer Valley Business Park Parcel 4 | | BE Deer Valley, LLC 40 Rockingham Drive Newport Beach, CA 92660 | Deer Valley Road and Country Hills | 055-071-090 | 5 buildings totaling 35,000 sq ft | 3.8 acres | PC approved DRB approved Under construction | | Gentry |
| UP-06-06 AR-06-06 | Deer Valley Business Park Silicon Valley College & office/flex building | | Chris Gnekow MS Walker & Associates 3551 Pegasus Drive Bakersfield, CA 93308 | Deer Valley Road at Country Hills | 055-071-072 | 30,000 sq ft + 17,200 sq ft | 5 acres | PC approved DRB approved College built | | Gentry |
| S-06-03 | Entry Signage | | City of Antioch | Various locations City wide | | Approval of new Antioch City signage | | DRB approved Council approved In plan check | | Wehrmeister |
| GP-06-02 UP-06-28 AR-06-20 | Fitzuren commercial building with produce market | | John Rivolli 427 Orchard View Ave Martinez, CA 94553 | 909 Fitzuren Road | 071-021-013 | Construct 2 story building with commercial and market uses | | Incomplete | | Morris |
| AR-08-06 | Gas City re-branding to Shell | | Promotions Plus Sign Co, 4920 Reseda Blvd. #250 Northridge, CA 91324 | 4198 Lone Tree Way | 055-071-092 | Re-branding of existing station to Shell Oil Co. | | DRB approved 7/9/08 | | Stahl |
| S-06-07 | Gateway monument signage | | Cal Neon Illuminart Signs 1012 Morse Avenue, Suite 9 Sunnyvale, CA 94809 | Gateway Center 2101 W 10 th Street | 074-051-005 | Installation of new monument sign | 1.9 acres | DRB approved Building permit issued | | Gentry |
| AR-07-04 | Golf Course Monument Sign | | Lone Tree Golf Course 4800 Golf Course Road Antioch, CA 94531 | 4800 Golf Course Road | 072-011-020 | Approval of monument sign installed without permits | | DRB denied 4/25/07 | | Stahl |
| PD-06-04 UP-06-21 S-08-01 | Hillcrest Summit | | Bedrock Ventures Inc. 4045 Balfour Avenue Oakland, CA 94610 | Hillcrest Avenue and E Tregallas | 052-100-055 | 1500 sq feet retail 35,077 sq ft office | 5 acres | PC approved 1/16/08 DRB approved 1/23/08 City Council approved 2/26/08 | | Gentry |
| PD-07-04 UP-07-21 AR-07-24 | Hillcrest Village | | Venture Corp. 125 E Sir Francis Drake, 3 rd Fl Larkspur, CA 94939 | Hillcrest Ave @ Wildflower | 052-140-002 | Mixed use commercial/retail approx 96,000 s.f. | | In progress | | |
| S-08-04 | Holy Cross Cemetery Monument Sign | | Catholic Cemetery PO Box 488 Lafayette, CA 94549 | 2200 E 18 th Street | 051-170-040 | Installation of new monument signage | | Incomplete | | Stahl |

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| UP-07-16 AR-07-12 | In Shape Health Club pool slide | | In Shape Health Clubs Inc 1016 E. Bianchi Rd, #A-23 Stockton, CA 95210 | 4065 Lone Tree Way | 072-012-084 | Add slide to outdoor pool | 17.8 acres | PC approved 4/2/08 DRB approved 4/9/08 In plan review | | Gentry |
| V-08-05 | Islamic Center fence | | Islamic Center of East Bay 315 W 18 th Street Antioch, CA 94509 | 315 W 18 th Street | 067-221-021 | Install a 4 foot fence within the landscape setback | | Accepted | | |
| AR-08-13 | Jack-in-the-Box sign and re-image | | Stantec Consulting 6070 West Oaks Blvd. #200 Rocklin, CA 95765 | 2705 Hillcrest Avenue | 052-012-057 | Repaint exterior of building and modify exterior signage | | Accepted | | |
| AR-07-18 | Jensen Office Building | | Terry Jensen 4913 Union Mine Ct Antioch, CA 94509 | Lone Tree Way | 071-101-022 | Design review of new 2 story office building | 0.23 acres | DRB approved11/28/07 In plan review | | Stahl |
| V-08-01 AR-08-04 | Juliet Plaza | | 2100 Holdings LLC 1280 11 th Avenue San Francisco, CA 94122 | 2100 L Street at Sycamore Drive | 074-343-034 | 7400 square foot retail soace | | Incomplete | | Stahl |
| FD-03-06 UP-03-26 AR-03-38 | Kaiser Medical Center | | Kaiser Foundation Hospitals 1950 Franklin Street 12 th Flr Oakland, CA 94605 | 6200 Deer Valley Road | 057-022-003 | 60,500 sq ft medical building | | Building constructed | | Oshinsky |
| UP-06-19 AR-06-24 | Little Angels Preschool | | Estella Sierra 1816 Hillcrest Avenue Antioch, CA 94509 | 1816 Hillcrest Avenue | 068-091-042 | Operation of new preschool | | PC approved DRB approved Building permit issued | | Gentry |
| UP-08-03 | Live Entertainment permit for Mutiny | | Street Titans, LLC 422 W 2 nd Street Antioch, CA 94509 | 422 W 2 nd Street | | Permit to allow recurring live entertainment at Mutiny | | PC approved 5/21/08 | | Stahl |
| UP-08-09 | Lone Tree Convenience Store | | BG Market 4040 Meadowlake Street Antioch, CA 94509 | 5005 Lone Tree Way | | Convenience store with liquor sales at Lone Tree Landing | | In progress | | Oshinsky |
| PD- AR-04-26 UP-04-21 | Lone Tree Landing | | John Tomasello 516 Nelly Court Alamo, CA 94507 | Lone Tree Way at Hillcrest | 056-012-024 | 81,690 sq feet retail center | 413,790 sq ft | Partially completed | | Oshinsky |
| AR-06-23 UP-06-24 | Lone Tree Landing Water Feature | | John Tomasello 516 Nelly Court Alamo, CA 94507 | Lone Tree Way at Hillcrest | 056-012-024 | New water feature on corner | | DRB approved 3/14/07 City Council approved 5/22/07 Completed | | Oshinsky |
| PD-07-02 UP-07-08 AR-07-11 | Markstein Distribution Center | | ARCO National 1155 Beecher Street San Leandro, CA 94577 | | | New 101,646 sq foot office/ distribution facility | | PC approved DRB approved 11/14/07 | | Morris |

Updated 8/15/2008

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| | | | | | | | | Under construction | | |
| UP-07-05 AR-07-06 | McDonald's Remodel | | McDonalds 299 Oak Road #900 Walnut Creek, CA 94597 | 2424 Mahogany Way | 074-370-011 | Remodel existing building and play place | | Lot merger approved 12/5/07 Resubmitting | | Gentry |
| S-07-03 | Meineke & Econo Lube Signage | | All Sign Services 1290 Waterfall Way Concord, CA 94521 | 1710 Auto Center Drive | 074-171-021 | Re-branding of existing Econo Lube site | | DRB approved 10/24/07 Under construction | | |
| UP-07-23 AR-08-01 | Metro PCS antenna at existing water tank site | | Network Development 1080 Marina Village Pkwy Alameda, CA 94501 | Neroly Road | 053-060-013 | Add antenna at existing non City owned water tank site | | PC approved 4/16/08 | | Stahl |
| UP-07-22 AR-07-25 | Metro PCS co-location Deer Valley Road | | Network Development 1080 Marina Village Pkwy Alameda, CA 94501 | 5201 Deer Valley Road | 05-170-006 | Add antenna to building roof top | | ZA approved 3/18/08 DRB approved 4/9/08 | | Stahl |
| UP-05-30 AR-05 | Perinatal Council | | Barbara Bunn McCullough 2648International Blvd Oakland, CA 94601 | 521 W 5 th Street | 066-143-003 | Addition to existing building | | PC approved 10/19/05 DRB approved 12/14/05 Under construction | | Stahl |
| V-08-02 | Perinatal Council | | Barbara Bunn McCullough 2648International Blvd Oakland, CA 94601 | 521 W 5 th Street | 066-143-004 | Variance to install wood fence instead of masonry brick wall | | Incomplete | | Stahl |
| UP-06-17 AR-06-15 V-06-03 | Produce Market | | Frank Hamed 131 Tully Road San Jose, CA 9511 | 914 A Street | 066-172-001 | Remodel building and operate produce market | 0.4 acres | Incomplete | | Gentry |
| S-06-04 | Raley's Monument Sign | | American Electric Sign 3710 Lone Tree Way #113 Antioch, CA 94509 | 3612 Lone Tree Way | 071-171-031 | Add monument sign | | DRB Approved 12/20/06 | | Stahl |
| AR-07-26 | Raley's Shopping Center remodel | | Cal-American 1925 Century Park East #2100 Los Angeles, CA 90067 | 3612 Lone Tree Way | 071-181-031 | Remodel of existing shopping center | | DRB denied 4/23/08 | | Stahl |
| UP-08-11 AR-08-11 V-08-03 | Ramada Inn Cell Site | | Black Dot Wireless 320 Commerce, Ste 200 Irvine, CA 92602 | 2436 Mahogany Way | 074-370-022 | New cell sites located in a new Ramada sign | | Incomplete | | Stahl |
| GP-07-01 Z-07-05 | Reynold's & Brown GP amendment and Rezone | | Reynold's and Brown 1200 Concord Avenue Concord, CA 94520 | Northwest corner of Lone Tree Way and Golf Course | 072-012-087 | Change GP and zoning to Neighborhood/Community Commercial zoning designation | | In progress | | Morris |

Updated 8/15/2008

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| | | | | Road | | | | | | |
| UP-06-13 | Rivertown Business Center | | Architectural Network, Inc. 111 Civic Drive #260 Walnut Creek, CA 94596 | I Street and 1 st Street | 066-091-010 | 16,000 sq ft new office/restaurant | | Extension Approved | | Oshinsky |
| AR-03-36 | Seventh Day Adventist Church | | Delta View Enterprises 3737 Lone Tree Way Antioch, CA 94509 | 2200 Country Hills | 055-071-105 | New 39,000 sq ft church | | DRB 2/21/04 DRB (landscape) 3/1/06 Under construction | | Stahl |
| AR-08-02 | Seventh Day Adventist Church 8-plex Administrative Housing | | Delta View Enterprises 3737 Lone Tree Way Antioch, CA 94509 | 2200 Country Hills | 055-071-105 | New 8-plex administrative housing unit. | | DRB approved 5/14/08 | | Stahl |
| UP-05-22 AR-05-22 | St Ignatius Church Expansion | | Roman Catholic Bishop, 3551 Contra Loma Blvd. Antioch, CA 94509 | 3351 Contra Loma Blvd | 071-370-026 | 12,995 sq ft expansion of existing church | | Building permit issued for on-site work | | Gentry |
| UP-05-31 AR-05-27 | Starbucks @ Hillcrest and Wildflower | | Java Acquisition company 0049 135 East 57 th Street, 23 rd Floor New York, NY 10022 | Hillcrest Ave & Wildflower | 052-460-011 | Starbucks and retail center | 3 acres | PC approved 11/7/07 DRB approved 11/14/07 | | Gentry |
| AR-07-16 S-07-05 | Starbucks at Somersville Towne Center | | Starbucks 17700 New Hope St. Ste 200 Fountain Valley, CA 92708 | 2500 Somersville Road | 074-450-036 | New Starbucks | | DRB approved 10/10/07 Under construction | | Gentry |
| UP-05-36 AR-05-31 | Sunset Drive Indoor Sports Center | | Steve Fosenburg PO Box 4516 Antioch, CA 94509 | 1210 Sunset Drive | 068-253-003 | Indoor Hockey Rink and batting cages | | Approved In plan check | | Wehrmeister |
| UP-07-14 AR-07-19 | T-Mobile cell site at Kaiser Deer Valley | | Alex Monk 185 Berry Street Suite 5300 San Francisco, CA 94107 | 2601 Deer Valley Road | 057-022-014 | T-mobile proposes to install wireless antennas on Kaiser roof top | | In progress | | Stahl |
| UP-07-03 | Tobin World | | MS Walker & Associates 3551 Pegasus Drive Bakersfield, CA 93308 | 2310 Country Hills Drive | 055-071-090 | Approval of 9600 sq ft school for autistic children | 9600 sq ft | PC approved 8/1/07 Under construction TCO issued | | Gentry |
| S-08-02 | Union 76 monument sign | | Promotions Plus Sign Co, 4920 Reseda Blvd. #250 Northridge, CA 91324 | 2701 Contra Loma Blvd. | 071-011-036 | Approval of new monument sign for existing service station | | DRB scheduled 8/27/08 | | Diaz |
| AR-07-21 | Vineyard Business Park Phase III | | Carnmer Properties PO Box 2665 Walnut Creek, CA 94595 | 1699 Vineyard Drive | 051-052-074 | 3 new multi tenant commercial buildings 36,640 s.f. total | | DRB approved 1/15/08 | | |

Updated 8/15/2008

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| AR-04-25 | WalMart Expansion | | Robert A. Karn & Associates 707 Beek Avenue Fairfield, CA 94553 | 4893 Lone Tree Way | 056-011-030 | 33,575 sq ft expansion with additional parking | | Resubmitted/In progress | | Gillarde |
| AR-07-09 | Williamson Ranch Office building | | John Blatter 350 Main St., Suite K Pleasanton, CA 94566 | Lone Tree Way | 056-011-058 | 2 story 20,026 s.f. office building | 1.25 acres | DRB approved 8/22/07 In plan review | | Gillarde |

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